

REVUB: User Manual

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1 The REVUB model (“Renewable Electricity Variability, Upscaling and Balancing”) was developed
2 specifically to address the challenge of optimising hydro-solar-wind complementarity through smart
3 hydropower operation and smart choice of solar-wind portfolios. We first explain the general principles
4 of the REVUB model (Note 1), based on which the different modules of the model are explained one
5 by one: hydropower plant classification (Note 2); simulation of hydropower generation and reservoir
6 dynamics (Note 3); and simulation and optimisation of joint hydro-solar-wind operation (Note 3 -
7 Note 5). An optional, additional assessment of pumped-storage potential with REVUB is described
8 in Note 6. Some notes on spinning reserve requirements are summarised in Note 7. An overview table
9 of terms and symbols used in the model description is given in Note 8. The REVUB code exists for
10 Python and MATLAB environments and can be accessed via <https://github.com/VUB-HYDR/REVUB>
11 and used under the MIT license. All equations given in this document are referenced in the code
12 wherever relevant/used. The ways to prepare input, run the code, and interpret output are given
13 in Note 9, Note 10 and Note 11. Examples of REVUB use in literature are enumerated in Note 12.

14 **Note 1 Principles of REVUB**

15 The basic idea of REVUB is to assess the potential of reservoir hydropower to assist in the grid inte-
16 gration of variable power generation, e.g. from solar PV and wind power. Since reservoir hydropower
17 can be flexibly dispatched, the premise is that every hydropower plant can help compensate for part
18 of the variability of the pooled solar/wind resources on the same grid^{1,2}. This requires adaptations,
19 down to hourly resolution, of the conventional reservoir rule curves applied to keep reservoir water
20 levels within acceptable ranges on seasonal and multiannual time scales.

21 REVUB calculates the adapted rule curves required for balancing a given solar/wind mix, and opti-
22 mises the amount of solar/wind power whose variability each hydropower plant can compensate, based
23 on three criteria: (i) reservoir lake levels must remain stable under the new rule curves, comparably
24 to conventional reservoir operation, on seasonal and multiannual time scales; (ii) the resulting hydro-
25 solar-wind power mix must be reliable, i.e. capable of consistently meeting a certain load from hour
26 to hour, month to month and year to year without failure (unless, in rare cases, extreme droughts
27 force hydropower curtailment); and (iii) downstream environmental flow constraints are never to be
28 violated. An overview of the calculation steps performed by REVUB is given in Fig. S1. The steps
29 outlined in this chart are described in more detail in the next sections, as indicated.

30 **Note 2 Hydropower plant categorisation**

31 In REVUB, hydropower plants are categorised into two groups, based on whether the average natural
32 inflow would take more or less than one year to fill the reservoir; in other words, whether the reservoir
33 is “large” or “small” compared to the inflow. For plants in the “large” category, rule curves can be
34 designed to ensure outflow and power output are relatively stable from month to month^{3,4}, enabling
35 the plant to serve as baseload provider. Such rule curves typically boil down to parameterisations of
36 required outflow as a function of lake level⁵. For hydropower plants in the “small” category, rule curves
37 should additionally take into account that during the wet season(s), certain fractions of the received
38 water need to be directly released from the reservoir without being stored, as reservoir capacity would
39 be insufficient for this⁶. Small hydropower plants thus operate partly as run-of-river plants.
40 In mathematical terms, the classification of hydropower plants as “large” or “small” is done by calcu-
41 lating the dimensionless filling time τ_{fill} :

$$\tau_{fill} = \frac{V_{max}/T_{year}}{Q_{in,nat}(t)}, \quad (S1)$$

42 where V_{max} is the reservoir volume (in m³), T_{year} is the number of seconds in a year, and $Q_{in,nat}(t)$
43 denotes natural reservoir inflow (in m³/s). By default, hydropower plants are classified by REVUB
44 as large or small based on whether their τ_{fill} is larger or smaller than unity, respectively; but this can
45 be changed by the user.



Figure S1: **Flowchart of the REVUB model approach**, explaining the steps taken in modelling hydro, solar and wind power and their integration. ELCC = Effective Load Carrying Capability. See also Note 9, Note 10 and Note 11 for the ways to prepare input, run the code, and interpret output.

Regardless of whether a plant is classified as large or small, it could be operated according to alternative rule curves with similar seasonal to multiannual outcomes as those resulting from conventional operation, but with additional patterns in water release from sub-daily to seasonal timescales, designed for balancing supply with demand in a power mix with a high share of variable renewable electricity (RE). This would mean allocating a portion of the inflowing water for flexible use and releasing it to generate extra power whenever needed to meet a certain load, such as during evening and night hours when solar PV output is low or zero.

Even for large hydropower plants, only part of the water intake can be allocated for flexible use, as a minimum stable outflow usually has to be guaranteed for at least two reasons: (i) safeguarding power system stability, since requirements for inertia impose having some synchronous capacity, such as from hydroturbine-driven generators, dispatched at all times⁷; and (ii) safeguarding downstream ecological integrity⁸. Thus, reservoir outflow must have a stable and a flexible component, which are denoted respectively $Q_{stable}(t)$ and $Q_{flexible}(t)$ (both in m^3/s). Overall flexibility can be increased by reducing $Q_{stable}(t)$ in favour of $Q_{flexible}(t)$. Essentially, to allocate a certain amount of water for flexible use, the stable outflow will have to be reduced by a comparable amount such that the overall water budget remains unchanged.

Total reservoir outflow may have two other components: a seasonal (“run-of-river”) component, denoted $Q_{RoR}(t)$, for small hydropower plants; and an overflow-prevention component⁵ $Q_{spill}(t)$, representing the release of water via spillways when filling levels approach critical values, e.g. during extremely wet periods. Thus, total reservoir outflow $Q_{out}(t)$ is, in general, given by

$$Q_{out}(t) = Q_{stable}(t) + Q_{flexible}(t) + Q_{RoR}(t) + Q_{spill}(t), \quad (S2)$$

for both large and small hydropower plants. Correspondingly, hydropower generation consists of components $P_{stable}^{hydro}(t)$, $P_{flexible}^{hydro}(t)$ and $P_{RoR}^{hydro}(t)$ (in MW)ⁱ.

ⁱIt is assumed that overflow prevention releases are never used for power generation, to avoid damaging turbine equipment and because such high flows would normally exceed turbine capacity anyway.

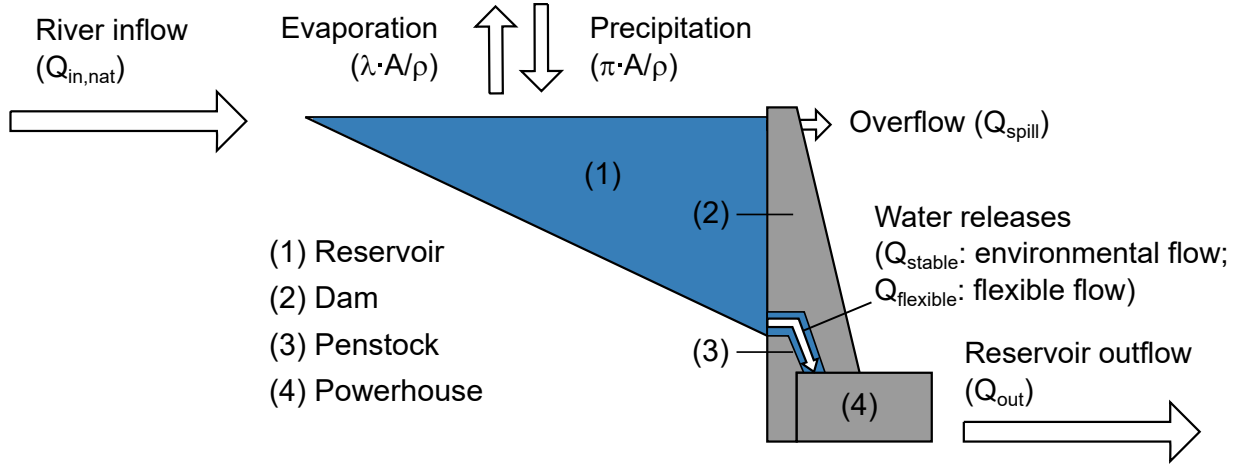


Figure S2: **Flowchart of the water gains and losses of a large hydropower plant as modelled in REVUB.** Gains consist of river discharge and lake surface precipitation; losses consist of reservoir outflows and lake surface evaporation.

In the next sections, the simulations in REVUB of flexibility provision by large and small hydropower plants are discussed in detail. Note 3 and Note 4 deal with large plants; Note 5 with small plants.

Note 3 Reservoir simulation for large hydropower plants

The volume of water $V(t)$ contained in a large hydropower plant's reservoir is given by the recursive relation

$$V(t + \Delta t) = V(t) + \left[Q_{in,nat}(t) - Q_{stable}(t) - Q_{flexible}(t) - Q_{spill}(t) + [\pi(t) - \lambda(t)] \frac{A(t)}{\rho} \right] \Delta t, \quad (S3)$$

where $\pi(t)$ and $\lambda(t)$ are respectively precipitation and evaporation flux ($\text{kg}/\text{m}^2/\text{s}$; see Methods); $A(t)$ is the surface area of the reservoir lake (m^2); ρ the density of water (taken to be $1000 \text{ kg}/\text{m}^3$); and Δt is the simulation time step (one hour is the default in REVUB). Seepage losses, which are usually very small in reservoirs^{6,9}, are neglected in the REVUB code (but could be included e.g. via a correction factor to total inflow). A schematic diagram of the involved water fluxes is given in Fig. S2.

Note 3.1 explains how $Q_{stable}(t)$ and the corresponding power generation $P_{stable}^{hydro}(t)$ are modelled for conventional, baseload-oriented operation, in which the flexible components are zero. Simulating conventional operation is necessary to have a reference time series of long-term lake volume fluctuations, based on which the balancing-oriented operation can be calibrated. Subsequently, Note 3.2 explains how $Q_{stable}(t)$ and $Q_{flexible}(t)$, and the corresponding power generation components $P_{stable}^{hydro}(t)$ and $P_{flexible}^{hydro}(t)$, are modelled for balancing-oriented operation.

Note 3.1 Conventional (baseload-oriented) operation

We denote conventional, baseload-oriented operational rules with the abbreviation "CONV". By definition, $Q_{flexible,CONV}(t)$ and $P_{flexible,CONV}^{hydro}(t)$ are zero. The default way of modelling $Q_{stable,CONV}(t)$ in REVUB is based on logarithmic-exponential release rules^{4,10}, which works well in case conventional operational rules are unknown, and can be determined on the basis of long-term average inflow:

$$Q_{stable,CONV}(t) = \left\{ \begin{array}{ll} \frac{\overline{Q_{in,nat}(t)}}{\left[d_{min} + \ln \left(\kappa \left[\frac{V_{CONV}(t)}{V_{max}} \right]^\phi + 1 \right) \right]}, & \text{for } V_{CONV}(t)/V_{max} < f_{opt} \\ \frac{\overline{Q_{in,nat}(t)}}{\left[\exp \left(\gamma \left[\frac{V_{CONV}(t)}{V_{max}} - f_{opt} \right]^2 \right) \right]}, & \text{for } V_{CONV}(t)/V_{max} \geq f_{opt} \end{array} \right\}, \quad (S4)$$

where d_{min} is the fraction of yearly average inflow required as minimum stable outflow; V_{max} is the maximum reservoir storage capacity; f_{opt} is the optimal filling fraction; and κ , ϕ and γ are constants.

91 κ and ϕ are given⁴ by

$$\kappa = f_{opt}^{-\phi} [\exp(1 - d_{min}) - 1], \quad (S5)$$

92 and

$$\phi = \alpha \tau_{fill}^{1/2}. \quad (S6)$$

93 Recommended default values are $f_{opt} = 80\%$, $\alpha = 2/3$, and $\gamma = 10$ based on generalised reservoir
 94 operation rules^{4,10}; for d_{min} , values may be chosen based on generalised environmental flow rules⁸
 95 and/or requirements for minimum turbinised flow to prevent turbines running at low efficiency.
 96 The overflow prevention component $Q_{spill,CONV}$ is modelled as

$$Q_{spill,CONV}(t) = \begin{cases} 0, & \text{for } V_{CONV}(t)/V_{max} < f_{spill} \\ \max \left[0, \left(Q_{in,nat}(t) + [\pi(t) - \lambda(t)] \frac{A_{CONV}(t)}{\rho} \right) (1 + \mu) - Q_{stable,CONV}(t) \right], & \text{for } V_{CONV}(t)/V_{max} \geq f_{spill} \end{cases}, \quad (S7)$$

97 where f_{spill} is the filling fraction at which the overflow prevention startsⁱⁱ, and μ represents a small
 98 fraction such that lake levels are brought below critical levels $f_{spill}V_{max}$ as quickly as possible without
 99 releasing unnaturally high flows downstream; default values are $f_{spill} = 95\%$ and $\mu = 0.1$, but these
 100 can be changed by the user.

101 To simulate minimum drawdown levels when facing drought-like situations, one further rule is added
 102 to equation (S4): outflow, and with it hydropower production, is automatically curtailed^{5,11} if the
 103 volume levels $V_{CONV}(t)$ dip below critical levels $f_{stop}V_{max}$, and only restarted once volumes have
 104 recovered to $f_{restart}V_{max}$. The values $f_{stop} = 10\%$ ¹¹ and $f_{restart} = 20\%$ are defaults in REVUB, but
 105 can be changed by the user.

106 The corresponding stable power output $P_{stable,CONV}^{hydro}(t)$ can then be calculated as

$$P_{stable,CONV}^{hydro}(t) = \min \left[Q_{stable,CONV}(t); Q_{turb}^{max} \right] \eta_{turb} \rho g h_{CONV}(t), \quad (S8)$$

107 where η_{turb} is the turbine efficiency (%), g the gravitational acceleration (9.81 m/s²), and $h(t)$ the
 108 hydraulic head (m), i.e. the difference in water level between the headwater behind the dam and the
 109 tailwater at the turbines. The efficiency of η_{turb} should be user-definedⁱⁱⁱ. The calculation of $h(t)$ is
 110 explained in Note 3.3. Q_{turb}^{max} is the maximum turbine throughput (at which the power generating
 111 capacity of the turbine is fully used), which is approximated with $Q_{turb}^{max} \approx P_{turb}^r / (\eta_{turb} \rho g h_{max})$, where
 112 P_{turb}^r is the rated power capacity of the hydropower plant and h_{max} is the maximum hydraulic head.
 113 With these rules, results are mostly independent of arbitrary initial conditions (convergence to the same
 114 time series happens typically within 2 simulation months). The initial condition $V_{CONV}(0) = f_{opt}V_{max}$
 115 (and the corresponding lake area and water level; see Note 3.3) are defaults in REVUB, but can be
 116 changed by the user.

117 We note that, in case the user wishes to include their own conventional reservoir rules, this is possible
 118 by correspondingly adapting the default REVUB code by adapting the lines referring to the above
 119 equations.

120 **Note 3.2 Balancing-oriented operation**

121 Reservoir operation oriented towards balancing solar and wind power variability is denoted with the
 122 abbreviation “BAL”. For reservoirs of large hydropower plants, BAL operation is modelled as follows.
 123 First, the needs for sub-daily to seasonal dispatching patterns must be established. The load difference
 124 $P_d(t)$ between total inflexible power generation (stable hydropower, solar power, and wind power) and
 125 power demand is calculated as:

$$\begin{aligned} P_d(t) &= P_{stable,BAL}^{hydro}(t) + c_{solar} \cdot CF_{solar}(t) + c_{wind} \cdot CF_{wind}(t) - L(t) \\ &= P_{inflexible}(t) - L(t). \end{aligned} \quad (S9)$$

ⁱⁱNote that every hydropower plant has a certain safety level, i.e. the dam is always somewhat higher than the maximum water level⁵, to mitigate flood risk. Because of this safety level, should the overflow procedure fail for any reason, the dam would not immediately overflow. However, flooding would occur along the shores of the lake, which is why it is always prudent to prevent straining the safety level.

ⁱⁱⁱThe efficiency of hydroturbines depends on the effective turbinised flow at each moment, but is typically above 80% in realistic ranges of the latter^{12,13}; the value d_{min} can be chosen such as to reflect the fact that turbines should not run at too low partial loads, at which their efficiencies can drop considerably.

Here, c_{solar} and c_{wind} represent a certain amount of solar PV and wind power capacity, respectively (in MW), whose value is to be optimised by REVUB; $CF_{solar}(t)$ and $CF_{wind}(t)$ represent the solar and wind capacity factor for each time step, respectively; and $L(t)$ represents a certain target load profile that is to be followed^{iv}. The time series $L(t)$, by default, is set as follows:

$$L(t) = P_{load} L_{norm}(t), \quad (S10)$$

with P_{load} a constant determining the average load to be followed and reflecting the constraints on overproduction, and $L_{norm}(t)$ the normalized ($\overline{L_{norm}(t)} = 1$) hour-to-hour load profile. P_{load} is calculated as

$$P_{load} = p_i(P_{inflexible}(t)), \quad (S11)$$

where $p_i(x)$ denotes the i^{th} percentile of a variable x . Here, i thus represents the percentile of $P_{inflexible}$ not exceeding P_{load} ; in other words, the percentage of time during which RE generation should not exceed the average load to be followed. Generally, the lower i , the higher the amount of allowed excess production (overproduction) as compared to $L(t)$.

In REVUB, the time series $CF_{solar}(t)$ and $CF_{wind}(t)$ must be provided as model input by the user. These could represent power generation from single locations, or weighted averages across the locations for on-grid solar or wind power selected for the region under scrutiny, to simulate the feed-in of solar and wind power from various locations into the same power grid. In case of the latter, we recommend assuming that the total capacity is distributed across locations within the region according to site-specific weight factors w_{solar}^n and w_{wind}^n . Then, $CF_{solar}(t)$ and $CF_{wind}(t)$ would be given by

$$CF_{solar}(t) = \frac{\sum_{n=1}^{N_{solar}} CF_{solar}^n(t) w_{solar}^n}{\sum_{n=1}^{N_{solar}} w_{solar}^n}; \quad CF_{wind}(t) = \frac{\sum_{n=1}^{N_{wind}} CF_{wind}^n(t) w_{wind}^n}{\sum_{n=1}^{N_{wind}} w_{wind}^n}, \quad (S12)$$

with $CF_{solar}^n(t)$ and $CF_{wind}^n(t)$ the capacity factors of solar PV or wind power for each time step, respectively, at each individual site with index n ; and N_{solar} and N_{wind} the number of sites for solar PV or wind power generation, respectively. The weight factors w_{solar}^n and w_{wind}^n represent preferences for certain sites over others for the development of solar PV and wind parks. Given that sites with a higher yield would typically tend to be preferred, a simple approach would be to take a site's weight factor to be equal to the multi-year average capacity factor for solar PV or wind power at that site:

$$w_{solar}^n = \overline{CF_{solar}^n(t)}; \quad w_{wind}^n = \overline{CF_{wind}^n(t)}. \quad (S13)$$

The capacity ratio $c_{solar} : c_{wind}$ should also be user-defined; it represents the relative share of solar and wind capacity to be deployed by the model. Sensitivity tests to find an optimal ratio can then be performed by running the model for several values of the capacity ratio.

Second, in BAL operation, $Q_{stable}(t)$ is reduced in favour of $Q_{flexible}(t)$ such that $L(t)$ can be met by the combination of stable hydropower, flexible hydropower, solar power and wind power. In the REVUB code, the default approach (which can be adapted by the user) is to take $Q_{stable,BAL}(t)$ as a fraction of the average inflow:

$$Q_{stable,BAL}(t) = (1 - C_{OR}) \overline{Q_{in,nat}(t)}. \quad (S14)$$

Here, the fraction C_{OR} denotes the ‘‘operating reserve coefficient’’¹⁴, and determines the amount of water available for flexible use. Theoretically, as $C_{OR} \rightarrow 1$, the hydropower plant in question would operate near-completely flexibly and provide almost no minimum stable load. This would also imply that the outflow of the dam could become zero for prolonged periods; for instance, when solar/wind power generation is high and/or demand is low. Such operation would violate (i) inertia requirements and minimum load constraints of the plant, and (ii) environmental flow requirements. As default, REVUB therefore uses an upper bound of $C_{OR}^{max} = 1 - d_{min} = 60\%$, such that the minimum

^{iv}Note that for the terms in equation (S9), MW and MWh are interchangeable units, due to the hourly time step employed in REVUB. Similarly, CF could be interpreted both as actual power generation divided by maximum potential generation in each hour (dimensionless fraction), or as power generation per unit of capacity (in hours).

164 outflow under BAL is always consistent with that under CONV. The selection of the optimal C_{OR} for
 165 each hydropower plant is explained in Note 4.
 166 $P_{stable,BAL}^{hydro}(t)$ is calculated analogously to $P_{stable,CONV}^{hydro}(t)$ in equation (S8):

$$P_{stable,BAL}^{hydro}(t) = \min \left[Q_{stable,BAL}(t); Q_{turb}^{max} \right] \eta_{turb} \rho g h_{BAL}(t). \quad (S15)$$

167 Third, the necessary amount of flexible outflow $Q_{flexible,BAL}(t)$ and corresponding flexibly produced
 168 power $P_{flexible,BAL}^{hydro}(t)$ are determined for the instances when $P_{inflexible}(t)$ cannot meet $L(t)$, i.e. when
 169 $P_d(t) < 0$. The following rule then applies for $P_{flexible,BAL}^{hydro}(t)$ to maximize the followed load under
 170 peak capacity constraints and ramping constraints¹⁵:

$$P_{flexible,BAL}^{hydro}(t) = \begin{cases} 0, & \text{for } P_d(t) \geq 0 \\ \min \left[Q_{turb,pot}^{flexible}(t) \eta_{turb} \rho g h_{BAL}(t); \min \left[|P_d(t)|; P_{flexible,BAL}^{hydro}(t-1) + \Delta P_{turb}^{ramp} \right] \right], & \text{for } P_d(t) < 0 \text{ \& } \Delta P_d(t) < 0 \\ \min \left[Q_{turb,pot}^{flexible}(t) \eta_{turb} \rho g h_{BAL}(t); \max \left[|P_d(t)|; P_{flexible,BAL}^{hydro}(t-1) - \Delta P_{turb}^{ramp} \right] \right], & \text{for } P_d(t) < 0 \text{ \& } \Delta P_d(t) \geq 0 \end{cases}, \quad (S16)$$

171 where $\Delta P_d(t) = P_d(t) - P_d(t-1)$ determines whether the hydropower plant should ramp up ($\Delta P_d(t) <$
 172 0) or down ($\Delta P_d(t) \geq 0$); ΔP_{turb}^{ramp} is the maximum ramp rate of the plant (in MW per time step);
 173 and

$$Q_{turb,pot}^{flexible}(t) = \max \left[0; Q_{turb}^{max} - Q_{stable,BAL}(t) \right]. \quad (S17)$$

174 This gives a flexible outflow

$$Q_{flexible,BAL}(t) = \frac{P_{flexible,BAL}^{hydro}(t)}{\eta_{turb} \rho g h_{BAL}(t)}. \quad (S18)$$

175 Fourth, the overflow prevention component $Q_{spill,BAL}(t)$ is calculated analogously to equation (S7):

$$Q_{spill,BAL}(t) = \begin{cases} 0, & \text{for } V_{BAL}(t)/V_{max} < f_{spill} \\ \max \left[0, \left(Q_{in,nat}(t) + [\pi(t) - \lambda(t)] \frac{A_{BAL}(t)}{\rho} \right) (1 + \mu) - Q_{stable,BAL}(t) - Q_{flexible,BAL}(t) \right], & \text{for } V_{BAL}(t)/V_{max} \geq f_{spill} \end{cases}. \quad (S19)$$

176 As in CONV, to ensure that lake levels do not dip precariously low, $Q_{stable,BAL}$ and $Q_{flexible,BAL}$ are
 177 reduced to zero when $V_{BAL}(t) < f_{stop} V_{max}$ and restarted once $V_{BAL}(t) \geq f_{restart} V_{max}$.

178 Since one needs the hydraulic head $h_{BAL}(t)$ to calculate $P_{stable,BAL}^{hydro}(t)$ from equation (S15), but $h_{BAL}(t)$
 179 follows only from the overall operation, which requires knowledge of $P_{stable,BAL}^{hydro}(t)$ to calculate $P_d(t)$
 180 according to equation (S9), this problem is solved iteratively by REVUB with an initial guess of
 181 $P_{stable,BAL}^{hydro}(t) = (1 - C_{OR}) P_{stable,CONV}^{hydro}(t)$, repeated until convergence (typically, 3-6 iterations suffice).
 182 The calculation of $h(t)$ is the same as for CONV and is explained in Note 3.3.

183 At given C_{OR} and given ratio $c_{solar} : c_{wind}$, REVUB optimises the above operation by identifying the
 184 time series $L(t) = L_{opt}(t)$, and the corresponding optimal $c_{solar} = c_{solar}^{opt}$ and $c_{wind} = c_{wind}^{opt}$, for which
 185 the resulting lake level time series is most comparable to what it would be under CONV operation.
 186 This optimisation is performed by finding the minimum of the relative deviation Ψ between the CONV
 187 and BAL lake levels across all time steps of an entire simulation period, as a function of c_{solar} and c_{wind} :

$$\Psi(c_{solar}, c_{wind}) = \frac{|(V_{BAL}(t) - V_{CONV}(t))|}{V_{CONV}(t)}, \quad (S20)$$

188 where

$$\min(\Psi) = \Psi(c_{solar}^{opt}, c_{wind}^{opt}). \quad (S21)$$

189 Note that the code could also be adapted to optimise lake levels compared to a certain mathematical
 190 rule curve, instead of to the outcome of “conventional” operational rules (Note 3.1). This would
 191 simply require exchanging $V_{CONV}(t)$ in equation (S20) by the corresponding rule curve of lake volume.
 192 Note furthermore that even when doing this, it is still useful to calculate the outcomes (hydropower
 193 generation and lake levels) resulting from conventional reservoir management, to verify (i) how well the
 194 rule curve can be followed *in general* under the given hydroclimate and occurrence of wet/dry years,
 195 and (ii) the extent to which the outcomes of flexible operation would differ from baseload-oriented
 196 operation.

197 REVUB assures that power droughts resulting from $V(t)$ dipping lower than $f_{stop} V_{max}$ can never be
 198 more severe under BAL operation than under CONV, by automatically discarding any solutions to
 199 equation (S21) where this would be the case.

Once the optimal solution is found, the Effective Load Carrying Capability (ELCC) of the hydro-solar-wind mix is calculated as follows. The maximum followable load $L_{followed}(t) = P_{followed}L_{norm}(t)$, which the hydro-solar-wind mix can meet without any load loss, is identified: this is the load at which the residual load ($L_{res}(t)$; the load minus the generation) has a maximum of zero. Thus, $P_{followed}$ is the value for which $\max[L_{res}(t)] = 0$, with $L_{res}(t)$ defined as:

$$L_{res}(t) = P_{followed}L_{norm}(t) - \left[P_{stable,BAL}^{hydro}(t) + P_{flexible,BAL}^{hydro}(t) + c_{solar}^{opt} \cdot CF_{solar}(t) + c_{wind}^{opt} \cdot CF_{wind}(t) \right]. \quad (S22)$$

The ELCC is then defined as the integral of $L_{followed}(t)$ over all time steps in a simulation year:

$$ELCC = \int_{year} L_{followed}(t) dt. \quad (S23)$$

The ELCC thus represents the total yearly load followed by each hydropower plant in combination with the solar and wind power whose variability it can compensate, under the optimal solution. The aggregate of ELCC across all hydropower plants represents the total followable load when all hydropower plants optimally contribute to compensating solar-wind variability; it is abbreviated $ELCC_{tot}$ hereafter.

Ideally, $L_{followed}(t)$ should be equal to $L_{opt}(t)$ (and it usually is), but due to peaking constraints of hydropower plants (eq. (S17)), this is not guaranteed in every case. When $L_{followed}(t) < L_{opt}(t)$, the power plant's peaking capabilities are insufficient to meet all required peaks in $L_{opt}(t)$ together with solar and wind power. In such cases, the hydropower plant should run at somewhat lower flexibility, i.e. lower C_{OR} , at which a lower $L_{opt}(t)$ will apply that would put less strain on the plant's peaking capabilities, ensuring that $L_{followed}(t) \approx L_{opt}(t)$. This resimulation is done automatically by the REVUB code (Note 4).

The total contributions of hydro, solar and wind power to yearly electricity generation, denoted respectively $E_{reservoir}^{hydro}$, E_{solar} and E_{wind} , are obtained by integrating their respective power output across all time steps in a simulation year. First, $E_{reservoir}^{hydro}$ is equal to

$$E_{reservoir}^{hydro} = E_{stable}^{hydro} + E_{flexible}^{hydro} = \int_{year} (P_{stable}^{hydro}(t) + P_{flexible}^{hydro}(t)) dt. \quad (S24)$$

Second, E_{solar} and E_{wind} are obtained by multiplying c_{solar}^{opt} and c_{wind}^{opt} by $CF_{solar}(t)$ and $CF_{wind}(t)$, respectively, and integrating:

$$\begin{aligned} E_{solar} + E_{wind} &= \int_{year} (P_{solar}(t) + P_{wind}(t)) dt \\ &= \int_{year} (c_{solar}^{opt} \cdot CF_{solar}(t) + c_{wind}^{opt} \cdot CF_{wind}(t)) dt. \end{aligned} \quad (S25)$$

Note 3.3 Head-volume-area relationships

Calculating the hydraulic head $h(t)$ for each time step requires knowing the bathymetry and volume-area-depth relationship of each reservoir. Typical curves approximating such relationships need to be calibrated on a reservoir-to-reservoir basis. The user should provide bathymetric curves as input to each simulation. In case these are not available, we recommend using an archetypal reservoir shape function^{16,17}, modelling reservoirs' area-volume relationships with the equation

$$A(t) = A_{max} \left[\frac{V(t)}{V_{max}} \right]^{(1 - C_{reservoir})}, \quad (S26)$$

where $C_{reservoir} = V_{max}/(A_{max}z_{max})$ is the "reservoir coefficient", and A_{max} and z_{max} represent the maximum reservoir lake area and depth, respectively.

For any $V(t + \Delta t)$ calculated using equation (S3), the corresponding $A(t + \Delta t)$ can then be calculated using equation (S26). To obtain the hydraulic head $h(t + \Delta t)$ at each time step, the incremental change $\Delta h(t)$ is added to the head $h(t)$ of the previous time step, using the first-order approximation

$$\Delta h(t) \approx \frac{V(t+1) - V(t)}{A(t)}. \quad (S27)$$

When using equation (S26), before any simulation according to CONV or BAL in REVUB, a dummy simulation spanning all possible values of V , and thus of A and h , should be run to obtain a calibration (h, V) curve. In CONV and BAL simulations, the head $h(t + \Delta t)$ can then always be obtained from this calibration curve after $V(t + \Delta t)$ has been determined from equation (S3).

Note 4 Peaking suitability of large hydropower plants

Since hydropower plants differ in terms of peaking capabilities, operational strategies must be selected with care. If hydropower plants are operated at a too high C_{OR} , the corresponding peaks in flexible water release may exceed the maximum turbine throughput on a structural basis (cf. equation (S17)), meaning that the plant will be structurally unable to meet peak demand as well as leading to loss of spinning reserves (see Note 7). Typically, this would first occur in the seasons with highest peak demand and/or when water levels are at their lowest. Therefore, each hydropower plant's operation should happen at an optimised value $C_{OR} = C_{OR}^{opt}$ that ensures this is not the case, while maintaining adequate levels of flexibility. In REVUB, the default procedure (which can be changed by the user) is to define the turbine utilisation rate $k_{turb}(t)$ at each time step:

$$k_{turb}(t) = \frac{Q_{stable}(t) + Q_{flexible}(t)}{Q_{turb}^{max}}, \quad (S28)$$

and define hydropower plant operation (at given C_{OR}) as unsuitable for peaking purposes when $p_{99}(k_{turb})$, i.e. the 99th percentile of k_{turb} , is unity (in other words, when turbine capacity is fully exhausted in at least one out of every 100 hours).

As default for each hydropower plant, REVUB uses $C_{OR}^{opt} = C_{OR}^{max}$, the maximum allowed operational flexibility. If operation is found to be unsuitable for peaking purposes at C_{OR}^{max} , the REVUB code automatically resimulates with incrementally reduced C_{OR} , until a value C_{OR}^{opt} is identified for which $p_{99}(k_{turb}) < 1$.

Note 5 Reservoir simulation for small hydropower plants

To assess the balancing potential of small hydropower plants, we define the alternative filling time $\tau_{fill,frac}$ corresponding to the amount of years it would take for a fixed fraction of the incoming flow, denoted $Q_{in,frac}(t)$, to fill the reservoir:

$$\tau_{fill,frac} = \frac{V_{max}/T_{year}}{Q_{in,frac}(t)}, \quad (S29)$$

where $Q_{in,frac}(t)$ is defined as

$$Q_{in,frac}(t) = f_{reg} Q_{in,nat}(t), \quad (S30)$$

with f_{reg} a suitable fraction, determined for each reservoir by solving $\tau_{fill,frac} = 1$; that is, f_{reg} represents the fraction of the incoming water that would take one year to fill the reservoir on average. The fraction $Q_{in,frac}(t)$ is then assumed to be “storable” and usable for balancing. REVUB assumes that the remainder of the flow, given by $Q_{in,nat}(t) - Q_{in,frac}(t) = (1 - f_{reg})Q_{in,nat}(t)$, passes through the reservoir without being stored, thus representing the seasonal “run-of-river” component $Q_{RoR}(t)$. Since f_{reg} can be calculated based on long-term average flow, such operation can be readily implemented as long as accurate measurements of inflow are available.

The term Q_{RoR} is appended in equation (S3) (and would be an additional entry under the “water releases” arrows in Fig. S2):

$$\begin{aligned} V(t + \Delta t) &= V(t) + \left[Q_{in,nat}(t) - Q_{RoR}(t) - Q_{stable}(t) - Q_{flexible}(t) - Q_{spill}(t) + [\pi(t) - \lambda(t)] \frac{A(t)}{\rho} \right] \Delta t \\ &= V(t) + \left[Q_{in,frac}(t) - Q_{stable}(t) - Q_{flexible}(t) - Q_{spill}(t) + [\pi(t) - \lambda(t)] \frac{A(t)}{\rho} \right] \Delta t, \end{aligned} \quad (S31)$$

and the corresponding seasonal power generation is then equal to

$$P_{RoR}^{hydro}(t) = \min \left[Q_{RoR}(t); \max \left[0; Q_{turb}^{max} - Q_{stable}(t) - Q_{flexible}(t) \right] \right] \eta_{turb} \rho g h(t). \quad (S32)$$

Electricity generation from the hydropower component, denoted E_{RoR}^{hydro} , is then equal to

$$E_{RoR}^{hydro} = \int_{year} P_{RoR}^{hydro}(t) dt. \quad (S33)$$

Dispatching such as described for large hydropower plants in the previous sections is done similarly for small hydropower plants, with the following adaptations: (i) the component $Q_{in,frac}(t)$ is used as reference flow instead of $Q_{in,nat}(t)$ in equation (S4); (ii) the rule is added that, as soon as reservoir levels drop precariously low (in this case, below $f_{restart}V_{max}$), the seasonal outflow (if nonzero) is temporarily stopped and the operation reverts to that of large hydropower plants, using the full inflow to stabilise water levels; and (iii) the seasonal power generation $P_{RoR}^{hydro}(t)$ is not included in equation (S9) as it is not expected to take part in the hour-to-hour load-following. Note, however, that if river discharge would be regulated by other reservoirs upstream in a cascade-like configuration, even $P_{RoR}^{hydro}(t)$ could become relatively stable throughout the year.

Note 6 Optional pumped-storage assessment

The REVUB code can also be used to assess the potential for increasing load-following potential by refurbishing large hydropower plants to pumped-storage schemes¹⁵, such that excess production (typically of solar PV during mid-day) can be used to pump water back up into the reservoir, enabling the energy to be stored for use at a later stage. This would involve (i) building a downstream reservoir with volume $V_{lower,max} \ll V_{max}$ to store part of the released water, from which it can be pumped back up into the reservoir, and (ii) ensuring the turbines can be operated in reverse mode and/or pumps are installed.

The hydrological balance components then change as follows. First, since environmental flow constraints still have to be met, only the component $Q_{flexible}(t)$ can be used for filling the lower reservoir while the component $Q_{stable}(t)$ has to be directly discharged downstream. The water balance of the lower reservoir is then given by

$$V_{lower}(t + \Delta t) = V_{lower}(t) + [Q_{flexible}(t) - Q_{pump}(t) - Q_{spill,lower}(t)] \Delta t, \quad (S34)$$

where $Q_{pump}(t)$ is the water pumped back up to the large reservoir for storage, and $Q_{spill,lower}(t)$ is the overflow component of the lower reservoir. The precipitation and evaporation terms are neglected here as the lower reservoir is assumed to have a much smaller surface area than the upper reservoir. The water balance of the large reservoir is then given (cf. equation (S3)) by

$$V(t + \Delta t) = V(t) + \left[Q_{in,nat}(t) - Q_{stable}(t) - Q_{flexible}(t) + Q_{pump}(t) - Q_{spill}(t) + [\pi(t) - \lambda(t)] \frac{A(t)}{\rho} \right] \Delta t, \quad (S35)$$

and the net outflow of the pumped-storage plant is given (cf. equation (S2)) by

$$Q_{out}(t) = Q_{stable}(t) + Q_{spill}(t) + Q_{spill,lower}(t). \quad (S36)$$

A schematic of this operation is shown in Fig. S3 (cf. Fig. S2). Note that pumped-storage operation is only useful for large hydropower plants, as small plants have to continuously discharge during large parts of the year to prevent spillage, and pumping water back up would thus not serve a purpose. The component $Q_{pump}(t)$ is calculated as follows. The power stored by pumping is given by

$$P_{pump}(t) = \begin{cases} 0, & \text{for } P_d(t) < 0 \\ \min \left[Q_{pump}^{pot}(t) \eta_{pump}^{-1} \rho g h(t); \min [P_d(t); P_{pump}(t-1) + \Delta P_{pump}^{ramp}] \right], & \text{for } P_d(t) \geq 0 \text{ \& } \Delta P_d(t) \geq 0 \\ \min \left[Q_{pump}^{pot}(t) \eta_{pump}^{-1} \rho g h(t); \max [P_d(t); P_{pump}(t-1) - \Delta P_{pump}^{ramp}] \right], & \text{for } P_d(t) \geq 0 \text{ \& } \Delta P_d(t) < 0 \end{cases}, \quad (S37)$$

where ΔP_{pump}^{ramp} is the maximum ramp rate for pumping, η_{pump} is the pumping efficiency, and

$$Q_{pump}^{pot}(t) = \min \left[\frac{V_{lower}(t)}{\Delta t}; Q_{pump}^{max} \right] \quad (S38)$$

with Q_{pump}^{max} the maximum pump throughput. The flow pumped back into the reservoir then equals

$$Q_{pump}(t) = \frac{P_{pump}(t)}{\eta_{pump}^{-1} \rho g h(t)}. \quad (S39)$$



Figure S3: **Flowchart of the water gains and losses of a large hydropower plant, including pumped storage.** Water gains and losses of a hydropower plant modelled as pumped-storage plant, with an additional lower reservoir and a flow of water in the upstream direction for temporary energy storage.

Finally, the overflow component of the lower reservoir is calculated as

$$Q_{spill,lower}(t) = \begin{cases} 0, & \text{for } (V_{lower,max} - V_{lower}(t)) / \Delta t \geq Q_{flexible}(t) \\ Q_{flexible}(t) - (V_{lower,max} - V_{lower}(t)) / \Delta t, & \text{for } (V_{lower,max} - V_{lower}(t)) / \Delta t < Q_{flexible}(t) \end{cases} \quad (S40)$$

Since the pumping allows a certain fraction of the water to be recycled for power generation, the values c_{solar}^{opt} and c_{wind}^{opt} resulting from the optimisation described in Note 3.2 will end up higher as compared to a situation without pumping component. In this way, pumped storage can help increase the load that can be carried by the hydro-solar-wind combination.

The REVUB code includes an optional section to perform the above operations and the required optimisation (this scenario is named “STOR” in the code, as opposed to “CONV” and “BAL”).

Note 7 Meeting spinning reserve requirements

In electricity networks, a certain reserve capacity, to be utilised in case of disruptions of supply, must always be available. The reserve capacity that is already online is denoted the spinning reserve, of which hydropower plants with reservoirs are typical providers. However, the flexible hydropower operation modeled by REVUB requires hydropower output to be increased during certain intervals to compensate for reductions in solar and/or wind power; thus, the remaining spinning reserves available to manage contingencies will consistently reach minimum values during those times.

The question is thus whether the hydropower plants could still respond to contingency events (e.g. failure of a transmission line leading to a solar power park temporarily being disconnected), despite being operated by flexible rule curves that lead to regular minima in the available spinning reserves. The spinning reserves $P_{spin}(t)$ from all hydropower plants within a certain geography can be calculated as

$$P_{spin}(t) = \sum_{\text{all hydro plants}} [1 - CF_{hydro}(t)] P_{turb}^r \Gamma(t), \quad (S41)$$

where $\Gamma(t)$ equals zero if the hydropower plant has temporarily undergone a drought-related shutdown, and unity otherwise; and $CF_{hydro}(t)$ is the capacity factor of each hydropower plant, calculated as

$$CF_{hydro}(t) = \frac{P_{stable}^{hydro}(t) + P_{flexible}^{hydro}(t) + P_{RoR}^{hydro}(t)}{P_{turb}^r}. \quad (S42)$$

To test the ability of hydropower to respond to supply disruptions of the added solar and wind power, the user should (ex-post) calculate the ratio (denoted ν) of $P_{spin}(t)$ to the total solar and wind power

generation assumed to feed into the same grid. Typical benchmarks of spinning reserve needs for high-RE systems are in the order of $\nu \sim 10 - 20\%$ ¹⁸.

Note 8 Glossary

The table below provides an overview of all described parameters used in the REVUB model and its inputs and outputs. The symbol of each parameter is provided alongside its unit, a description of what it represents in the model, its data type (constant, variable, time series), its use in the model (as input, output, intermediate result, or used for preparing input), and its applicability across various components of the model. Here, “scenario” denotes a certain simulation setting: different scenarios may have different solar/wind mixes, different constraints on overproduction, different pools of hydropower plants contributing to flexibility, etc.

| Symbol | Unit | Description | Type | Used as/for | Applicable to |
|--------------------------|--------------|---|--------------|-------------|---|
| $A(t)$ | m^2 | Reservoir lake surface area | Time series | Output | each hydropower plant & each scenario |
| A_{max} | m^2 | Maximum reservoir lake surface area | Constant | Input | each hydropower plant |
| C_{OR} | - | Operating reserve coefficient: Fraction of yearly reservoir inflow available for flexible use | Variable | - | each hydropower plant |
| C_{OR}^{max} | - | Maximum allowed operating reserve coefficient taking into account environmental flow needs | Constant | Input | general |
| C_{OR}^{opt} | - | Optimal operating reserve coefficient | Constant | Output | each hydropower plant & each scenario |
| c_{solar} | MW | Installed capacity of solar panels | Constant | Output | each hydropower plant & each scenario |
| c_{solar}^{opt} | MW | Optimal installed solar power capacity needed to follow optimal load $L_{opt}(t)$ | Constant | Output | each hydropower plant & each scenario |
| c_{wind} | MW | Installed capacity of wind turbines | Constant | Output | each hydropower plant & each scenario |
| c_{wind}^{opt} | MW | Optimal installed wind power capacity needed to follow optimal load $L_{opt}(t)$ | Constant | Output | each hydropower plant & each scenario |
| $CF_{hydro}(t)$ | - | Capacity factor of hydropower plants | Time series | Output | each hydropower plant & each scenario |
| $CF_{solar}(t)$ | - | Weighted average capacity factor of solar panels across locations | Time series | Input | each scenario |
| $CF_{solar}^n(t)$ | - | Capacity factor of solar panels in each location with index n | Time series | Input | each solar power site |
| $CF_{wind}(t)$ | - | Weighted average capacity factor of wind turbines across locations | Time series | Input | each scenario |
| $CF_{wind}^n(t)$ | - | Capacity factor of wind turbines in each location with index n | Time series | Input | each wind power site |
| d_{min} | - | Percentage of average reservoir inflow required as minimum environmental outflow | Constant | Input | general |
| ΔP_{turb}^{ramp} | MW/min | Maximum ramp rate of hydropower plant | Constant | Input | general |
| ΔP_{pump}^{ramp} | MW/min | When simulating pumped-storage potential: Maximum ramp rate of pumps | Constant | Input | general |
| $E_{reservoir}^{hydro}$ | GWh/year | Total yearly hydropower generation | Yearly total | Output | each hydropower plant & each scenario |
| E_{stable}^{hydro} | GWh/year | Total yearly hydropower generation from stable reservoir outflow component | Yearly total | Output | each hydropower plant & each scenario |
| $E_{flexible}^{hydro}$ | GWh/year | Total yearly hydropower generation from flexible reservoir outflow component | Yearly total | Output | each hydropower plant & each scenario |
| E_{RoR}^{hydro} | GWh/year | Total yearly hydropower generation from seasonal run-of-river outflow component | Yearly total | Output | each small hydropower plant & each scenario |
| E_{solar} | GWh/year | Total yearly solar power generation | Yearly total | Output | each hydropower plant & each scenario |
| E_{wind} | GWh/year | Total yearly wind power generation | Yearly total | Output | each hydropower plant & each scenario |
| ELCC | GWh/year | Effective Load Carrying Capability. Total yearly load followed by hydro-solar-wind without loss of load, ensuring long-term lake level stability, and meeting environmental flow requirements. Integral of $L_{followed}(t)$ over all time steps in a year. | Yearly total | Output | each hydropower plant & each scenario |
| $ELCC_{tot}$ | GWh/year | Aggregate of ELCC across all power plants. Also called “total load-following potential” of hydro-solar-wind. | Yearly total | Output | each scenario |
| η_{turb} | - | Hydroturbine conversion efficiency | Constant | Input | general |
| η_{pump} | - | When simulating pumped-storage potential: Pumping efficiency | Constant | Input | general |

| Symbol | Unit | Description | Type | Used as/for | Applicable to |
|---------------------------|----------------------|--|-----------------------------------|--------------|---|
| f_{opt} | - | Optimal filling fraction of hydropower reservoir | Constant | Input | general |
| f_{spill} | - | Reservoir filling fraction at which overflow prevention via spillways is initiated | Constant | Input | general |
| f_{stop} | - | Low reservoir filling fraction at which hydropower generation is curtailed | Constant | Input | general |
| $f_{restart}$ | - | Reservoir filling fraction at which hydropower generation is restarted after curtailment | Constant | Input | general |
| f_{reg} | - | Fraction of natural inflow that gives filling time equal to unity | Constant | Intermediate | each small hydropower plant |
| g | m/s ² | Gravitational acceleration | Constant | Input | general |
| γ | - | Conventional reservoir rule parameter | Constant | Input | general |
| $\Gamma(t)$ | - | Binary function indicating whether hydropower plant is operating (1) or not (0) | Time series | Output | each hydropower plant & each scenario |
| $h(t)$ | m | Hydraulic head: Difference in water level between headwater (behind the dam) and tailwater (at the turbines) | Time series | Output | each hydropower plant & each scenario |
| h_{max} | m | Maximum hydraulic head of hydropower scheme | Constant | Input | each hydropower plant |
| $k_{turb}(t)$ | - | Hydroturbine utilisation rate | Time series | Output | each hydropower plant & each scenario |
| κ | - | Conventional reservoir rule parameter | Constant | Input | general |
| $L(t)$ | MW | Load to be followed | Time series | Intermediate | each scenario |
| $L_{opt}(t)$ | MW | Optimal load to be followed by hydro-solar-wind mix, ensuring long-term reservoir lake level stability | Time series | Output | each hydropower plant & each scenario |
| $L_{followed}(t)$ | MW | Actual followed load under optimal solution at zero loss of load (ideally equal to $L_{opt}(t)$) | Time series | Output | each hydropower plant & each scenario |
| $L_{res}(t)$ | MW | Residual load: Difference between actual followed load and total hydro-solar-wind power generation | Time series | Intermediate | each hydropower plant & each scenario |
| $L_{norm}(t)$ | - | Normalised load curve shape | Time series | Input | each scenario |
| $\lambda(t)$ | kg/m ² /s | Evaporation flux on reservoir lake surface | Time series | Input | each hydropower plant |
| μ | - | Constant used in modelling overflow prevention via spillways | Constant | Input | general |
| n | - | Index for different locations of solar and wind power generation | Index | - | solar power and wind power sites |
| N_{solar} | - | Total number of solar power generation sites connected to the same power grid | Constant | Input | each scenario |
| N_{wind} | - | Total number of wind power generation sites connected to the same power grid | Constant | Input | each scenario |
| $\nu(t)$ | - | Ratio of spinning reserves to total solar and wind power generation | Time series | Output | each hydropower plant & each scenario |
| P_{turb}^r | MW | Rated hydroturbine capacity | Constant | Input | each hydropower plant |
| $P_{stable}^{hydro}(t)$ | MW | Power generated by stable component of reservoir outflow | Time series | Output | each hydropower plant & each scenario |
| $P_{flexible}^{hydro}(t)$ | MW | Power generated by flexible component of reservoir outflow | Time series | Output | each hydropower plant & each scenario |
| $P_{RoR}^{hydro}(t)$ | MW | Power generated by seasonal run-of-river component of reservoir outflow | Time series | Output | each small hydropower plant & each scenario |
| $P_{inflexible}(t)$ | MW | Inflexible power generation (stable hydro + solar + wind) | Time series | Intermediate | each hydropower plant & each scenario |
| $P_{solar}(t)$ | MW | Solar power generation | Time series | Output | each hydropower plant & each scenario |
| $P_{wind}(t)$ | MW | Wind power generation | Time series | Output | each hydropower plant & each scenario |
| $P_{followed}$ | MW | Average actual followed load under optimal solution | Constant | Output | each hydropower plant & each scenario |
| P_{load} | MW | Average load to be followed | Constant | Intermediate | each hydropower plant & each scenario |
| $P_{spin}(t)$ | MW | Spinning reserves available from all hydropower plants | Time series | Output | each hydropower plant & each scenario |
| $P_{pump}(t)$ | MW | When simulating pumped-storage potential: Power used for pumping | Time series | Output | each large hydropower plant & each scenario |
| $P_d(t)$ | MW | Difference between total inflexible power generation (stable hydro + solar + wind) and to-be-followed load | Time series | Output | each hydropower plant & each scenario |
| ϕ | - | Conventional reservoir rule parameter | Constant | Input | general |
| $\pi(t)$ | kg/m ² /s | Precipitation flux on reservoir lake surface | Time series | Input | each hydropower plant |
| Ψ | - | Relative deviation between simulated lake levels under balancing-oriented and conventional operation, respectively | Function of c_{solar}, c_{wind} | Intermediate | each hydropower plant & each scenario |
| $Q_{in,frac}(t)$ | m ³ /s | Part of natural inflow that gives filling time equal to unity | Time series | Intermediate | each small hydropower plant |

| Symbol | Unit | Description | Type | Used as/for | Applicable to |
|------------------------------|-------------------|---|-------------|--------------|---|
| $Q_{in,nat}(t)$ | m ³ /s | Natural river discharge into reservoir | Time series | Input | each hydropower plant |
| $Q_{out}(t)$ | m ³ /s | Total reservoir outflow, consisting of stable, flexible, run-of-river and spilling components | Time series | Output | each hydropower plant & each scenario |
| $Q_{stable}(t)$ | m ³ /s | Stable component of reservoir outflow | Time series | Output | each hydropower plant & each scenario |
| $Q_{flexible}(t)$ | m ³ /s | Flexible component of reservoir outflow | Time series | Output | each hydropower plant & each scenario |
| $Q_{RoR}(t)$ | m ³ /s | Seasonal run-of-river component of reservoir outflow (zero for large hydropower plants) | Time series | Output | each small hydropower plant |
| $Q_{spill}(t)$ | m ³ /s | Spilling component of reservoir outflow | Time series | Output | each hydropower plant & each scenario |
| Q_{turb}^{max} | m ³ /s | Maximum hydroturbine throughput | Constant | Input | each hydropower plant |
| $Q_{turb,flexible}^{pot}(t)$ | m ³ /s | Maximum potential outflow available for flexible hydropower generation, before accounting for needs and ramping constraints | Time series | Intermediate | each hydropower plant & each scenario |
| $Q_{pump}(t)$ | m ³ /s | When simulating pumped-storage potential: Pumped flow | Time series | Output | each large hydropower plant & each scenario |
| Q_{pump}^{max} | m ³ /s | When simulating pumped-storage potential: Maximum pumping throughput | Constant | Input | each large hydropower plant |
| ρ | kg/m ³ | Density of water | Constant | Input | general |
| t | hours | Time | Variable | - | general |
| T_{year} | seconds | Number of seconds in a year | Constant | Input | general |
| τ_{fill} | - | Filling time: number of years it takes (on average) to fill reservoir with natural inflow | Constant | Intermediate | each hydropower plant |
| $\tau_{fill,frac}$ | - | Filling time: number of years it takes (on average) to fill reservoir with fraction f_{reg} of natural inflow | Constant | Intermediate | each small hydropower plant |
| $V(t)$ | m ³ | Volume of water in reservoir | Time series | Output | each hydropower plant & each scenario |
| V_{max} | m ³ | Maximum reservoir volume | Constant | Input | each hydropower plant |
| $V_{lower}(t)$ | m ³ | When simulating pumped-storage potential: Volume of lower reservoir | Time series | Output | each large hydropower plant & each scenario |
| $V_{lower,max}$ | m ³ | When simulating pumped-storage potential: Maximum volume of lower reservoir | Constant | Input | each large hydropower plant |
| w_{solar}^n | - | Weight factor for capacity to be installed in each solar power site | Constant | Input | each solar power site |
| w_{wind}^n | - | Weight factor for capacity to be installed in each wind power site | Constant | Input | each wind power site |
| z_{max} | m | Maximal reservoir depth | Constant | Pre-input | each hydropower plant |

Note 9 Running the model: Input (A)

The initialisation of the REVUB simulation is done through the file `A_REVUB_initialise_minimum_example`. In this file, all parameters that should be defined by the user (through accompanying Excel files) are indicated by `[Set by user]`. This includes various types of data:

- *Time-related parameters* and *model parameters* referring to the length of the time series to simulate, and to various quantities used in the hydropower modelling, according to the equations introduced in this Manual which are all referenced to their equation number in the code. These quantities are the same across all hydropower plants to be modelled;
- *Static parameters*, which are constants specific to each hydropower plant, and thus to be entered as 1-dimensional arrays with length equal to the number of hydropower plants for which to run a simulation, with each element representing the corresponding value for the corresponding hydropower plant;
- *Time series* of important parameters whose value needs to be known for each time step before a simulation can be performed, namely reservoir inflow, evaporation, precipitation, solar/wind power capacity factor, and the shape of the electricity demand profile. These values should be read in by the code as 3-dimensional matrices, with the following dimensions: *[number of time slices (default: hours) per year; number of years covered by the simulation; number of hydropower plants included in the simulation]*.^v

^vNote that the REVUB code is designed to take into account the extra days occurring in leap years; for

- *Bathymetric relationship* for the modelled hydropower plants. These values should be read in by the code as an array with three columns and a user-determined number of rows; the first column should represent reservoir volume, and the second and third column the corresponding area and hydraulic head values.

Note 10 Running the model: Core code (B)

The actual core code of REVUB is contained in the file `B_REVUB_main_code`. Once the input data has been loaded using the file `A_REVUB_initialise_minimum_example`, the user can principally run this core code directly. The first lines of this code contain parameters related to accuracy and speed of computation denoted [Set by user], which can be tuned (through an accompanying Excel file):

- `N_ELCC` determines the accuracy (the number of discrete steps between zero and maximum power generation) with which the zero-crossing of L_{res} in equation (S22) is determined.
- `f_init_BAL_start`, `f_init_BAL_step` and `f_init_BAL_end` determine the range (start, step size, and end) of $E_{solar} + E_{wind}$ (cf. equation (S25)), expressed as a fraction of $E_{reservoir, CONV}^{hydro}$ (cf. equation (S24)), in which the REVUB code starts searching for the solution to equation (S21). Note that the code gives a warning message to the user in case this range turns out to be inadequate (i.e. if no global minimum in Ψ is found). The same ranges should also be given for STOR scenarios (`f_init_STOR_start`, `f_init_STOR_step` and `f_init_STOR_end`) in case the user wishes to model these.
- `N_refine_BAL` determines the accuracy with which the solution to equation (S21) is determined. After the initial search for this minimum in the range [`f_init_BAL_start` : `f_init_BAL_step` : `f_init_BAL_end`] (see previous point), the REVUB model can zoom in to the range around this minimum to identify its value with increased accuracy, using a step size reduced by a factor of ten. The number of times with which this is done is determined by `N_refine_BAL`. Thus, `N_refine_BAL = 1` means that the initial search is deemed accurate enough, whereas each +1 in `N_refine_BAL` increases the accuracy of identification of the minimum in Ψ by one digit. Accordingly, each +1 also increases computation time proportionally. For users wishing to model STOR scenarios, the same principle applies to `N_refine_STOR`.
- `psi_min_threshold` is zero by default, but can be set higher to speed up computation time in case the search for the minimum in Ψ takes too long. This parameter ensures that the zooming-in to higher accuracies (see previous point) is stopped as soon as $\min(\Psi)$ ends up below `psi_min_threshold`. It can thus be a compromise for users wishing to have high accuracy of determining $\min(\Psi)$ (i.e. setting `N_refine_BAL/STOR > 1`) but not at a high cost of computational speed.
- `X_max_BAL` determines the amount of iterative loops employed by the model to get a converged estimate of $P_{stable, BAL}^{hydro}$ (cf. equation (S9) and the explanation below equation (S19)). Each +1 also increases computation time proportionally. For users wishing to model STOR scenarios, the same principle applies to `X_max_STOR`.

Note 11 Running the model: Output graphics (C)

The results of the REVUB simulation are post-processed with two separate files, named `C_REVUB_plotting` and `C_REVUB_plotting_multiple`, which generate several standardised figures based on the input and output of the model. The two files serve a somewhat different purpose:

the purposes of preparing these data sets, if the simulation period contains leap years, the number of elements along the first dimension of these matrices should thus reflect the number of time slices (hours) in a leap year, and the data for non-leap years should be appended with *nan* values to reach the same length.

- The file `C_REVUB_plotting_individual` is used to plot simulation results pertaining to a single (user-selected) hydropower plant.
- The file `C_REVUB_plotting_multiple` is used to aggregate simulation results pertaining to (a user-selected set of) all hydropower plants. Based on a user-defined total electricity demand, it shows how much of this total demand can be met by hydro-solar-wind power on all involved timescales, and how much would remain to be met by other power sources.

Note 11.1 Results for individual power plants

The figures generated by the file `C_REVUB_plotting_individual` are described below.

- Figure 1 shows (a) the (h, V) and (b) the (A, V) bathymetric calibration curves used as input to the model.
- Figure 2 shows (a) the full time series of hydraulic head $h(t)$ under CONV, BAL and (if modelled) STOR, (b) the frequency spectrum of these hydraulic head curves such that e.g. specific temporal signatures, such as diurnal dispatch in solar-heavy systems, can be discerned, and (c) the monthly median and interquartile ranges of natural inflow $Q_{in,nat}(t)$ and outflow $Q_{out}(t)$ (equation S2) under CONV, BAL and (if modelled) STOR.
- Figure 3 shows (a) the full time series of lake volume $V(t)$ under CONV, BAL and (if modelled) STOR, and (b) the monthly average time series of natural inflow $Q_{in,nat}(t)$ and outflow $Q_{out}(t)$ under CONV, BAL and (if modelled) STOR.
- Figure 4 shows the monthly average composition of the hydro-solar-wind mix supported by the selected hydropower plant, under the BAL scenario and for a user-defined year (see below). The figure indicates hydropower generation (by stable, flexible and RoR components) and the optimal solar and wind power contribution identified by REVUB. The achieved ELCC, whose profile reflects that of $L_{norm}(t)$, is also indicated. In case a STOR scenario was simulated, a corresponding extra figure will be produced for that scenario, additionally indicating the pump-stored part of solar/wind power generation.
- Figure 5 is analogous to Figure 4, but at yearly resolution and reflecting the entire simulated time series.
- Figure 6 is analogous to Figure 4, but at hourly (full) resolution for a user-defined time slice (see below).
- Figure 7 shows approximated reservoir release rules in the BAL scenario for a user-defined hour of the day during a user-defined month. The plot shows the median and interquartile range of needed reservoir release (minus the RoR and spill components, i.e. $Q_{stable} + Q_{flexible}$) versus the median hydraulic head, with each data point denoting results from one simulation year. A linear fit to these data points is also shown.

At the beginning of the code, a few parameters denoted [Set by user] are loaded from an Excel file, where they can be changed to adapt the data to be plotted. These are as follows:

- `plot_HPP` is the index of the hydropower plant for which to plot results in all Figures.
- `plot_year` is the index of the simulation year for which to plot results in Figures 4 and 6.
- `plot_month` is the month in which to start the time slice in Figure 6.
- `plot_day_month` is the day of the month defined by `plot_month` on which to start the time slice in Figure 6.
- `plot_num_days` is the number of days for which to plot results in Figure 6.

- `plot_rules_month` is the month(s) of the year for which to plot results in Figure 7. This can be an array, e.g. [1, 4] would denote that the curves in Figure 7 are plotted both for January and for April.
- `plot_rules_hr` is the hour(s) of day during the month defined by `plot_rules_month` for which to plot results in Figure 7. This can be an array, e.g. [8, 20] would denote that the curves in Figure 7 are plotted both for 8 a.m. and 8 p.m.

Note 11.2 Results for multiple power plants

The file `C.REVUB_plotting_multiple` serves to show to what extent the investigated hydropower, solar power and wind power plants could contribute to the overall power mix of a given territory. The principle of this file is as follows:

- To run the file, the user must first define an overall electricity demand curve, denoted `P_total_hourly` (see below).
- The file then plots the aggregate power generation from all investigated hydro, solar and wind plants under BAL and STOR, and compares it to `P_total_hourly`.
- Any shortfalls in renewable power generation are then assumed to be filled up by thermal power plants. This reflects the assumption of a priority of dispatch for renewables.
- When renewable power generation exceeds `P_total_hourly` by a certain amount, this amount is assumed to be curtailed.

In this way, the file allows to calculate the total power mix (hydro/solar/wind/thermal) suggested by the streamlined hydro-solar-wind operation as simulated by REVUB.

The figures produced by the file are described below.

- Figure 1 shows the monthly average composition of the hydro-solar-wind mix under the BAL scenario for a user-defined year (see below). The figure indicates the total power demand `P_total_hourly`, and how this power demand is met by the aggregate hydropower generation (by stable, flexible and RoR components) from all hydropower plants, the aggregate of all solar and wind power, and the necessary other (thermal) power generation. Any curtailed solar/wind power is shown as such. The curve representing $ELCC_{tot}$ is also included. In case a STOR scenario was simulated, a corresponding extra figure will be produced for that scenario, additionally indicating the pump-stored part of solar/wind power generation. (In this case, small hydropower plants for which no STOR scenario is available (cf. section Note 6) are included according to their BAL results.)
- Figure 2 is analogous to Figure 1, but at yearly resolution and reflecting the entire simulated time series.
- Figure 3 is analogous to Figure 1, but at hourly (full) resolution for a user-defined time slice (see below).

At the beginning of the code, a few parameters denoted [Set by user] are loaded from an Excel file, where they can be changed to adapt the data to be plotted. These are as follows:

- `plot_HPP_multiple` is an array containing the indices of the hydropower plants whose results are to be aggregated in the Figures. The user can thus select all, or a selection of, the simulated hydropower plants.
- `plot_year_multiple` is the index of the simulation year for which to plot results in Figures 1 and 3.
- `plot_month_multiple` is the month in which to start the time slice in Figure 3.

- `plot_day_month_multiple` is the day of the month defined by `plot_month` on which to start the time slice in Figure 3.
- `plot_num_days_multiple` is the number of days for which to plot results in Figure 3.
- `P_total_hourly` is the total power demand (for all time steps of the simulation) against which the hydro-solar-wind power generation is compared. We recommend that this is taken to be equal to $P_{total}^{av} L_{norm}(t)$ (cf. equation (S10)), with P_{total}^{av} the average total power demand (in MW), to be specified by the user.

Note 12 Examples of model use

The REVUB model has so far been used in, and/or inspired the methods of, the following publications/documents:

- S. Sterl, I. Vanderkelen, C.J. Chawanda, D. Russo, R.J. Brecha, A. van Griensven, N.P.M. van Lipzig, and W. Thiery. Smart renewable electricity portfolios in West Africa. *Nature Sustainability* **3**, 710–719 (2020). <https://doi.org/10.1038/s41893-020-0539-0>.
- S. Sterl, P. Donk, P. Willems, and W. Thiery. Turbines of the Caribbean: Decarbonising Suriname’s electricity mix through hydro-supported integration of wind power. *Renewable and Sustainable Energy Reviews* **134** (2020) 110352. <https://doi.org/10.1016/j.rser.2020.110352>.
- P. Donk, S. Sterl, W. Thiery, and P. Willems. REVUB-Light: A parsimonious model to assess power system balancing and flexibility for optimal intermittent renewable energy integration—A study of Suriname. *Renewable Energy* **173**, 57–75 (2021). <https://doi.org/10.1016/j.renene.2021.03.117>.
- S. Sterl, D. Fadly, S. Liersch, H. Koch, and W. Thiery. Linking solar and wind power in eastern Africa with operation of the Grand Ethiopian Renaissance Dam. *Nature Energy* **6**, 407–418 (2021). <https://doi.org/10.1038/s41560-021-00799-5>.
- S. Sterl, A. Devillers, C.J. Chawanda, A. van Griensven, W. Thiery, and D. Russo. A spatiotemporal atlas of hydropower in Africa for energy modelling purposes. *Open Research Europe* **1**, 29 (2021). <https://doi.org/10.12688/openreseurope.13392.3>.
- S. Sterl and W. Thiery. La faisabilité du solaire PV pour remplacer la centrale hydroélectrique de Koukoutamba en Guinée: Étude quantitative. Vrije Universiteit Brussel, Brussels, Belgium (2022). <http://dx.doi.org/10.13140/RG.2.2.26548.83848>.
- P. Donk, S. Sterl, W. Thiery, and P. Willems. A policy framework for power system planning towards optimized integration of renewables under potential climate change – The Small Island Developing States perspective. *Energy Policy* **177** (2023). <https://doi.org/10.1016/j.enpol.2023.113526>.

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- [6] Liersch, S. *et al.* Water resources planning in the Upper Niger River basin: Are there gaps between water demand and supply? *Journal of Hydrology: Regional Studies* **21**, 176 – 194 (2019).
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