

AE 675

Coding Assignment

Group Members

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Case 1

Part (a)

One of the diagonals of the square was used to divide the square into 2 equal triangular elements.

The element-wise terms of the 2D heat conduction equation were calculated (in general) by hand and then implemented in the code file. The determination of the natural coordinates and subsequent calculation of the Jacobian and required matrices were done through code.

The final equation was brought into the form of $AX = B$ so that $X = B \setminus A$ can be directly obtained.

$Q_0 = 1000 * 0.01$ to divide the 1KW power provided throughout the thickness (1cm) of the sheet

Result :

[298, 298, 914/3, 934/3]

Part (b)

Each triangular element had one side of the square as its base and the opposite vertex at the centre of the square, which coincides with the application of the point heat source.

The element-wise terms of the PDE were calculated and implemented. Matrices were formed for the shape functions and cartesian coordinates of the

nodes. All calculations were done on MATLAB through corresponding matrix operations.

Individual terms for each element were coded separately and then assembled at the end.

Result :

298

298

303

303

303

Part (c)

The pattern identified by writing the PDE for parts (a) and (b) led to a generalisation where a loop is run for each element and the similar terms were added to a larger sum

These sums of terms were then used to generate the assembly equation. Simplification due to known nodal temperatures and forming of $AX = B$ equation followed.

Result :

298.0000	302.5575	303.1770	301.0088
298.0000	302.6460	302.6460	303.9735
301.0088	303.1770	302.5575	

Part (d)

The same code and logic implemented in part (c) was used in part (d) too with minor changes. The number of elements was increased to 100 and number of nodes to 101.

Plotting the contours and line plots for each case, it is easily seen that as the number of elements is increased, the curve is smoother and more realistic (temperature gradients are expected to be smooth in real life). The difference between adjacent nodal temperatures also decreases drastically as the number of elements is increased.

Result : (split into columns for better visualisation)

298.0000	298.0000	300.5548	302.6420	303.2224
298.0000	298.0000	300.8606	302.6207	303.2018
298.0000	298.0000	301.1452	302.5916	303.1715
298.0000	298.0000	301.4067	302.6743	303.1323
298.0000	298.0000	301.6434	302.7539	303.0848
298.0000	298.0000	301.8539	302.8300	303.0300
298.0000	298.0000	302.0375	302.9018	302.9687
298.0000	298.0000	302.1944	302.9687	302.9018
298.0000	298.0000	302.3251	303.0300	302.8300
298.0000	298.0000	302.4309	303.0848	302.7539
298.0000	298.3965	302.5135	303.1323	302.6743
298.0000	298.7851	302.5751	303.1715	302.5916
298.0000	299.1644	302.6178	303.2018	302.6207
298.0000	299.5329	302.6438	303.2224	302.6420
298.0000	299.8888	302.6552	303.2328	302.6540
298.0000	300.2302	302.6540	303.2328	302.6552

302.6438	302.3251	301.4067	299.8888	304.0509
302.6178	302.1944	301.1452	299.5329	
302.5751	302.0375	300.8606	299.1644	
302.5135	301.8539	300.5548	298.7851	
302.4309	301.6434	300.2302	298.3965	

Case 2

The matrix equations and code-building procedure followed in parts (c), (d) of Case 1 was followed. The only change was in the equation, which introduced an additional term due to the heat convection through one of the sides.

Another change is the absence of known nodal temperatures. As such, Case 1 involved giving Dirichlet BCs, while Case 2 provided Neumann BCs.

Result : (split into columns for better visualisation)

295.7903	298.0058	296.2450	299.3430	301.5253
295.9102	298.0765	296.0619	299.6965	301.5576
296.0619	298.0765	295.9102	300.0213	301.5718
296.2450	298.0058	295.7903	300.3152	301.5703
296.4569	297.8704	296.2828	300.5766	301.5554
296.6930	297.6817	296.7654	300.8047	301.5290
296.9455	297.4542	297.2365	300.9994	301.4928
297.2037	297.2037	297.6941	301.1618	301.5955
297.4542	296.9455	298.1361	301.2932	301.6944
297.6817	296.6930	298.5601	301.3959	301.7888
297.8704	296.4569	298.9633	301.4723	301.8780

301.9612	301.5703
302.0373	301.5718
302.1053	301.5576
302.1643	301.5253
302.2130	301.4723
302.2506	301.3959
302.2761	301.2932
302.2891	301.1618
302.2891	300.9994
302.2761	300.8047
302.2506	300.5766
302.2130	300.3152
302.1643	300.0213
302.1053	299.6965
302.0373	299.3430
301.9612	298.9633
301.8780	298.5601
301.7888	298.1361
301.6944	297.6941
301.5955	297.2365
301.4928	296.7654
301.5290	296.2828
301.5554	303.3052