

I Curvature Function

Along a curve defined by h = f(x), for an infinitesimal arc length, ds, with unit normal vector \hat{n} , and unit tangent vector, \hat{t} , as $ds \to 0$,

$$ds^2 = dx^2 + dy^2 \tag{1}$$

$$\frac{ds}{dx} = \sqrt{1 + \left(\frac{dy}{dx}\right)^2} \tag{2}$$

let $\vec{r}(x)$ be a position vector function for the curve h = f(x), such that $\vec{r}(x) = \langle x, f(x) \rangle$ and $\|\vec{r}(x)\| = \sqrt{x^2 + (f(x))^2}$, then the tangent vector along the curve is defined as,

$$\vec{t} = \frac{d\vec{r}}{ds} \tag{3}$$

and the unit tangent vector,

$$\hat{t} = \frac{d\vec{r}/ds}{\|d\vec{r}/ds\|} \tag{4}$$

where, $\frac{d\vec{r}}{ds} = \langle 1, f'(x) \rangle$ and $\frac{d\vec{r}}{ds} = \sqrt{1 + (f'(x))^2}$; expanding,

$$\hat{t} = <\frac{1}{\sqrt{1+(f'(x))^2}}, \frac{f'(x)}{\sqrt{1+(f'(x))^2}}>$$
 (5)

Curvature κ is defined as,

$$\kappa = \frac{1}{R} = \left\| \frac{\hat{d}t}{ds} \right\| = \left\| \frac{\hat{d}t}{dx} \cdot \frac{dx}{ds} \right\| \tag{6}$$

calculating the derivatives, first,

$$\frac{d\hat{t}}{dx} = <\frac{d}{dx}\left(\frac{1}{\sqrt{1+(f'(x))^2}}\right), \frac{d}{dx}\left(\frac{f'(x)}{\sqrt{1+(f'(x))^2}}\right) > \tag{7}$$

$$\frac{d}{dx}\left(\frac{1}{\sqrt{1+(f'(x))^2}}\right) = -\frac{1}{2}\left(1+(f(x))^2\right)^{3/2} \cdot 2f'(x)f''(x) \tag{8}$$

$$= -f'(x) f''(x) \left(1 + (f(x))^2\right)^{3/2} \tag{9}$$

$$\frac{d}{dx}\left(\frac{f'(x)}{\sqrt{1+(f'(x))^2}}\right) = \frac{f''(x)}{(1+(f(x))^2)^{1/2}} - \frac{(f'(x))^2 f''(x)}{(1+(f(x))^2)^{3/2}}$$
(10)

therefore,

$$\frac{d\hat{t}}{dx} = \langle -\frac{f'(x)f''(x)}{(1+(f(x))^2)^{3/2}}, \frac{f''(x)}{(1+(f(x))^2)^{1/2}} - \frac{(f'(x))^2 f''(x)}{(1+(f(x))^2)^{3/2}} \rangle$$
(11)

further simplifying,

$$\frac{d\hat{t}}{dx} = \frac{\langle -f'(x)f''(x), f''(x) \rangle}{(1 + (f(x))^2)^{3/2}}$$
(12)

second, from equation 2,

$$\frac{dx}{ds} = \left(1 + (f(x))^2\right)^{-1/2} \tag{13}$$

from equations 12 and 13,

$$\frac{d\hat{t}}{ds} = \frac{\langle -f'(x)f''(x), f''(x) \rangle}{(1 + (f(x))^2)^{3/2}} \cdot (1 + (f(x))^2)^{-1/2}$$
(14)

then curvature can be written as,

$$\kappa = \left\| \frac{d\hat{t}}{ds} \right\| = \frac{\|\langle -f'(x)f''(x), f''(x) \rangle\|}{(1 + (f(x))^2)^{3/2}} \cdot (1 + (f(x))^2)^{-1/2}$$
 (15)

$$\kappa = \frac{\left[(-f'(x)f''(x)^2 + (f''(x))^2 \right]^{1/2}}{(1 + (f(x))^2)^{3/2}} \cdot \left(1 + (f(x))^2 \right)^{-1/2} \tag{16}$$

$$\kappa = \frac{f''(x)}{(1 + (f(x))^2)^{3/2}}$$
(17)

The derivative of curvature,

$$\frac{d\kappa}{dx} = \frac{d}{dx} \left(f''(x) \right) \cdot \frac{1}{\left(1 + (f'(x))^2 \right)^{3/2}} + \frac{d}{dx} \left(\frac{1}{\left(1 + (f'(x))^2 \right)^{3/2}} \right) \cdot f''(x) \tag{18}$$

$$= \frac{f'''(x)}{(1 + (f'(x))^2)^{3/2}} - \frac{3}{2} \left(1 + (f'(x))^2 \right)^{-5/2} \cdot 2f'(x)f''(x) \cdot f''(x) \tag{19}$$

$$\frac{d\kappa}{dx} = \frac{f'''(x)}{(1 + (f'(x))^2)^{3/2}} - \frac{3f'(x)(f''(x))^2}{(1 + (f'(x))^2)^{5/2}}$$
(20)

II Evolution Equation

Starting with the Young-Laplace equation,

$$p_v - p_l = \sigma \kappa + \Pi \tag{21}$$

$$\frac{dp_v}{dx} - \frac{dp_l}{dx} = \frac{d}{dx} \left(\sigma \kappa \right) + \frac{d\Pi}{dx}$$
 (22)

assuming vapor pressure to be constant, $dp_v/dx = 0$,

$$\frac{d}{dx}\left(\sigma\kappa\right) = -\left(\frac{dp_l}{dx} + \frac{d\Pi}{dx}\right) \tag{23}$$

$$\left(\frac{d\sigma}{dx}\right)\kappa + \sigma\left(\frac{d\kappa}{dx}\right) = -\left(\frac{dp_l}{dx} + \frac{d\Pi}{dx}\right)$$
(24)

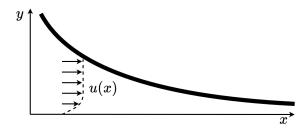
with $\sigma = \sigma_o + \gamma \cdot T_i$ and $\frac{d\sigma}{dx} = \gamma \cdot \frac{\partial T_i}{\partial x}$, as well as equations 17 and 20,

$$\gamma \frac{\partial T_i}{\partial x} \left(\frac{h''(x)}{(1 + (h'(x))^2)^{3/2}} \right) + \sigma \left(\frac{h'''(x)}{(1 + (h'(x))^2)^{3/2}} - \frac{2h'(x)(h''(x))^2}{(1 + (h'(x))^2)^{5/2}} \right) = -\left(\frac{dp_l}{dx} + \frac{d\Pi}{dx} \right)$$
(25)

$$\frac{\gamma}{\sigma} \frac{\partial T_i}{\partial x} h''(x) + h'''(x) - \frac{3h'(x)(h''(x))^2}{1 + (h'(x))^2} = -\frac{1}{\sigma} \left(1 + (h'(x))^2 \right)^{3/2} \left(\frac{dp_l}{dx} + \frac{d\Pi}{dx} \right)$$
(26)

$$h'''(x) = \frac{3h'(x)(h''(x))^2}{1 + (h'(x))^2} - \frac{\gamma}{\sigma} \frac{\partial T_i}{\partial x} h''(x) - \frac{1}{\sigma} \left(1 + (h'(x))^2 \right)^{3/2} \left(\frac{dp_l}{dx} + \frac{d\Pi}{dx} \right)$$
(27)

III Liquid Pressure Gradient



The Navier-Stokes momentum equation with lubrication approximation,

$$\frac{\partial^2 u}{\partial y^2} = \frac{1}{\mu} \frac{\partial p}{\partial x} \tag{28}$$

integrating with respect to y,

$$\frac{\partial u}{\partial y} = \frac{1}{\mu} \frac{\partial p}{\partial x} y + c_1 \tag{29}$$

applying Marangoni condition at the free surface, i.e., at y = h, $\frac{\partial u}{\partial y} = -\frac{1}{\mu} \frac{\partial \sigma}{\partial x}$,

$$\frac{\partial u}{\partial y}\Big|_{y=h} = -\frac{1}{\mu} \frac{\partial \sigma}{\partial x} = \frac{1}{\mu} \frac{\partial p}{\partial x} + c_1 \tag{30}$$

$$c_1 = -\frac{1}{\mu} \left(\frac{\partial \sigma}{\partial x} + h \frac{\partial p}{\partial x} \right) \tag{31}$$

integrating equation 29,

$$u(y) = \frac{1}{\mu} \frac{\partial p}{\partial x} y^2 + c_1 \cdot y + c_2 \tag{32}$$

applying no-slip condition at the solid wall, i.e., at y = 0, u = 0,

$$u(0) = \frac{1}{\mu} \frac{\partial p^2}{\partial x} + c_1(0) + c_2 \tag{33}$$

$$\therefore c_2 = 0 \tag{34}$$

substituting equations 31 and 34 into equation 32,

$$u(y) = \frac{1}{\mu} \frac{\partial p}{\partial x} y^2 - \frac{1}{\mu} \left(\frac{\sigma}{x} + h \frac{\partial p}{\partial x} \right) y$$
 (35)

the liquid mass flow is defined by the integral,

$$\dot{\Gamma} = \int_0^h \rho L \cdot u(y) \, dy \tag{36}$$

where, L is the depth in z,

$$= \rho L \int_0^h \left(\frac{1}{\mu} \frac{\partial p}{\partial x} y^2 - \frac{1}{\mu} \left(\frac{\sigma}{x} + h \frac{\partial p}{\partial x} \right) y \right) dy \tag{37}$$

$$= \rho L \left\{ \left[\frac{1}{\mu} \frac{\partial p}{\partial x} \cdot \frac{y^3}{3} \right] \right|_0^h - \left[\frac{1}{\mu} \left(\frac{\partial \sigma}{\partial x} + h \frac{\partial p}{\partial x} \right) \frac{y^2}{2} \right] \right|_0^h \right\}$$
 (38)

$$= \rho L \left\{ \left[\frac{1}{\mu} \frac{\partial p}{\partial x} \cdot \frac{h^3}{3} \right] - \left[\frac{1}{\mu} \left(\frac{\partial \sigma}{\partial x} + h \frac{\partial p}{\partial x} \right) \frac{h^2}{2} \right] \right\}$$
 (39)

$$\dot{\Gamma} = -\frac{\rho L}{\mu} \left(\frac{1}{6} \frac{\partial p}{\partial x} h^3 + \frac{1}{2} \frac{\partial \sigma}{\partial x} h^2 \right)$$
(40)

For an evaporation mass flux, \dot{m}'' , the evaporation rate, \dot{m} ,

$$\frac{\partial \dot{m}}{\partial x} = \int_0^L \dot{m}'' \, dz = L \cdot \dot{m}'' \tag{41}$$

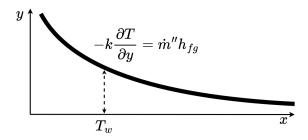
then mass conservation dictates,

$$\frac{\partial \dot{\Gamma}}{\partial x} + \frac{\partial \dot{m}}{\partial x} = 0 \tag{42}$$

$$\dot{m} = -\frac{\rho}{\mu} \left(\frac{1}{6} \frac{\partial p}{\partial x} h^3 + \frac{1}{2} \frac{\partial \sigma}{\partial x} h^2 \right) \tag{43}$$

$$\left| \frac{\partial p}{\partial x} = 6 \frac{\dot{m}''}{h^3} \frac{\mu}{\rho} - 3h \frac{\partial \sigma}{\partial x} \right| \tag{44}$$

IV Interface Temperature Distribution



Using steady-state one-dimensional approximation,

$$\frac{\partial^2 T}{\partial y^2} = 0 \qquad \to \qquad \frac{\partial T}{\partial y} = c_1 \tag{45}$$

at
$$y = h$$
, $\frac{\partial T}{\partial y} = -\dot{m}'' \cdot \frac{h_{\rm fg}}{k}$

$$\therefore c_1 = -\dot{m}'' \cdot \frac{h_{\text{fg}}}{k} \tag{46}$$

integrating,

$$T(y) = -\dot{m}'' \cdot \frac{h_{\rm fg}}{k} y + c_2 \tag{47}$$

at y = 0, $T = T_w$, $\therefore c_2 = T_w$,

$$T(y) = -\dot{m}'' \cdot \frac{h_{\rm fg}}{k} y + T_w \tag{48}$$

then surface temperature,

$$T_i = T(h) = -\frac{h_{\text{fg}}}{k} h(x) \dot{m}''(x) + T_w(x)$$
(49)

V Computational Logic

