# Sensitivity Analysis of High-Dimensional Models with Correlated Inputs<sup>\*</sup>

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# Abstract

Sensitivity analysis is an important tool used in many domains of computational science to either gain insight into the mathematical model and interaction of its parameters or study the uncertainty propagation through the input-output interactions. In many applications, the inputs are stochastically dependent, which violates one of the essential assumptions in the state-of-the-art sensitivity analysis methods. Consequently, the results obtained ignoring the correlations provide values which do not reflect the true contributions of the input parameters. This study proposes an approach to address the parameter correlations using a polynomial chaos expansion method and Rosenblatt and Cholesky transformations to reflect the parameter dependencies. Treatment of the correlated variables is discussed in context of variance and derivative-based sensitivity analysis. We demonstrate that the sensitivity of the correlated parameters can not only differ in magnitude, but even the sign of the derivative-based index can be inverted, thus significantly altering the model behavior compared to the prediction of the analysis disregarding the correlations. Numerous experiments are conducted using workflow automation tools within the VECMA toolkit.

*Keywords:* Global sensitivity analysis, Uncertainty quantification, Parameter Correlation, Sobol index, Polynomial Chaos Expansion

# 1. Nomenclature

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- Q A set of uncertain input parameters  $Q_i$
- *D* A number of the input parameters
- $\rho_{Q_i}$  Parameter probability density function
- **q** A set of parameter realizations
- $oldsymbol{Y}$  Vector of the application model outputs
- $U \qquad \text{An application model } \boldsymbol{Y} = U(\boldsymbol{\mathfrak{t}}, \boldsymbol{x}, \boldsymbol{Q})$
- *P* Degree of the polynomial basis
- $\Psi$  Polynomial basis
- **a** Polynomial coefficients for the basis  $\Psi$
- $\hat{(\cdot)}$  Quantities related to the polynomial
- approximation of the true model

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<b>τ</b> π	<b>T</b> 7 ·
V	variance operator
$\mathbb E$	Expectation value operator
$S_i$	Variance-based sensitivity index
$S_i^{\mathcal{D}}$	Derivative-based sensitivity index
$(\cdot)^*$	Denotes the correlated variables/samples
$oldsymbol{\mu}$	Mean vector of the uncertain parameters
$\mathcal{C}$	Covariance matrix of the parameters
C	Correlation matrix of the parameters
L	Cholesky factor of the correlation matrix
${\cal P}$	Permutation vector
$\kappa$	Dissipation rate of the container
$T_{env}$	Ambient temperature
$T_0$	Initial temperature of the liquid

# 2. Introduction

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Sensitivity analysis (SA) is a technique for understanding how changes in the input parameters influence the uncertainty in the output of a model or simulation. SA facilitates the understanding of how the outputs of a model change with respect

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to variations in the input parameters. It it particularly useful for complex models, in order to determine which parameters cause the greatest vari-

<sup>14</sup> ation of the output, and quantify the sensitivity of <sup>66</sup> the model to changes in these parameters. Addi-

tionally, SA can be used to improve the accuracy of a model by identifying and reducing sources of

<sup>18</sup> uncertainty in the input data. Two SA methods are studied in this manuscript, a global variance-

20 based method, where the sensitivity is computed over the support of the input distributions. A lo-

<sup>22</sup> cal derivative-based method is considered as well, where the sensitivity is studied only in the vicinity

of a fixed input point. The variance-based SA method [1] quantifies the

26 sensitivity of each input parameter by estimating its contribution to the overall variance of the model

<sup>28</sup> output. This is achieved by decomposing the variance of the model output by splitting it into con-

<sup>30</sup> tributions which arise due to the impact of the input parameters or their interaction, and the pa-

32 rameters are assigned a sensitivity index based on their relative contributions. This sensitivity index

is also known as the Sobol index [2]. Variance-based methods allow full exploration of the input space,

<sup>36</sup> accounting also for the interactions and nonlinear responses. The variance-based sensitivity is used

especially in the context of uncertainty quantification, where the input parameters are usually char-

<sup>40</sup> acterized by a probability density function, modeling their uncertain nature or reflecting the uncer-

42 tainty in the data collection method. The current state-of-the-art of variance-based SA comprises two

- <sup>44</sup> main methodologies quasi-Monte Carlo (QMC) [2] and the methods based on model surrogates such
- <sup>46</sup> as polynomial chaos expansion (PCE) [3, 4]. Both approaches are based on sampling the input pa-

<sup>48</sup> rameters from the given probability distributions, <sup>100</sup> where the model is evaluated for the values of the

<sup>50</sup> parameter samples. In case of the QMC approach, <sup>102</sup> this process is repeated thousands of times, and sta-

52 tistical metrics such as the mean and variance are computed from the resulting series of model outnute. On the other hand, the superplaider habing

<sup>54</sup> puts. On the other hand, the general idea behind PCE is to approximate the model input-output re- <sup>106</sup>

<sup>56</sup> lationship with a polynomial expression, which is then used to directly obtain the statistical metrics 108

<sup>58</sup> such as mean and variance, while the first and total-order Sobol indices can also be calculated directly <sup>110</sup>
<sup>60</sup> from the polynomial model [5].

In case of the derivative-based analysis, the sensitivity information comprise computation of the par-

tial derivative of the model output with respect to an input parameter at some fixed point in the input space. The analytical derivative is often unknown, thus standard methods such as finite differences (FD) are used. The domain of the FD study is local, since such analysis can consider only vicinity around a single parameter and its fixed operating point. However, this shortcoming can be circumvented by exploiting a surrogate model where the derivative can be computed analytically. This, in turn, allows one to study sensitivity considering interactions between multiple parameters via correlations. In this manuscript, the derivative-based sensitivity indices are computed from the PCE surrogate model, in order to obtain information about the interaction of correlated variables.

While the variance-based SA is used more during the initial phases of model design, where the goal is to understand the behavior of a model or simulation and the sources of uncertainty in its inputs. It can be used to guide model calibration by identifying the most important parameters, determine the range of input values that result in acceptable output values. Similarly, it can be used to optimize the design of a system by identifying the inputs that have the greatest impact on the performance of the system, and exploring the trade-offs between different design options [6]. On the other hand, the derivative-based sensitivity is particularly useful in operational context, where it is used to understand how changes in the input variables affect the output of a system or process. This can guide design of the robust control systems which are resilient to variations in the system's inputs. Alternatively, it can be used to manage risk by understanding how changes in input variables affect the risk of a system or process. For example, in finance, partial derivatives can be used to calculate the sensitivity of the value of a portfolio to changes in the underlying asset prices or guide forward hedging ratios in commodity trading [7].

### 2.1. Motivation and Research Context

Correlation of the input parameters is a common phenomenon in many scientific and engineering models and there have been few studies conducted on sensitivity analyses with correlated parameters. Since the standard SA methods assume that the parameters are stochastically independent, this can have a significant impact on the results of the analysis. The presence of parameter correlations renders several assumptions no longer valid,

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- e.g. the polynomials in the PCE are no longer orthogonal. Additionally, if two input parameters are 166
- highly correlated, it may be erroneous to draw conclusions about which of the two parameters has a 168
- <sup>118</sup> greater impact on the output of the model using standard SA methods. Similarly, the results do not <sup>170</sup>
- provide adequate information to determine the sensitivity of the model to variations in these inputs. 172
- <sup>122</sup> Consequently, the presence of correlation between the input parameters can lead to biased estimates <sup>174</sup>
- 124 of the model sensitivity, which can lead to incorrect conclusions about the importance of the inputs and 176
- the input-output interactions. For example, when considering the context of energy market models, 178
- <sup>128</sup> the input parameters such as the cost of fossil fuel resources (liquid fuels and natural gas) account for <sup>180</sup>
- $^{130}\,$  the majority of the variance in the total energy system cost. However, these parameters are often  $_{182}\,$
- tightly correlated, and applying the state-of-the-art SA methods ignoring the correlation may lead to an 184
- <sup>134</sup> optimistic risk assessment of voltage instability, the cost of power generation, a line overload risk, and <sup>186</sup>
- <sup>136</sup> a power shortage expectation [8, 9].

# 2.2. Literature Review and Related Work

- <sup>138</sup> There are two directions in the literature how to deal with the correlations during SA; (i) decom-
- <sup>140</sup> position of the traditional sensitivity indicies into <sup>190</sup> correlated and uncorrelated parts [10, 11] and (ii)
- <sup>142</sup> introducing new sets of indices which contain all <sup>192</sup> correlations and indices which are reduced by the
- <sup>144</sup> contributions due to the correlation [12, 13, 14]. <sup>194</sup> The definition of the first order Sobol indices
- <sup>146</sup> was extended to consider parameter dependencies <sup>196</sup> in [15]. The method extends the QMC framework,
- 148 such that the sampling is performed considering the conditional probability densities of the individual 198
- <sup>150</sup> inputs. In case of dependent normal distributions, the samples are transformed using the Cholesky de-<sup>200</sup>
- <sup>152</sup> composition of the correlation matrix. The number of model evaluations required to obtain both the
- <sup>154</sup> first and total order indices for a simple linear model <sub>202</sub> with three inputs was 2<sup>16</sup>, which is prohibitive for
- 156 real-world complex models. The interpretation of 204 the indices is also not clear, as in some cases the to-
- tal Sobol index is smaller than the first order one. In [10, 11], the classical first order Sobol index is 206
- 160 split into various components. These components represent uncorrelative, interactive and correlative 208
- <sup>162</sup> contributions of a given parameter to the output variance. However, the interpretation of these con-<sup>210</sup>
- <sup>164</sup> tributions, as well as of total order indices, remains

unclear. In this approach, the surrogate model is set up using independent joint input distribution. The polynomials of the PCE expansion are evaluated with the dependent samples, subsequently used to compute the covariance of the components functions. Analysis of covariance is then used to compute the resulting indices and their decomposition into the three components.

A new set of the indices for correlated inputs was introduced by Mara and Tarantola [12, 13, 14]. Two distinct indices represent correlated and uncorrelated contributions of a given variable. These allow to distinguish between the mutual dependent contribution and the independent contribution of the parameter to the model response variance. The dependent parameters are decorrelated using the Gram–Schmidt procedure and Rosenblatt transformation, such that standard SA methods such as PCE or QMC frameworks can be used. However, since the SA is no longer performed using the original parameters, additional attention needs to be put to interpretation of the sensitivity indices. Additionally, different permutations of the decorrelated variables can be obtained, thus resulting in multiple set of the indices.

# 2.3. Contribution and Organization

SA with correlated parameters is studied in this work. The decorrelation approach is based on transformation of the input parameter space, such that the SA is performed using the independent distributions, following the approach (ii) and the work of Mara and Tarantola [12, 13, 14]. The contributions are the following:

- The correlated SA approach is studied in context of both variance-based and derivativebased sensitivities;
- Two transformations are used in order to reflect the stochastic dependencies in the input parameters, Cholesky decomposition of the correlation matrix and the Rosenblatt transformation;
- The methods are implemented within EasyVVUQ SA framework, aiming to leverage large-scale computational resources to make state-of-the-art uncertainty quantification algorithms available and accessible to a wide range of computational scientists;

- Demonstrate the importance of the parameter <sup>252</sup> correlations in the SA and provide extensive numerical experiments accompanied by a com-<sup>254</sup> prehensive interpretation of the results.
- <sup>216</sup> The following Sec. 3 discusses various aspects of <sup>2</sup> the SA, introducing both variance and derivative
- <sup>218</sup> based indices. The treatment of the correlated variables and modifications of the SA algorithm are in-
- troduced in Sec. 4. The application model used in the numerical experiments is presented in Sec. 5.
- Finally, extensive numerical experiments and their analysis is provided in Sec. 6. The paper concludes
- <sup>224</sup> in Sec. 7 outlining also future research directions.

#### 3. SA Method without Correlations

- The model is usually a complex interaction between its input parameters and outputs, and is
- treated in a black box fashion for the purpose of non-intrusive SA. Consider a model U that is de-
- fined over a time horizon **t**, space dimension  $\boldsymbol{x}$ and a set of D uncertain input parameters  $\boldsymbol{Q} = \{Q_1, Q_2, \dots, Q_D\}$ , such that

 $\boldsymbol{Y} = U(\boldsymbol{t}, \boldsymbol{x}, \boldsymbol{Q}). \tag{1}^{262}$ 

The model includes uncertain parameters that can <sup>264</sup> be collectively described by a joint multivariate

probability density function  $\rho_{Q}$ . If the uncertain <sup>266</sup> <sup>236</sup> parameters are statistically independent, the mul-

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tivariate probability density function  $\rho_{Q}$  can be 268 238 defined by separate univariate probability density

functions  $\rho_{Q_i}$ , one for each uncertain parameter  $Q_i$ , 270

$$\rho_{\boldsymbol{Q}} = \prod_{i=1}^{D} \rho_{Q_i}, \qquad (2)^{272}$$

where unit normal distributions are assumed, such that  $\rho_{Q_i} \sim \mathcal{N}(\mu = 0, \sigma = 1)$ .

- <sup>242</sup> The main computational pattern of the SA in both MC and PCE consists of drawing the samples <sub>278</sub>
- <sup>244</sup> **q** from the input parameter space  $\rho_{\mathbf{Q}}$  and evaluating the model  $U(\mathbf{t}, \mathbf{x}, \mathbf{q})$  at these points. The num-
- $_{246}$  ber N of such evaluations in the PCE approach

$$N = \begin{pmatrix} D+P\\P \end{pmatrix} \tag{3}$$

is a function of the polynomial degree P of the basis and the dimension D of the parameters, where

N grows fast, especially with the increasing dimen-  $^{286}$ 

 $_{250}$   $\,$  sion of the parameters. Based on these model evaluations, the true response of the model  ${\pmb Y}$  is fitted  $_{288}$ 

onto a polynomial basis  $\Psi = \{\Psi_p, p = 0, \ldots, P\}$ with a polynomial degree up to P. The basis needs to be orthogonal with respect to the input distributions  $\rho_{Q_i}$ . The polynomial model  $\hat{Y} = \hat{U}(\mathbf{t}, \mathbf{x}, \mathbf{Q})$  is build such that the true model is approximated by the polynomial expansion,  $U(\mathbf{t}, \mathbf{x}, \mathbf{Q}) \approx \hat{U}(\mathbf{t}, \mathbf{x}, \mathbf{Q})$ , and the model outputs are similar  $\mathbf{Y} \approx \hat{\mathbf{Y}}$ . The surrogate model  $\hat{U}(\mathbf{t}, \mathbf{x}, \mathbf{Q})$  is built from the polynomial basis  $\Psi$  as

$$\hat{U}(\mathbf{t}, \boldsymbol{x}, \boldsymbol{Q}) = \sum_{p \in P} a_p \Psi_p(\boldsymbol{Q}) 
= a_0 \Psi_0 + \sum_{p \in P} \sum_{i=1}^D a_p^i \Psi_p^i(Q_i) 
+ \sum_{p \in P} \sum_{i,j=1,j>i}^D a_p^{ij} \Psi_p^{ij}(Q_i, Q_j) 
\vdots 
+ \sum_{p \in P} a_p^{12...D} \Psi_p^{12...D}(Q_1, ..., Q_D), \quad (4)$$

where  $\Psi_0 = 1$  is a zero order polynomial,  $\Psi_p^i(Q_i)$  is a single dimensional polynomial up to degree p for a single input  $Q_i$ ,  $\Psi_p^{ij}(Q_i, Q_j)$  denotes polynomial order up to p of combination of two inputs  $Q_i, Q_j$ , etc. The polynomial coefficients  $a_p$  follow similar notation. In the non-intrusive variant of the method, the polynomial basis  $\Psi$  is constructed using, e.g., the three terms recurrence or the discretized Stieltjes method [3, 16]. The orthogonality of the polynomials holds in case the Q parameters are independent, i.e., the joint density can be expressed as a product of the individual marginal densities from Eq. (2).

A set of the polynomial coefficients  $a_p$  is determined such that the PCE model  $\hat{U}$  approximates the true model response Y. In point collocation, the approximation is built such that it minimizes the error at a set of collocation nodes compared to the true model response. Hammersley sampling [3] from the distribution is used to choose the collocation points. This results in a set of linear equations for the polynomial coefficients, which are solved using e.g. Tikhonov regularization. The overall algorithm is summarized in Alg. 1, where the SA is described in the following sections.

#### 3.1. Variance-based Sensitivity

Variance-based SA [1] determines the impact of the input parameters which can be used to asses the Algorithm 1 SA Method without Correlations.

- 1. Generate samples  $\mathbf{q}_1, \ldots, \mathbf{q}_N$  from the independent multivariate distribution  $\rho_{\mathbf{Q}}$ .
- 2. Evaluate the true model  $\boldsymbol{Y}_1 = U(\boldsymbol{x}, \mathbf{t}, \mathbf{q}_1), \dots, \boldsymbol{Y}_N = U(\boldsymbol{x}, \mathbf{t}, \mathbf{q}_N)$  at  $\mathbf{q}_i \in \rho_{\boldsymbol{Q}}$ .
- 3. Create a polynomial expansion  $\Psi_1, \ldots, \Psi_P$  up <sup>316</sup> to the *P*-th degree from  $\rho_{\boldsymbol{Q}}$ .
- 4. Solve the linear regression problem:  $\boldsymbol{Y}_n = {}^{318} \sum_p a_p \Psi_p(\boldsymbol{Q}_n)$  for  $a_1, \ldots, a_p$ . 5. Construct the model approximation
- 5. Construct the model approximation  $U(\boldsymbol{x}, \mathbf{t}, \boldsymbol{Q}) \approx \hat{U}(\boldsymbol{x}, \mathbf{t}, \boldsymbol{Q}) = \sum_{p} a_{p} \Psi_{p}(\boldsymbol{Q})$
- 6. Perform the SA using the surrogate model  $\hat{U}(\boldsymbol{x}, \mathbf{t}, \boldsymbol{Q})$ .

role of the parameters in the model, i.e., determine <sup>290</sup> if the parameter contributes intrinsically or via the

parameter interactions, or asses the relative importance of the individual parameters. Additionally, variance-based sensitivity quantifies the output un-

<sup>294</sup> certainty and its propagation through the model <sup>328</sup> from the uncertain inputs [4, 16]. Following the <sup>296</sup> variance decomposition [2], the total output variance  $V(Y_n)$  of *n*-th model output from Eq. (1) can

<sup>298</sup> be decomposed as

$$V(Y_n) = \sum_{i} V_i + \sum_{i} \sum_{j>i} V_{ij} + \ldots + V_{12\dots D}, \quad (5)$$
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where the partial variances are defined as

$$V_i = \mathbb{V}(\mathbb{E}(Y_n | Q_i)), \tag{6}$$

$$V_{ij} = \mathbb{V}(\mathbb{E}(Y_n | Q_i, Q_j)) - V_i - V_j, \qquad (7)$$

and so on, and the total variance is  $V(Y_n) = \mathbb{V}(\mathbb{E}(Y_n))$ . The polynomial coefficients can be post-

<sup>302</sup> processed to compute quantities of interest such <sup>340</sup> as mean, variance and other statistical moments

- <sup>304</sup> or variance-based sensitivity indices [5, 10]. The <sup>342</sup> sensitivity indices in the variance-based measures,
- <sup>306</sup> known as Sobol indices [2], are defined as the fraction of the variance of the component functions with
- respect to the total variance. The first order sensitivity index  $S_i$  measures the contribution of the i-th parameter,

$$S_i = \frac{V_i}{V(Y_n)}.$$
(8)

The total order sensitivity index  $S_i^T$  includes not <sup>350</sup> only the intrinsic contribution of the parameter itself as is the case for the first order index, but also <sup>352</sup> interactions with other parameters are considered,

$$S_i^T = \frac{\sum_{\alpha} V_a}{V(Y_n)},\tag{9}$$

where  $\alpha$  is a set of all multi-indices which contain i. It necessarily holds that  $0 \leq S_i \leq S_i^T \leq 1$ , and in case the model is additive and there are no parameter interactions, i.e. the higher order terms are zero, then

$$\sum_{i} S_i = 1. \tag{10}$$

#### 3.2. Derivative-based Sensitivity

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Derivative-based sensitivity indices express how much does the model output change if a small perturbation is applied to some of the inputs. The analytical derivatives of the complex models are not known, thus the usual practice is to use automatic differentiation tools or adopt approximations techniques such as finite differences to evaluate the numerical derivatives. The model derivative with respect to the parameter  $Q_i$  at a fixed point  $Q_i^0$  is expressed as

$$S_i^{\mathcal{D}} = \left. \frac{\partial Y_n}{\partial Q_i} \right|_{Q_i^0}.$$
 (11)

The shortcoming of this approach is that the resulting index can be computed only in the vicinity of the operating point of the given model configuration or its applicability for the SA of a single variable at a time, ignoring any possible interactions between the parameters.

Alternatively, the derivative-based sensitivity index can be evaluated by constructing the surrogate model  $\hat{U}$  and compute the derivative of the polynomial expression with respect to a given parameter. With this approach, the interaction of the parameters can be incorporated in the SA via the parameter correlations. Thus, the sensitivity indices of the individual parameters can incorporate interaction with other parameters using the procedure proposed in this paper. This approach can be used for both variance-based and derivative-based sensitivities.

#### 4. SA Method with Correlations

When considering models with correlated parameters, the polynomial expansion (4) cannot be used to accurately represent the model sensitivity since



Figure 1: Independent normal distribution (left) of the input space and the corresponding transformed parameter space with  $\rho_{\mathcal{C}} = 0.8$  (right). The contour lines illustrate the multivariate probability density function.

it doesn't distinguish whether the parameter is con- 400 354 tributing to the model directly or through a correla-

tion with another variable. This can lead to incor- 402 rect conclusions about the variance-based decompo-

- sition, where the importance of the input parame- 404 358 ters to the model and the sensitivity of the model
- to variations in these parameters no longer reflects the true parameter interactions in the model.

In order to address the parameter dependency,

- $_{362}\,$  the parameters must be decorrelated prior to applying the SA. This approach is adopted in the  $_{406}\,$
- <sup>364</sup> procedure of Mara and Tarantola [12, 13, 14]. In their original work, the samples are drawn from <sup>406</sup>

the correlated joint distribution and define a set of new variables, which are characterized by the con-

ditional probability density functions and as such can be treated as independent. In this work, the

- collocation points are sampled using the independent unit normal distributions  $\rho_{Q} = \mathcal{N}^{D}(\boldsymbol{\mu}, I)$ ,
- $_{372}\,$  while the model is evaluated using the transformed samples considering also the dependencies. Fig. 1  $_{412}\,$
- <sup>374</sup> illustrates this principle, the independent collocation nodes and their transformation to the target 414
- <sup>376</sup> correlated distribution  $\rho_{Q}^{*} = \mathcal{N}^{D}(\boldsymbol{\mu}, \mathcal{C})$ . Since the linear relationship between the random variables is 416
- characterized using the Pearson and Spearman correlation coefficients, the correlated samples can be 418
- obtained from the independent ones using two different methods; (i) Rosenblatt transformation [17] 420
- and (ii) Cholesky decomposition of the correlation matrix [18].

## 384 4.1. Cholesky Decomposition

Independent samples with an identity correlation matrix are drawn from a joint multivariate distri-<sup>426</sup> bution

$$\boldsymbol{Q} \sim \mathcal{N}^D(\boldsymbol{\mu}, I). \tag{12}$$

Since the components  $Q_i$  are random variables with zero mean and unit variance with zero correlation, 430 we have  $\mathbb{E}(Q_i Q_j) = \delta_{ij}$ . Hence,  $\mathbb{E}(QQ^T) = I$ . The joint probability of the independent variables can be expressed as the product of the marginal distributions. On the other hand, the joint distribution of the dependent variables

$$\boldsymbol{Q}^* \sim \mathcal{N}^D(\boldsymbol{\mu}, \mathcal{C}). \tag{13}$$

can be expressed as a product of the conditional distributions, which are not known. An alternative approach is it to introduce a transformation between the two spaces of the variables, such that the independent variables Q can be transformed to  $Q^*$  and vice versa. The transformation is defined via the Cholesky decomposition of the correlation matrix. The Cholesky decomposition of the correlation matrix C is computed such that L = chol(C), and  $LL^T = C$ , where

$$L = \begin{pmatrix} c_{11} & & \\ c_{21} & c_{22} & \\ c_{31} & c_{32} & c_{33} \end{pmatrix}.$$
 (14)

The uncorrelated samples Q are then transformed to samples that contain the correlations between the variables, as given by the correlation matrix, such that the transformed samples behave as drawn from the correlated distribution, i.e.,  $Q^* = T(Q) = LQ$ , where T is the transformation operator,

$$\begin{pmatrix} Q_1^* \\ Q_2^* \\ Q_3^* \end{pmatrix} = \begin{pmatrix} c_{11} & & \\ c_{21} & c_{22} & \\ c_{31} & c_{32} & c_{33} \end{pmatrix} \begin{pmatrix} Q_1 \\ Q_2 \\ Q_3 \end{pmatrix}.$$
(15)

The random vector  $\mathbf{Q}^*$  behaves such that  $\mathbb{E}(\mathbf{Q}^*\mathbf{Q}^{*T}) = \mathbb{E}((L\mathbf{Q})(L\mathbf{Q})^T) = \mathbb{E}(L\mathbf{Q}\mathbf{Q}^T L^T) = L\mathbb{E}(\mathbf{Q}\mathbf{Q}^T)L^T = LIL^T = C$ , since expectation is a linear operator. Hence, the transformed random vector  $\mathbf{Q}^*$  has the desired correlation matrix C and  $\mathbf{Q}^* \sim \mathcal{N}^D(\boldsymbol{\mu}, \mathcal{C})$ . One of the requirements for the Cholesky decomposition is that the matrix is positive definite. In practice, the sample covariance matrix is always at least positive semi-definite [19]. In certain situations, the eigenvalues of a covariance matrix can be zero. This can happen when the set of parameters includes constant or perfectly correlated variables, or the sample size is too small. In this work, the covariance matrix is always assumed to be positive definite.

### 4.2. Rosenblatt Transformation

The Rosenblatt transformation [17] allows for a vector of independent random variables Q generated from the distribution  $\rho_Q$  to be transformed

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# Algorithm 2 SA Method with Correlations.

Generation of samples and their transformation:

- 1. Generate samples  $\mathbf{q}_1, \ldots, \mathbf{q}_N$  from the independent multivariate distribution  $\rho_{\mathbf{Q}}$ .
- 2. Transform the samples  $\mathbf{q}_i \in \rho_{\mathbf{Q}}$  to  $\mathbf{q}_i^* \in \rho_{\mathbf{Q}}^*$ ,  $i = 1, \dots, N$ , using:
  - (a) Cholesky transformation  $\mathbf{q}_i^* = T(\mathbf{q}_i) = \mathbf{q}_i L$  from (14).
  - (b) Rosenblatt transformation  $\mathbf{q}_i^* = T(\mathbf{q}_i)$  from (18).

Construction of the surrogate model:

- 1. Evaluate the true model  $\boldsymbol{Y}_1^* = U(\boldsymbol{x}, \mathbf{t}, \mathbf{q}_1^*), \dots, \boldsymbol{Y}_N^* = U(\boldsymbol{x}, \mathbf{t}, \mathbf{q}_N^*)$  at  $\mathbf{q}_i^* \in \rho_{\boldsymbol{Q}}^*$ .
- 2. Create a polynomial expansion  $\Psi_1, \ldots, \Psi_P$  up to the *P*-th degree from  $\rho_Q$ .
- 3. Solve the linear regression problem:  $\boldsymbol{Y}_n^* = \sum_p a_p \Psi_p(\boldsymbol{Q}_n)$  for  $a_1, \ldots, a_p$ .
- 4. Construct the model approximation  $U(\boldsymbol{x}, \mathbf{t}, \boldsymbol{Q}^*) \approx \hat{U}(\boldsymbol{x}, \mathbf{t}, \boldsymbol{Q}) = \sum_p a_p \Psi_p(\boldsymbol{Q}).$

Algorithm 3 Evaluation of the Sensitivity Indices.

Variance-based analysis:

1. Compute the variance-based indices  $S_i$  from the coefficients of  $\hat{U}(\boldsymbol{x}, \boldsymbol{t}, \boldsymbol{Q})$  according to (8) [5, 10].

Derivative-based analysis:

- 1. Compute the partial derivatives of the polynomial model  $\hat{U}(\boldsymbol{x}, \boldsymbol{t}, \boldsymbol{Q})$  with respect to  $Q_i$  according to (11).
- 2. Evaluate the derivatives at the point of interest, e.g. the mean value of the parameters, in order to obtain the sensitivity indices  $S_i^{\mathcal{D}}$ .

to the target distribution  $\rho_{Q}^{*}$  which contains cor-<sup>446</sup> <sup>432</sup> relations between the variables. The transformed

samples  $Q^* = T(Q)$  behave as if they were drawn 448 434 from the target density  $\rho_Q^*$ .

The Rosenblatt transformation can be derived

from a probability decomposition of a bivariate random variable  $Q^* = (Q_1^*, Q_2^*)$  with a correlation as

$$\rho_{\boldsymbol{Q}}^* = \rho_{Q_1} \rho_{Q_2|Q_1}, \tag{16} \quad {}_{452}$$

<sup>438</sup> where  $\rho_{Q_1}$  is a marginal density function, and <sup>454</sup>  $\rho_{Q_2|Q_1}$  is a conditional density. In a general mul-

440 tivariate case, the density decomposition has the 456 form

$$\rho_{\boldsymbol{Q}}^* = \rho_{Q_1} \prod_{d_i=2}^{D} \rho_{Q_{d_i}}', \qquad (17)^{458}$$

where  $\rho'_{Q_{d_i}} = \rho_{Q_{d_i}} | \rho_{Q_1}, \dots, \rho_{Q_{d_{i-1}}}$  is conditioned on all components with lower indices. A forward 462

<sup>444</sup> Rosenblatt transformation is then defined as

$$T = \left(F_{Q'_1}, \dots, F_{Q'_d}\right),\tag{18}$$

where  $F_{Q'_{d_i}}$  is the cumulative distribution function

$$F_{Q'_{d_i}} = \int_{-\infty}^{q_{d_i}} \rho_{Q'_{d_i}} \left( r \mid q_1, \dots, q_{d_i-1} \right) \mathrm{d}r.$$
(19)

Note also that the Rosenblatt transformation is not limited to only Gaussian distributions. In this work, the implementation of the transformation implemented in the Chaospy [3] package is used.

# 4.3. SA Method with Correlations

The SA algorithm introduced in Alg. 1 needs to be modified in presence of the correlated inputs in order to correctly represent the input-output interactions and the sensitivity indices. The changes are summarized in the modified method presented in Alg. 2.

The modified method first needs to generate the parameter samples including the correlations. As before, the set of the parameter samples  $\mathbf{q}$  is generated from the independent joint distribution  $\rho_{\boldsymbol{Q}}$  which are subsequently transformed according to the stochastic dependency structure. The correlated samples  $\mathbf{q}^* = T(\mathbf{q})$  can be obtained using either the Cholesky or Rosenblatt transformations.

Having created the correlated samples, the modified method next evaluates the true model using the correlated samples  $\mathbf{Y}^* = U(\mathbf{x}, \mathbf{t}, \mathbf{q}^*)$ . The surrogate model is constructed in the transformed coordinate space compared to the independent model, reflecting the correlated contributions which affect

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the model outputs. This coordinate space is transformed implicitly, by mapping the polynomial expansion generated from the independent distribu-512

tion  $\rho_{Q}$ , to the space of the correlated model outputs  $\boldsymbol{Y}_{n}^{*}$ . In other words, the linear regression

$$\boldsymbol{Y}_{n}^{*} = \sum_{n} a_{p}(t) \Psi_{p}(\mathbf{q}_{n}) \tag{20}$$

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- <sup>476</sup> is solved, where the left-hand side term is in the <sup>518</sup> correlated space, while the polynomial expansion
- <sup>478</sup> and the samples  $\mathbf{q}_n$  at the right-hand side is from the uncorrelated space. Such surrogate model is
- then used to perform the SA summarized in Alg. 3.

#### 4.4. Interpretation of the Sensitivity Indices

<sup>482</sup> The sensitivity indices computed following the <sup>526</sup> method presented in Alg. 2 and 3 need to be inter-

- <sup>484</sup> preted differently, compared to their counterparts <sub>528</sub> computed without any parameter dependencies (see
- <sup>496</sup> Sec. 3.1 and 3.2). One needs to consider the fact that the parameter transformations effectively in-
- 438 troduce new variables, which are a combination of the original ones in case of linear dependencies. 530
- <sup>490</sup> Consequently, the resulting indices either include the effects of the parameter itself together with its
- <sup>492</sup> dependence with other inputs or it can represents the sensitivity index without its mutual dependent

<sup>494</sup> contributions with other parameters. When applying the transformation a particular

- <sup>496</sup> ordering of the parameters is assumed, e.g., the <sup>534</sup> natural ordering  $\mathcal{P}_1 = (1, 2, \dots, D)$  with the pa-<sup>498</sup> rameters  $\mathcal{P}_1 \mathbf{Q} = (Q_1, Q_2, \dots, Q_D)$ . The transfor- <sup>536</sup>
- mation is then applied sequentially, where the first
- <sup>500</sup> parameter is kept unmodified, while the others are <sup>538</sup> transformed according to the particular correlation
- <sup>502</sup> structure. Considering a vector of the input param- <sup>540</sup> eters  $\mathcal{P}_1 \boldsymbol{Q}$ , the correlated vector is formed as

$$Q_1^* = Q_1,$$
  

$$Q_2^* = Q_2 | Q_1,$$
  

$$Q_3^* = Q_3 | Q_1 Q_2,$$
(21)

$$Q_D^* = Q_D | Q_1 Q_2 \dots Q_{D-1}.$$

<sup>504</sup> The resulting sensitivity indices obtained by applying the SA with correlations using the trans-

:

- formed samples  $Q^* = (Q_1^*, Q_2^*, \dots, Q_D^*)$  need to be interpreted differently, since different variables
- have been used compared to the original variables  ${}_{552}$ Q. One needs to distinguish between the Full and

Independent indices. The Full index includes the effects of the parameter itself together with its dependence with all other inputs. On the other hand, the Independent index represents the contribution of a parameter without its mutual dependent interactions with other parameters. Using the permutation  $\mathcal{P}_1$ , the Full index for the parameter  $Q_1$ is obtained, together with the Independent index for the parameter  $Q_D$ . The Full index is obtained for the first parameter in the permuted vector  $\mathcal{P}_1 Q$ , while the independent index corresponds to the last parameter in the permuted vector. The sensitivity indices of the remaining variables in the vector  $\mathcal{P}_1 \mathbf{Q}$ , that is  $(Q_2, \ldots, Q_{D-1})$ , express the marginal contribution of  $Q_i$ , i = 2, ..., D - 1 to the output variance without its correlative contributions with parameters  $Q_j, \forall j : j < i$ . Thus, under the permutation  $\mathcal{P}_1$  the Full index for the parameter  $Q_1$  is defined as

$$S_1 = \frac{\mathbb{V}(\mathbb{E}(Y_n | Q_1^*))}{\mathbb{V}(Y_n)},$$
(22)

while the Independent index for the parameter  $Q_D$  is defined as

$$S_D = \frac{\mathbb{V}(\mathbb{E}(Y_n | Q_D^*))}{\mathbb{V}(Y_n)}.$$
(23)

Note that the Full index is computed for the parameter  $Q_1^* = Q_1$  which is chosen from its marginal distribution  $\rho_{Q_1}$  and that it carries mutual contributions to the total variance due to the dependence on other parameters  $Q_j$ , j > 1. On the other hand, the Independent index for the parameter  $Q_D^* = Q_D |Q_1 Q_2 \dots Q_{D-1}$  does not contain the mutual contributions with other parameters, since the parameter was drawn from the conditional distribution  $\rho_{Q_D} |Q_1 Q_2 \dots Q_{D-1}$ .

In order to compute the remaining Full and Independent indices, different permutations need to be used. For example  $\mathcal{P}_2 = (2, \ldots, D, 1)$ , such that  $\mathcal{P}_2 \mathbf{Q} = (Q_2, Q_3, \ldots, Q_D, Q_1)$  from which the Full index of parameter  $Q_2$  and Independent index of  $Q_1$ can be determined. Overall, there exist D! different permutations. However, both indices for all parameters can be obtained by circularly reordering the input vector  $\mathbf{Q}$ , i.e., performing the SA D times in total, as summarized in Tab. 1.

# 5. Application Model

The coffee cup model [4] simulates a cooling process of a liquid contained in an open container. The

Table 1: Sensitivity indices for different parameter permutations  $\mathcal{P}_i$ .

Permutation	Full Index	Marginal Indices	Independent Index
$\mathcal{P}_1 = (1, 2, 3, \dots, D)$	$Q_1$	$Q_2,\ldots,Q_{D-1}$	$Q_D$
$\mathcal{P}_2 = (2, 3, \dots, D, 1)$	$Q_2$	$Q_3,\ldots,Q_D$	$Q_1$
$\mathcal{P}_3 = (3, \dots, D, 1, 2)$	$Q_3$	$Q_4,\ldots,Q_D,Q_1$	$Q_2$
:	:		:
$\mathcal{P}_D = (D, 1, 2, \dots, D-1)$	$Q_D$	$Q_1,\ldots,Q_{D-2}$	$Q_{D-1}$

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model uses Newton's law of cooling to evolve the  $_{588}$  temperature T over the simulation time t,

$$\frac{dT(t)}{dt} = -\kappa(T(t) - T_{env}). \tag{24}$$

- The parameter  $\kappa$  characterizes the container containing the liquid and the rate at which it dissipates
- the heat to the environment. Ambient temperature of the environment is represented by the parameter
- $T_{env}$ , while the initial temperature of the liquid is specified by the constant  $T_0 = 95^{\circ}$ C.
- In this study, the SA of the  $\kappa$  and  $T_{env}$  parameters is studied. Due to the measurement error, in-
- $_{564}~$  sufficient knowledge of the physical model or other reasons, the parameters  $\kappa$  and  $T_{env}$  cannot be as-
- 566 signed an exact numerical value representing the modeled physical system. Instead the parameters
- <sup>568</sup> are modeled as uncertain and they are described with probability distributions. A normal distribu-
- tion  $\mathcal{N}(\mu, \sigma)$  is assumed in this work, with a given mean  $\mu$  and standard deviation  $\sigma$  for each parameter.

$$\kappa = \mathcal{N}(0.05, 0.008), \tag{25}$$

$$T_{env} = \mathcal{N}(20, 1.5). \tag{25}$$

On top of the uncertainty in the individual pa-

<sup>574</sup> rameters, these parameters might be correlated <sup>612</sup> with each other. The correlation captures a physi-

- <sup>576</sup> cal property of the container's material and its heat <sup>614</sup> transfer rate, witch changes depending on the ambi-
- ent temperature of the environment. For example, as the ambient temperature  $T_{env}$  increases, the ma-
- terial dissipates the heat more efficiently, increasing  $_{616}$  also the value of the parameter  $\kappa$ . The stochastic
- $_{\rm 582}$  dependency of the two parameters is described us-  $_{\rm 618}$  ing a correlation matrix C with correlation between
- 584 the parameters specified by  $\rho_{\mathcal{C}}$  ,

$$C = \begin{pmatrix} 1.0 & \rho_{\mathcal{C}} \\ \rho_{\mathcal{C}} & 1.0 \end{pmatrix}.$$
 (26) 622

Fig. 1 illustrates the probability density function of 624 the parameters, both with and without the correla-

tion. The goal of the SA is to analyze the impact  $_{\rm 626}$ 

of the uncertain parameters to the outcome of the model, considering also the correlation between the parameters.

#### 5.1. Software Tools and Libraries

The VECMA toolkit, or VECMAtk [20], is used to manage the simulations required for the analysis. It enables automated verification, validation and UQ for complex applications, irrespective of their source domain. VECMAtk is optimized for large scale computations, and can be deployed on emerging high-performance computing (HPC) platforms. The toolkit has previously been used for a range of applications, such as a COVID model [21] (with computational complexity in order of  $10^4$  core hours per experiment), a molecular dynamics model [22] (experiments consumed  $2 \cdot 10^6$  core hours), and a range of other applications [6].

The EasyVVUQ package [16], a component of the VECMA toolkit, has been developed to facilitate forward UQ for HPC applications. EasyVVUQ supports the definition of custom UQ and SA procedures, which may include sampling and analysis, without requiring users to modify their core applications. It has been applied successfully to a diverse set of applications, and is able to cope with procedures that require thousands of simulation runs. EasyVVUQ is open source and written in Python 3.

### 6. Numerical Experiments

Numerical experiments are performed using the model introduced in Sec. 5. The initial condition for the differential equation (24) used hereafter is  $T_0 = 95^{\circ}$ C. The simulation time covers first t = 200 minutes of the cooling process, with the time discretized into 150 time steps of length  $\Delta t = 80 s$ . The parameter distributions used in the numerical experiments, if not stated otherwise, are defined in Eq. (25) and (26). The surrogate model is constructed using polynomials up to the third order, unless specified otherwise.



Figure 2: Surrogate models  $\hat{U}_{\rho_0}$ ,  $\hat{U}_{\rho_c}$  for the coffee cup model with independent and correlated inputs at various time instants.



Figure 3: Difference between the surrogate models  $\hat{U}_{\rho_0}$  and  $\hat{U}_{\rho_c}$  with independent and correlated inputs at various time instants.

6.1. Surrogate Models

- <sup>628</sup> The polynomial surrogates of the model (24) are <sup>634</sup> examined in the vicinity of the mean value of the pa-
- rameters (25). The surrogate model is built for each 636 time instant of the discretized time horizon, depict-
- $_{\rm 632}$   $\,$  ing the model output as a function of the particular  $\,$   $_{\rm 638}$

values of the input parameters. The surrogate models at various time instants t for the coffee cup are illustrated in Fig. 2, demonstrating the effect of the correlation in the parameters. Note that while the difference between the two models is small near the begging of the simulation time, the gap between



Figure 4: Statistical moments of the coffee cup model.

the two grows as the time progresses. The changesin the final temperature profile are exaggerated bythe interaction of the parameters within the model

<sup>642</sup> over time, thus the effect of the correlation is particularly visible at advanced simulation time, i.e.,

 $t > 20 - 30 \, min$ . The absolute difference between the uncorrelated and correlated surrogate models

<sup>646</sup>  $e = \hat{U}_{\rho_{\mathcal{C}}} - \hat{U}_{\rho_{0}}$  with  $\rho_{\mathcal{C}} = 0.8$  is illustrated in Fig. 3. It is also important to highlight different curvature of the surrogate models, since during the

- <sup>648</sup> vature of the surrogate models, since during the derivative-based analysis a partial derivative of the
- <sup>650</sup> surrogate with respect to a parameter is evaluated at the mean value of the parameters. Similarly as
- <sup>652</sup> before, the curvature difference between the two models  $\hat{U}_{\rho_{\mathcal{C}}}$ ,  $\hat{U}_{\rho_0}$  grows with the proceeding sim-
- 654 ulation time.

# 6.2. SA with Uncorrelated Parameters

- <sup>656</sup> In case the correlation matrix C is an identity matrix, i.e., there is no correlation between the pa-
- $_{658}$  rameters, the model evolution is shown in Fig. 4. The model variance due to the uncertainty in the  $_{690}$
- <sup>660</sup> input parameters is shown as well. Note that the model variance at the initial point is zero, thus the
- <sup>662</sup> Sobol indices are not defined at this time instant.

#### Variance-based Indices

- <sup>664</sup> The corresponding sensitivity indices are shown <sup>696</sup> in Fig. 5, replicating the values of the variance-
- based Sobol indices from previous works, e.g., [4].
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   The difference of the first and total order variance-
- based indices, shown in the left panel of Fig. 5, are  $_{700}$  less than  $10^{-4}$ , indicating there are no higher order
- $_{\rm 670}$  parameter interactions. The first order Sobol index  $_{\rm 702}$  of the  $\kappa$  parameter is the most influential in the first
- <sup>672</sup> 75 minutes, while the ambient temperature parameter dominates in the remaining simulation time.
- <sup>674</sup> After reaching near equilibrium, i.e. the ambient and the coffee cup temperature difference is less
- than  $\approx 0.1^{\circ}$ C, the ambient temperature parameter 708



Figure 5: First-order Sobol and derivative-based indices considering the independent parameters.



Figure 6: Derivative-based indices using linear and logarithmic y-axis scale. Note that the absolute values of the sensitivity indices are used in the latter case.

explains nearly all of the output variance as shown in Fig. 4. Intuitively, this is an expected behavior or the model, since the end state of the coffee cup after reaching the equilibrium is the environment temperature. Since there are no higher order interactions, the first order Sobol indices add up to one. Consequently, the behavior of the indices is necessarily complementary for the two parameters, i.e., if one index is increasing, the other is proportionally decreasing and vice versa.

#### Derivative-based Indices

The derivative-based indices, shown in the right panel of Fig. 5, provide an insight into the model around the vicinity of a fixed point, in this case the mean value of the model parameters. Following the definition in Eq. (11), the values of the derivativebased index correspond to the slope of a tangent line to the model surface at the given spatial point and time instant. The magnitude of the individual derivative-based sensitivity indices differs by more than two orders of magnitude, thus the sensitivity indices are shown also in the logarithmic scale (considering their absolute values) in Fig. 6. Note that the sensitivity of the parameter  $T_{env}$  is near zero at the beginning of the simulation, which reflects the fact that it has very small contribution to the model output as the temperature of the coffee cup is driven mainly by the heat transfer constant. As the time progresses, the sensitivity of  $T_{env}$  increases and approaches one, meaning that a change of the ambient temperature will have the proportional effect on the model output. This reflects the fact that the final

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(b) Full  $(\mathcal{P}_2)$  and Independent  $(\mathcal{P}_1)$  sensitivity indices of  $T_{env}$ .

Figure 7: Variance-based indices considering correlated parameters ( $\rho_{\mathcal{C}} = 0.4$ ) and the absolute difference with the uncorrelated indices from Fig. 5.

temperature of the coffee cup is equal to the ambient temperature, thus the change in the ambient

temperature induces an equal change in the final  $_{712}$  state of the coffee cup. On the other hand, the sen-  $_{762}$ 

sitivity of the parameter  $\kappa$  is significantly larger but the sensitivity of the parameter decreases over the  $_{764}$ 

simulation time, since the heat transfer is driven mainly by the temperature gradient between the 766

coffee cup and the surrounding environment which

 $_{718}$   $\,$  is largest in the begging of the simulation. As this  $_{768}$  temperature differential decreases, the heat trans-

<sup>720</sup> fer becomes less significant. Note also the negative <sup>770</sup> value of the sensitivity index, meaning that as the

 $_{722}~$  heat transfer parameter  $\kappa$  increases, the output of  $_{772}~$  the model, that is the coffee cup temperature, de-

<sup>724</sup> creases due to a larger effect of the heat transfer.

# 6.3. SA with Parameter Dependency

Next, the correlation matrix  $\mathcal{C}$  is modified, such that the off-diagonal elements are no longer zero,  $_{778}$ 

<sup>728</sup> indicating parameter correlation. If not stated otherwise, the numerical experiments use the value 780

 $_{730}$   $\rho_{\mathcal{C}} = 0.4$  for the Pearson correlation coefficient. The ordering of the indices in SA with correlations be-

<sup>732</sup> comes important and the SA needs to be performed for different permutations, as detailed in Sec. 4.4. 784

### 734 Variance-based Indices

The Sobol indices for the correlated parameters and their difference relative to the baseline experiment with independent parameters is shown in Fig. 7. In order to obtain the complete set of the Full order and Independent indices for both parameters, the SA needs to be executed twice, each time with different parameter permutation. First the permutation  $\mathcal{P}_1 = (\kappa, T_{env})$  is used to obtain the Full order index of the  $\kappa$  and the Independent index for the parameter  $T_{env}$ . Using the second permutation,  $\mathcal{P}_2 = (T_{env}, \kappa)$ , the Full order index of the  $T_{env}$  and the Independent index for the parameter  $\kappa$  are obtained.

The Full order and Independent indices for the parameter  $\kappa$  are shown in Fig. 7a, comparing them to the sensitivity index shown in the previous section with uncorrelated parameters. Considering the Full order index of the  $\kappa$  parameter (permutation  $\mathcal{P}_1$ ), the contribution of this parameter to the output variance near the end of the simulation time is increased compared to the independent case. Since the parameters are positively correlated, increasing the value of parameter  $\kappa$  induces growth also in the  $T_{env}$  parameter, thus increasing the end state equilibrium temperature of the coffee cup. Previously, there was no such interaction of the parameters, thus the variance-based index of the  $\kappa$  parameter was zero at the end of the simulation time. However, the Full index is lower around the simulation time  $t \approx 100 \, min$  compared to the uncorrelated case. This is due to to the fact that increasing  $\kappa$  induces growth of the  $T_{env}$  parameter, which in turn decreases the temperature gradient. Considering the dynamics of the model in (24), the induced of the ambient temperature counteracts the elevated heat transfer, thus the sensitivity of the heat transfer parameter has decreased. When the Independent index is considered (permutation  $\mathcal{P}_2$ ), the effect of the correlation is removed and the index is nearly identical to the independent case in the simulation time t > 100min. However, in the simulation time around  $t \approx 50$  the sensitivity of the  $\kappa$  parameters has increased, thus emphasizing the importance of the parameter at the time instants when the temperature gradient is large. Fig. 7a also shows the absolute difference of the Full order and Independent index compared to the uncorrelated case, in order to illustrate the magnitude of the difference.

The behavior of the first order Sobol index for  $T_{env}$  parameter, as shown in Fig. 7b, is opposite to that of the  $\kappa$  parameter. The Full order index (permutation  $\mathcal{P}_2$ ) matches the independent case at the end of the simulation time (since it was already at the maximum value of 1). Removal of the con-

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Figure 8: Complementary behaviors of the indices.

- <sup>790</sup> tribution of the correlation decreases the value of the index. The magnitude of the change is propor-<sup>792</sup> tional to the difference in the  $\kappa$  parameter indices
- (Full vs. Independent index). This behavior of the
- <sup>794</sup> indices can be interpreted such that the portion of the output variance can be explained by both pa<sup>796</sup> rameters simultaneously since they are correlated.
- It can be equally said that some output variance is <sup>828</sup> explained either by one or the other parameter. In
- an extreme case of the perfect correlation,  $\rho_{12} = 1$ ,  $_{830}$
- it is equivalent to say that the output variance is explained either by one or the other parameter, since 832
- $_{\rm 802}~$  the value of one parameter completely determines the value of the other.  $_{\rm 834}$
- It is also interesting to observe the complement of the indices to one, shown in Fig. 8. Consider 836
- the Full index of the  $\kappa$  parameter, as shown in Fig. 8a. Its complement to one explains the output \$38
- variance contributed by the other parameter alone without its correlated contribution with  $\kappa$ . In case 840
- of two parameters, this complement is the Independent Sobol index of the  $T_{env}$  parameter. In general 842
- $_{\rm ^{812}}$  case with a set of D parameters, complement of the Full index of the parameter i explains the amount of  $_{\rm ^{844}}$
- variance contributed by the remaining D-1 parameters without their correlated contribution with *i*. <sup>846</sup>
- A similar relationship is observed between the complement of the Full index of  $T_{env}$  and Independent index of  $\kappa$  in Fig. 8b. Note the presence of a numer-
- ical error in this case, in order to eliminate it, the <sup>850</sup> indices should be computed with higher order poly-
- nomials in the PCE analysis (see Sec. 6.5). Simi- <sup>852</sup> larly, Fig. 8c,d illustrate the relationship between
- the complement of the Independent indices and the <sup>854</sup> Full indices of the other parameter.



(b) Full  $(\mathcal{P}_2)$  and Independent  $(\mathcal{P}_1)$  sensitivity indices of  $T_{env}$ .



#### Derivative-based Indices

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Behavior of the derivative-based indices in the correlated case for the parameter  $\kappa$  is shown in Fig. 9a. In Sec. 6.2 it was shown that the significance of the heat transfer diminishes toward the end of the simulation time,  $t > 150 \min$ , and the value of the derivative-based index approaches zero. This is due to the fact that the final equilibrium is completely determined by the ambient temperature parameter  $T_{env}$ . However, when we consider correlation between the parameters and the Full order index (permutation  $\mathcal{P}_1$ ) the significance of the parameter  $\kappa$  is increased since the Full order index includes also the interaction with the other parameters due to the correlations. In physical terms, it can be interpreted such as when the parameter  $\kappa$ is increased, the ambient temperature  $T_{env}$  will be increased due to their positive correlation  $\rho_{\mathcal{C}} = 0.4$ . Consequently, the final temperature of the coffee cup will be increased as well and this is reflected accordingly in the Full order index of the  $\kappa$  parameter which is no longer zero as in the uncorrelated case. It is also interesting to observe the behavior around the simulation time  $t \approx 20 \min$ . Note that the magnitude of the Full order index is reduced compared to the uncorrelated case. The reason for this is again the correlated interaction with the  $T_{env}$  parameter. Studying the effect of increasing the  $\kappa$  incurs also an increase in the  $T_{env}$  due to their correlation. This however reduces the temperature gradient when assuming constant initial



(b) First order Independent index of the  $T_{env}$  parameter.

Figure 10: Sobol indices considering dependent parameters with increasing correlation  $\rho_{\mathcal{C}}$  and permutation  $(\kappa, T_{env})$ , showing also difference with respect to the uncorrelated indices.

- temperature of the coffee cup, thus the cooling process is reduced, even though the heat transfer coef-
- ficient was increased. This effect is represented by the reduced magnitude of the Full order index of  $\kappa$
- parameter around the simulation time  $t \approx 20 min$ . Similar logic applies when considering the Inde-
- <sup>862</sup> pendent index. Consider the Independent index of <sup>8</sup> the  $T_{env}$  parameter (permutation  $\mathcal{P}_1$ ) in Fig. 9b.
- In the uncorrelated case, the equilibrium near the find of the simulation time, t > 150 min, was com-
- <sup>866</sup> pletely determined by the  $T_{env}$  parameter. In the <sup>888</sup> correlated case, after removing the effect of the cor-
- relation, the Independent index is proportionally <sup>890</sup> reduced since a part of the ambient temperature mouth mag induced by the effect of the maximum <sup>892</sup>
- growth was induced by the effect of the  $\kappa$  parameter and the Independent index eliminates these pa-
- <sup>872</sup> rameter interactions.

# 6.4. Parameters with Increasing Correlation

- <sup>874</sup> It is important to understand the effect of the correlation to the value of the indices. In this section,
- the correlation  $\rho_{\mathcal{C}}$  is gradually increasing in increments of 0.2, ranging from zero all the way to one
- <sup>878</sup> (i.e. from no correlation up to perfect correlation). <sup>902</sup> The largest value of the correlation is slightly re-

duced,  $\rho_{\mathcal{C}} = 1.0 - \epsilon$ ,  $\epsilon = 10^{-10}$ , in order to preserve positive definiteness of the correlation matrix C.

#### 6.4.1. Variance-based Sensitivity

The study of the First order Sobol indices is first performed considering the permutation  $(\kappa, T_{env})$ , which is used to compute Full Sobol index for  $\kappa$  and an Independent index for  $T_{env}$  shown in Fig. 10. It can be observed that as the correlation increases, the Full index of  $\kappa$  at  $t > 125 \min$  in Fig. 10a is gradually increasing, while at the same time the Independent index of the other parameter in Fig. 10b proportionally decreases. This reflects the fact that due to the correlation, the Full index  $\kappa$  becomes gradually more significant due to its correlation with the  $T_{env}$  parameter, not because of the parameter  $\kappa$  itself. On the other hand, the amount of the variance explained by  $T_{env}$  alone decreases with increasing correlation, because of its interaction with  $\kappa$ . In the limit situation when  $\rho_{12} = 1$ , the parameters alone become insignificant and all of the variance is explained by their correlated interaction. Note that the Independent index is zero (Fig. 10b) while the Full index is one (Fig. 10a).

Similar effect can be observed using the permuta-

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(b) First order Independent index of the  $T_{env}$  parameter.

Figure 11: Derivative-based indices considering dependent parameters with increasing correlation  $\rho_{\mathcal{C}}$  and permutation  $(\kappa, T_{env})$ , showing also difference relative to the uncorrelated indices.

tion  $(T_{env}, \kappa)$  used to compute Independent Sobol index for  $\kappa$  and the Full index for  $T_{env}$ .

#### 906 6.4.2. Derivative-based Sensitivity

The effect of increasing correlation for the <sup>908</sup> derivative-based sensitivity indices is shown in Fig. 11. It shows the indices obtained from the per-

mutation  $(\kappa, T_{env})$ , which corresponds to the permutation  $\mathcal{P}_1$  in Fig. 9. It can be seen that the in-

- <sup>912</sup> creasing correlation intensifies the effects described in Sec. 6.3. Note that in the extreme case of cor-
- <sup>914</sup> relation  $\rho_{\mathcal{C}} = 1.0$  the Independent index becomes zero across the whole simulation, as the parameter
- $T_{env}$  is completely explained by the parameter  $\kappa$ . Note that, as opposed to the variance-based sensi-
- <sup>918</sup> tivity indices, this doesn't mean that the Full order index is equal to one across the simulation time, <sub>930</sub>
- $_{\rm 920}~$  since the range of the index values is not bound to the interval (0, 1) nor there is any property similar  $_{\rm 932}$

# <sup>922</sup> to Eq. (10).

#### 6.5. Convergence Analysis

<sup>924</sup> The convergence of the QMC method is tested, <sup>936</sup> which is later used as a reference value for the PCE



Figure 12: Convergence of the QMC method for Sobol indices using permutation  $(\kappa, T_{env})$  with correlation  $\rho_{\mathcal{C}} = 0.417$ .

method. The QMC method is run with an increasing number of samples, and the resulting first order indices are shown in Fig. 12. The absolute difference between the indices is well below the threshold of significance 0.05, thus the method is considered to have converged. The rather arbitrary value of 0.05 is frequently accepted for this type of analysis for distinguishing important parameters from the unimportant ones [23], thus similar idea can be applied to declare a method to converge.

The PCE method is run with an increasing polynomial order, ranging from 2nd to 7th order. Fig-

934



(b) First order index of the  $T_{env}$  parameter.

Figure 13: Convergence of PCE method for variance-based indices with increasing polynomial order (PO) using permu-964 tation  $(\kappa, T_{env})$  with correlation  $\rho_{\mathcal{C}} = 0.417$ .



(b) First order index of the  $T_{env}$  parameter.

Figure 14: Convergence of PCE method for derivative-based 984 indices using permutation  $(\kappa, T_{env})$  with correlation  $\rho_{\mathcal{C}}$  = 0.417.

- 986 ure 13 illustrates that the variance-based indices 938 computed by the PCE method differ from the refer-
- ence value of the QMC by less than 0.05 for polyno-940 mial order three and higher orders. For the fourth
- polynomial order, the difference is below 0.01. For 942 992 practical purposes the analysis can be run with
- 944 third of fourth order polynomials. The difference 994 in the initial point is attributed to the fact that the
- variance in this point is zero and the variance-based 946 Sobol indices are not defined, thus the difference is 998

meaningless here. Convergence of the derivativebased indices with the surrogate polynomial order are shown in Figure 14.

#### 7. Conclusions and Future Work

The SA methods introduced in this paper provides a comprehensive way to quantify the uncertainty and sensitivity of a model with correlated inputs. As demonstrated in the numerical experiments, the sensitivity indices ignoring parameter correlations significantly differ from their counterparts which do account for the correlation. This can have profound implications for assessing the influence of the individual indices on the model sensitivity. In case of the variance-based sensitivity, the model uncertainty can be over/under-estimated at the presence of the correlation. In case of the derivative-based indices, it was demonstrated that the sensitivity of the associated parameters can not only differ in magnitude, but even invert the sign of the derivative-based index, thus reversing the model behavior compared to the prediction of the study disregarding the correlations. In conclusion, it is essential to consider the parameter correlations during the SA in order to get realistic estimation of the sensitivity indices.

A comprehensible and easy to understand application model in this work was intentionally chosen in order to intuitively understand the input-output interactions and to clearly demonstrate the impact of the input parameter correlations on the sensitivity indices. In the follow-up work we will apply the method to a large-scale model from the domain of energy markets, where the input parameters such as fossil fuel prices are often correlated. We will evaluate the impact of the correlations on the sensitivity analysis, and explore also associated highperformance computational aspects.

#### References

- A. Saltelli, Sensitivity analysis in practice: A guide to [1]assessing scientific models, Wiley, Chichester Hoboken, N.J, 2004, ISBN 978-0-470-87094-5.
- I. Sobol, Global sensitivity indices for nonlinear mathematical models and their monte carlo estimates, Mathematics and Computers in Simulation 55 (1) (2001) 271-280. doi:https://doi.org/10.1016/S0378-4754(00) 00270-6.
- J. Feinberg, H. P. Langtangen, Chaospy: An open [3] source tool for designing methods of uncertainty quantification, Journal of Computational Science 11 (2015) 46 - 57.doi:https://doi.org/10.1016/j.jocs.2015. 08.008.

- [4] S. Tennøe, G. Halnes, G. T. Einevoll, Uncertainpy: A 1064 Python toolbox for uncertainty quantification and sensitivity analysis in computational neuroscience, Fron- 1066
- 1002 tiers in Neuroinformatics 12 (2018) 49. doi:10.3389/ fninf.2018.00049.

1000

- 1004 [5] B. Sudret, Global sensitivity analysis using polynomial chaos expansions, Reliability Engineering & Sys- 1070
- 1006 tem Safety 93 (7) (2008) 964–979, bayesian Networks in Dependability. doi:https://doi.org/10.1016/j. 1072
- ress.2007.04.002.
  [6] D. W. Wright, R. A. Richardson, W. Edeling, et al., 1074
  Building confidence in simulation: Applications of
- 1012
   EasyVUQ, Advanced Theory and Simulations 3 (8) 1076

   1012
   (2020) 1900246. arXiv:https://onlinelibrary. wiley.com/doi/pdf/10.1002/adts.201900246, 1078
- 1014 doi:https://doi.org/10.1002/adts.201900246.
- [7] J. C. Hull, Options, Futures, and Other Derivatives, 9th 1060
   Edition, Pearson, 2021, ISBN 978-0133456318.
- [8] C. Shuai, Y. Deyou, G. Weichun, L. Chuang, C. Guowei, 1082
   <sup>1018</sup> K. Lei, Global sensitivity analysis of voltage stability in the power system with correlated renewable energy, 1084
- 1020
   Electric Power Systems Research 192 (2021) 106916.

   doi:https://doi.org/10.1016/j.epsr.2020.106916.
   1086
- [9] J. Kardoš, D. Kourounis, O. Schenk, R. Zimmerman, BELTISTOS: A robust interior point method for largescale optimal power flow problems, Electric Power Systems Research 212 (2022) 108613. doi:https://doi.1090
- org/10.1016/j.epsr.2022.108613.
   [10] Y. Caniou, Global sensitivity analysis for nested and 1092
   multiscale modelling, Ph.D. thesis, Universitè Blaise
- Pascal (11 2012). 1090 [11] G. Li, H. Rabitz, P. E. Yelvington, O. O. Oluwole,
- F. Bacon, C. E. Kolb, J. Schoendorf, Global sensitivity 1096 analysis for systems with independent and/or correlated inputs, The Journal of Physical Chemistry A 114 (19) 1098
- 1034 (2010) 6022–6032. doi:10.1021/jp9096919. [12] T. A. Mara, W. E. Becker, Polynomial chaos expansion
- [12] T. A. Mara, W. E. Beckel, Forynomial chaos expansion
   for sensitivity analysis of model output with dependent inputs, Reliability Engineering & System Safety
   214 (2021) 107795. doi:https://doi.org/10.1016/j.
- ress.2021.107795. 1040 [13] T. A. Mara, S. Tarantola, Variance-based sensitivity indices for models with dependent inputs, Reliability 1042 Engineering & System Safety 107 (2012) 115–121. doi: https://doi.org/10.1016/j.ress.2011.08.008.
- [14] T. A. Mara, S. Tarantola, P. Annoni, Non-parametric methods for global sensitivity analysis of model output with dependent inputs, Environmental Modelling & Software 72 (2015) 173-183. doi:https://doi.org/ 10.1016/j.envsoft.2015.07.010.
- [15] S. Kucherenko, S. Tarantola, P. Annoni, Estimation of global sensitivity indices for models with de-
- pendent variables, Computer Physics Communications 183 (4) (2012) 937–946. doi:https://doi.org/10. 1016/j.cpc.2011.12.020.
- [16] R. A. Richardson, D. W. Wright, W. Edeling, V. Jancauskas, J. Lakhlili, P. V. Coveney, EasyVVUQ: A li-
- brary for verification, validation and uncertainty quantification in high performance computing, Journal of
  Open Research Software 8 (2020) 11. doi:http://doi.
- org/10.5334/jors.303. 1060 [17] M. Rosenblatt, Remarks on a Multivariate Transformation, The Annals of Mathematical Statistics 23 (3) 1062 (1952) 470 - 472. doi:10.1214/aoms/1177729394.
  - [18] M. Neine, D. Curran, An algorithm to generate corre-

lated input-parameters to be used in probabilistic sensitivity analyses, Journal of market access & health policy 9 (1) (2020) 1857052–1857052. doi:10.1080/20016689. 2020.1857052.

- [19] U. Lorenzo-Seva, P. J. Ferrando, Not positive definite correlation matrices in exploratory item factor analysis: Causes, consequences and a proposed solution, Structural Equation Modeling: A Multidisciplinary Journal 28 (1) (2021) 138-147. arXiv:https: //doi.org/10.1080/10705511.2020.1735393, doi:10. 1080/10705511.2020.1735393.
- [20] D. Suleimenova, H. Arabnejad, W. N. Edeling, D. Coster, et al., Tutorial applications for verification, validation and uncertainty quantification using VECMA toolkit, Journal of Computational Science 53 (2021) 101402. doi:https://doi.org/10.1016/j. jocs.2021.101402.
- [21] W. Edeling, H. Arabnejad, R. Sinclair, D. Suleimenova, et al., The impact of uncertainty on predictions of the CovidSim epidemiological code, Nature Computational Science 1 (2) (2021) 128–135. doi:10.1038/ s43588-021-00028-9.

URL https://doi.org/10.1038/s43588-021-00028-9

- [22] M. Vassaux, S. Wan, W. Edeling, P. V. Coveney, Ensembles are required to handle aleatoric and parametric uncertainty in molecular dynamics simulation, Journal of Chemical Theory and Computation 17 (8) (2021) 5187-5197. arXiv:https://doi.org/10.1021/ acs.jctc.1c00526, doi:10.1021/acs.jctc.1c00526.
- [23] X.-Y. Zhang, M. Trame, L. Lesko, S. Schmidt, Sobol sensitivity analysis: A tool to guide the development and evaluation of systems pharmacology models, CPT: Pharmacometrics & Systems Pharmacology 4 (2) (2015) 69-79. arXiv:https://ascpt. onlinelibrary.wiley.com/doi/pdf/10.1002/psp4.6, doi:https://doi.org/10.1002/psp4.6.