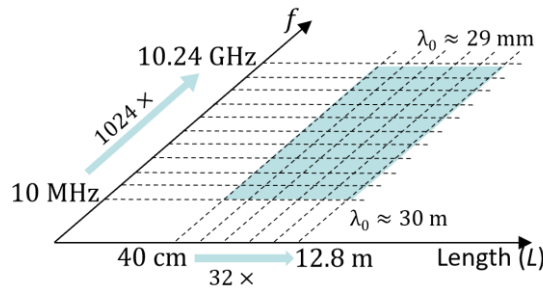


### Description of Scattering Object

A perfect electrically conducting (PEC) hexagonal prism with a “cramped cobra” shaped duct.

### Length Scale and Frequency Range

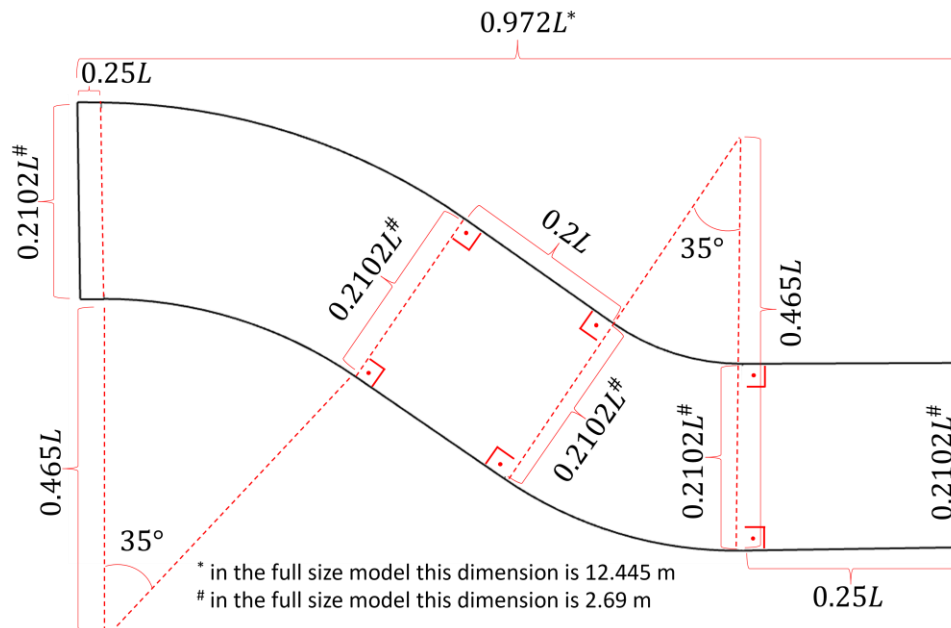
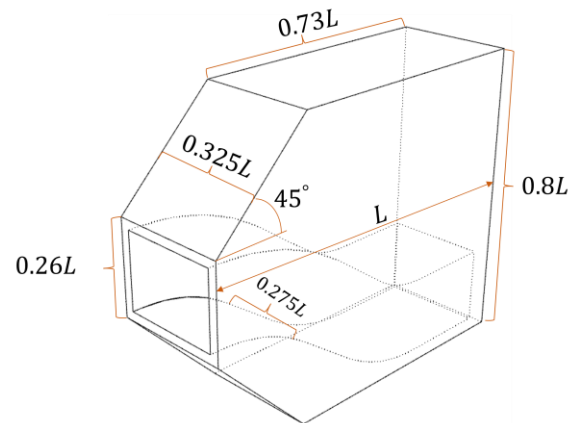


The problems of interest cover a range of 32x in physical length scale and 1024x in frequency; the ranges are logarithmically sampled to yield 66 scattering problems. Because the camera boxes are PEC, there are only 16+1 unique scattering problems in Problem Set IIISB. In these problems, the model sizes are in the range  $0.013 \leq L/\lambda_0 \leq 438$ , where  $\lambda_0$  is the free-space wavelength.

### Interesting Features

1. The camera box is designed as a host structure to enable reproducible RCS measurements of ducts. The flat-plate geometrical features of the housing promote strong backscattering in certain directions that are minimally affected by the scattering characteristics of any voids in the box [1]. Unlike Problem Set IIISA, the front aperture is open to reveal a “cramped cobra” shaped duct<sup>1</sup>, whose precise dimensions are given in the diagram below.

2. The sampling of the frequency range is distorted for this problem: scattering from the smallest camera box at frequencies  $f \in \{10, 20, 40, 80, 160, 320, 640, 1280, 2560, 5120, 7000, 10240\}$  MHz are included in the problem set. This distortion is because of publicly available measurement data [1] and adds 1 unique scattering problem to the set.



<sup>1</sup> The duct is referred to as the “cramped cobra duct” because its dimensions are similar but not identical to the COBRA cavity described in [2] and related publications.

**Quantities of Interest**

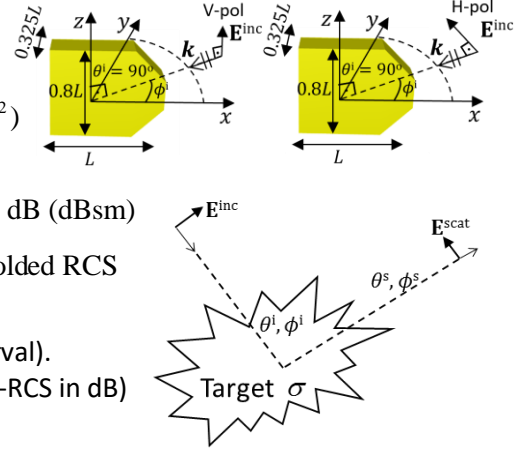
Radar cross section (RCS) definition

$$\sigma_{vu}(\theta^s, \phi^s, \theta^i, \phi^i) = \lim_{R \rightarrow \infty} 4\pi R^2 \frac{|\hat{v}(\theta^s, \phi^s) \mathbf{E}^{\text{scat}}(\theta^s, \phi^s)|^2}{|\hat{u}(\theta^i, \phi^i) \mathbf{E}^{\text{inc}}(\theta^i, \phi^i)|^2} : \text{RCS (m}^2\text{)}$$

$$\sigma_{vu,\text{dB}}(\theta^s, \phi^s, \theta^i, \phi^i) = 10 \log_{10} \sigma_{vu} : \text{RCS in dB (dBsm)}$$

$$\sigma_{vu,\text{dB}}^{\text{TH}}(\theta^s, \phi^s, \theta^i, \phi^i) = \max(\sigma_{vu,\text{dB}}, TH_{vu,\text{dB}}) - TH_{vu,\text{dB}} : \text{Thresholded RCS}$$

1. Set  $\theta^i = 90^\circ$ . Vary  $0^\circ \leq \phi^i \leq 180^\circ$  (every  $0.5^\circ$  in the interval).
2. Compute back-scattered  $\sigma_{\theta\theta,\text{dB}}$  and  $\sigma_{\phi\phi,\text{dB}}$  (the VV- and HH-RCS in dB) at  $N_\phi = 361$  scattering directions.

**Performance Measures**

Error Measure: Simulation errors shall be quantified using

$$\text{avg. err}_{uu,\text{dB}}^{\text{TH}} = \frac{1}{2\pi} \int_0^{2\pi} |\sigma_{uu,\text{dB}}^{\text{TH}}(\phi^s) - \sigma_{uu,\text{dB}}^{\text{ref},\text{TH}}(\phi^s)| d\phi^s \approx \frac{1}{N_\phi} \sum_{n=1}^{N_\phi} |\sigma_{uu,\text{dB}}^{\text{TH}}(\phi^s) - \sigma_{uu,\text{dB}}^{\text{ref},\text{TH}}(\phi^s)| \text{ (dB) for } u \in \{\theta, \phi\}$$

where

$$TH_{uu,\text{dB}} = \max_{\phi^s} \sigma_{uu,\text{dB}}^{\text{ref}} - 80 \text{ (dB)}$$

This error measure discounts errors in RCS values below  $TH$ .

Cost Measure: Simulation costs shall be quantified using observed wall-clock time and peak memory/core

$$t_{\text{main}}^{\text{wall}} \text{ (s) and } mem_{\text{main}}^{\text{maxcore}} \text{ (bytes)}$$

as well as the “serialized” CPU time and total memory requirement

$$t_{\text{main}}^{\text{total}} = N_{\text{proc}} \times t_{\text{main}}^{\text{wall}} \text{ (s) and } mem_{\text{main}}^{\text{max}} = N_{\text{proc}} \times mem_{\text{main}}^{\text{maxcore}} \text{ (bytes)}$$

Here,  $N_{\text{proc}}$  denotes the number of processes used in a parallel simulation. It is expected that results will be reported for at least 2 runs: “Efficient” (small  $N_{\text{proc}}$ ) and “Fast” (large  $N_{\text{proc}}$ ).

**Study 1: Error vs. Cost Sweep**

Fix frequency and fix camera box dimensions. Simulate many error levels (proxy: mesh densities) for 4 cases:

Case 1:  $f=10$  MHz,  $L=40$  cmCase 2:  $f=7$  GHz,  $L=40$  cmCase 3:  $f=10$  MHz,  $L=6.4$  mCase 4:  $f=320$  MHz,  $L=6.4$  m

It's recommended to simulate as many error levels (mesh densities) as possible. 3-5 error levels is typical.

A typical error-vs.-cost study will consist of  $4 \times 3 = 12$ -20 simulations.**Study 2: Frequency Sweep**

Fix camera box dimensions and error level (proxy: mesh density). Simulate many frequencies for 4 cases:

Case 1:  $L=40$  cm, error level 1 (coarsest mesh)Case 2:  $L=6.4$  m, error level 1 (coarsest mesh)Case 3:  $L=40$  cm, error level 2 (finer mesh)Case 4:  $L=6.4$  m, error level 2 (finer mesh)Frequencies shall be chosen as  $f \in \{10, 20, 40, \dots, 5120, 10240\}$  MHz. It's recommended to simulate as many frequencies as possible. A full frequency-sweep study will consist of  $4 \times 11 = 44$  simulations.**Study 3: Size Sweep**

Fix frequency and error level (proxy: mesh density). Simulate many sizes for 4 cases:

Case 1:  $f=10$  MHz, error level 1 (coarsest mesh)Case 2:  $f=320$  MHz, error level 1 (coarsest mesh)Case 3:  $f=10$  MHz, error level 2 (finer mesh)Case 4:  $f=320$  MHz, error level 2 (finer mesh)

Dimensions shall be chosen as  $L \in \{40, 80, 120, \dots, 640, 1280\}$  cm. It's recommended to simulate as many sizes as possible. A full size-sweep study will consist of  $4 \times 7 = 28$  simulations.

### Reference Quantities of Interest

The following RCS data are made available in the benchmark to enable participants to calibrate their simulators:

8 RCS measurement results corresponding to the smallest cobra-ducted camera box ( $L=40$  cm) at frequencies  $f \in \{2560, 5120, 7000, 10240\}$  MHz. These data are provided for  $\phi^i$  sampled every  $0.5^\circ$ . Note that the high return at  $\phi^i = 90^\circ$  saturated the instrumentation radar at 10240 MHz; thus, the measured RCS values near that look angle are inaccurate. The same phenomenon can be observed in Fig. 3 in [1].

4 RCS simulation results for the smallest cobra-ducted camera box at the above 4 frequencies found by using the ARCHIE-AIM code, a frequency-domain FFT-accelerated integral-equation solver developed at UT Austin [3]-[5].

### References

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