

→ Optimal of Coherent Reception : PSK, FSK, QPSK

(or)

Comparison of digital modulation techniques with P_e

(or)

P_e for various Data Txion techniques :-

→ BPSK system :- It provides minimum P_e because it satisfies optimum condition $s_1(t) = -s_2(t)$

For BPSK system, $s_1(t) = A \cos \omega_0 t$

$$s_2(t) = -A \cos \omega_0 t$$

$$\therefore s_1(t) = -s_2(t)$$

$$P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s}{N} \right)^{1/2}$$

$$E_s = \int_0^T s_1^2(t) dt = \int_0^T s_2^2(t) dt = \int_0^T (A \cos \omega_0 t)^2 dt$$

$$= A^2 \int_0^T \frac{(1 + \cos 2\omega_0 t)}{2} dt$$

$$= \frac{A^2}{2} \left[t + \frac{\sin 2\omega_0 t}{2\omega_0} \right]_0^T$$

$$\therefore P_e = \frac{1}{2} \operatorname{erfc} \left[\frac{A^2 T}{2N} \right]^{1/2}$$

$$\Rightarrow E_{st} = \frac{A^2}{2} T$$

→ BPSK in a correlator (imperfect phase synchronization)

$$S_o(T) = \frac{1}{T} \int_0^T s_i(t) [s_1(t) - s_2(t)] dt$$

let $s_i(t)$ is Rxed by correlator, for BPSK system, the sampled o/p is

$$S_{01}(T) = \frac{1}{T} \int_0^T A \cos \omega_0 t \left[A \cos \omega_0 t - (-A \cos \omega_0 t) \right] dt$$

$$= \frac{A^2}{T} \int_0^T 2 \cos^2 \omega_0 t dt$$

$$= \frac{2A^2}{T} \int_0^T \left[\frac{1 + \cos 2\omega_0 t}{2} \right] dt$$

$$\Rightarrow S_{01}(T) = \frac{A^2}{T} \left[t + \frac{\sin 2\omega_0 t}{2\omega_0} \right]_0^T = \frac{A^2}{T} T = CA^2T \quad \left\{ \because C = \frac{1}{T} \right\}$$

Similarly when $S_2(t)$ is Rxed, then

$$S_{02}(T) = \frac{1}{T} \int_0^T (-A \cos \omega_0 t) \left[A \cos \omega_0 t - (-A \cos \omega_0 t) \right] dt$$

$$= \frac{1}{T} \int_0^T -2A^2 \cos^2 \omega_0 t dt$$

$$\Rightarrow S_{02}(T) = -\frac{2A^2}{T} \int_0^T \cos^2 \omega_0 t dt = -CA^2T$$

$$\therefore P_0(T) = S_{01}(T) - S_{02}(T) = CA^2T - (-CA^2T) = 2CA^2T$$

Suppose now local s/g used at correlator is $2A \cos(\omega_0 t + \phi)$ where ϕ is some fixed phase offset instead of $2A \cos \omega_0 t$, then correlator o/p $S_0(T)$ is either $CA^2T \cos \phi$ or $-CA^2T \cos \phi$.

$$S_0(T) = \pm CA^2T \cos \phi$$

$$S_0(T) = \frac{1}{T} \int_0^T A \cos \omega_0 t (2A \cos(\omega_0 t + \phi)) dt$$

$$= \frac{2A^2}{T} \int_0^T \cos \omega_0 t \cos(\omega_0 t + \phi) dt$$

$$= \frac{2A^2}{2T} \int_0^T [\cos(2\omega_0 t + \phi) + \cos \phi] dt$$

$$= \frac{A^2}{T} \left[\frac{\sin(2\omega_0 t + \phi)}{2\omega_0} + t \cos \phi \right]_0^T$$

$$\Rightarrow S_{01}(T) = \frac{A^2}{T} T \cos \phi = CA^2T \cos \phi$$

$$\text{but } S_{02}(T) = -CA^2T \cos \phi$$

$$\therefore S_0(T) = \pm CA^2T \cos \phi$$

$$P_0(T) = 2CA^2T \cos \phi$$

& energy becomes $E_s \cos^2 \phi$

$\therefore P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s}{n} \right)^{1/2}$ can be replaced as

$$P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s \cos^2 \phi}{n} \right)^{1/2}$$

$$\Rightarrow \boxed{P_e = \frac{1}{2} \operatorname{erfc} \left[\frac{E_s \cos^2 \phi}{n} \right]} \quad \left\{ \begin{array}{l} \because \cos \phi \text{ is decreasing fn,} \\ P_e \text{ is low, if } \phi \text{ is low.} \end{array} \right.$$

When there is a phase offset ϕ in the BPSK Rxen using a correlator Rxen the phase offset ϕ increases P_e which inturn deteriorates the performance of BPSK system. In comm. system with P_e in the range 10^{-4} to 10^{-7} , if $\phi = 25^\circ$, P_e is increased by a factor 10 than that of a system with $\phi = 0$.

→ BFSK system :-

$$S_1(t) = A \cos(\omega_0 + \Omega)t \quad ; \quad P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{\sqrt{E_s}}{n} \right)^{1/2}$$

$$S_2(t) = A \cos(\omega_0 - \Omega)t$$

$$\text{where } \nu^2_{\max} = \int_{-\infty}^{\infty} \frac{|P(f)|^2}{G_n(f)} df = \int_0^T \frac{P^2(t)}{n/2} dt$$

$$\left\{ \because \text{Using Parseval's theorem, } \int_{-\infty}^{\infty} |P(f)|^2 df = \int_0^T P^2(t) dt \right\}$$

$$\therefore \nu^2_{\max} = \frac{2}{n} \int_0^T \left(A \cos(\omega_0 + \Omega)t - A \cos(\omega_0 - \Omega)t \right)^2 dt$$

$$= \frac{2}{n} A^2 \left[\int_0^T (-2 \sin \omega_0 t \sin \Omega t) dt \right]^2$$

$$= \frac{2}{n} A^2 \cdot 4 \int_0^T \sin^2 \omega_0 t \sin^2 \Omega t dt$$

$$= \frac{8A^2}{n} \int_0^T \left(\frac{1 - \cos 2\omega_0 t}{2} \right) \left(\frac{1 - \cos 2\Omega t}{2} \right) dt$$

$$= \frac{8A^2}{4n} \int_0^T [1 - \cos 2\omega_0 t - \cos 2\Omega t + \cos 2\omega_0 t \cos 2\Omega t] dt$$

$$= \frac{8A^2}{4n} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\Omega T}{2\Omega} + \frac{\sin 2(\omega_0 + \Omega)T}{4(\omega_0 + \Omega)} + \frac{\sin 2(\omega_0 - \Omega)T}{4(\omega_0 - \Omega)} \right]$$

$$\Rightarrow V_{\max}^2 = \frac{8A^2}{4\eta} \int_0^T \left[1 - \cos 2\omega_0 t - \cos 2\Omega t + \frac{1}{2} \left[\cos 2(\omega_0 + \Omega)t + \cos 2(\omega_0 - \Omega)t \right] \right] dt$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\eta} \left[t - \frac{\sin 2\omega_0 t}{2\omega_0} - \frac{\sin 2\Omega t}{2\Omega} + \frac{1}{2} \left[\frac{\sin 2(\omega_0 + \Omega)t}{2(\omega_0 + \Omega)} + \frac{\sin 2(\omega_0 - \Omega)t}{2(\omega_0 - \Omega)} \right] \right]_0^T$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\eta} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\Omega T}{2\Omega} + \frac{1}{4} \frac{\sin 2(\omega_0 + \Omega)T}{(\omega_0 + \Omega)} + \frac{1}{4} \frac{\sin 2(\omega_0 - \Omega)T}{(\omega_0 - \Omega)} \right]$$

2nd method

$$V_{\max}^2 = \frac{2A^2}{\eta} \int_0^T \left(A \cos(\omega_0 + \Omega)t - A \cos(\omega_0 - \Omega)t \right)^2 dt$$

$$= \frac{2A^2}{\eta} \int_0^T \left[\cos^2(\omega_0 + \Omega)t + \cos^2(\omega_0 - \Omega)t - 2 \cos(\omega_0 + \Omega)t \cos(\omega_0 - \Omega)t \right] dt$$

$$= \frac{2A^2}{\eta} \int_0^T \left[\frac{1 + \cos 2(\omega_0 + \Omega)t}{2} + \frac{1 + \cos 2(\omega_0 - \Omega)t}{2} - \left[\cos 2\omega_0 t + \cos 2\Omega t \right] \right] dt$$

$$= \frac{2A^2}{\eta} \left[\frac{1}{2} \left(t + \frac{\sin 2(\omega_0 + \Omega)t}{2(\omega_0 + \Omega)} \right) + \frac{1}{2} \left(t + \frac{\sin 2(\omega_0 - \Omega)t}{2(\omega_0 - \Omega)} \right) - \frac{\sin 2\omega_0 t}{2\omega_0} - \frac{\sin 2\Omega t}{2\Omega} \right]_0^T$$

$$= \frac{2A^2}{\eta} \left[\frac{T}{2} + \frac{\sin 2(\omega_0 + \Omega)T}{4(\omega_0 + \Omega)} + \frac{1}{2}T + \frac{\sin 2(\omega_0 - \Omega)T}{4(\omega_0 - \Omega)} - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\Omega T}{2\Omega} \right]$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\eta} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\Omega T}{2\Omega} + \frac{1}{4} \frac{\sin 2(\omega_0 + \Omega)T}{(\omega_0 + \Omega)} + \frac{1}{4} \frac{\sin 2(\omega_0 - \Omega)T}{(\omega_0 - \Omega)} \right]$$

For $\omega_0 \gg \Omega$

$$\text{then } V_{\max}^2 = \frac{2A^2}{\eta} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\Omega T}{2\Omega} + \frac{1}{4} \frac{\sin 2\omega_0 T}{\omega_0} + \frac{1}{4} \frac{\sin 2\omega_0 T}{\omega_0} \right]$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\eta} \left[T - \frac{\sin 2\Omega T}{2\Omega} \right]$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2 T}{\eta} \left[1 - \frac{\sin 2\pi T}{2\pi T} \right]$$

$$\therefore V^2 \text{ is max when } \boxed{\sin 2\pi T = -1} \Rightarrow 2\pi T = 3\pi/2$$

$$\therefore V_{\max}^2 = \frac{2A^2 T}{\eta} \left[1 - \frac{(-1)}{3\pi/2} \right]$$

$$= \frac{2A^2 T}{\eta} \left[1 + \frac{2}{3\pi} \right] = 2.42 \frac{A^2 T}{\eta}$$

$$= 4.84 \frac{A^2 T}{2\eta}$$

$$\begin{aligned} \therefore P_e &= \frac{1}{2} \operatorname{erfc} \left(\frac{V^2}{8} \right)^{1/2} = \frac{4.84}{\eta} \left(\frac{A^2 T}{2} \right) \\ &= \frac{1}{2} \operatorname{erfc} \left(\frac{4.84}{\eta} E_s \right)^{1/2} = \frac{4.84}{\eta} E_s \end{aligned}$$

$$\Rightarrow \boxed{P_e = \frac{1}{2} \operatorname{erfc} \left(0.6 \frac{E_s}{\eta} \right)^{1/2}} \quad \left\{ \because E_s = \frac{A^2 T}{2} \right\}$$

Comparing $P_e|_{\text{BPSK}}$ & $P_e|_{\text{BFSK}}$ systems, the same probability of error can be achieved if the sig energy in BPSK is 0.6 time as large as that of FSK. Hence a two decibels increase in the fixed sig power is required for BFSK system to possess the same probability of error, the reason for this is in BPSK,

$\boxed{S_1(t) = -S_2(t)}$ where this condition has been failed in BFSK system.

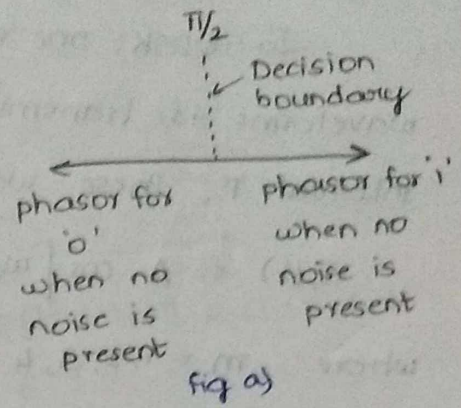
$$\therefore \boxed{P_e|_{\text{BPSK}} < P_e|_{\text{BFSK}}}$$

→ Non-coherent detection of FSK :- When the phase of incoming sig is not used in receiving a sig at Rx, it is called non-coherent detection.

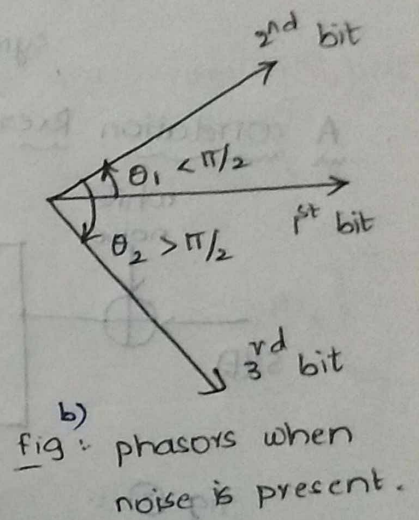
$$P_e|_{\text{Non-coherent detection of FSK}} = \frac{1}{2} e^{-E_s/2\eta}$$

→ Differential Phase Shift Keying (DPSK)

In DPSK, always a previous bit should be taken as reference. Decision boundary is considered at an angle $\frac{\pi}{2}$. Therefore when the phase difference b/w two consecutive bits differ by $< \frac{\pi}{2}$, we decide it as bit '1' was sent & if the phase difference b/w two consecutive bits differ by $> \frac{\pi}{2}$, we decide it as '0' bit was sent.



From fig(b), consider an example of 111 as Rxed bits. DPSK Rxer compares 1st bit with 2nd bit & reads an angle θ_1 , $\theta_1 < \frac{\pi}{2}$. Therefore it decides as '1' bit is received as 2nd bit.



Again DPSK Rxer compares 2nd bit with 3rd bit & reads an angle θ_2 , $\theta_2 > \frac{\pi}{2}$. Therefore it decides that '0' bit was transmitted which is an error.

$$P_e |_{\text{DPSK}} = \frac{1}{2} e^{-E_s/n}$$

→ Comparison of P_e for different systems ∴

$$P_e |_{\text{BPSK}} = \frac{1}{2} \text{erfc} \sqrt{\frac{E_s}{n}}$$

$$P_e |_{\text{DPSK}} = \frac{1}{2} e^{-E_s/n}$$

$$P_e |_{\text{Non-coherent FSK}} = \frac{1}{2} e^{-E_s/2n}$$

$$P_e |_{\text{BFSK}} = \frac{1}{2} \text{erfc} \sqrt{0.6 \frac{E_s}{n}}$$

