

→ Optimal or Coherent Reception : PSK, FSK, QPSK

(or) Comparison of digital modulation techniques with Pe

(or) Pe for various Data Txion techniques :-

→ BPSK system :- It provides minimum (P_e) because it satisfies optimum condition $s_1(t) = s_2(t)$

$$\text{For BPSK system, } s_1(t) = A \cos \omega_0 t \quad 0 \leq t \leq T$$

$$s_2(t) = -A \cos(\omega_0 t + \pi) \quad T \geq t \geq 0$$

$$\therefore s_1(t) = s_2(t)$$

$$P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s}{N_0} \right)^{1/2}$$

$$E_s = \int_0^T s_1^2(t) dt = \int_0^T s_2^2(t) dt = \int_0^T (A \cos \omega_0 t)^2 dt = \int_0^T A^2 \cos^2 \omega_0 t dt = \frac{A^2}{2} \int_0^T (1 + \cos 2\omega_0 t) dt = \frac{A^2}{2} \left[t + \frac{\sin 2\omega_0 t}{2\omega_0} \right]_0^T$$

$$\therefore P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{A^2 T}{2N_0} \right)^{1/2}$$

$$\Rightarrow E_{sr} = \frac{A^2}{2} T$$

→ BPSK in a correlator (imperfect phase synchronization)

$$(X)_d + (X)_i = (X)_c(T) = \frac{1}{T} \int_0^T s_i(t) [s_1(t) \overline{s_2(t)}] dt$$

Let $s_i(t)$ is Rxxed by correlator, for BPSK system, the sampled o/p is

$$S_{01}(T) = \frac{1}{T} \int_0^T A \cos \omega_0 t [A \cos \omega_0 t - (-A \cos \omega_0 t)] dt$$

$$= \frac{A^2}{T} \int_0^T 2 \cos \omega_0 t dt$$

$$= \frac{2A^2}{T} \int_0^T \left[\frac{1 + \cos 2\omega_0 t}{2} \right] dt$$

$$S_{01}(T) = \frac{A^2}{T} \left[t + \frac{\sin 2\omega_0 t}{2\omega_0} \right]_0^T = \frac{A^2}{T} T = CA^2 T$$

$$\therefore C = \frac{1}{T}$$

similarly when $S_{02}(T)$ is Rxed, then

$$S_{02}(T) = \frac{1}{T} \int_0^T (-A \cos \omega_0 t) [A \cos \omega_0 t - (-A \cos \omega_0 t)] dt$$

$$= \frac{1}{T} \int_0^T -2A^2 \cos^2 \omega_0 t dt = -CA^2 T$$

$$\therefore S_{02}(T) = -\frac{2A^2}{T} \int_0^T \cos^2 \omega_0 t dt = -CA^2 T$$

$$\therefore P_0(T) = S_{01}(T) - S_{02}(T) = CA^2 T - (-CA^2 T) = 2CA^2 T$$

Suppose now local sig used at correlator is $2A \cos(\omega_0 t + \phi)$

where ϕ is some fixed phase offset instead of $2A \cos \omega_0 t$,

then correlator o/p $S_0(T)$ is either $CA^2 \cos \phi$ or $-CA^2 \cos \phi$.

$$S_0(T) = \frac{1}{T} \int_0^T A \cos \omega_0 t (2A \cos(\omega_0 t + \phi)) dt$$

$$= \frac{2A^2}{T} \int_0^T \cos \omega_0 t \cos(\omega_0 t + \phi) dt$$

$$= \frac{1}{2\pi} \int_0^T [\cos(2\omega_0 t + \phi) + \cos \phi] dt$$

$$= \frac{A^2}{T} \left[\frac{\sin(2\omega_0 t + \phi)}{2\omega_0} + t \cos \phi \right]_0^T$$

$$\therefore S_{01}(T) = \frac{A^2}{T} T \cos \phi = CA^2 \cos \phi$$

$$\text{but } S_{02}(T) = -CA^2 \cos \phi$$

$$\therefore S_0(T) = \pm CA^2 \cos \phi$$

$$P_0(T) = 2CA^2 \cos \phi$$

& energy becomes $E_s \cos^2 \phi$ & fluctuation $\propto \frac{1}{T}$

$\therefore P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s \cos^2 \phi}{n} \right)^{1/2}$ can be replaced as

$$P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{E_s \cos^2 \phi}{n} \right)^{1/2}$$

$$\Rightarrow P_e = \frac{1}{2} \operatorname{erfc} \left[\frac{E_s \cos^2 \phi}{n} \right]^{1/2} \quad \begin{cases} \because \cos \phi \text{ is decreasing fn,} \\ \text{Pe is low, if } \phi \text{ is low.} \end{cases}$$

When there is a phase offset ϕ in the BPSK Rxer using a correlator Rxer the phase offset [which increases] P_e which in turn deteriorates the performance of BPSK system. In comm. system with P_e in the range 10^{-4} to 10^{-7} , if $\phi = 25^\circ$ P_e is increased by a factor 10 than that of a system with $\phi = 0$.

$$T_{A2} = (T_{A1}) - T_{A2} \approx (T)_{\text{co2}}$$

\rightarrow BFSK system:

$$S_1(t) = A \cos(\omega_0 + \Delta)t \cos \phi \quad \text{so } P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{\sqrt{n}}{8} \right)^{1/2} = (T)_{\text{co2}} \quad \therefore$$

$$S_2(t) = A \cos(\omega_0 - \Delta)t$$

$$\text{where } V^2 = \int_{-\infty}^{\infty} \frac{|P(f)|^2}{G_n(f)} df \quad \text{from } \int_0^T \frac{P^2(t) dt}{n^{1/2}} \text{ is root mean square}$$

\therefore Using Parseval's theorem, $\int_{-\infty}^{\infty} |P(f)|^2 df = \int_0^T P^2(t) dt$

$$\therefore V^2_{\max} = \frac{2}{n} \int_0^T (A \cos(\omega_0 + \Delta)t - A \cos(\omega_0 - \Delta)t)^2 dt = (T)_{\text{co2}}$$

$$= \frac{2}{n} A^2 \left[\int_0^T (-2 \sin \omega_0 t \sin \Delta t) dt + (\omega_0 + \Delta)^2 \right]$$

$$= \frac{2}{n} A^2 \left[4 \int_0^T \sin^2 \omega_0 t \sin^2 \Delta t dt \right]$$

$$= \frac{8A^2}{n} \int_0^T \left(\frac{1 - \cos 2\omega_0 t}{2} \right) \left(\frac{1 - \cos 2\Delta t}{2} \right) dt$$

$$= \frac{8A^2}{4n} \int_0^T [1 - \cos 2\omega_0 t - \cos 2\Delta t + \cos 2\omega_0 t \cos 2\Delta t] dt = (T)_{\text{co2}}$$

$$\therefore V^2_{\max} = (T)_{\text{co2}}$$

$$\Rightarrow V_{\max}^1 = \frac{8A^2}{4\pi} \int_0^T [1 - \cos 2\omega_0 t - \cos 2\pi t + \frac{1}{2} [\cos 2(\omega_0 + \pi)t + \cos 2(\omega_0 - \pi)t]] dt$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\pi} \left[t - \frac{\sin 2\omega_0 t}{2\omega_0} - \frac{\sin 2\pi t}{2\pi} + \frac{1}{2} \left[\frac{\sin 2(\omega_0 + \pi)t}{2(\omega_0 + \pi)} + \frac{\sin 2(\omega_0 - \pi)t}{2(\omega_0 - \pi)} \right] \right]$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\pi} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\pi T}{2\pi} + \frac{1}{4} \frac{\sin 2(\omega_0 + \pi)T}{(\omega_0 + \pi)} + \frac{1}{4} \frac{\sin 2(\omega_0 - \pi)T}{(\omega_0 - \pi)} \right]$$

2nd method

$$V_{\max}^2 = \frac{2A^2}{\pi} \int_0^T (A \cos (\omega_0 + \pi)t - A \cos (\omega_0 - \pi)t)^2 dt$$

$$= \left(\frac{2A^2}{\pi} \right) \int_0^T (\cos^2 (\omega_0 + \pi)t + \cos^2 (\omega_0 - \pi)t - 2 \cos (\omega_0 + \pi)t \cos (\omega_0 - \pi)t) dt$$

$$= \frac{2A^2}{\pi} \int_0^T \left[\frac{1 + \cos 2(\omega_0 + \pi)t}{2} + \left[\frac{1 + \cos 2(\omega_0 - \pi)t}{2} \right] - \left[\cos 2\omega_0 t + \cos 2\pi t \right] \right] dt$$

$$= \frac{2A^2}{\pi} \left[\frac{1}{2} \left(t + \frac{\sin 2(\omega_0 + \pi)t}{2(\omega_0 + \pi)} \right) + \frac{1}{2} \left(t + \frac{\sin 2(\omega_0 - \pi)t}{2(\omega_0 - \pi)} \right) \right]$$

$$= \frac{2A^2}{\pi} \left[\frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\pi T}{2\pi} \right]$$

$$= \frac{2A^2}{\pi} \left[\frac{T}{2} + \frac{\sin 2(\omega_0 + \pi)T}{4(\omega_0 + \pi)} + \frac{1}{2} T + \frac{\sin 2(\omega_0 - \pi)T}{4(\omega_0 - \pi)} \right]$$

$$= \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\pi T}{2\pi}$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\pi} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\pi T}{2\pi} + \frac{1}{4} \frac{\sin 2(\omega_0 + \pi)T}{(\omega_0 + \pi)} + \frac{1}{4} \frac{\sin 2(\omega_0 - \pi)T}{(\omega_0 - \pi)} \right]$$

For $\omega_0 > \omega$

$$\text{then } V_{\max}^2 = \frac{2A^2}{\pi} \left[T - \frac{\sin 2\omega_0 T}{2\omega_0} - \frac{\sin 2\pi T}{2\pi} + \frac{1}{4} \frac{\sin 2\omega_0 T}{\omega_0} + \frac{1}{4} \frac{\sin 2\omega_0 T}{\omega_0} \right]$$

$$\Rightarrow V_{\max}^2 = \frac{2A^2}{\pi} \left[T - \frac{\sin 2\pi T}{2\pi} \right]$$

$$\Rightarrow \sqrt{V_{\max}^2} = \frac{2A^2 T}{n} \left[1 - \frac{\sin 2\pi T}{2\pi T} \right]$$

$\therefore V^2$ is max when $\boxed{\sin 2\pi T = -1} \Rightarrow 2\pi T = 3\pi/2$

$$\sqrt{V_{\max}^2} = \frac{2A^2 T}{n} \left[1 - \frac{(-1)}{3\pi/2} \right]$$

$$= \frac{2A^2 T}{n} \left[1 + \frac{2}{3\pi} \right] = 2.42 \frac{A^2 T}{n} \\ = 4.84 \frac{A^2 T}{2n}$$

$$\therefore P_e = \frac{1}{2} \operatorname{erfc} \left(\frac{V^2}{8} \right)^{1/2} \\ = \frac{1}{2} \operatorname{erfc} \left(\frac{4.84}{n} \frac{E_s}{8} \right)^{1/2} \\ = \frac{4.84}{n} E_s$$

$$\Rightarrow P_e = \frac{1}{2} \operatorname{erfc} \left(0.6 \frac{E_s}{n} \right)^{1/2} \quad \left\{ \because E_s = \frac{A^2 T}{2} \right\}$$

Comparing $P_e |_{\text{BPSK}}$ & $P_e |_{\text{BFSK}}$ systems, the same probability of error can be achieved if the sig. energy in BPSK is 0.6 time as large as that of FSK. Hence a two decibels increase in the Txed sig power is required for BFSK system to possess the same probability of error, the reason for this is in BPSK,

$$S_1(t) = -S_2(t)$$

where this condition has been failed.

in BFSK system.

$$\therefore \boxed{P_e |_{\text{BPSK}} < P_e |_{\text{BFSK}}}$$

→ Non-coherent detection of FSK :- When the phase of incoming s/g is not used in receiving a s/g at Rxer, it is called non-coherent

detection. $P_e |_{\text{Non-coherent detection of FSK}}$,

$$P_e = \frac{1}{2} e^{-\frac{E_s}{2n}}$$

→ Differential Phase shift Keying (DPSK)

In DPSK, always a previous bit should be taken as reference. Decision boundary is considered at an angle $\frac{\pi}{2}$. Therefore when the phase difference b/w two consecutive bits differ by $< \frac{\pi}{2}$, we decide it as bit 'i' was sent & if the phase difference b/w two consecutive bits differ by $> \frac{\pi}{2}$, we decide it as 'o' bit was sent.

From fig(b), consider an example of 111

as Rxed bits. DPSK Rxer compares 1st bit with 2nd bit & reads an angle θ_1 , $\theta_1 < \frac{\pi}{2}$. Therefore it decides as 'i' bit is received as 2nd bit.

Again DPSK Rxer compares 2nd bit with 3rd bit & reads an angle θ_2 , $\theta_2 > \frac{\pi}{2}$. Therefore it decides that 'o' bit was transmitted which is an error.

$$P_e |_{\text{DPSK}} = \frac{1}{2} e^{-\frac{E_s}{n}}$$

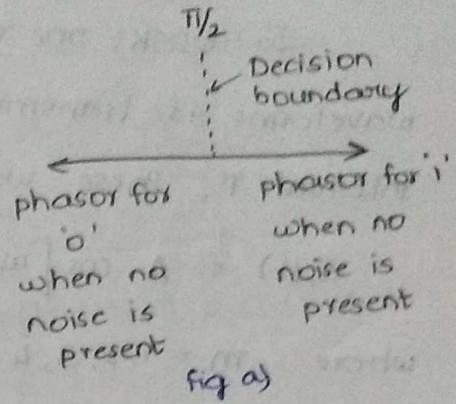


fig a)

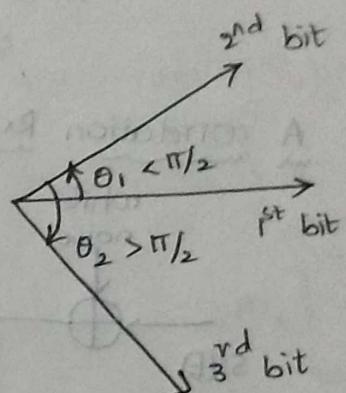


fig b) phasors when noise is present.

→ Comparison of P_e for different systems ::

$$P_e |_{\text{BPSK}} = \frac{1}{2} \operatorname{erfc} \sqrt{\frac{E_s}{n}}$$

$$P_e |_{\text{DPSK}} = \frac{1}{2} e^{-\frac{E_s}{n}}$$

$$P_e |_{\text{Non-coherent FSK}} = \frac{1}{2} e^{-\frac{E_s}{2n}}$$

$$P_e |_{\text{BFSK}} = \frac{1}{2} \operatorname{erfc} \sqrt{0.6 \frac{E_s}{n}}$$

