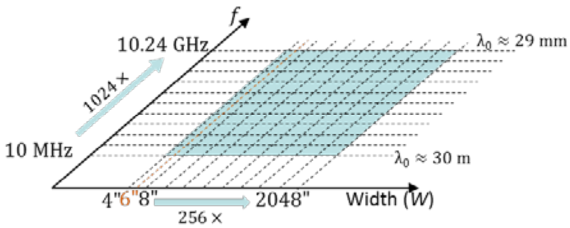
Description of Scattering Object

A perfect electrically conducting (PEC) plate of size $W \times 7W/4 \times 64$ mil.

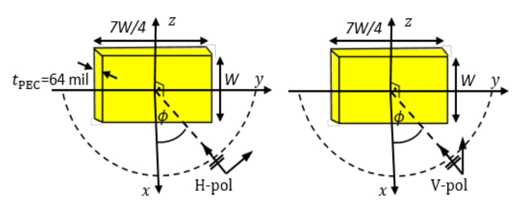
Length Scale and Frequency Range



The problems of interest cover a range of 512x in physical length scale and 1024x in frequency; the ranges are logarithmically sampled to yield 110 scattering problems. Because the plates are PEC, there are only 20 + 12 unique scattering problems in Problem Set IIB. In these problems, the plate sizes are in the range $0.0033 \le W/\lambda_0 \le 1776$, where λ_0 is the free-space wavelength. The dimensions of the plates was chosen to approximately match the plate targets in [1].

Interesting Features

1. The logarithmic sampling is distorted along the length axis and an extra plate of $W = 6$ in is introduced because of publicly available measurement data corresponding to this size [2]. The sampling is also distorted along the frequency axis: scattering from the plate of $W = 6$ in at frequencies $f \in \{10,$ 20, 40, 80, 160, 320, 640, 1280, 2560, 5120, 7000, 10240$\}$ MHz are included in the problem set because of publicly available measurement data [2]. These distortions add 12 unique scattering problems to the set.
2. The thin side wall presents meshing and accurate integration challenges.



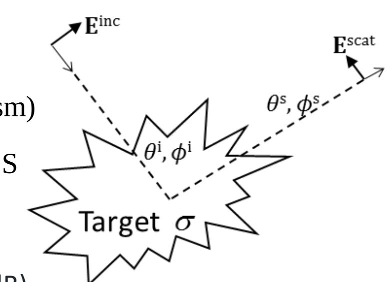
Quantities of Interest

Radar cross section (RCS) definition

$$\sigma_{vu}\left(\theta^{\mathrm{s}},\phi^{\mathrm{s}},\theta^{\mathrm{i}},\phi^{\mathrm{i}}\right)=\lim_{R\to\infty}4\pi R^2\frac{\left|\hat{v}\left(\theta^{\mathrm{s}},\phi^{\mathrm{s}}\right)\bullet\mathbf{E}^{\mathrm{scat}}\left(\theta^{\mathrm{s}},\phi^{\mathrm{s}}\right)\right|^2}{\left|\hat{u}\left(\theta^{\mathrm{i}},\phi^{\mathrm{i}}\right)\bullet\mathbf{E}^{\mathrm{inc}}\left(\theta^{\mathrm{i}},\phi^{\mathrm{i}}\right)\right|^2} \quad : \text{RCS } (\mathrm{m}^2)$$

$$\sigma_{vu,\mathrm{dB}}\left(\theta^{\mathrm{s}},\phi^{\mathrm{s}},\theta^{\mathrm{i}},\phi^{\mathrm{i}}\right)=10\log_{10}\sigma_{vu} \quad : \text{RCS in dB (dBsm)}$$

$$\sigma^{TH}_{vu,\mathrm{dB}}\left(\theta^{\mathrm{s}},\phi^{\mathrm{s}},\theta^{\mathrm{i}},\phi^{\mathrm{i}}\right)=\max(\sigma_{vu,\mathrm{dB}},TH_{vu,\mathrm{dB}})-TH_{vu,\mathrm{dB}} \quad : \text{Thresholded RCS}$$



1. Set $\theta^{\mathrm{i}} = 90^{\mathrm{o}}$. Vary $0^{\mathrm{o}} \le \phi^{\mathrm{i}} \le 90^{\mathrm{o}}$ (every 0.5^{o} in the interval).
2. Compute back-scattered $\sigma_{\theta\theta,\mathrm{dB}}$ and $\sigma_{\phi\phi,\mathrm{dB}}$ (the VV- and HH-RCS in dB) at $N_\phi = 181$ directions.

Performance Measures

Error Measure: Simulation errors shall be quantified using

$$avg.err^{TH}_{uu,\mathrm{dB}}=\frac{1}{2\pi}\int_0^{2\pi}\left|\sigma^{TH}_{uu,\mathrm{dB}}\left(\phi^{\mathrm{s}}\right)-\sigma^{\mathrm{ref},TH}_{uu,\mathrm{dB}}\left(\phi^{\mathrm{s}}\right)\right|d\phi^{\mathrm{s}}\approx\frac{1}{N_\phi}\sum_{n=1}^{N_\phi}\left|\sigma^{TH}_{uu,\mathrm{dB}}\left(\phi^{\mathrm{s}}\right)-\sigma^{\mathrm{ref},TH}_{uu,\mathrm{dB}}\left(\phi^{\mathrm{s}}\right)\right| \text{ (dB) for } u\in\{\theta,\phi\}$$

where

$$TH_{uu,\mathrm{dB}}=\max_{\phi^{\mathrm{s}}}\sigma^{\mathrm{ref}}_{uu,\mathrm{dB}}-80 \text{ (dB)}$$

This error measure discounts errors in RCS values below TH .

Cost Measure: Simulation costs shall be quantified using observed wall-clock time and peak memory/core

$$t^{\mathrm{wall}}_{\mathrm{main}} \text{ (s) and } mem^{\mathrm{maxcore}}_{\mathrm{main}} \text{ (bytes)}$$

as well as the "serialized" CPU time and total memory requirement

$$t_{\rm main}^{\rm total} = N_{\rm proc} \times t_{\rm main}^{\rm wall} \text{ (s)}$$
$$mem_{\rm main}^{\rm max} = N_{\rm proc} \times mem_{\rm main}^{\rm maxcore} \text{ (bytes)}$$

Here, $N_{\rm proc}$ denotes the number of processes used in a parallel simulation. It is expected that results will be reported for at least 2 runs: "Efficient" (small $N_{\rm proc}$) and "Fast" (large $N_{\rm proc}$).

Study 1: Error vs. Cost Sweep

Fix frequency and fix plate dimensions. Simulate many error levels (proxy: mesh densities) for 4 cases:

Case 1: f=10 MHz, W=6 in
Case 2: f=7 GHz, W=6 in (a measurement frequency)
Case 3: f=10 MHz, W=128 in
Case 4: f=320 MHz, W=128 in

It's recommended to simulate as many error levels (mesh densities) as possible. 3-5 error levels is typical. A typical error-vs.-cost study will consist of 4x3-5=12-20 simulations.

Study 2: Frequency Sweep

Fix plate dimensions and error level (proxy: mesh density). Simulate many frequencies for 4 cases:

Case 1: W=6 in, error level 1 (coarsest mesh)
Case 2: W=128 in, error level 1 (coarsest mesh)
Case 3: W=6 in, error level 2 (finer mesh)
Case 4: W=128 in, error level 2 (finer mesh)

Frequencies shall be chosen as $f \in \{10, 20, 40, \ldots, 5120, 10240\}$ MHz. It's recommended to simulate as many frequencies as possible. A full frequency-sweep study will consist of 4x11=44 simulations.

Study 3: Size Sweep

Fix frequency and error level (proxy: mesh density). Simulate many sizes for 4 cases:

Case 1: f=10 MHz, error level 1 (coarsest mesh)
Case 2: f=320 MHz, error level 1 (coarsest mesh)
Case 3: f=10 MHz, error level 2 (finer mesh)
Case 4: f=320 MHz, error level 2 (finer mesh)

Dimensions shall be chosen as $W \in \{4, 8, 16, \ldots, 1024, 2048\}$ in. It's recommended to simulate as many sizes as possible. A full size-sweep study will consist of 4x10=40 simulations.

Reference Quantities of Interest

The following RCS data are made available in the benchmark to enable participants to calibrate their simulators:

4 RCS measurement results corresponding to the W=6 in plate at frequencies $f \in \{2560, 5120, 7000, 10240\}$ MHz. The HH-polarized data are the same as those plotted in Fig. 6 of [2]; they are provided for $\phi^{\rm i}$ sampled every 0.25°.

4 RCS simulation results for the W=6 in at the above 4 frequencies found by using the ARCHIE-AIM code, a frequency-domain FFT-accelerated integral-equation solver developed at UT Austin [3]-[5].

References

[1] A. C. Woo, H. T. G. Wang, M. J. Schuh, and M. L. Sanders, "EM programmer's notebook-benchmark plate radar targets for the validation of computational electromagnetics programs," in *IEEE Ant. Propag. Mag.*, vol. 34, no. 6, pp. 52-56, Dec 1992.

[2] J. T. Kelley, D. A. Chamulak, C. Courtney, and A. E. Yilmaz, "Increasing the material diversity in the Austin RCS Benchmark Suite using thin plates," in *Proc. Ant. Meas. Tech. Assoc. (AMTA) Symp.*, Nov. 2020.

[3] M. F. Wu, G. Kaur, and A. E. Yılmaz, "A multiple-grid adaptive integral method for multi-region problems," *IEEE Trans. Antennas Propag.*, vol. 58, no. 5, pp. 1601-1613, May 2010.

[4] F. Wei and A. E. Yılmaz, "A more scalable and efficient parallelization of the adaptive integral method part I: algorithm," *IEEE Trans. Antennas Propag.*, vol. 62, no.2, pp. 714-726, Feb. 2014.

[5] J. W. Massey, V. Subramanian, C. Liu, and A. E. Yılmaz, "Analyzing UHF band antennas near humans with a fast integral-equation method," in *Proc. EUCAP*, Apr. 2016.