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4 CONTENTS

# Prerequisites

Each chapter of the book match a specific objective. I first introduce the subject with a brief description, try to find some solutions for the specific issues and show the results.

The code is only visible on the html version of the book, so please refer to this format if you need any further information (open the index.html file).

This book is written using the R bookdown package, which can be installed from CRAN or Github:

To compile this example to PDF, you need XeLaTeX. You are recommended to install TinyTeX (which includes XeLaTeX): https://yihui.name/tinytex/.

# Light Interception

#### 2.1 Introduction

In STICS, the light interception is either computed using a simple Beer law assuming a homogeneous, turbid canopy, or a radiation transfer model that consider the plants leaf area index, canopy shape, height and density. The Beer law option is very simple but generally fairly accurate for high density homogeneous crops, but may rapidly yield unsatisfying predictions for stands with higher structural complexity (e.g. perennial plantations or mixed crops). For mixed crops, the model uses the radiation transfer model in a particular manner that is described in further details below.

For the case of intercrops, the model first set the taller crop as "dominant", and the shorter crop as "dominated". The model then compute the radiation interception of each one according to the dominancy, the structure (height, width, light extinction coefficient...) and position (interrow distance, row orientation) of the species. Of course, the dominancy of each plant species can be inverted if the dominated plant become taller than the dominant plant, and the model checks every day for such a case.

To facilitate understanding, we will use a common intercrop example throughout the whole document. We take a mixed crop simulated for the day of the year 1 with a global radiation of 25 MJ m-2 day-1 (= 12 MJ m-2 day-1 of PAR), and a diffuse fraction of light of 0.4, an interrow spacing of 1 meter, a shape of 1 (1= rectangle, 2= upside triangle and 3= downside rectangle), a canopy width of 0.2 meter, a canopy thickness of 0.1 meter, a row orientation of 0 relative to the North-South axis at latitude 43.61 degrees north, an LAI of 2, a light extinction coefficient of 0.2. The canopy of the dominant plant is 1 meter above the dominated plant. All code used in this document can be viewed in each section by clicking on the Code button on the right.

# 2.2 Plant shape

Each plant radiation interception is computed using an approximation of its shape (P\_forme= 1, rectangle, = 2 upside triangle, = 3 downside triangle), leaf area index (lai or p(i)%lai(ens,n)), height, width, density at emergence and leaf area density (dfol).

#### 2.2.1 Plant width computation

First, the plant width is computed using the formplante function. This computation is possible thanks to the relationship between two ways for computing the plant leaf area, where one of them uses the plant width:

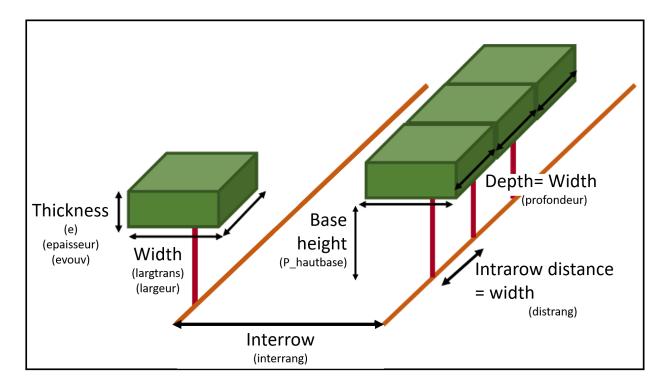


Figure 2.1: Diagram representing the different parameters used to compute plant width. The different names used in the model are shown between parenthesis

- First, assuming the plant has a square footprint (i.e. plant projection is square), we can find the plant leaf area using the leaf area index (lai) and the plant density:  $LA = \frac{(lai+laisen+eai)}{densite} \text{ which is the equivalent to: } LA = (lai+laisen+eai) \cdot interrang \cdot distrang$  where lai is the leaf area index, laisen is the senescent leaf area index, eai is the equivalent leaf area of the photosynthetic organs that are not leaves (e.g. flower buds), interrang is the inter-row spacing and distrang the intra-row distance.
- Second, using the leaf area density and the plant volume such as:  $LA = dfol \cdot largeur \cdot epaisseur \cdot profondeur$  for a cuboid and  $LA = dfol \cdot \frac{1}{2} \cdot (largeur \cdot epaisseur \cdot profondeur)$  for a triangular prism, where dfol is the leaf area density, largeur is the plant width (also called largtrans), epaisseur is the plant thickness and profondeur is the plant depth.

Knowing both equations, and assuming the two following hypothesis:

- 1. The plant depth is equal to the plant width
- 2. The intra-row distance between two plants is equal to the plant width

We can now compute the plant width as:  $largeur = \sqrt{\frac{(lai+laisen+eai)\cdot interrang}{dfol\cdot varrapforme}}$ 

where varrapforme (or raptrans further) is the ratio between the plant thickness and width and is computed as  $varrapforme = \frac{(hauteur - P_{hautbase})}{largeur}$  where hauteur is the total plant height, P\_hautbase is the plant (i.e. crown) base height and largeur is the plant width (see fig 2.1 for more details)

Original	Modified	Definition
hauteur	hauteur	Height
largeur	largtrans	Width
varrapforme	raptrans	Thickness/Width Ratio
enouv	enouv	Thickness

Table 2.1: Variable name modification in the formplante function

#### 2.2.2 Plant width correction

If the dominated plant is higher than the base height of the dominant plant, the radiation interception of the dominant plant is partially reduced, by reducing the volume that can intercept light to the canopy volume above the dominated plant only. This correction is made to consider the competition for light between the two species, and is computed according to the shape of the plant.

Consequently, the model first compute the height of the dominated plant (sc%originehaut) by looking for the maximum height between the sunlit and shaded part of the dominated plant:

sc%originehaut = max(p(i+1)%hauteur(sc%AO),p(i+1)%hauteur(sc%AS))

sc%originehaut is fixed to 0 (= soil) while computing the dominated plant.

Hence, the new thickness (enouv) is computed as:  $enouv = largeur \cdot |varrapforme| + hauteurzero$ , and is used to re-compute the shape of the plant:

- The new thickness to width ratio (raptrans, formerly varrapforme):  $raptrans = \frac{enouv}{largeur}$  for rectangle shaped plants,
- The new width (largtrans, formerly largeur):  $largtrans = \frac{enouv}{varrapforme}$  for upsided triangle shaped plants,
- The new width (largtrans, formerly largeur):  $raptrans = \frac{enouv}{largtrans}$  for downsided triangle shaped plants,

All variable names are changed, whether there is a correction or not. Here is a summary table:

Upside triangle is a triangle with its base at the bottom, while downside triangle is a triangle with the base at the top.

The correction of the shape of the plant can be summarised in the following diagram (2.2):

The correction of the shape of the plant is only used to compute the light transmitted to a plane at the dominated plant or soil height. The targeted plant interception is computed using its whole leaf area index and a light extinction coefficient.

# 2.3 Light interception

The light intercepted by a plant species is obtained by computing the light reaching a horizontal plane below its canopy, either at the height of the dominated plant (for the dominant plant) of the soil (for the dominated plant). Therefore, the light incident on this plane is either coming from:

• The incident light coming from the atmosphere, divided into two components, namely the diffuse and direct light. This light is called rdroit in the model,

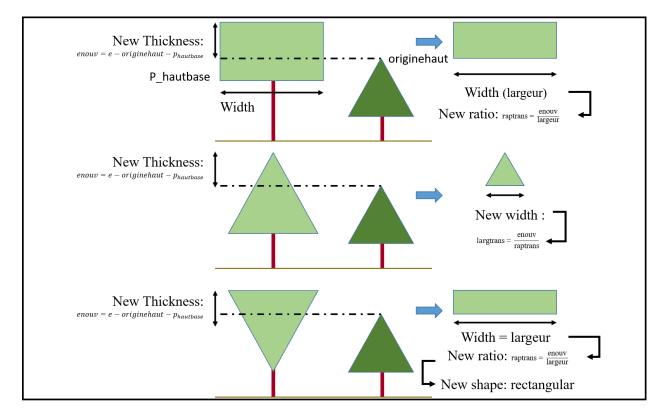


Figure 2.2: Competition for radiation interception of the dominant plant induced by a high dominated plant

• The light transmitted by the dominant crop, which is called rtrans, and that is generally of lower quality for photosynthesis. The effect of light quality is wrapped in the equivalent density formalism, see 5 for more details.

Consequently, numerous points (20, or 200 if the inter-row is lower than 1 m) are equally distributed every meter along the inter-row (i.e. one point every 5 cm, or every 0.5 cm with 200 points), at the height of the plane. These points are used to discretize the computation of the incident light at the surface of the plane. Hence, the total number of points to simulate is computed using the interval parameter, which is equal to 200 if the inter-row is lower than 1 meter or 20 if more. It is then used to compute the total number of points to simulate as:  $N_{points} = \frac{ir}{2} \cdot interval$ 

In practice, the model really simulates only half of the inter-row, because it is considered that the other half have the same light conditions at daily time-scale. For example, if we take an interrow of 10 meters, the model simulates 100 points equally distributed from 0 to 5 meters.

Here is an example of the X position on the plane, starting from the left-hand side of the row, using an inter-row spacing of 1 meter and a plant width of 0.2 meter:

```
if(ir<1.0){
  interval = 200
}else{
  interval = 20.
}
i = 1:(ir / 2 * interval)</pre>
```

```
x= (i-1) / interval
cat(paste("x=", paste(x, collapse = ", ")))
```

x = 0, 0.05, 0.1, 0.15, 0.2, 0.25, 0.3, 0.35, 0.4, 0.45

The points are then divided into two groups:

- The sunlit points, which are located directly under the crown of the targeted crop.
- The shaded points, which are not directly under the crop crown, *i.e.* they have the sky above them.

Then the semi-hemisphere above each point is discretized onto 2 x 23 angles: 23 angles from top to right, and 23 angles from top to left. These angles are used to compute kgdiffus, the atmospheric diffuse radiation incident to the X point. However, if the X point is below the targeted crop canopy (X<1/2), only the 23 angles from the top to the right are used to compute kgdiffus (considering that Xs are only computed from the left-hand plants row until the middle of the inter-row, see fig.2.3 for more details).

The model determines the two angles ( $\theta_1$  and  $\theta_2$ ) between which the point only receive incident light coming from the atmosphere (rdroit). Using these two angles (or their tangent, G), the model computes:

- 1. The daily direct radiation (i.e. cumulated hourly radiation) that is incoming only during the time period between two hours (h1 and h2) when the sun angle is between  $\theta_1$  and  $\theta_2$ . Function kgeom called in rtrans.
- 2. The incident diffuse radiation for all angles between  $\theta_1$  and  $\theta_2$ . Function kdiff called in rtrans.
- 3. The light transmitted to the plane by the target crop for all angles below  $\theta_1$  or above  $\theta_2$ .

In practice, all points with an x position lower than  $\frac{largeur}{2}$  are shaded, and all other are sunlit, so the model computes the diffuse radiation coming from the atmosphere only for one quarter of the hemisphere for shaded Xs; the other quarter will receive transmitted light because all angles are superior to  $\theta_2$ .

Main functions used are transrad, rtrans, kdiff and kgeom.

The position of  $\theta_1$  and  $\theta_2$  (and their tangent) depends from three components: the crop shape, its inter-row spacing, and the sun azimuth (see fig. 2.3).

#### 2.3.1 Incident direct radiation from the atmosphere

The incident direct radiation for each X point is computed for all angles of the hemisphere between  $\theta_1$  and  $\theta_2$  (see 2.3), and summed up to integrate the semi-hemisphere of each point.

Here is an example of the computation of the direct proportion received at each X point for a crop using the kgeom() function:

```
decangle= function(j){
  theta1 = 2 * pi * (j - 80) / 365
  theta2 = 0.034 * (sin(2 * pi * j / 365) - sin(2 * pi * 80 / 365))
  theta = theta1 - theta2
  decangle = asin(0.3978 * sin(theta))
}
thetacrit= function(lat,j,tgh,alpha){
```

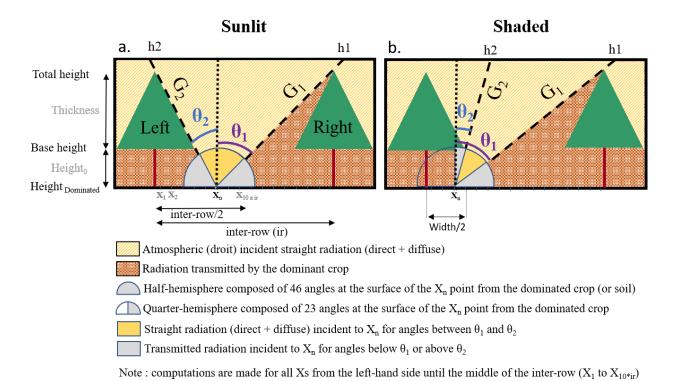


Figure 2.3: Diagram of the computation workflow of STICS for radiation interception for two X points placed above the dominated plant species. a. The X point is considered sunlit; b. The X point is considered shaded (right under the dominant plant canopy), so only the right-hand side of the semi-hemisphere is computed for atmospheric radiation

```
acrit = 0.0
  bcrit = 0.0
 a = 0.0
 b = 0.0
 thetacr = 0.0
 hcritprec= 0
 n = 3
  dec = decangle(j)
 hprec = 0.0
 pi = 4 * atan(1.0)
 theta= rep(0,180)
 for(i in 1:(18 * n)){
   theta[i] = 10. / n * (i - 1)
   theta[i] = (theta[i] - 90) / 180 * pi
   # Sun position (h,azim)
   sinh = sin(lat) * sin(dec) + cos(lat) * cos(dec) * cos(theta[i])
   h = asin(sinh)
   cosazim = (-cos(lat) * sin(dec) + sin(lat) * cos(dec) * cos(theta[i])) / cos(h)
   cosazim = pmin(1.0, cosazim)
   if(theta[i]!=0.0){
      azim = acos(cosazim) * theta[i] / abs(theta[i])
   }else{
     azim = 0.0
   }
   if(sinh<0.0){h = 0.0}
   # Critical height
   hcrit = atan(tgh * abs(sin(azim + alpha + 0.00001)))
    # test for h = hcrit
   if (hcritprec >= hprec & hcrit <= h & i > 1){
      # Linear interpolation:
     acrit = (hcrit - hcritprec) / (theta[i] - theta[i-1])
     bcrit = hcrit - acrit * theta[i]
      a = (h - hprec) / (theta[i] - theta[i-1])
      b = h - a * theta[i]
      if(a!=acrit){thetacr = (b - bcrit) / (acrit - a)}
      hcritprec = hcrit
      hprec = h
   }
 }
 return(thetacr)
e = abs(1 * rap) # Thickness of the plant crown
                # Init.
xprec= 0
limite = 1 / 2
if(ir<1.0){interval = 200.}else{interval = 20.}</pre>
if(1>ir/2.){1 = ir/2.}
if(e>0.0){
```

```
limite2 = 1/2 * (haut/e+1)
}else{
  P_forme = 1
}
\# NB : is it sure that it is (haut/e+1) and not (haut/(e+1)) ?
# Saving some intermediate results for output here (not in the real function):
x_s = (1:(ir / 2 * interval))
Output= data.frame(x_index= x_s,
                   x_{value} = (x_s-1)/interval,
                    theta1= rep(NA_real_,length(x_s)),
                   theta2= rep(NA_real_,length(x_s)),
                    theta1_deg= rep(NA_real_,length(x_s)),
                    theta2_deg= rep(NA_real_,length(x_s)),
                   kg= rep(0,length(x_s)))
# Loop over Xs:
for(i in x_s){
  x = (i-1) / interval
  if(xprec <= 1/2 &x >= 1/2) \{ilim = i\}
  xprec = x
  # kdir:
  # Rectangle:
  if(P_forme==1){
    tgh1 = (haut + e) / (ir - x - limite)
    theta1 = thetacrit(lat,j,tgh1,alpha)
    if(x>limite){
      tgh2 = (haut + e) / (x - limite)
      theta2 = thetacrit(lat,j,tgh2,alpha)
    }else if(x < limite){</pre>
      tgh2 = haut / (-x + limite)
      theta2 = -thetacrit(lat,j,tgh2,alpha)
      \# x == limite
      theta2 = 0
    }
  }
  # Downside Triangle:
  if (P_forme==2 & rap<0.){</pre>
    tgh1 = (haut + e) / (ir - x - limite)
    theta1 = thetacrit(lat,j,tgh1,alpha)
    if (x > limite){
      tgh2 = (haut + e) / (x - limite)
      theta2 = thetacrit(lat,j,tgh2,alpha)
    }else if(x < limite){</pre>
      tgh2 = (haut + e) / (x - limite)
      theta2 = -thetacrit(lat,j,tgh2,alpha)
    }else{
      theta2 = 0
```

```
}
  }
  # Upside Triangle:
  if (P_forme==2&rap>0.){ then
    tgh1 = (haut + e) / (ir - x - limite)
    theta1 = thetacrit(lat,j,tgh1,alpha)
    if (x < limite2){</pre>
      if (x > limite){
        tgh2 = haut / (x - limite)
        theta2 = thetacrit(lat,j,tgh2,alpha)
      }else if(x < limite){</pre>
        tgh2 = haut / (limite - x)
        theta2 = -thetacrit(lat,j,tgh2,alpha)
      }else{
        theta2 = 0.0
    }else if(x >= limite2){
      tgh2 = (haut + e) / x
      theta2 = thetacrit(lat,j,tgh2,alpha)
  }
  \# NB: is there a missing else here ? kg is modified just after...
  if(e > 2.1e-2){
   kg = cos(theta1)
    kg = cos(theta2)
  kg = 0.5 * (cos(pi/2 + theta1) + cos(pi/2 + theta2))
  kg = max(kg,0.0)
  Output$theta1[Output$x_index==i] = theta1
  Output$theta2[Output$x_index==i] = theta2
  Output$kg[Output$x_index==i] = kg
}
Output$theta1_deg= (pi/2+Output$theta1)*180/pi
Output$theta2_deg= (pi/2-Output$theta2)*180/pi
colnames(Output) = c("X index","X value (m)","Theta 1 (rad)","Theta 2 (rad)",
                     "Theta 1 (deg)", "Theta 2 (deg)", "kgdirect")
kable(Output, caption= paste("Example of the computation of the incident direct",
                              "radiation ratio kgdirect. See introduction section",
                              "for further details on the crop."))
```

Where  $\theta_1$  and  $\theta_2$  are the angles visible in fig.3 and kgdirect the proportion of the semi-hemisphere that receive direct light, considering sun position throughout the day by using stand latitude, day of year and row orientation. In the model,  $\theta_1$  and  $\theta_2$  are computed in radian relative to the vertical plane above X. To provide a simpler representation,  $\theta_1$  and  $\theta_2$  are also given in degrees relative to the horizontal plane (i.e. soil or dominated plant species surface) in tab.2.2.

X index	X value (m)	Theta 1 (rad)	Theta 2 (rad)	Theta 1 (deg)	Theta 2 (deg)	kgdirect
1	0.00	-0.7563093	0.1163553	46.66667	83.33333	0.2850744
2	0.05	-0.7563093	0.0581776	46.66667	86.66667	0.3140484
3	0.10	-0.6981317	0.0000000	50.00000	90.00000	0.3213938
4	0.15	-0.6981317	-0.0581776	50.00000	93.33333	0.3504662
5	0.20	-0.6399541	-0.1163553	53.33333	96.66667	0.3566258
6	0.25	-0.6399541	-0.1745329	53.33333	100.00000	0.3854034
7	0.30	-0.5817764	-0.2327106	56.66667	103.33333	0.3900624
8	0.35	-0.5235988	-0.2908882	60.00000	106.66667	0.3934016
9	0.40	-0.4654211	-0.2908882	63.33333	106.66667	0.3678012
10	0.45	-0.4654211	-0.3490659	63.33333	110.00000	0.3954097

Table 2.2: Example of the computation of the incident direct radiation ratio kgdirect. See introduction section for further details on the crop.

### 2.3.2 Incident diffuse radiation from the atmosphere

The incident diffuse radiation for all angles between  $\theta_1$  and  $\theta_2$  is computed using G, the apparent tangent to the considered  $\theta$ . First the model computes it for  $\theta_1$ , and uses it as a threshold under which no diffuse radiation comes from the atmosphere because only transmitted radiation reaches this angle for the considered X point. Second, the model tests if the X point is below the target crop canopy, and if not it computes G for G0, and applies the same methodology, with G0 being the upper threshold this time. This method avoids computing the left-hand quarter of the hemisphere since it receives only transmitted light necessarily if it is under the targeted crop.

Here is an example of the computation of the diffuse proportion received at each X point for the same crop as above (interrow= 1 meter, width= 0.2 meter, thickness= 0.1 meter, height= 1 meter) using the kdif() function:

```
# Initializations:
htab= c(9.23, 9.23, 9.23, 9.23, 10.81, 10.81, 26.57,
        26.57, 26.57, 31.08, 31.08, 31.08, 31.08, 31.08, 47.41,
        47.41, 47.41, 52.62, 52.62, 69.16, 69.16, 69.16)
aztab= c(12.23,59.77,84.23,131.77,156.23,36,108,0,72,144,23.27,48.73,95.27,
         120.73, 167.27, 0, 72, 144, 36, 108, 0, 72, 144)
SOCtab= c(0.0043, 0.0043, 0.0043, 0.0043, 0.0043, 0.0055,
          0.0055, 0.0140, 0.0140, 0.0140, 0.0197, 0.0197,
          0.0197, 0.0197, 0.0197, 0.0336, 0.0336, 0.0336,
          0.0399, 0.0399, 0.0495, 0.0495, 0.0495)
xprec= 0
if(ir<1.0){interval = 200.}else{interval = 20.}</pre>
if(1>ir/2.){1 = ir/2.}
# Saving some intermediate results for Output_diff here (not in the real function):
x_s = (1:(ir / 2 * interval))
Output_diff= data.frame(x_index= rep(x_s,each=23),
                   x_{value} = rep((x_s-1)/interval, each=23),
                   Angle = rep(1:23, length(x_s)),
                   G1= rep(NA_real_,length(x_s)*23),
                   G2= rep(NA_real_,length(x_s)*23),
                   hcrit= rep(0, length(x s)*23),
                   kgdiffus= rep(0,length(x_s)*23))
```

```
# Loop over Xs:
for(i in x s){
 x = (i-1) / interval
 if(xprec <= 1/2 &x >= 1/2) \{ilim = i\}
 xprec = x
 # kdif:
 x = \min(x, ir/2)
 e = abs(l*rap)
 kgdiffus = 0.
 # Computing for the right-hand of the row:
 G1 = \frac{haut+e}{(ir-x-1/2)} # the apparent tangent h1
 for(j in 1:23){
   hcrit = atan(G1*sin(aztab[j]/180*pi))/pi*180
   if(hcrit<htab[j]){</pre>
     kgdiffus = kgdiffus+SOCtab[j]
     ####### Not in the real function #######
     Output_diff$kgdiffus[Output_diff$x_index==i&Output_diff$Angle==j]= SOCtab[j]
     }
   ####### Not in the real function #######
   Output_diff$hcrit[Output_diff$x_index==i&Output_diff$Angle==j]= hcrit
   Output_diff$G1[Output_diff$x_index==i&Output_diff$Angle==j]= G1
   }
 # Computing for the left-hand row, if the point is not a shaded point:
 if(x>1/2){
   G2 = \frac{haut+e}{(x-1/2)} # the apparent tangent h2
   for(j in 1:23){
     hcrit = atan(G2*sin(aztab[j]/180*pi))/pi*180
     if(hcrit < htab[j]){</pre>
       kgdiffus = kgdiffus+SOCtab[j]
       ####### Not in the real function #######
       Output_diff$kgdiffus[Output_diff$x_index==i&Output_diff$Angle==j]=
         Output_diff$kgdiffus[Output_diff$x_index==i&Output_diff$Angle==j]+SOCtab[j]
       ####### Not in the real function #######
     Output_diff$hcrit[Output_diff$x_index==i&Output_diff$Angle==j]= hcrit
     Output_diff$G2[Output_diff$x_index==i&Output_diff$Angle==j]= G2
     }
 }
}
colnames(Output_diff) = c("X index","X value (m)", "angle", "G1 (tangent)",
                       "G2 (tangent)", "hcrit", "kgdiffus")
if(knitr:::pandoc_to() == "html") {Output_diff}else{
```

Table 2.4: Example of the computation of the incident diffuse radiation ratio kgdiffus. See introduction section for further details on the crop.

X index	kgdiffus
1	0.3489
2	0.3489
3	0.3489
4	0.4061
5	0.3864
6	0.3864
7	0.3864
8	0.4023
9	0.4023
10	0.3624

Table 2.3: Computation of the diffuse light incident on each point x. Ten first rows only, for the full data, please refer to the html version of this book

X index	X value (m)	angle	G1 (tangent)	G2 (tangent)	hcrit	kgdiffus
1	0	1	1.222222	NA	14.51577	0.000
1	0	2	1.222222	NA	46.56057	0.000
1	0	3	1.222222	NA	50.56789	0.000
1	0	4	1.222222	NA	42.35117	0.000
1	0	5	1.222222	NA	26.22654	0.000
1	0	6	1.222222	NA	35.69363	0.000
1	0	7	1.222222	NA	49.29501	0.000
1	0	8	1.222222	NA	0.00000	0.014
1	0	9	1.222222	NA	49.29501	0.000
1	0	10	1.222222	NA	35.69363	0.000

The total diffuse radiation incident to each point X is simply the cumulative of each angle:

```
suppressWarnings(suppressPackageStartupMessages(library(dplyr)))
Output_diff%<>%
    group_by(`X index`)%>%
    summarise(kgdiffus= sum(kgdiffus))

kable(Output_diff,caption= paste("Example of the computation of the incident diffuse",
    "radiation ratio kgdiffus. See introduction section for further details on the crop."))
```

X index	X value (m)	Total incident ratio	Atmospheric ratio (rdroit)	Transmitted ratio (rtransmis)	Light environ
1	0.00	0.7727202	0.3106046	0.4621155	Shaded
2	0.05	0.7784515	0.3279890	0.4504624	Shaded
3	0.10	0.7799044	0.3323963	0.4475082	Sunlit
4	0.15	0.7931983	0.3727197	0.4204785	Sunlit
5	0.20	0.7918188	0.3685355	0.4232833	Sunlit
6	0.25	0.7975112	0.3858020	0.4117092	Sunlit
7	0.30	0.7984328	0.3885975	0.4098354	Sunlit
8	0.35	0.8011901	0.3969610	0.4042292	Sunlit
9	0.40	0.7961262	0.3816007	0.4145254	Sunlit
10	0.45	0.7963256	0.3822058	0.4141198	Sunlit

Table 2.5: Example of the computation of the total incident radiation ratio. See introduction section for further details on the crop.

# 2.3.3 Total diffuse and direct radiation from the atmosphere incident to each X point

The total radiation from the atmosphere incident to each X point is computed by using the incident diffuse (rdif) and direct (rdirect) radiation coming from the atmosphere weighted respectively by the previously computed kgdiffus and kgdirect as follow:  $rdroit = (kgdiffus \cdot rdif) + (kgdirect \cdot rdirect)$ 

## 2.3.4 Light transitted by the dominant crop to the X points

The light transmitted by the dominant crop to the dominated crop (rtransmis) is computed using the total radiation from the atmosphere incident to each X point (rdroit) and the effective targeted plant leaf area index as follow:

$$rtransmis = (1.0 - rdroit) \cdot e^{-P_{ktrou} \cdot (lai + eai)}$$

where  $P_{ktrou}$  is the targeted plant light extinction coefficient, lai the plant leaf area index, and eai the equivalent leaf area index, which represent the photosynthetic surface that is not from leaves (e.g. wheat ears, rapeseed pods, pea pods or grapes during their green stage).

#### 2.3.5 Total light incident to X points

The total light incident to each X point is the sum of the three components: atmospheric diffuse light, atmospheric direct light and transmitted light by the dominant crop. Taking our previous example again, this computation leads to:

The Total incident ratio is computed as: Total incident ratio= rdroit+rtransmis. It is the proportion of the incident light from the atmosphere that reach the point on the plane below the plant canopy. This light either comes directly from the sky (rdroit) or passing through the plant canopy (rtransmis). Consequently, the first point X of our example that is right under the plant canopy receives in average incident\_light\$Total[1]\*100% of the light coming from the atmosphere: incident\_light\$rdroit[1]\*100% of the light directly from the sky (either direct or diffuse light) + incident\_light\$rtransmis[1]\*100% of the light that is transmitted by the plant above.

#### 2.3.6 Total radiation incident to the plane

After computing the total incident ratio for each point, the model averages the values between the so-called sunlit and shaded components. Each point positioned right under the plant canopy is considered shaded,

Table 2.6: Example of the computation of the total incident radiation ratio for each light environment for a horizontal plane below the targeted plant canopy. See introduction section for further details on the crop.

STICS variable name	Light environment	Total incident light ratio
rombre	Shaded	0.7755858
rsoleil	Sunlit	0.7943134

and all other is considered sunlit (see fig. 2.3). using our previous example, this computation gives:

Finally, both ratios are used to compute the intercepted PAR raint (MJ m-2 d-1) of the target plant as:  $raint = P_{parsurrg} \cdot trg \cdot (1 - (rombre \cdot surf AO) - (rsoleil \cdot surf AS))$ 

where  $P_{parsurrg}$  is a coefficient to compute PAR (Photosynthetically Active Radiation) from the global radiation, trg is the active radiation (either global radiation or radiation transmitted below the dominant crop), rombre and rsoleil are the ratio of incident light for shaded and sunlit components of the plane, and surfAO and surfAS are the relative surfaces (0 to 1) of the shaded and sunlit components of the plane. The computation of trg is further described in Chapter 3.

For our example, the crop would have intercepted NA, NA MJ m-2 day-1 of radiation, with a PAR of 12.5 W m-2, an rombre of 0.7755858, NA, an rsoleil of NA, 0.7943134 and a relative surface of 0.2 and 0.8 for the shaded and sunlit component respectively.

The relative surfaces (0 to 1) of the shaded and sunlit components of the plane (surfAO and surfAS) that are computed during the dominant plant computation are then used as the shaded and sunlit surfaces for the dominated plant.

## 2.4 Summary

The interception of the targeted plant is obtained by:

- 1. Computing the light that is incident at a horizontal plane at the height of the dominated plant (or the soil) and
- 2. Substracting this incident light to the global PAR, which gives the PAR intercepted by the target plant.

This process is applied iteratively to the dominant and the dominated plant to compute both species PAR interception while taking account for their respective structure (shape, height, width...).

# 2.5 Discussion and proposed modifications

The dominated plant interception is computed in two separate computations, one for the sunlit component, and one for the shaded component, and interception is then weighted by their relative surface. The dominant plant is considered having 100% of its surface that is sunlit, so all this computation is made only for its sunlit part.

The radiation above the dominant plant (trg) is the global radiation, but the radiation above the dominated plant (also trg) is computed as:  $trq = trq \cdot rsoleil$ 

where rsoleil is the average proportion of light intercepted by the sunlit area of the plane below the dominant plant.

This computation is only right for the sunlit component of the dominated plant. A modification is proposed, discussed and tested on Chapter 3.

# Light incident to the dominated crop (trg)

## 3.1 Computing the trg incident to the dominated plant

For the moment, STICS compute the radiation incident above the dominated (or associated) plant as:

Which means that trg for the dominated plant (i > 1) is computed as the global atmospheric radiation, reduced by the average proportion of light intercepted by the sunlit area of the plane below the dominant plant. This computation does not consider that the average proportion of light incident above the shaded part of the dominated plant (rombre) is different from rsoleil. See Chapter 2 for more details.

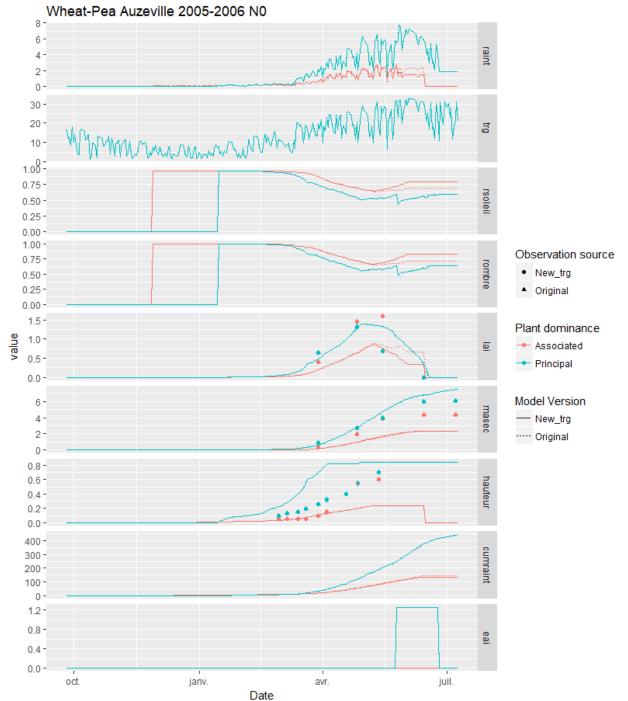
# 3.2 Proposed solution

We propose to change this computation to take the relevant incident light according to the light regime of the dominated plant under computation:

With this new computation, the radiation incident above the dominant plant depends from the component (shaded or sunlit) under consideration, and is computed using the geometry of the dominant plant (for atmospheric+transmitted light computation).

## 3.3 Results

A comparison of the two was made using the sticRs package, from which a summary plot was extracted:



The comparison between both indicated that the dominated plant intercepted more PAR with the original computation (raint), due to its wrong light regime (rsoleil for both AS and AO). While the dry mass and height of the dominated plant did not change, its LAI was previously higher on the end of the rotation, which increased the rsoleil and rombre of the ground (visible as associated ones). These simulations also showed that the wheat (dominant) eai was highly overestimated, which will be fixed in the next simulations.

# Wheat EAI parameterization

## 4.1 Introduction

The simulations outputs from Chapter 3 have shown that the wheat ears equivalent photosynthetic surface area (eai) was probably overestimated by a 3-4 factor. This surface is computed using the fruit dry mass (maenfruit) and a parameter (P\_sea) as follow:

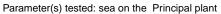
$$eai = P_{sea} \cdot \frac{maenfruit}{100}$$

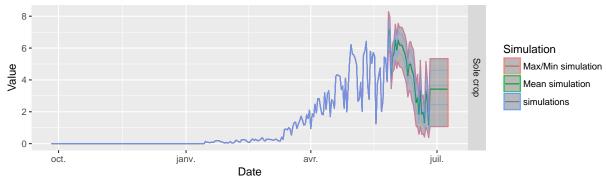
This parameter was originally equal to 100, meaning that each gram of fruit dry mass gave 1 m2 of equivalent LAI. This value was probably overestimated, but before re-parameterizing the plant, we first needed to know the model sensitivity to this parameter.

# 4.2 Model sensitivity to the P\_sea parameter

The model sensitivity was assessed using the sticRs package using values from 10 to 90 for the P\_sea parameter. The results are shown below (see html version of this book for interactivity):

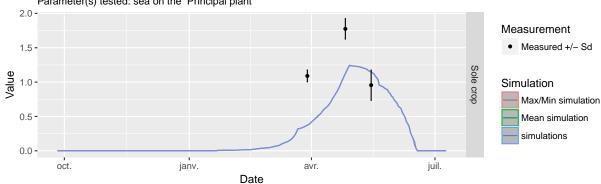
#### Sensitivity analysis for the raint variable



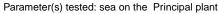


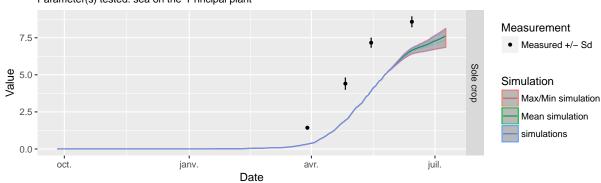
#### Sensitivity analysis for the lai\_n variable



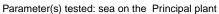


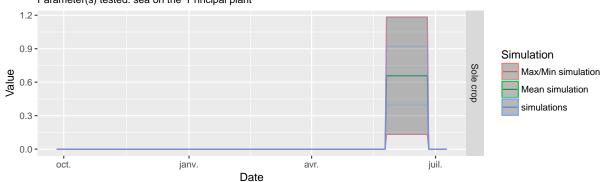
### Sensitivity analysis for the masec\_n variable





#### Sensitivity analysis for the eai variable

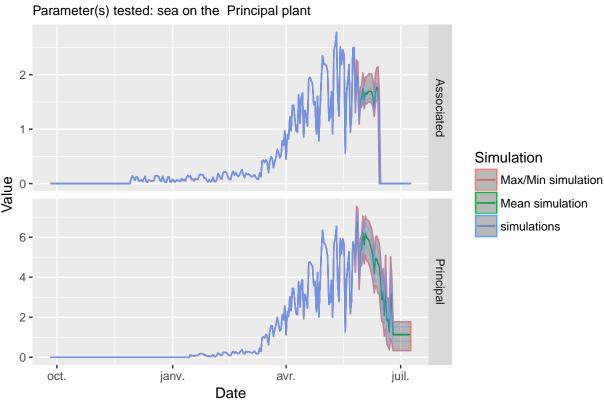




The results show that the higher the P\_sea, the higher the eai, and hence increasing the light interception (raint), which induced a higher aboveground dry mass (masec). The plant LAI is not influenced by the P\_sea though, because there is no retroactions on this variable.

In the case of intercrops, the  $P\_sea$  parameter can influence the dominated plant also, because less light is transmitted when  $P\_sea$  is high:

# Sensitivity analysis for the raint variable



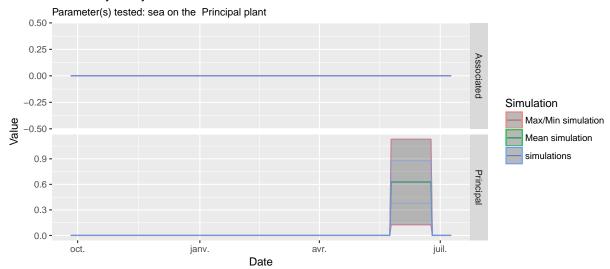
The other variables are not much impacted though:

juil.

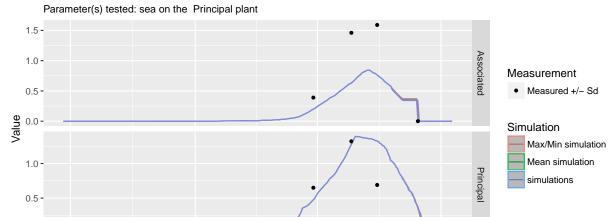
0.0 -

oct.

#### Sensitivity analysis for the eai variable



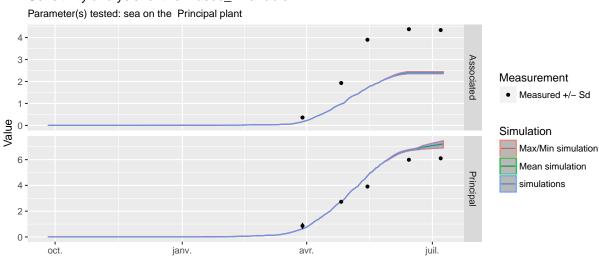
### Sensitivity analysis for the lai\_n variable



avr.

## Sensitivity analysis for the masec\_n variable

janv.



avr.

Date

## 4.3 Parameterization of the P\_sea parameter

Knowing that the key outputs from the model are not much impacted by the P\_sea parameter as soon as its value is not unreasonable, we tested several values of the parameter (i.e. 20, 50 and 80) and compared the outputs of the model against measurements for several types of management: Wheat in sole crop, Pea in sole crop, Wheat in self-intercrop, Pea in self-intercrop, and a Wheat-Pea intercrop. The results are available on this page. In short, the value we kept for the wheat was 20.

# Plant density and equivalent plant density

#### 5.1 Introduction

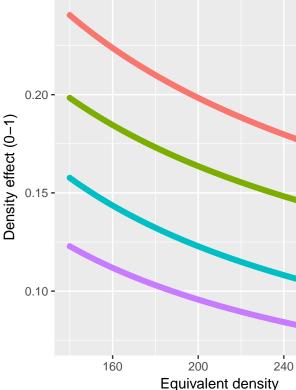
The plant density, which is related to the interrow distance, seems to be an important formalism to describe the crop, and particularly for mixed crops. Several computations are made to represent plant competition in the STICS model, making the density effect a complex process. Lets describe each step of the process to have a clearer representation in mind.

# 5.2 The density effect on LAI

In the model, the plant density is taken as a negative effect upon the LAI growth as soon as a threshold of LAI is reached. This threshold (P\_laicomp) represents the moment when the leaf surface of a plant start becoming competitive for light against another plant (from the same species or not). So whenever the LAI is higher than P\_laicomp, the effect of the density (efdensite) become closer to 0 (the effect is null when equal to 1, and maximum at 0). This effect is computed as:  $ef_{densite} = \min \left\{ 1.0 \; ; \; e^{P_{adens} \cdot \frac{log(densite equiv)}{P_{bdens}}} \right\}$  or more simply:  $ef_{densite} = \min \left\{ 1.0 \; ; \; (\frac{densite equiv}{P_{bdens}})^{P_{adens}} \right\}$ 

Replace the equation in the model to simplify too?

# Equivalent density / density effe



Here is a plot representing the density effect along the equivalent density:

So the higher the density, the higher the negative effect on LAI.

# 5.3 The equivalent density

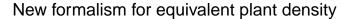
In sole crops, the density effect is straightforward. However, under the case of mixed crops, the density effect can be higher for the dominated plant compared to its equivalent in sole crops. Indeed, a pea in sole crop would have a given competition with other close plants, but a different one when mixed with wheat, where the same density of wheat can give higher competition effect for light because it is taller.

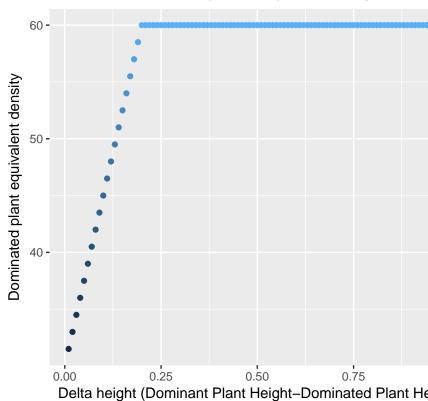
Then the density effect is computed as an equivalent density instead (densiteequiv), that can differ from the sowing density for the dominated crop to increase the negative effect of efdensite compared to a sole crop.

The previous implementation in STICS was simple. The dominated plant had a doubled equivalent density compared to its actual density. After some discussion with the STICS intercrop team, Sebastian Munz modified the STICS code to implement a new formalism to define the equivalent density as a function of the height difference between the plants as follow:

$$density_{Equivalent} = \begin{cases} \Delta_{height} > hauteur_{threshold} & density_{p2} + \frac{density_{p1}}{P_{bdensp1}} \cdot P_{bdensp2} \\ \Delta_{height} < hauteur_{threshold} & density_{p2} + slope \cdot abs \left| \Delta_{height} \right| \end{cases}$$
 with  $diffx = \frac{density_{p1}}{P_{bdensp1}} \cdot P_{bdensp2}$  and  $slope = \frac{diffx}{hauteur_{threshold}}$ 

Here is an exemple with a wheat-pea intercrop with a plant density of 140 for the wheat as the principal

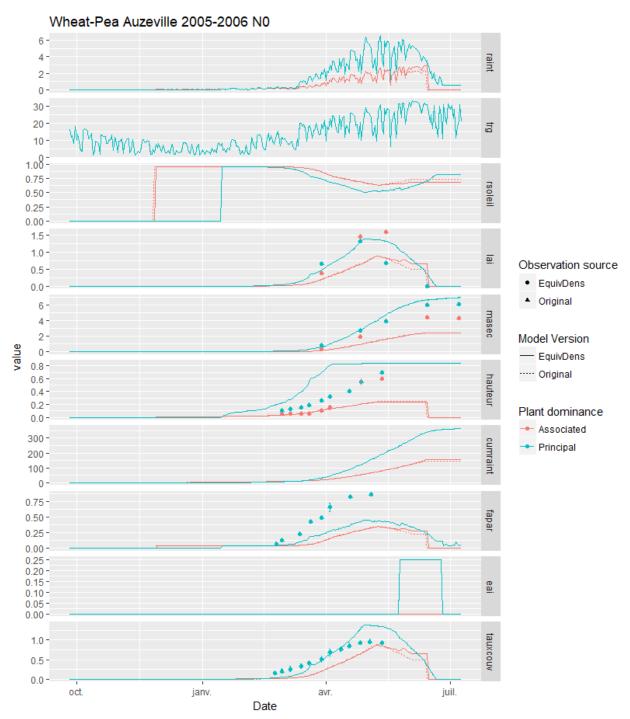




species and 30 for the pea as the associated species:

The new formalism has several implications in the model, notably that the dominated plant is less impacted by the competition with the dominant plant when both have approximately the same height.

A comparison of the two formalisms was made using the sticRs package, from which a summary plot was ex-



tracted:

The results showed that the new equivalent density computation is less severe for the dominated plant compared to the previous formalism. Consequently, the dominated plant intercepts more light (see cumraint and fapar) and has a higher LAI.

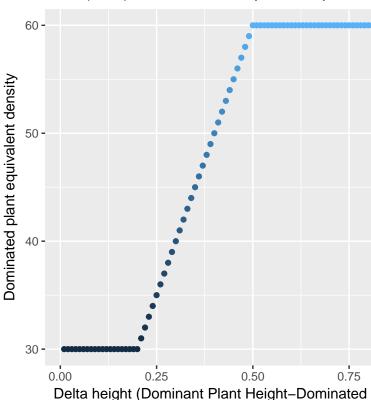
Now the next step is to parameterize well the parameters for the wheat and the pea.

## 5.4 Proposition for a newer equivalent density

E.Justes, proposed a new (third) equivalent density computation that would have no increase in equivalent density until a given threshold (hauteur\_threshold\_1), after which a progressive increase in the equivalent density would happen until the maximum allowed. in this computation, the slope would be computed by the model, and the resulting equivalent density would be as follows:

$$density_{Equivalent} = \begin{cases} \Delta_{height} < hauteur_{threshold_1} & density_{p2} \\ \Delta_{height} > hauteur_{threshold_1} & b + \Delta_{height} \cdot slope \\ \Delta_{height} > hauteur_{threshold_2} & Max_{equDens} \end{cases}$$
 with 
$$slope = \frac{Max_{equDens}}{hauteur_{threshold_2} - hauteur_{threshold_1}}$$

## New (third) formalism for equivalent plant d



Here is the resulting plot for the same Wheat-Pea intercrop:

This formalism would include three parameters:

- hauteur threshold 1: the difference in height below which no competition is occurring
- hauteur threshold 2: the difference in height below which a progressive competition is occurring
- Max\_equDens: the maximum equivalent density allowed.

# 5.5 Proposition to remove the old explicit interspecies density competition effect

For the moment, the competition induced by the density of the other species was re-included in the equivalent density computation using the P\_bdensp1 and P\_bdensp2 parameters, which come from the sole crop

formalism, where it is used to consider intra-species competition effect.

The equivalent density was originally set up to consider the decrease in light quality when a plant has another plant above it. Adding another computation of competition based on the density of the other plant could be redundant, because it is already considered during the light interception (see 6 and 2).

Consequently, we propose to remove this computation from the equivalent density formalism, and to let the P\_bdensp1 and P\_bdensp2 parameters being used to compute the efdensite variable only.

We now have to test this proposition.

# Interrow spacing

#### 6.1 Introduction

The inter-row is the distance between two rows of the same plant species. It is straightforward for monocrops, but a bit more complicated for intercrops. Indeed, the inter-row parameter can have unexpected adverse effects for intercrops. Here is a simple design with a field with two plant species sowed with the same inter-row:

So far, so good. Now what happens if we set a different inter-row spacing for the two species?

## 6.2 Inter-row spacing for mixed crops in the model

Whereas the model as a notion of the position of the plants along the interrow considering the same plant species (i.e. Principal or Associated), it does not explicitly position the different plant species between each other. Indeed, the light interception of the dominant plant is first computed using its geometry and a plane at the height of the dominated plant. Then, the light interception of the dominated plant is computed using the average light incident on the previous plane (separated between shaded and sunlit component), the plant geometry, and a second plane right above the soil. So when computing its light interception, the dominated plant do not consider at all the dominant plant interrow spacing, but only the light it transmits. Of course the dominant plant interrow spacing does impact the light that is transmitted to the dominated plant, but it is not an explicit description of the interrow spacing.

Here is a depiction of how the model describe the interrow for intercrops:

The model does effectively compute half the interrow light interception only, because it is assumed that the other half have the same light regime at daily time-scale. First the interrow of the dominant plant is used to position the left and right dominant plants. The model then computes the golbal radiation (trg) that is transmitted to the Plane 1, which is then used to compute the light intercepted by the dominant plant. The light transmitted to the Plane 1 is divided into two light regimes: a shaded component (surface right under the dominant plant canopy) and a sunlit component (the opposite).

Second, the light incident on the Plane 1 is used as the trg for the dominated plant, and the same computation than for the dominant plant is performed for the shaded and sunlit components of the dominated plant, and then integrated at species-scale using both light interception and relative surface.

To conclude, we see that the interrow spacing can only impact the light interception as a density effect (more plants per m2, closer intra-species canopy), but not as a pure geometrical effect.

For more details on how the trg is computed, see Chapter 3, and for more details on light interception, see Chapter 2.

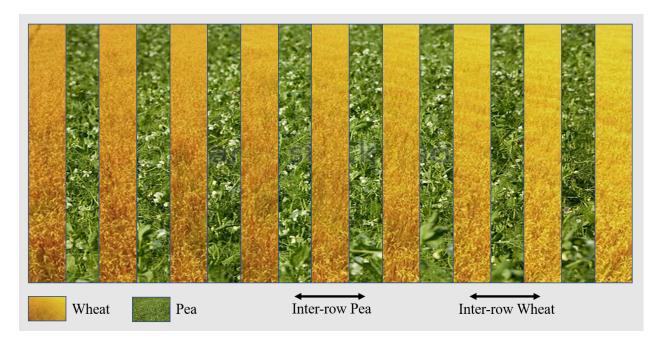


Figure 6.1: Pea-Wheat intercrop using the same inter-row spacing for the two crops

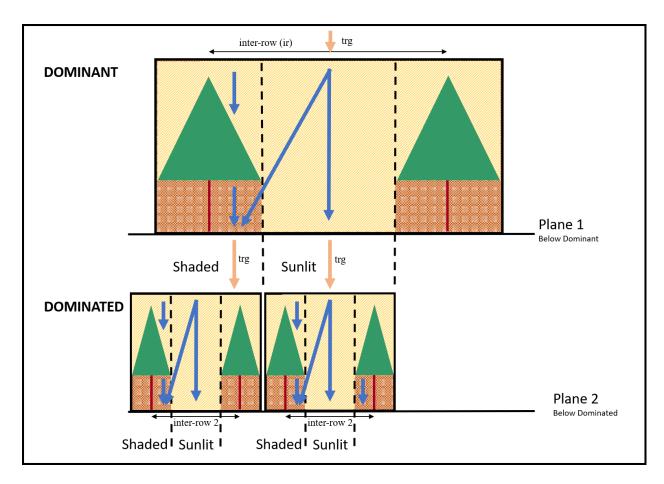


Figure 6.2: Interrow effect on light interception for intercrops in the STICS model