

1. Special case:- when 1 & 0 are equiprobable, i.e.,
we have $P_1 = P_0 = \frac{1}{2}$, $\lambda_{opt} = 0$

In this case, will $P_{01} = P_{10}$ (put $\lambda = 0$ in
expressions of
 P_{01} & P_{10} to
note it)

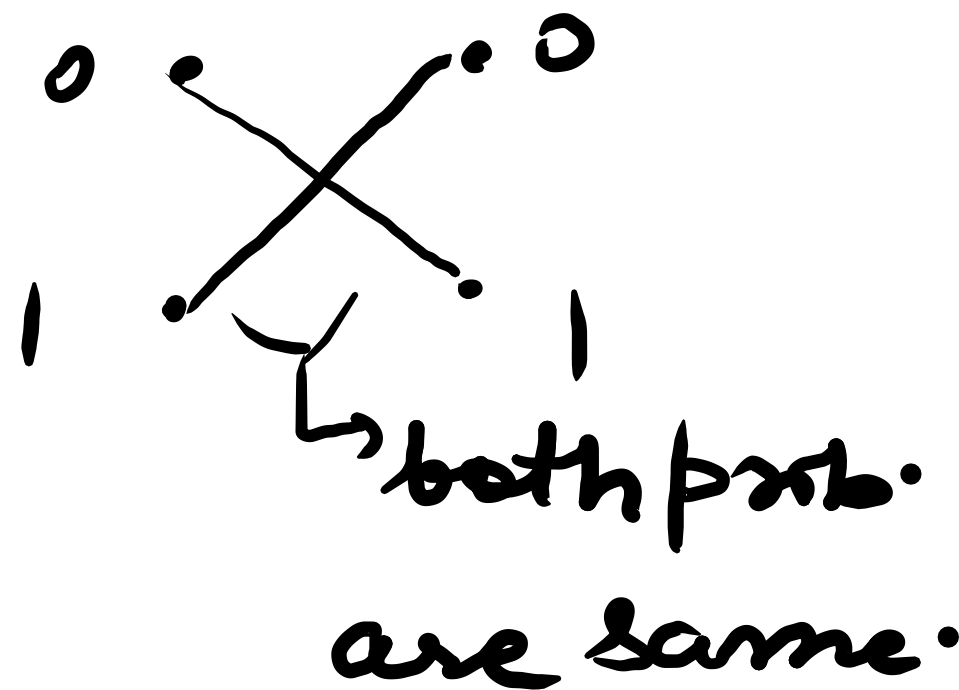
the above result is intuitive as
in the case of equiprobable binary
symbols, we should choose the threshold at
the midpoint b/w the pulse heights - A & A
representing the two symbols 0 & 1.

→ channels for which $P_{01} = P_{10}$, are called

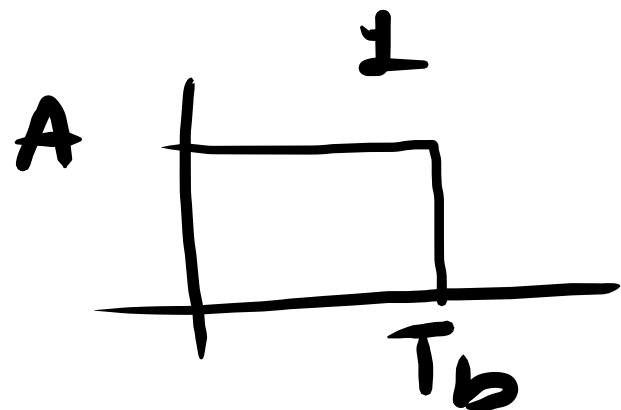
Binary symmetric channels (BSC)

In the special case ①,

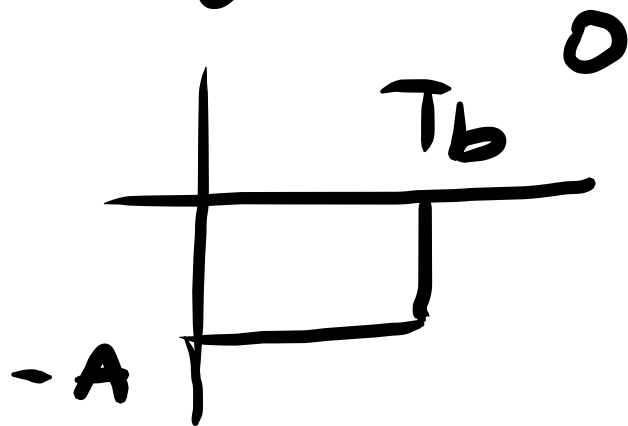
$$P_e = \frac{1}{2} \operatorname{erfc} \left(A / \sqrt{N_0 T_b} \right)$$



→ What is the Tx'd signal energy per bit (E_b)



or



$$\rightarrow A^2 T_b \triangleq E_b$$

(In case of polar NRZ)

$$P_e = \frac{1}{2} \operatorname{erfc} \left(\sqrt{\frac{E_b}{N_0}} \right)$$

This shows that for $P_0 = P_1 = \frac{1}{2}$ & $\lambda_{opt} = 0$

P_e depends solely on $\frac{E_b}{N_0}$, ratio of Tx. signal energy per bit to the noise spectral density

Passband signals (PB)

Given a message signal $m(t)$ of B.W. W Hz. how do you send it over a PB channel centered around f_c ? $f_c \gg W$

1. $u_p(t) = m(t) \cos(2\pi f_c t)$
2. $v_p(t) = m(t) \sin(2\pi f_c t)$

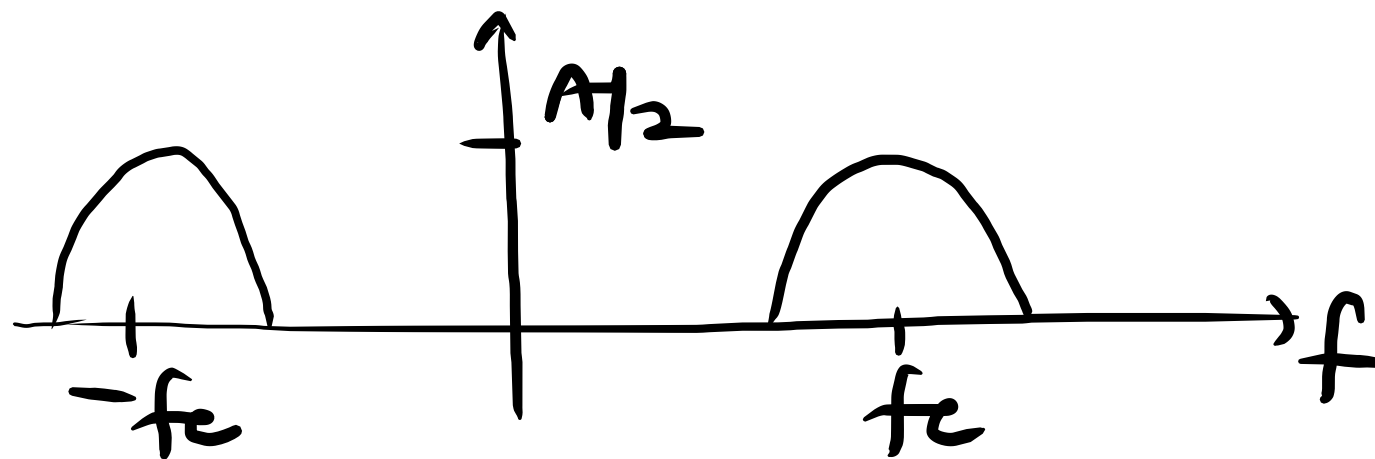
see fig. 4.6
on pg 258 for
the plot of P_e vs
 $\frac{E_b}{N_0}$ dB on a
log scale

Given $M(f)$
which is F.T. of
 $m(t)$, find
 $U_p(f)$ & $V_p(f)$

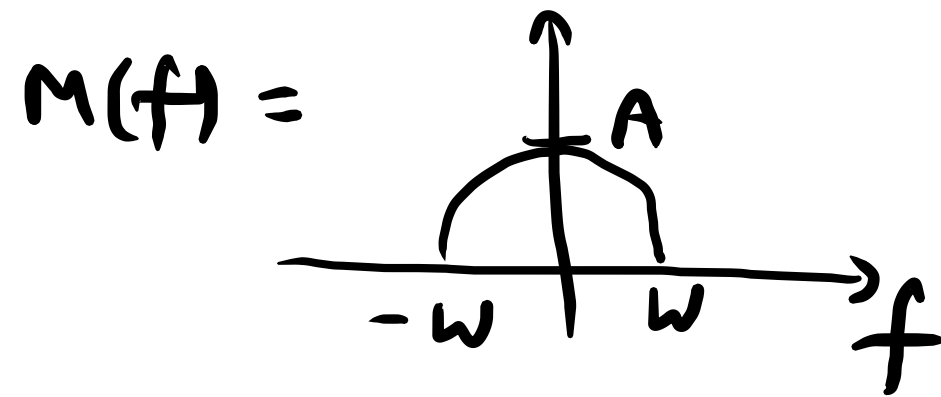
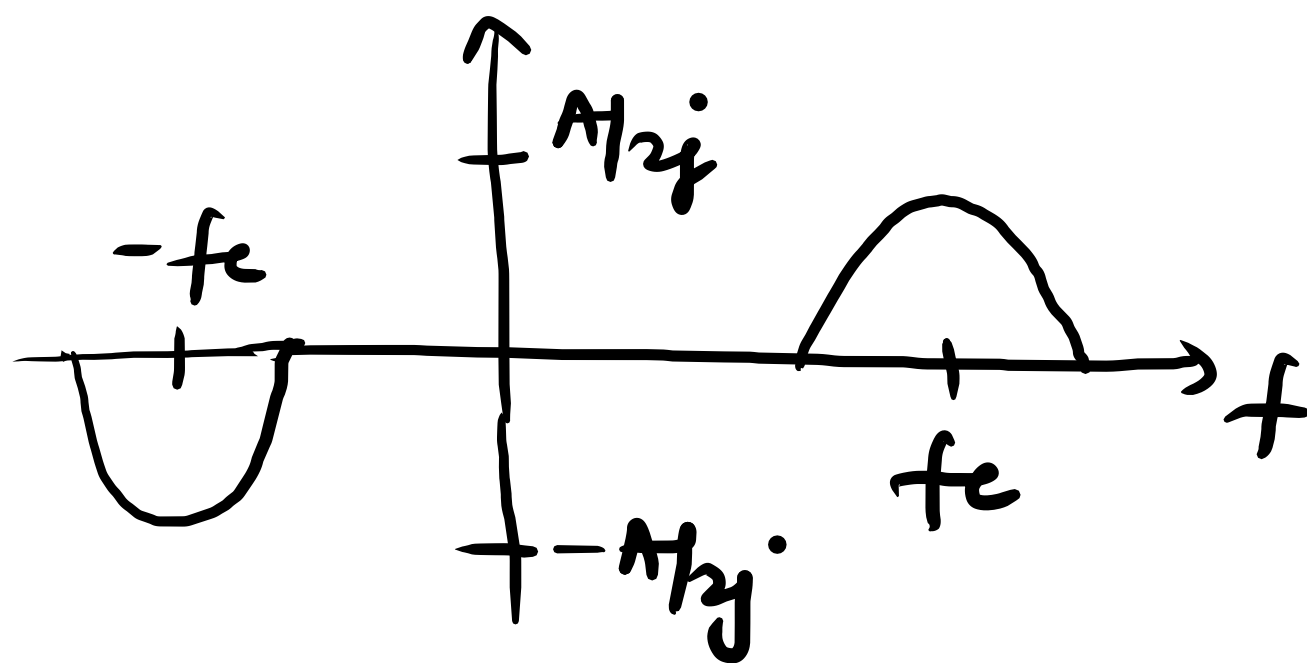
$$U_p(f) = \frac{1}{2} [M(f-f_c) + M(f+f_c)]$$

$$V_p(f) = \frac{1}{2j} [M(f-f_c) - M(f+f_c)]$$

$$U_p(f) =$$



$$V_p(f)$$



Baseband (BB) Signal
 $u(t)$ - if the energy
 is concentrated in
 a band around DC
 &

$U(f) \approx 0, |f| > W$
 Passband (PB) Signal
 $u(t)$ - if the energy

is concentrated in a band away from DC, with

$$U(f) \approx 0, \quad |f \pm f_c| > W \quad \text{--- ②}$$

$f_c + W$
 $f_c - W$

where $f_c > W > 0$

* A channel modeled as a linear time-invariant system is said to be PB if its T.F. satisfies ②.

$-f_c - W$
 $-f_c + W$

→ $|U_p(f)|$ & $|V_p(f)|$ have freq. content in a band around f_c & are PB signals

→ If we use both sine & cosine carriers, we can construct a PB signal of the form -

$$u_p(t) = \underbrace{u_I(t)}_{I} \cos(2\pi f_c t) - \underbrace{u_Q(t)}_{Q} \sin(2\pi f_c t) \quad (4)$$

where $u_I(t)$ & $u_Q(t)$ are **real** BB signals of B.W. at most W , with $f_c > W$.

$u_I(t) \rightarrow$ In-phase Component (I)

$u_Q(t) \rightarrow$ Quadrature Component (Q)

orthogonality of I & Q channels · (this is what

$$\int_{-\infty}^{\infty} \underline{I} \underline{Q} dt = 0$$

zero DC component

allows you to
Construct $u_p(t)$ in (4))

$$x(t) \rightarrow x(f) = \int_{-\infty}^{\infty} x(t) e^{-j2\pi ft} dt$$

$$\underline{\int_{-\infty}^{\infty} x(t) dt = 0} \Rightarrow x(0) = 0$$