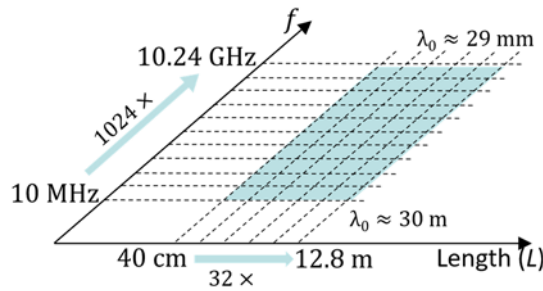


Description of Scattering Object

A perfect electrically conducting (PEC) hexagonal prism with a “cramped cobra” shaped duct.

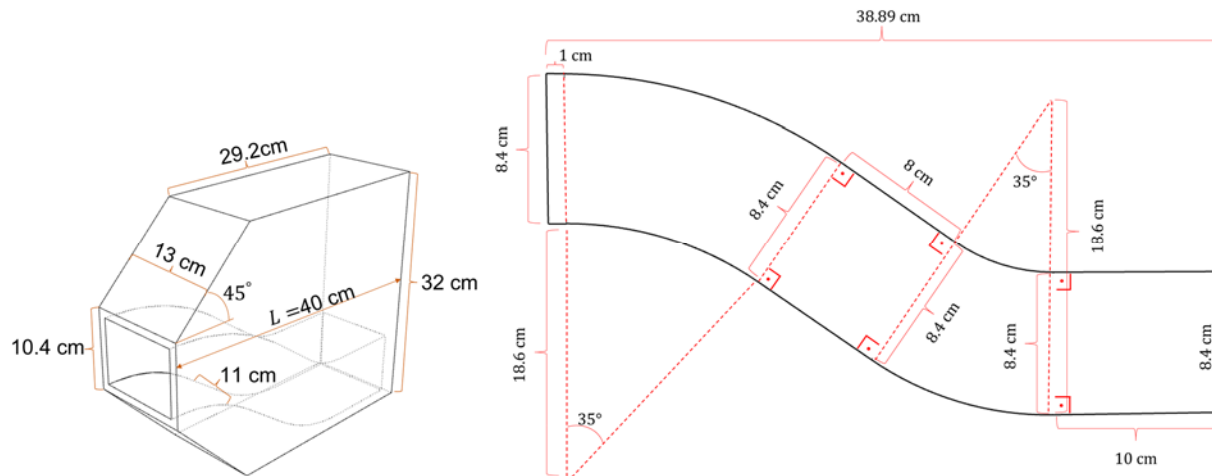
Length Scale and Frequency Range



The problems of interest cover a range of 32x in physical length scale and 1024x in frequency; the ranges are logarithmically sampled to yield 66 scattering problems. Because the camera boxes are PEC, there are only 16+1 unique scattering problems in Problem Set IIISB. In these problems, the model sizes are in the range $0.013 \leq L/\lambda_0 \leq 438$, where λ_0 is the free-space wavelength.

Interesting Features

1. The camera box is designed as a host structure to enable reproducible RCS measurements of ducts. The flat-plate geometrical features of the housing promote strong backscattering in certain directions that are minimally affected by the scattering characteristics of any voids in the box [1]. Unlike Problem Set IIISA, the front aperture is open to reveal a “cramped cobra” shaped duct¹, whose precise dimensions are given in the diagram below.
2. The diagram below shows the dimensions of the smallest cobra-ducted camera box in the problem set. The sampling of the frequency range is distorted for this problem: scattering from the smallest camera box at frequencies $f \in \{10, 20, 40, 80, 160, 320, 640, 1280, 2560, 5120, 7000, 10240\}$ MHz are included in the problem set. This distortion is because of publicly available measurement data [1] and adds 1 unique scattering problem to the set.
3. The other 5 cobra-ducted camera boxes in the problem set IIISB are obtained by scaling all dimensions of the geometry proportionally.



¹ The duct is referred to as the “cramped cobra duct” because its dimensions are similar but not identical to the COBRA cavity described in [2] and related publications.

Quantities of Interest

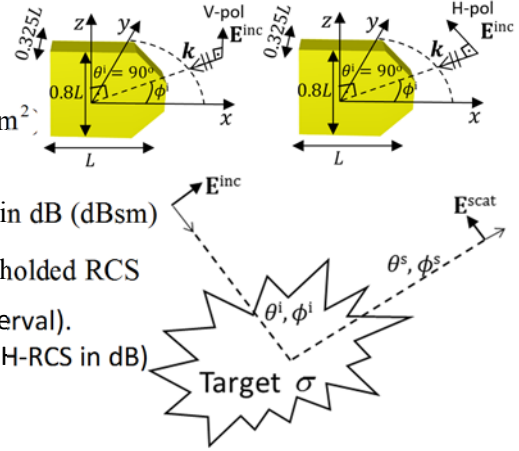
Radar cross section (RCS) definition

$$\sigma_{vu}(\theta^s, \phi^s, \theta^i, \phi^i) = \lim_{R \rightarrow \infty} 4\pi R^2 \frac{|\hat{v}(\theta^s, \phi^s) \cdot \mathbf{E}^{\text{scat}}(\theta^s, \phi^s)|^2}{|\hat{u}(\theta^i, \phi^i) \cdot \mathbf{E}^{\text{inc}}(\theta^i, \phi^i)|^2} : \text{RCS (m}^2\text{)}$$

$$\sigma_{vu,\text{dB}}(\theta^s, \phi^s, \theta^i, \phi^i) = 10 \log_{10} \sigma_{vu} : \text{RCS in dB (dBsm)}$$

$$\sigma_{vu,\text{dB}}^{\text{TH}}(\theta^s, \phi^s, \theta^i, \phi^i) = \max(\sigma_{vu,\text{dB}}, TH_{vu,\text{dB}}) - TH_{vu,\text{dB}} : \text{Thresholded RCS}$$

1. Set $\theta^i = 90^\circ$. Vary $0^\circ \leq \phi^i \leq 180^\circ$ (every 0.5° in the interval).
2. Compute back-scattered $\sigma_{\theta\theta,\text{dB}}$ and $\sigma_{\phi\phi,\text{dB}}$ (the VV- and HH-RCS in dB) at $N_\phi = 361$ scattering directions.

**Performance Measures**

Error Measure: Simulation errors shall be quantified using

$$\text{avg. err}_{uu,\text{dB}}^{\text{TH}} = \frac{1}{2\pi} \int_0^{2\pi} |\sigma_{uu,\text{dB}}^{\text{TH}}(\phi^s) - \sigma_{uu,\text{dB}}^{\text{ref,TH}}(\phi^s)| d\phi^s \approx \frac{1}{N_\phi} \sum_{n=1}^{N_\phi} |\sigma_{uu,\text{dB}}^{\text{TH}}(\phi^s) - \sigma_{uu,\text{dB}}^{\text{ref,TH}}(\phi^s)| \text{ (dB) for } u \in \{\theta, \phi\}$$

where

$$TH_{uu,\text{dB}} = \max_{\phi^s} \sigma_{uu,\text{dB}}^{\text{ref}} - 80 \text{ (dB)}$$

This error measure discounts errors in RCS values below TH .

Cost Measure: Simulation costs shall be quantified using observed wall-clock time and peak memory/core

$$t_{\text{main}}^{\text{wall}} \text{ (s) and } mem_{\text{main}}^{\text{maxcore}} \text{ (bytes)}$$

as well as the “serialized” CPU time and total memory requirement

$$t_{\text{main}}^{\text{total}} = N_{\text{proc}} \times t_{\text{main}}^{\text{wall}} \text{ (s) and } mem_{\text{main}}^{\text{max}} = N_{\text{proc}} \times mem_{\text{main}}^{\text{maxcore}} \text{ (bytes)}$$

Here, N_{proc} denotes the number of processes used in a parallel simulation. It is expected that results will be reported for at least 2 runs: “Efficient” (small N_{proc}) and “Fast” (large N_{proc}).

Study 1: Error vs. Cost Sweep

Fix frequency and fix camera box dimensions. Simulate many error levels (proxy: mesh densities) for 4 cases:

Case 1: $f=10$ MHz, $L=40$ cmCase 2: $f=7$ GHz, $L=40$ cmCase 3: $f=10$ MHz, $L=6.4$ mCase 4: $f=320$ MHz, $L=6.4$ m

It's recommended to simulate as many error levels (mesh densities) as possible. 3-5 error levels is typical. A typical error-vs.-cost study will consist of $4 \times 3 = 12$ simulations.

Study 2: Frequency Sweep

Fix camera box dimensions and error level (proxy: mesh density). Simulate many frequencies for 4 cases:

Case 1: $L=40$ cm, error level 1 (coarsest mesh)Case 2: $L=6.4$ m, error level 1 (coarsest mesh)Case 3: $L=40$ cm, error level 2 (finer mesh)Case 4: $L=6.4$ m, error level 2 (finer mesh)

Frequencies shall be chosen as $f \in \{10, 20, 40, \dots, 5120, 10240\}$ MHz. It's recommended to simulate as many frequencies as possible. A full frequency-sweep study will consist of $4 \times 11 = 44$ simulations.

Study 3: Size Sweep

Fix frequency and error level (proxy: mesh density). Simulate many sizes for 4 cases:

Case 1: $f=10$ MHz, error level 1 (coarsest mesh)Case 2: $f=320$ MHz, error level 1 (coarsest mesh)Case 3: $f=10$ MHz, error level 2 (finer mesh)Case 4: $f=320$ MHz, error level 2 (finer mesh)

Dimensions shall be chosen as $L \in \{40, 80, 120, \dots, 640, 1280\}$ cm. It's recommended to simulate as many sizes as possible. A full size-sweep study will consist of $4 \times 7 = 28$ simulations.

Reference Quantities of Interest

The following RCS data are made available in the benchmark to enable participants to calibrate their simulators:

8 RCS measurement results corresponding to the smallest cobra-ducted camera box ($L=40$ cm) at frequencies $f \in \{2560, 5120, 7000, 10240\}$ MHz. These data are provided for ϕ^i sampled every 0.5° . Note that the high return at $\phi^i = 90^\circ$ saturated the instrumentation radar at 10240 MHz; thus, the measured RCS values near that look angle are inaccurate. The same phenomenon can be observed in Fig. 3 in [1].

4 RCS simulation results for the smallest cobra-ducted camera box at the above 4 frequencies found by using the ARCHIE-AIM code, a frequency-domain FFT-accelerated integral-equation solver developed at UT Austin [3]–[5].

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