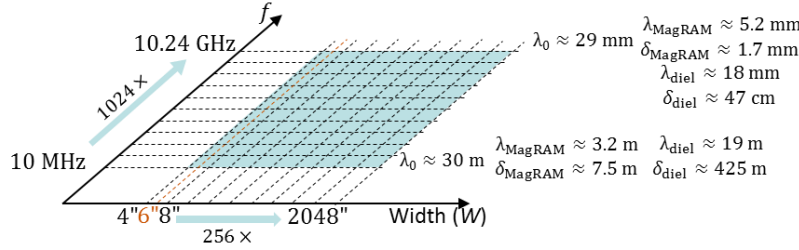


### Description of Scattering Object

A homogeneous low-loss dielectric plate of size  $W \times 7W/4 \times 1.5$  mm coated with a 1.5 mm thick lossy magneto-dielectric material.

### Length Scale and Frequency Range



The problems of interest cover a range of 512x in physical length scale and 1024x in frequency; the ranges are logarithmically sampled to yield 110 scattering problems. Because of the extra data for the  $W = 6$  in plate, there are  $110 + 12$  unique scattering problems in

Problem Set IIF. In these problems, the plate sizes are in the range  $0.0033 \leq W/\lambda_0 \leq 1776$ ,  $2.4 \times 10^{-4} \leq W/\delta_{\text{diel}} \leq 111$ , and  $1.3 \times 10^{-2} \leq W/\delta_{\text{MagRAM}} \leq 3.2 \times 10^4$ , where  $\lambda_0$  is the free-space wavelength,  $\delta_{\text{diel}}$  is the penetration depth in the dielectric, and  $\delta_{\text{MagRAM}}$  is the penetration depth in the magnetic radar absorbing (MagRAM) material. The length and width of the dielectric plates were chosen to approximately match the plate targets in [1], while the thickness of the plate and of the coating were chosen to match an available sample of ARC Technologies' DD-13490, a flexible silicone rubber microwave absorber [2].

### Interesting Features

1. The logarithmic sampling is distorted along the length axis and an extra plate of  $W = 6$  in is introduced because of publicly available measurement data corresponding to this size [3]. The sampling is also distorted along the frequency axis: scattering from the plate of  $W = 6$  in at frequencies  $f \in \{10, 20, 40, 80, 160, 320, 640, 1280, 2560, 5120, 7000, 10240\}$  MHz are included in the problem set because of publicly available measurement data [3]. These distortions add 12 unique scattering problems to the set.
2. The thin side wall presents meshing and accurate integration challenges.
3. The lossy magneto-dielectric material introduces extra uncertainties and sensitivities to RCS measurements and simulations [4].
4. The material diversity and junction in the composite object present challenges for RCS simulations [3].

### Quantities of Interest

Radar cross section (RCS) definition

$$\sigma_{vu}(\theta^s, \phi^s, \theta^i, \phi^i) = \lim_{R \rightarrow \infty} 4\pi R \frac{|\hat{v}(\theta^s, \phi^s) \cdot \mathbf{E}^{\text{scat}}(\theta^s, \phi^s)|^2}{|\hat{u}(\theta^i, \phi^i) \cdot \mathbf{E}^{\text{scat}}(\theta^i, \phi^i)|^2} : \text{RCS (m}^2\text{)}$$

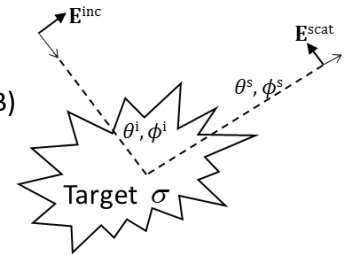
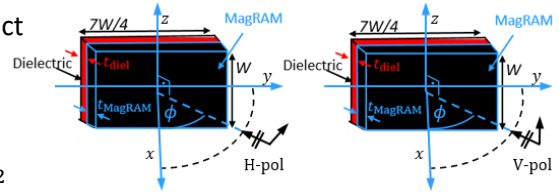
$$\sigma_{vu,\text{dB}}(\theta^s, \phi^s, \theta^i, \phi^i) = 10 \log_{10} \sigma_{vu} : \text{RCS in dB (dBsm)}$$

$$\sigma_{vu,\text{dB}}^{TH}(\theta^s, \phi^s, \theta^i, \phi^i) = \max(\sigma_{vu,\text{dB}}, TH_{vu,\text{dB}}) - TH_{vu,\text{dB}} : \text{Thresholded RCS}$$

1. Set  $\theta^i = 90^\circ$ . Vary  $0^\circ \leq \phi^i \leq 180^\circ$  (every  $0.5^\circ$  in the interval).
2. Compute back-scattered  $\sigma_{\theta\theta,\text{dB}}$  and  $\sigma_{\phi\phi,\text{dB}}$  (the VV- and HH-pol RCS in dB) at  $N_\phi = 361$  scattering directions.

### Material Properties

The material properties of the dielectric and the MagRAM may be found in the problem description documents for Problem Set IIC-Thin Dielectric Plates and Problem Set IID-Thin MagRAM Plates.



### Performance Measures

**Error Measure:** Simulation errors shall be quantified using

$$avg. err_{uu, dB}^{TH} = \frac{1}{2\pi} \int_0^{2\pi} |\sigma_{uu, dB}^{TH}(\phi^s) - \sigma_{uu, dB}^{ref, TH}(\phi^s)| d\phi^s \approx \frac{1}{N_\phi} \sum_{n=1}^{N_\phi} |\sigma_{uu, dB}^{TH}(\phi_n^s) - \sigma_{uu, dB}^{ref, TH}(\phi_n^s)| \quad (\text{dB}) \quad \text{for } u \in \{\theta, \phi\}$$

where

$$TH_{uu, dB} = \max_{\phi^s} \sigma_{uu, dB}^{ref} - 80 \quad (\text{dB})$$

This error measure discounts errors in RCS values smaller than  $TH$ .

**Cost Measure:** Simulation costs shall be quantified using observed wall-clock time and peak memory/process

$$t^{wall}(\text{s}) \text{ and } mem^{maxproc}(\text{bytes})$$

as well as the “serialized” CPU time and total memory requirement

$$t^{total} = N_{proc} \times t^{wall}(\text{s}) \text{ and } mem^{max} = N_{proc} \times mem^{maxproc}(\text{bytes})$$

Here,  $N_{proc}$  denotes the number of processes used in a parallel simulation. It is expected that results will be reported for at least 2 runs: “Efficient” (small  $N_{proc}$ ) and “Fast” (large  $N_{proc}$ ).

### Study 1: Error vs. Cost Sweep

Fix frequency and fix plate dimensions. Simulate many error levels (proxy: mesh densities) for 4 cases:

Case 1:  $f=10$  MHz,  $W=6$  in

Case 2:  $f=7$  GHz,  $W=6$  in (measurement frequency)

Case 3:  $f=10$  MHz,  $W=128$  in

Case 4:  $f=320$  MHz,  $W=128$  in

It’s recommended to simulate as many error levels (mesh densities) as possible. 3-5 error levels is typical.

A typical error-vs.-cost study will consist of  $4 \times 3 = 12$  simulations.

### Study 2: Frequency Sweep

Fix plate dimensions and error level (proxy: mesh density). Simulate many frequencies for 4 cases:

Case 1:  $W=6$  in, error level 1 (coarsest mesh)

Case 2:  $W=128$  in, error level 1 (coarsest mesh)

Case 3:  $W=6$  in, error level 2 (finer mesh)

Case 4:  $W=128$  in, error level 2 (finer mesh)

Frequencies shall be chosen as  $f \in \{10, 20, 40, \dots, 5120, 10240\}$  MHz. It’s recommended to simulate as many frequencies as possible. A full frequency-sweep study will consist of  $4 \times 11 = 44$  simulations.

### Study 3: Size Sweep

Fix frequency and error level (proxy: mesh density). Simulate many sizes for 4 cases:

Case 1:  $f=10$  MHz, error level 1 (coarsest mesh)

Case 2:  $f=320$  MHz, error level 1 (coarsest mesh)

Case 3:  $f=10$  MHz, error level 2 (finer mesh)

Case 4:  $f=320$  MHz, error level 2 (finer mesh)

Dimensions shall be chosen as  $W \in \{4, 8, 16, \dots, 1024, 2048\}$  in. It’s recommended to simulate as many sizes as possible. A full size-sweep study will consist of  $4 \times 10 = 40$  simulations.

### Reference Quantities of Interest

The following RCS data are made available in the benchmark to enable participants to calibrate their simulators:

4 RCS measurement results corresponding to the  $W=6$  in plate at frequencies  $f \in \{2560, 5120, 7000, 10240\}$  MHz. They are provided for  $\phi^i$  sampled every  $0.25^\circ$ . The HH-polarized data are the same as those plotted in Fig. 8 of [3].

### References

- [1] A. C. Woo, H. T. G. Wang, M. J. Schuh and M. L. Sanders, “EM programmer's notebook-benchmark radar targets for the validation of computational electromagnetics programs,” *IEEE Ant. Propag. Soc. Mag.*, vol. 35, no. 1, pp. 84-89, Feb. 1993.

- [2] ARC Technologies, "Technical Data Sheet DD-13490. [Online]. Available: <http://arc-tech.com/pdf/DD-13490%20Rev%20C.pdf>
- [3] J. T. Kelley, D. A. Chamulak, C. Courtney, and A. E. Yilmaz, "Increasing the material diversity in the Austin RCS Benchmark Suite using thin plates," in *Proc. Ant. Meas. Tech. Assoc. (AMTA) Symp.*, Nov. 2020.
- [4] J. T. Kelley, B. MacKie-Mason, D. A. Chamulak, M. Martin, K. Crouch, C. C. Courtney, and A. E. Yilmaz, "Towards quantifying the effect of material uncertainty on RCS predictions of composite targets," in *Proc. ACES Symp.*, May 2024.