

Modelling and Control of Manipulators

Homework No. 01

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Abbreviations

$$\cos(\theta_i) \rightarrow c_i$$

$$\sin(\theta_i) \rightarrow s_i$$

$$\cos(\theta_i + \theta_j) \rightarrow c_{ij}$$

$$\sin(\theta_i + \theta_j) \rightarrow s_{ij}$$

1 Introduction

This report will provide the analytical solution of direct and inverse kinematic of ABB IRB-7600 manipulator. Due to the complexity of matrices, MATLAB is used to resolve the complex matrices. The link to the files can be approached by using on the following link:

<https://drive.google.com/drive/folders/1iRiX2OGMy9HkMI5LzrG8tXgPTa5P6t7m?usp=sharing>

2 Denavit-Hartenberg (DH) Parameters for ABB IRB-7600 Manipulator

Placement of axes should follow the rules provided below:

1. Draw the manipulator
2. Identify the axes of rotation or translation (for revolute and prismatic joints)
3. Assign the i^{th} axis to the i^{th} axis of rotation/translation
4. Find the common perpendiculars between the $i-1z$ and iz axes (if those axes intersect the common perpendicular is defined along $i-1z \times iz$)
5. Define the ix axes – the axis $i-1z$ coincides with the common perpendicular between the $i-1z$ and iz axes and points from $i-1z$ to iz
6. Determine the iy axes $iy = iz \times ix$
7. The base coordinate frame 0 should be located in such a way that α_0 , a_0 and θ_1 or d_1 are equal to 0, where ${}_0z = {}_1z$ and ${}_0P = {}_0P$

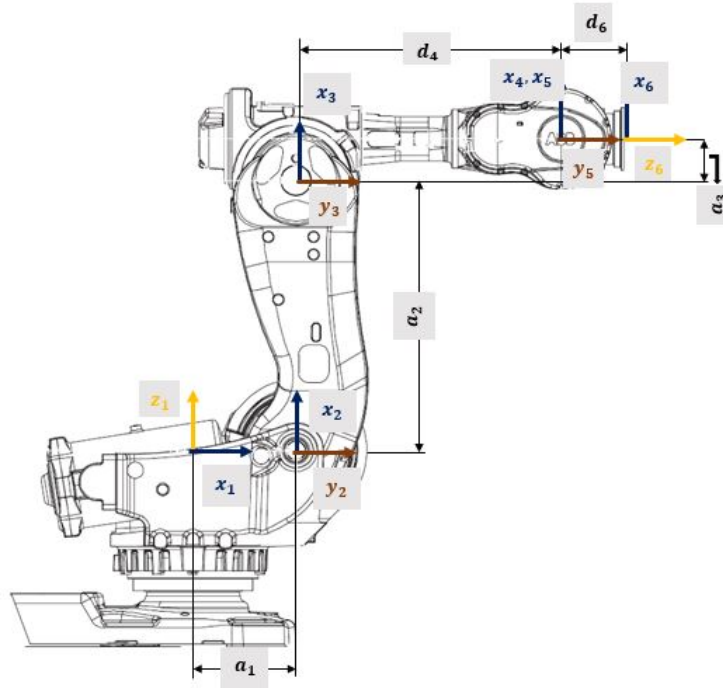


Figure 1: Placement of Axes for ABB IRB-7600 Manipulator

Determination of the link and joint parameters follow the rules stated below:

1. a_{i-1} : the distance between axes $i-1z$ and iz measured along $i-1x$
2. α_{i-1} : the angle between axes $i-1z$ and iz measured around $i-1x$
3. d_i : the distance between axes $i-1x$ and ix measured along iz
4. θ_i : the angle between axes $i-1x$ and ix measured around iz

i	α_{i-1}	a_{i-1}	d_i	θ_i
0	0	0	0	θ_1
1	$-\pi/2$	$a_1 = 410$	0	$\theta_2 := \theta_2 - \pi/2$
2	0	$a_2 = 1075$	0	θ_3
3	$-\pi/2$	$a_3 = 165$	$d_4 = 1056$	θ_4
4	$\pi/2$	0	0	θ_5
5	$-\pi/2$	0	$d_6 = 250$	θ_6

3 Direct Kinematics

Direct Kinematics follows the below stated formula:

$${}^0_n\mathcal{T} = {}^0_1\mathcal{T}_2^1\mathcal{T} \dots {}^{n-1}_n\mathcal{T}$$

$${}^0_n\mathcal{T} = \prod_{i=1}^n {}^{i-1}_i\mathcal{T}$$

$${}^0_1\mathcal{T} = \begin{pmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^1_2\mathcal{T} = \begin{pmatrix} c_2 & -s_2 & 0 & a_1 \\ 0 & 0 & 1 & 0 \\ -s_2 & -c_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^2_3\mathcal{T} = \begin{pmatrix} c_3 & -s_3 & 0 & a_2 \\ s_3 & c_3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^3_4\mathcal{T} = \begin{pmatrix} c_4 & -s_4 & 0 & a_3 \\ 0 & 0 & 1 & d_4 \\ -s_4 & -c_4 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^4_5\mathcal{T} = \begin{pmatrix} c_5 & -s_5 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ s_5 & c_5 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^5_6\mathcal{T} = \begin{pmatrix} c_6 & -s_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ -s_6 & -c_6 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$\mathcal{T}_d = \begin{pmatrix} r_{11} & r_{12} & r_{13} & p_x \\ r_{21} & r_{22} & r_{23} & p_y \\ r_{31} & r_{32} & r_{33} & p_z \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^0_2\mathcal{T} = \begin{pmatrix} c_1 c_2 & -c_1 s_2 & -s_1 & a_1 c_1 \\ c_2 s_1 & -s_1 s_2 & c_1 & a_1 s_1 \\ -s_2 & -c_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^0_3\mathcal{T} = \begin{pmatrix} c_1 c_2 c_3 - c_1 s_2 s_3 & -c_1 c_2 s_3 - c_1 c_3 s_2 & -s_1 & a_1 c_1 + a_2 c_1 c_2 \\ c_2 c_3 s_1 - s_1 s_2 s_3 & -c_2 s_1 s_3 - c_3 s_1 s_2 & c_1 & a_1 s_1 + a_2 c_2 s_1 \\ -c_2 s_3 - c_3 s_2 & s_2 s_3 - c_2 c_3 & 0 & -a_2 s_2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^0_4\mathcal{T} = \begin{pmatrix} s_1 s_4 + c_4 \sigma_1 & c_4 s_1 - s_4 \sigma_1 & -c_1 c_2 s_3 - c_1 c_3 s_2 & a_1 c_1 + a_3 \sigma_1 - d_4 (c_1 c_2 s_3 + c_1 c_3 s_2) + a_2 c_1 c_2 \\ c_4 \sigma_2 - c_1 s_4 & -c_1 c_4 - s_4 \sigma_2 & -c_2 s_1 s_3 - c_3 s_1 s_2 & a_1 s_1 + a_3 \sigma_2 - d_4 (c_2 s_1 s_3 + c_3 s_1 s_2) + a_2 c_2 s_1 \\ -c_4 \sigma_3 & s_4 \sigma_3 & s_2 s_3 - c_2 c_3 & -a_2 s_2 - a_3 \sigma_3 - d_4 (c_2 c_3 - s_2 s_3) \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

where

$$\sigma_1 = c_1 c_2 c_3 - c_1 s_2 s_3$$

$$\sigma_2 = c_2 c_3 s_1 - s_1 s_2 s_3$$

$$\sigma_3 = c_2 s_3 + c_3 s_2$$

$${}^0_5\mathcal{T} = \begin{pmatrix} c_5 \sigma_5 - s_5 \sigma_1 & -c_5 \sigma_1 - s_5 \sigma_5 & s_4 \sigma_7 - c_4 s_1 & a_1 c_1 + a_3 \sigma_7 - d_4 \sigma_1 + a_2 c_1 c_2 \\ -s_5 \sigma_2 - c_5 \sigma_6 & s_5 \sigma_6 - c_5 \sigma_2 & c_1 c_4 + s_4 \sigma_8 & a_1 s_1 + a_3 \sigma_8 - d_4 \sigma_2 + a_2 c_2 s_1 \\ -s_5 \sigma_4 - c_4 c_5 \sigma_3 & c_4 s_5 \sigma_3 - c_5 \sigma_4 & -s_4 \sigma_3 & -a_2 s_2 - a_3 \sigma_3 - d_4 \sigma_4 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

where

$$\sigma_1 = c_1 c_2 s_3 + c_1 c_3 s_2$$

$$\sigma_2 = c_2 s_1 s_3 + c_3 s_1 s_2$$

$$\begin{aligned}
\sigma_3 &= c_2 s_3 + c_3 s_2 \\
\sigma_4 &= c_2 c_3 - s_2 s_3 \\
\sigma_5 &= s_1 s_4 + c_4 \sigma_7 \\
\sigma_6 &= c_1 s_4 - c_4 \sigma_8 \\
\sigma_7 &= c_1 c_2 c_3 - c_1 s_2 s_3 \\
\sigma_8 &= c_2 c_3 s_1 - s_1 s_2 s_3
\end{aligned}$$

$${}_6^0\mathcal{T}_d = \begin{pmatrix} s_6 \sigma_4 - c_6 \sigma_2 & s_6 \sigma_2 + c_6 \sigma_4 & -c_5 \sigma_8 - s_5 \sigma_9 \\ -c_6 \sigma_1 - s_6 \sigma_5 & s_6 \sigma_1 - c_6 \sigma_5 & s_5 \sigma_7 - c_5 \sigma_6 \\ s_4 s_6 \sigma_{10} - c_6 \sigma_3 & s_6 \sigma_3 + c_6 s_4 \sigma_{10} & c_4 s_5 \sigma_{10} - c_5 \sigma_{11} \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} a_1 c_1 - d_6 (c_5 \sigma_8 + s_5 \sigma_9) + a_3 \sigma_{13} - d_4 \sigma_8 + a_2 c_1 c_2 \\ a_1 s_1 - d_6 (c_5 \sigma_6 - s_5 \sigma_7) + a_3 \sigma_{12} - d_4 \sigma_6 + a_2 c_2 s_1 \\ -a_2 s_2 - a_3 \sigma_{10} - d_4 \sigma_{11} - d_6 (c_5 \sigma_{11} - c_4 s_5 \sigma_{10}) \\ 1 \end{pmatrix} \quad (1)$$

where

$$\begin{aligned}
\sigma_1 &= s_5 \sigma_6 + c_5 \sigma_7 \\
\sigma_2 &= s_5 \sigma_8 - c_5 \sigma_9 \\
\sigma_3 &= s_5 \sigma_{11} + c_4 c_5 \sigma_{10} \\
\sigma_4 &= c_4 s_1 - s_4 \sigma_{13} \\
\sigma_5 &= c_1 c_4 + s_4 \sigma_{12} \\
\sigma_6 &= c_2 s_1 s_3 + c_3 s_1 s_2 \\
\sigma_7 &= c_1 s_4 - c_4 \sigma_{12} \\
\sigma_8 &= c_1 c_2 s_3 + c_1 c_3 s_2 \\
\sigma_9 &= s_1 s_4 + c_4 \sigma_{13} \\
\sigma_{10} &= c_2 s_3 + c_3 s_2 \\
\sigma_{11} &= c_2 c_3 - s_2 s_3 \\
\sigma_{12} &= c_2 c_3 s_1 - s_1 s_2 s_3 \\
\sigma_{13} &= c_1 c_2 c_3 - c_1 s_2 s_3
\end{aligned}$$

4 Inverse Kinematics

We will compare the matrix ${}_4^1\mathcal{T}$ with ${}_4^1\mathcal{T}_d$ and will find the corresponding θ_1, θ_2 and θ_3

$${}_4^1\mathcal{T}_d = \begin{pmatrix} c_5 c_6 \sigma_6 - c_5 s_6 \sigma_4 - s_5 \sigma_2 & c_6 \sigma_4 + s_6 \sigma_6 & c_5 \sigma_2 + c_6 s_5 \sigma_6 - s_5 s_6 \sigma_4 & c_1 p_x + p_y s_1 - d_6 \sigma_2 \\ c_5 c_6 \sigma_5 - c_5 s_6 \sigma_3 - s_5 \sigma_1 & c_6 \sigma_3 + s_6 \sigma_5 & c_5 \sigma_1 + c_6 s_5 \sigma_5 - s_5 s_6 \sigma_3 & c_1 p_y - p_x s_1 - d_6 \sigma_1 \\ c_5 c_6 r_{31} - r_{33} s_5 - c_5 r_{32} s_6 & c_6 r_{32} + r_{31} s_6 & c_5 r_{33} + c_6 r_{31} s_5 - r_{32} s_5 s_6 & p_z - d_6 r_{33} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

where

$$\begin{aligned}
\sigma_1 &= c_1 r_{23} - r_{13} s_1 \\
\sigma_2 &= c_1 r_{13} + r_{23} s_1 \\
\sigma_3 &= c_1 r_{22} - r_{12} s_1 \\
\sigma_4 &= c_1 r_{12} + r_{22} s_1 \\
\sigma_5 &= c_1 r_{21} - r_{11} s_1 \\
\sigma_6 &= c_1 r_{11} + r_{21} s_1
\end{aligned}$$

$${}_4^1\mathcal{T} = \begin{pmatrix} c_4 c_{23} & -c_{23} s_4 & -s_{23} & a_1 + a_2 c_2 + a_3 c_{23} - d_4 s_{23} \\ -s_4 & -c_4 & 0 & 0 \\ -c_4 s_{23} & s_4 s_{23} & -c_{23} & -c_{23} d_4 - a_2 s_2 - a_3 s_{23} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

4.1 Solution for θ_1

By comparing the terms ${}^1_4\mathcal{T}_{(2,4)}$ with ${}^1_4\mathcal{T}_{d(2,4)}$, we will get θ_1 .

$$a_2 c_2 + a_3 c_{23} - d_4 s_{23} = c_1 p_x + p_y s_1 - d_6 \sigma_2$$

By rearranging the above equation and taking squares on both sides, we will reduce the equation for θ_1 .

$$\theta_1 = \begin{pmatrix} -2 \operatorname{atan} \left(\frac{p_x - d_6 r_{13} + \sigma_1}{p_y - d_6 r_{23}} \right) \\ 2 \operatorname{atan} \left(\frac{d_6 r_{13} - p_x + \sigma_1}{p_y - d_6 r_{23}} \right) \end{pmatrix}$$

where

$$\sigma_1 = \sqrt{d_6^2 r_{13}^2 + d_6^2 r_{23}^2 - 2 d_6 p_x r_{13} - 2 d_6 p_y r_{23} + p_x^2 + p_y^2}$$

4.2 Solution for θ_3

It can be seen that there are two possible solutions for θ_1

$${}^0_2\mathcal{T}^{-1} {}^0_5\mathcal{T} = {}^0_2\mathcal{T}^{-1} {}^0_6\mathcal{T}_d {}^5_6\mathcal{T}^{-1}$$

$${}^2_5\mathcal{T}_d = \begin{pmatrix} c_6 \sigma_4 - s_6 \sigma_3 & c_1 c_2 r_{13} - r_{33} s_2 + c_2 r_{23} s_1 & -c_6 \sigma_3 - s_6 \sigma_4 & \\ s_6 \sigma_1 - c_6 \sigma_2 & -c_2 r_{33} - c_1 r_{13} s_2 - r_{23} s_1 s_2 & c_6 \sigma_1 + s_6 \sigma_2 & \\ c_6 \sigma_7 - s_6 \sigma_6 & \sigma_5 & -c_6 \sigma_6 - s_6 \sigma_7 & \\ 0 & 0 & 0 & \end{pmatrix} \begin{pmatrix} c_1 c_2 p_x - p_z s_2 - a_1 c_2 + c_2 p_y s_1 + d_6 r_{33} s_2 - c_2 d_6 r_{23} s_1 - c_1 c_2 d_6 r_{13} \\ a_1 s_2 - c_2 p_z + c_2 d_6 r_{33} - c_1 p_x s_2 - p_y s_1 s_2 + c_1 d_6 r_{13} s_2 + d_6 r_{23} s_1 s_2 \\ c_1 p_y - p_x s_1 - d_6 \sigma_5 \\ 1 \end{pmatrix} \quad (2)$$

where

$$\sigma_1 = c_2 r_{32} + c_1 r_{12} s_2 + r_{22} s_1 s_2$$

$$\sigma_2 = c_2 r_{31} + c_1 r_{11} s_2 + r_{21} s_1 s_2$$

$$\sigma_3 = c_1 c_2 r_{12} - r_{32} s_2 + c_2 r_{22} s_1$$

$$\sigma_4 = c_1 c_2 r_{11} - r_{31} s_2 + c_2 r_{21} s_1$$

$$\sigma_5 = c_1 r_{23} - r_{13} s_1$$

$$\sigma_6 = c_1 r_{22} - r_{12} s_1$$

$$\sigma_7 = c_1 r_{21} - r_{11} s_1$$

$${}^2_5\mathcal{T} = \begin{pmatrix} c_3 c_4 c_5 - s_3 s_5 & -c_5 s_3 - c_3 c_4 s_5 & c_3 s_4 & a_2 + a_3 c_3 - d_4 s_3 \\ c_3 s_5 + c_4 c_5 s_3 & c_3 c_5 - c_4 s_3 s_5 & s_3 s_4 & c_3 d_4 + a_3 s_3 \\ -c_5 s_4 & s_4 s_5 & c_4 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

From ${}^2_5\mathcal{T}_{d(1,4)} = {}^2_5\mathcal{T}_{(1,4)}$

$$a_2 + a_3 c_3 - d_4 s_3 = p_x c_1 c_2 - a_1 c_2 - p_z s_2 - d_6 (r_{13} c_1 c_2 - r_{33} s_2 + r_{23} c_2 s_1) + p_y c_2 s_1$$

From ${}^2_5\mathcal{T}_{d(2,4)} = {}^2_5\mathcal{T}_{(2,4)}$

$$d_4 c_3 + a_3 s_3 = d_6 (r_{33} c_2 + r_{13} c_1 s_2 + r_{23} s_1 s_2) - p_z c_2 + a_1 s_2 - p_x c_1 s_2 - p_y s_1 s_2$$

Now rearranging the equation

$$\begin{aligned} a_2 + a_3 c_3 - d_4 s_3 &= s_2 (d_6 r_3 \mathfrak{Z} - p_z) - c_2 (a_1 + c_1 (-p_x + d_6 r_1 \mathfrak{Z}) - p_y s_1 + d_6 r_2 \mathfrak{Z} s_1) \\ d_4 c_3 + a_3 s_3 &= c_2 (d_6 r_{33} - p_z) + s_2 (a_1 + c_1 (-p_x + d_6 r_{13}) - p_y s_1 + d_6 r_{23} s_1) \end{aligned}$$

Introducing the following substitutions

$$\begin{aligned} E &= d_6 r_3 \mathfrak{Z} - p_z \\ F &= a_1 + c_1 (-p_x + d_6 r_1 \mathfrak{Z}) - p_y s_1 + d_6 r_2 \mathfrak{Z} s_1 \end{aligned}$$

Substituting and squaring both sides the following standard system of equations is obtained:

$$\begin{aligned} (a_2 + a_3 c_3 - d_4 s_3)^2 &= (s_2 E - c_2 F)^2 \\ (d_4 c_3 + a_3 s_3)^2 &= (c_2 E + s_2 F)^2 \end{aligned}$$

Combining the two equations after squaring

$$\begin{aligned} a_3 c_3 + \frac{-E^2 - F^2 + a_2^2 + a_3^2 + d_4^2}{2a_2} &= d_4 s_3 \\ G &= \frac{-E^2 - F^2 + a_2^2 + a_3^2 + d_4^2}{2a_2} \end{aligned}$$

Thus, we get

$$a_3 c_3 + G = d_4 s_3$$

From this solving for θ_3

$$\theta_3 = \begin{pmatrix} \arctan \left(\frac{G d_4 - \sqrt{a_3^2 (-G^2 + a_3^2 + d_4^2)}}{(a_3^2 + d_4^2) \sqrt{1 - \frac{(-G d_4 + \sqrt{a_3^2 (-G^2 + a_3^2 + d_4^2)})^2}{a_3^2 + d_4^2}}} \right) \\ \arctan \left(\frac{G d_4 + \sqrt{a_3^2 (-G^2 + a_3^2 + d_4^2)}}{(a_3^2 + d_4^2) \sqrt{1 - \frac{(G d_4 + \sqrt{a_3^2 (-G^2 + a_3^2 + d_4^2)})^2}{a_3^2 + d_4^2}}} \right) \end{pmatrix}$$

4.3 Solution for θ_2

Now, by comparing the terms ${}^1_4 \mathcal{T}_{(3,4)}$ with ${}^1_4 \mathcal{T}_{d(3,4)}$, we will get θ_2 .

$$\begin{aligned} -c_{23} d_4 - a_2 s_2 - a_3 s_{23} &= p_z - d_6 r_{33} \\ -c_{23} d_4 - a_3 s_{23} &= p_z - d_6 r_{33} + a_2 s_2 \\ -(c_2 c_3 - s_2 s_3) d_4 - a_3 (s_2 c_3 + c_3 s_2) &= p_z - d_6 r_{33} + a_2 s_2 \end{aligned}$$

Rearranging both sides and taking squares, we will get θ_2 .

$$\theta_2 = \begin{pmatrix} 2 \operatorname{atan} \left(\frac{a_2 + \sigma_1 + a_3 c_3 - d_4 s_3}{c_3 d_4 - p_z + a_3 s_3 + d_6 r_{33}} \right) \\ 2 \operatorname{atan} \left(\frac{a_2 - \sigma_1 + a_3 c_3 - d_4 s_3}{c_3 d_4 - p_z + a_3 s_3 + d_6 r_{33}} \right) \end{pmatrix}$$

where

$$\sigma_1 = \sqrt{a_2^2 + 2 a_2 a_3 c_3 - 2 a_2 d_4 s_3 + a_3^2 c_3^2 + a_3^2 s_3^2 + c_3^2 d_4^2 + d_4^2 s_3^2 - d_6^2 r_{33}^2 + 2 d_6 p_z r_{33} - p_z^2}$$

There will be multiple possible solutions for θ_2 depending on θ_3

It should be noted that the θ_2 we get here should be transformed into θ'_2 .

$$\theta_2 := \theta_2 - \frac{\pi}{2}$$

From this point θ_2 should be considered as updated.

4.4 Solution for θ_5

Now, We will compare the matrix ${}^3_6 \mathcal{T}$ with ${}^3_6 \mathcal{T}_d$ and will find the corresponding θ_4, θ_5 and θ_6

$${}^0_3 \mathcal{T}^{-1} {}^0_6 \mathcal{T} = {}^0_3 \mathcal{T}^{-1} {}^0_6 \mathcal{T}_d$$

$${}^3_6\mathcal{T}_d = \begin{pmatrix} r_{11}\sigma_1 + r_{21}\sigma_3 - r_{31}\sigma_6 & r_{12}\sigma_1 + r_{22}\sigma_3 - r_{32}\sigma_6 & r_{13}\sigma_1 + r_{23}\sigma_3 - r_{33}\sigma_6 \\ -r_{11}\sigma_2 - r_{21}\sigma_4 - r_{31}\sigma_5 & -r_{12}\sigma_2 - r_{22}\sigma_4 - r_{32}\sigma_5 & -r_{13}\sigma_2 - r_{23}\sigma_4 - r_{33}\sigma_5 \\ c_1 r_{21} - r_{11} s_1 & c_1 r_{22} - r_{12} s_1 & c_1 r_{23} - r_{13} s_1 \\ 0 & 0 & 0 \\ p_x \sigma_1 - a_1 c_{23} - a_2 c_3 + p_y \sigma_3 - p_z \sigma_6 \\ a_2 s_3 + a_1 s_{23} - p_x \sigma_2 - p_y \sigma_4 - p_z \sigma_5 \\ c_1 p_y - p_x s_1 \\ 1 \end{pmatrix} \quad (3)$$

where

$$\begin{aligned} \sigma_1 &= c_1 c_2 c_3 - c_1 s_2 s_3 \\ \sigma_2 &= c_1 c_2 s_3 + c_1 c_3 s_2 \\ \sigma_3 &= c_2 c_3 s_1 - s_1 s_2 s_3 \\ \sigma_4 &= c_2 s_1 s_3 + c_3 s_1 s_2 \\ \sigma_5 &= c_2 c_3 - s_2 s_3 \\ \sigma_6 &= c_2 s_3 + c_3 s_2 \end{aligned}$$

$${}^3_6\mathcal{T} = \begin{pmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_6 s_4 - c_4 c_5 s_6 & -c_4 s_5 & a_3 - c_4 d_6 s_5 \\ c_6 s_5 & -s_5 s_6 & c_5 & d_4 + c_5 d_6 \\ -c_4 s_6 - c_5 c_6 s_4 & c_5 s_4 s_6 - c_4 c_6 & s_4 s_5 & d_6 s_4 s_5 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

By comparing the element ${}^3_6\mathcal{T}_{(2,3)}$ with ${}^3_6\mathcal{T}_{d(2,3)}$, we will get θ_5 .

$$c_5 = -r_{13}\sigma_2 - r_{23}\sigma_4 - r_{33}\sigma_5$$

where

$$\begin{aligned} \sigma_2 &= c_1 c_2 s_3 + c_1 c_3 s_2 \\ \sigma_4 &= c_2 s_1 s_3 + c_3 s_1 s_2 \\ \sigma_5 &= c_2 c_3 - s_2 s_3 \end{aligned}$$

$$\theta_5 = \begin{pmatrix} \arccos(-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3)) \\ -\arccos(-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3)) \end{pmatrix}$$

We can convert cos inverse in terms of tan inverse

$$\theta_5 = \begin{pmatrix} \arctan \frac{\sqrt{1 - (-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3))^2}}{(-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3))} \\ -\arctan \frac{\sqrt{1 - (-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3))^2}}{(-r_{13}(c_1 c_2 s_3 + c_1 c_3 s_2) - r_{23}(c_2 s_1 s_3 + c_3 s_1 s_2) - r_{33}(c_2 c_3 - s_2 s_3))} \end{pmatrix}$$

4.5 Solution for θ_4

Now, by comparing the terms ${}^3_6\mathcal{T}_{(3,3)}$ with ${}^3_6\mathcal{T}_{d(3,3)}$, we will get θ_4 .

$$\begin{aligned} s_4 s_5 &= c_1 r_{23} - r_{13} s_1 \\ s_4 &= \frac{c_1 r_{23} - r_{13} s_1}{s_5} \end{aligned}$$

$$\theta_4 = \begin{pmatrix} \arcsin\left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right) \\ \pi - \arcsin\left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right) \end{pmatrix}$$

We can write sin inverse in terms of tan inverse as under

$$\theta_4 = \begin{pmatrix} \arctan \frac{\left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right)}{\sqrt{1 - \left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right)^2}} \\ \pi - \arctan \frac{\left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right)}{\sqrt{1 - \left(\frac{c_1 r_{23} - r_{13} s_1}{s_5}\right)^2}} \end{pmatrix}$$

4.6 Solution for θ_6

Now, by comparing the terms $\frac{1}{4}\mathcal{T}_{(3,1)}$ with $\frac{1}{4}\mathcal{T}_{d(3,1)}$, we will get θ_6 .

$$-c_4 s_6 - c_5 c_6 s_4 = c_1 r_{21} - r_{11} s_1$$

Squaring both sides we get

$$(-c_4 s_6 - c_5 c_6 s_4)^2 = (c_1 r_{21} - r_{11} s_1)^2$$

By solving the equations analytically, we get

$$\theta_6 = \left(2 \operatorname{atan} \left(\frac{c_4 - \sigma_1}{c_5 s_4 - c_1 r_{21} + r_{11} s_1} \right) \right)$$

where

$$\sigma_1 = \sqrt{-c_1^2 r_{21}^2 + 2 c_1 r_{11} r_{21} s_1 + c_4^2 + c_5^2 s_4^2 - r_{11}^2 s_1^2}$$

5 Conclusion

It is to be concluded that if we follow Denavit-Hartenberg method, we can end up finding the kinematic model, that is Direct and Inverse Kinematics, of ABB IRB-7600 Robot. There are two ways regarding the placement of axes and determining the parameters but the report solely follows the method described in the lectures which is also stated in the report.