

Abstract

The pursuit of practical nuclear fusion is focused on the deuterium-tritium (D-T) fuel cycle, widely considered the most feasible pathway for near-term power generation. A critical challenge, however, is the reliance on tritium, a radioactive isotope with an extremely limited external supply, necessitating a self-sufficient fuel cycle. The D-T fusion reaction produces most of its energy as 14.1 MeV neutrons, which can in turn be used to regenerate tritium through neutron-lithium interactions. The reactor subsystem that performs this function—the breeder blanket—is therefore essential for the viability of the D-T fuel cycle. It must simultaneously extract heat, shield reactor components, and maintain tritium self-sufficiency. This project applies Monte Carlo neutron transport simulations using `OpenMC` to investigate the neutronic performance of advanced breeder blanket designs, including heterogeneous and functionally graded geometries. The study aims to quantify how variations in material composition and spatial structure influence the tritium breeding ratio (TBR) and neutron flux profiles, and explores the potential for automated optimisation of blanket parameters through computational frameworks. The outcomes will inform the feasibility and efficiency of next-generation blanket concepts relevant to future magnetic confinement fusion reactors such a DEMO and STEP.

Neutron Transport and Tritium Breeding Modelling in Nuclear
Fusion Reactor Breeder Blankets
MPhys Project Report

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October 28, 2025

1 INTRODUCTION

The pursuit of practical nuclear fusion represents one of the most ambitious and potentially transformative scientific endeavours of the twenty-first century. As global energy demand continues to rise and the environmental impacts of fossil fuel use become ever clearer, fusion offers the prospect of a near-limitless, low-carbon energy source. Fusion energy aims to replicate, on Earth, the processes that power the Sun — combining light nuclei to release energy through mass-energy conversion. Unlike conventional nuclear fission, fusion promises inherent safety, reduced long-lived radioactive waste, and abundant fuel sources.

Among the various fusion reactions studied, the deuterium-tritium (D-T) reaction has emerged as the most viable for near-term applications due to its relatively high cross-section at achievable plasma temperatures and its favourable energy yield. However, the practical realisation of a D-T reactor introduces challenges that extend far beyond plasma confinement and heating. Chief among these is the supply of tritium, a radioactive isotope that does not occur naturally in significant quantities and must be produced artificially.

This challenge has led to the development of the breeder blanket concept — an integrated structure surrounding the plasma that captures energetic neutrons produced in fusion reactions and uses them to generate tritium through interactions with lithium. In addition to tritium production, breeder blankets also serve several critical roles: moderating neutron flux, capturing energy for conversion to electricity, and protecting reactor components from radiation damage.

Understanding the behaviour of neutrons within the blanket region is therefore central to the success of any D-T fusion system. Computational modelling of neutron transport, energy deposition, and tritium breeding provides vital insights into how different blanket materials and geometries perform under fusion-like conditions. These neutronics studies inform the design and optimisation of test blanket modules and full-scale reactor concepts.

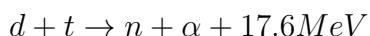
This project contributes to that effort by using advanced Monte Carlo simulations to model neutron interactions within candidate breeder blanket materials. Through this, it aims to identify promising compositions and geometries capable of sustaining tritium self-sufficiency in future fusion power plants.

2 THEORY

2.1 Fundamentals of Nuclear Fusion

Nuclear fusion is the process by which two light atomic nuclei combine, or “fuse,” to form a single heavier nucleus. This process releases a tremendous amount of energy if the mass of the final nucleus is less than the combined mass of the reactants, with the “lost” mass converted to energy according to $E = mc^2$.

For terrestrial power generation, the most promising reaction is that between the two heavy isotopes of hydrogen, deuterium (d) and tritium (t) [1, 2]:



This D-T reaction is the primary focus of mainstream fusion research, as it has a fusion cross-section ($\langle \sigma v \rangle$, an averaged measure of reaction chance given temperature effects [3]) significantly higher than other candidate reactions (like D-D or D- ^3He) at the “low” plasma temperatures achievable with current magnetic confinement technology (Fig. 1) [2].

To initiate fusion, the positively charged nuclei must be given enough kinetic energy to overcome their mutual electrostatic repulsion, known as the Coulomb barrier. In Magnetic

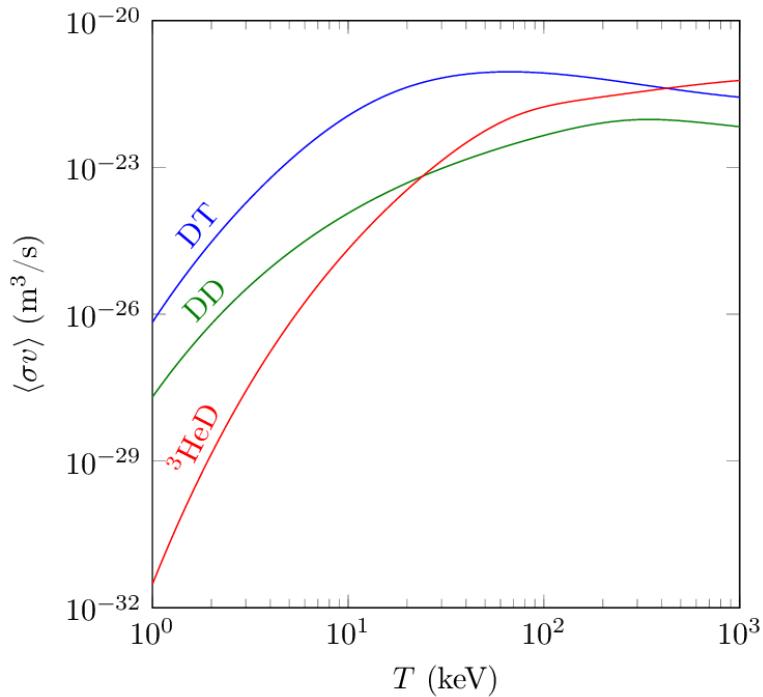


Figure 1: A comparison of fusion reaction reactivities ($\langle \sigma v \rangle$) as a function of ion temperature (keV) for the D-T, D-D, and D- ${}^3\text{He}$ fuel cycles. The D-T reaction’s reactivity peaks at a lower temperature and is significantly larger than the alternatives, making it the most accessible reaction for current and near-term fusion devices. Adapted from [4].

Confinement Fusion (MCF) devices, such as the **tokamak** [5], this is achieved by heating the D-T gas into a plasma state at temperatures exceeding 100 million Kelvin. The hot plasma is then confined by powerful magnetic fields, preventing it from touching the reactor walls. The 17.6 MeV of energy released is partitioned between the two products: the alpha particle (α , a helium nucleus) carries 3.5 MeV, while the neutron (n) carries 14.1 MeV [2].

This energy split is fundamental to the reactor’s operation. The charged alpha particle remains trapped by the magnetic fields, depositing its energy into the plasma and helping to sustain its high temperature (a process known as “plasma burning”). The neutron, being electrically neutral, is un-bothered by the magnetic fields and escapes the plasma immediately, carrying 80% of the energy with it [2].

2.2 Neutron Transport and Interactions

The 14.1 MeV neutron is the primary vehicle for both energy extraction and fuel production. Once it leaves the plasma, it travels into the surrounding structures, chiefly the extbf{breeder blanket}. The study of its journey and interactions with the blanket materials is the domain of **neutron transport** [6].

As the neutron moves through matter, it interacts with atomic nuclei via two main processes: scattering and absorption. The probability of any specific interaction occurring is defined by the material’s extbf{microscopic cross-section} (σ), a value that is highly dependent on the energy of the incident neutron [6]. These cross-sections are meticulously measured and compiled in comprehensive libraries such as the Evaluated Nuclear Data File (ENDF) [7].

Key interactions within the blanket include:

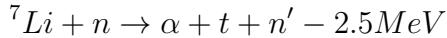
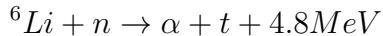
- **Scattering:** The neutron collides with a nucleus and “bounces” off, transferring a portion

of its kinetic energy to the nucleus. In **elastic scattering** (**n,n**), kinetic energy is conserved. In **inelastic scattering** (**n,n'**), the neutron excites the nucleus, which then de-excites by emitting a gamma ray, resulting in a larger energy loss for the neutron. Both processes are crucial for **moderation**—slowing the fast 14.1 MeV neutrons down. This thermal energy, deposited in the blanket material, is what is ultimately extracted by a coolant to generate electricity.

- **Absorption:** The neutron is captured by a nucleus. This can be a **radiative capture** (**n, γ**) event, where the nucleus emits a gamma ray. This is often a parasitic reaction, as it removes a neutron from the system that could have been used for breeding. Alternatively, the absorption can induce **charged particle emission**, such as (n,p) or (n, α) reactions. This is the fundamental mechanism used for tritium breeding [6].

2.3 Tritium Breeding and Neutron Multiplication

The primary nuclear function of the blanket is to use the fusion neutrons to “breed” new tritium fuel. This is accomplished by bombarding lithium isotopes with the neutrons. There are two reactions that produce tritium:

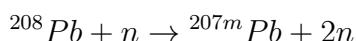


The 6Li reaction is exothermic and has a very large cross-section for low-energy (thermal) neutrons, making it the primary breeding reaction of interest [8]. The 7Li reaction is endothermic, requiring high-energy neutrons (a “threshold” reaction), and is generally less effective.

The critical metric for the blanket’s success is the **Tritium Breeding Ratio (TBR)**, defined as the ratio of tritium atoms produced in the blanket to the tritium atoms consumed in the plasma [9]. Due to inevitable fuel cycle losses (e.g., incomplete plasma burn-up, decay during extraction), the blanket must breed more tritium than is consumed. To achieve a self-sufficient fuel cycle, a TBR > 1.0 is mandatory, with most reactor designs targeting a value of 1.1 or higher [10, 11].

This presents a “neutron economy” challenge. The D-T reaction produces one neutron, and the primary 6Li breeding reaction consumes one neutron [12]. This leaves no margin for neutrons that are inevitably lost, either by leaking out of the blanket or through parasitic absorption in structural materials (like steel) [12].

To overcome this deficit, the blanket must include a **neutron multiplier** [13, 8]. These are materials that undergo an **(n,2n)** reaction, where one high-energy incident neutron strikes a nucleus and causes two neutrons to be emitted. The two most viable multiplier materials are Beryllium (Be) and Lead (Pb) [8].



By incorporating these materials, the single 14.1 MeV fusion neutron can be multiplied into two or more lower-energy neutrons. These neutrons are then moderated (slowed down) within the blanket until they are at the optimal thermal energy to be captured by 6Li , thus enabling a TBR significantly greater than one [8].

3 LITERATURE REVIEW

3.1 The D-T Reaction and the Tritium Fuel Imperative

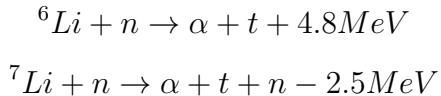
The deuterium-tritium (D-T) fusion reaction, $d + t \rightarrow n + \alpha + 17.6\text{MeV}$, has been the leading candidate for first-generation fusion power plants since its potential was identified in the 1940s [1]. Its primary advantage lies in its high fusion cross-section (σ_f) at plasma temperatures achievable with current technology, significantly higher than other candidates like D-D or D- ^3He reactions. Furthermore, 80 emitted neutron, which allows for energy to be efficiently extracted from the plasma core [2].

This reliance on the D-T reaction, however, creates a fundamental logistical challenge: the fuel cycle is not self-contained. While deuterium is abundant in seawater, tritium is a radioactive isotope with a short half-life of 12.32 years and is not found in nature in any significant quantity. The world's current tritium supply is a by-product of heavy-water-moderated fission reactors, such as CANDU reactors. Multiple analyses of this supply chain have concluded that global stockpiles are extremely limited and face serious shortages [14, 15], *even without* the projected demand from a future fleet of fusion power plants.

Therefore, for fusion energy to be a sustainable and viable long-term power source, any commercial D-T reactor must breed its own tritium. This has led to the development of in-situ fuel production systems, known as **Tritium Breeder Blankets**.

3.2 Breeder Blanket: Concept, Function, and Evolution

A breeder blanket is a complex component surrounding the plasma-containing vacuum vessel. Its primary function is to intercept the 14.1 MeV fusion neutrons and use them to induce tritium-producing reactions in lithium. The two key breeding reactions are:



While ${}^7\text{Li}$ can breed, the ${}^6\text{Li}$ reaction is exothermic and possesses a much larger reaction cross-section for the thermalised neutrons dominant in a blanket, making it the primary breeding isotope.

The concept of a “breeder” blanket predates its application in fusion; it was first developed as a method to use fusion neutrons to produce fissile materials, such as ${}^{233}\text{U}$ and ${}^{239}\text{Pu}$, for fission reactors [16, 17, 18]. Today, the design must also perform several other critical functions, including shielding the superconducting magnets from intense neutron radiation and extracting the fusion energy (via neutron thermalisation) for power conversion.

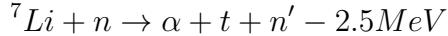
The key metric for a blanket's performance is the **Tritium Breeding Ratio (TBR)**, defined as the ratio of tritium atoms produced in the blanket to the tritium atoms consumed in the plasma. Due to inevitable losses from neutron capture in structural materials, decay, and incomplete fuel burn-up, a TBR significantly greater than 1.0 is required to achieve tritium self-sufficiency [10, 11].

However, the D-T reaction produces only one neutron, and the ${}^6\text{Li}$ reaction consumes one neutron. This leaves no margin for losses. To achieve a $\text{TBR} > 1$, most blanket designs must include a **neutron multiplier** material. The most effective materials for this are beryllium (${}^9\text{Be}$) and lead (${}^{208}\text{Pb}$), which undergo $(n, 2n)$ reactions (spallation) when struck by high-energy fusion neutrons, effectively turning one incident neutron into two [8].

3.3 The Role of Neutron Multipliers

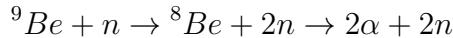
The D-T fusion reaction produces a single 14.1 MeV neutron, while the primary breeding reaction, ${}^6Li(n,\alpha)t$, consumes one neutron. This 1-to-1 neutron economy leaves no margin for inevitable losses due to parasitic absorption in structural materials or neutrons escaping the blanket. To achieve the required Tritium Breeding Ratio (TBR) greater than unity, a blanket must therefore incorporate a **neutron multiplier** [13].

While natural lithium itself has a minor neutron-multiplying reaction via the high-energy ($n,n't$) reaction with 7Li :



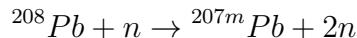
This reaction is endothermic, consuming 2.5 MeV of energy, and its cross-section is insufficient on its own to guarantee tritium self-sufficiency [8]. Therefore, dedicated multiplier materials are required, with the two primary candidates being Beryllium (Be) and Lead (Pb).

- **Beryllium (Be):** Beryllium, specifically the isotope 9Be , is an extremely effective neutron multiplier with a low energy threshold for its ($n,2n$) reaction:



It is widely used in conceptual solid breeder designs, such as the Helium-Cooled Pebble Bed (HCPB) and Water-Cooled Pebble Bed (WCPB), often in the form of beryllium pebbles or beryllide ceramics ($Be_{12}Ti$) [19, 20]. It is also a key component in the molten salt FLiBe ($2LiF - BeF_2$) [21, 22]. However, beryllium has two major drawbacks: it is a scarce resource, and its dust is “ridiculously toxic” [23], posing significant safety, handling, and manufacturing challenges.

- **Lead (Pb):** Lead, typically natural lead or lead enriched in ${}^{208}Pb$, is the other main multiplier candidate. It undergoes a high-energy ($n,2n$) reaction:



Lead’s primary advantage is that it can be seamlessly integrated into a liquid breeder, forming the $Li_{17}Pb_{83}$ eutectic alloy. This allows the material to serve as breeder, multiplier, and coolant simultaneously [24, 13]. While it avoids the toxicity issues of beryllium, lead is a high-Z (high atomic number) material. This means it can also be a source of parasitic neutron absorption, particularly for the low-energy thermal neutrons that are most effective for breeding with 6Li . Furthermore, its activation by high-energy neutrons can lead to the production of long-lived radioisotopes, complicating waste disposal [25].

The choice of multiplier, therefore, represents a critical trade-off between neutronic efficiency, material toxicity, resource availability, and long-term waste management [8, 23].

3.4 Major Breeder Blanket Architectures

Blanket designs are broadly divided into two categories—liquid and solid—based on the phase of the lithium-bearing breeder material.

3.4.1 Liquid Breeder Concepts

Liquid breeders (LBs) are attractive because the breeding medium can simultaneously function as the coolant, simplifying the design and allowing for continuous tritium extraction outside the reactor [21].

- **Lithium-Lead (Li-Pb):** This is one of the most mature concepts, typically using the eutectic alloy $Li_{17}Pb_{83}$ [26, 24]. The lead acts as both a neutron multiplier and the primary component of the alloy, while the eutectic composition provides a low melting point, which is crucial for circulation [26]. This concept is the basis for the **Dual-Cooled Lithium-Lead (DCLL)** blanket, a primary candidate for the European DEMO reactor [27, 13]. A key challenge for all liquid metal blankets is magnetohydrodynamics (MHD), where the strong magnetic fields of the tokamak induce currents in the flowing metal, creating a drag force that inhibits circulation [13].
- **Molten Salts:** An alternative LB concept uses molten fluorine or chlorine salts. The most prominent example is **FLiBe (2LiF - BeF₂)**, which advantageously combines the breeder (LiF) and multiplier (BeF₂) into a single, low-conductivity fluid [21]. This is the reference design for the **Affordable Robust Compact (ARC)** reactor concept from MIT [22, 25, 28]. A wide variety of other salt compositions, including LiF-PbF₂ and novel chlorine-based salts, are also under investigation to optimise breeding, temperature, and material compatibility [29, 30].

3.4.2 Solid Breeder Concepts

Solid breeders (SBs) use lithium-based ceramics, typically in the form of packed pebble beds, which eliminates MHD issues and offers high chemical stability [31, 32].

- **Materials and Design:** The leading candidate materials are lithium metatitanate (Li_2TiO_3) and lithium orthosilicate (Li_4SiO_4), often mixed with separate beryllium-based pebbles (e.g., $Be_{12}Ti$) as a multiplier [8, 33]. A review by [8] provides a comprehensive survey of these and other solid-phase options.
- **Implementations:** These materials form the basis of several major international designs. The **Chinese Fusion Engineering Test Reactor (CFETR)** is developing a **Water-Cooled Pebble Bed (WCPB)** blanket using $Li_2TiO_3/Be_{12}Ti$ pellets [20, 34]. European and Japanese DEMO concepts have focused on **Helium-Cooled Pebble Bed (HCPB)** designs, which are also being developed for ITER Test Blanket Modules [35, 19, 36].

The primary challenges for SB concepts are the complex engineering required for cooling (either with high-pressure helium or water) and the difficulty of extracting tritium, which must diffuse out of the solid ceramic and can be trapped in radiation-induced vacancies [37].

3.5 Neutronics Modelling and the Research Gap

Evaluating the TBR and other neutronic parameters of these complex designs is extremely difficult to do experimentally. While small-scale mockups provide crucial data on material properties and tritium release [38, 39], they cannot replicate the full neutron spectrum and geometry of a power plant [38].

Consequently, the field relies heavily on computational modelling, particularly **Monte Carlo (MC) simulations**. The probabilistic nature of neutron transport—defined by scattering, absorption, and multiplication cross-sections—is ideally suited to the statistical sampling methods of MC codes [40, 6].

- **OpenMC and Paramak:** This project uses **OpenMC**, a state-of-the-art, open-source MC code that has been validated against other established codes (like MCNP) and shown to accurately reproduce TBR and neutron flux calculations for fusion systems [41, 42]. It is increasingly used in fusion research for its robust capabilities [43, 44]. To manage the complex reactor geometry, we use **Paramak**, a Python-based CAD framework that automates the construction of parametric tokamak models compatible with OpenMC [45].
- **The Research Gap and Project Motivation:** A review of the literature reveals that decades of research have narrowed the focus to a small selection of “safe” materials (e.g., Li-Pb, Li_4SiO_4 , Li_2TiO_3) chosen not only for breeding but for their structural, chemical, and cost properties [12, 9]. This necessary pragmatism has left many other material combinations, particularly those in complex molten salt systems, comparatively unexplored.

While systematic neutronic studies have been performed [8, 29, 46], they often use simplified 1D models or focus on a limited set of parameters. Recent work using OpenMC and Paramak [47] has demonstrated the power of this new toolchain, but provides an opportunity for expansion.

This project fills this gap. By leveraging the automated workflow of OpenMC and Paramak, we will conduct a broad, systematic investigation of TBR performance. This work builds upon previous studies by exploring a wider range of breeder materials (including less-common salts) and, crucially, by systematically varying key parameters such as **6Li enrichment, blanket thickness, and material composition ratios** in a realistic 3D geometry. This systematic parameter sweep will provide a comprehensive dataset to identify optimal design points that previous, more narrowly-focused studies may have overlooked.

REFERENCES

1. Paris MW and Chadwick MB. A lost detail in D-T fusion history. Physics Today. 2023 Oct 1; 76:10–11. DOI: 10.1063/PT.3.5317. Available from: <https://pubs.aip.org/physicstoday/article/76/10/10/2912725/A-lost-detail-in-D-T-fusion-history> [Accessed on: 2025 Oct 14]
2. Heckrotte W and Hiskes J. Some factors in the choice of D-D, D-T or D- 3He mirror fusion power systems. Nuclear Fusion. 1971 Oct; 11:471–84. DOI: 10.1088/0029-5515/11/5/009. Available from: <https://doi.org/10.1088/0029-5515/11/5/009> [Accessed on: 2025 Oct 8]
3. Lilley J. Nuclear Physics: Principles and Applications. Manchester Physics Series. John Wiley & Sons, 2008
4. Jakobs M. Fusion Energy - Burning Questions. 2016. Publisher: Unpublished. DOI: 10.13140/RG.2.2.20211.04646. Available from: <https://www.researchgate.net/doi/10.13140/RG.2.2.20211.04646> [Accessed on: 2025 Oct 27]
5. Wesson J. Tokamaks. 4th. Oxford University Press, 2011

6. Kuridan RM. Neutron Transport: Theory, Modeling, and Computations. Graduate Texts in Physics. Cham: Springer Nature Switzerland, 2023. DOI: 10.1007/978-3-031-26932-5. Available from: <https://link.springer.com/10.1007/978-3-031-26932-5> [Accessed on: 2025 Oct 7]
7. Brown D, Chadwick M, Capote R, Kahler A, Trkov A, Herman M, et al. ENDF/B-VIII.0: The 8 th Major Release of the Nuclear Reaction Data Library with CIELO-project Cross Sections, New Standards and Thermal Scattering Data. Nuclear Data Sheets. 2018 Feb; 148:1–142. DOI: 10.1016/j.nds.2018.02.001. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0090375218300206> [Accessed on: 2025 Oct 7]
8. Hernández F and Pereslavtsev P. First principles review of options for tritium breeder and neutron multiplier materials for breeding blankets in fusion reactors. Fusion Engineering and Design. 2018 Dec; 137:243–56. DOI: 10.1016/j.fusengdes.2018.09.014. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379618306392> [Accessed on: 2025 Oct 8]
9. Federici G, Boccaccini L, Cismondi F, Gasparotto M, Poitevin Y, and Ricapito I. An overview of the EU breeding blanket design strategy as an integral part of the DEMO design effort. Fusion Engineering and Design. 2019 Apr; 141:30–42. DOI: 10.1016/j.fusengdes.2019.01.141. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379619301590> [Accessed on: 2025 Oct 7]
10. Sawan M and Abdou M. Physics and technology conditions for attaining tritium self-sufficiency for the DT fuel cycle. Fusion Engineering and Design. 2006 Feb; 81:1131–44. DOI: 10.1016/j.fusengdes.2005.07.035. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379605006393> [Accessed on: 2025 Oct 8]
11. Meschini S, Ferry SE, Delaporte-Mathurin R, and Whyte DG. Modeling and analysis of the tritium fuel cycle for ARC- and STEP-class D-T fusion power plants. Nuclear Fusion. 2023 Dec 1; 63:1–34. DOI: 10.1088/1741-4326/acf3fc. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/acf3fc> [Accessed on: 2025 Oct 8]
12. Shatalov G, Abdou M, Antipenkov A, Daenner W, Gohar Y, Kuroda T, et al. Breeder and test blankets in ITER. Fusion Engineering and Design. 1991 Dec; 16:85–93. DOI: 10.1016/0920-3796(91)90185-S. Available from: <https://linkinghub.elsevier.com/retrieve/pii/092037969190185S> [Accessed on: 2025 Oct 7]
13. Malang S, Deckers H, Fischer U, John H, Meyder R, Norajitra P, et al. Self-cooled blanket concepts using Pb-7Li as liquid breeder and coolant. Fusion Engineering and Design. 1991 Apr 2; 14:373–99. DOI: 10.1016/0920-3796(91)90020-Q. Available from: <https://www.sciencedirect.com/science/article/pii/092037969190020Q> [Accessed on: 2025 Oct 14]
14. Kovari M, Coleman M, Cristescu I, and Smith R. Tritium resources available for fusion reactors. Nuclear Fusion. 2018 Feb 1; 58:1–10. DOI: 10.1088/1741-4326/aa9d25. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/aa9d25> [Accessed on: 2025 Oct 8]
15. Pearson RJ, Antoniazzi AB, and Nuttall WJ. Tritium supply and use: a key issue for the development of nuclear fusion energy. Fusion Engineering and Design. 2018 Nov; 136:1140–8. DOI: 10.1016/j.fusengdes.2018.04.090. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S092037961830379X> [Accessed on: 2025 Oct 8]
16. Moir RW. The fusion breeder. Journal of Fusion Energy. 1982 Oct; 2:351–67. DOI: 10.1007/BF01063686. Available from: <http://link.springer.com/10.1007/BF01063686> [Accessed on: 2025 Oct 8]
17. Lee JD. U.S.-DOE FUSION-BREEDER PROGRAM: BLANKET DESIGN AND SYSTEM PERFORMANCE. Proceedings of the Third International Conference on Emerging Nuclear Energy Systems. 1983 :1–37. Available from: <https://www.osti.gov/servlets/purl/6012859>

18. Maniscalco JA, Berwald DH, Moir RW, Lee JD, and Teller E. The Fusion Breeder — an Early Application of Nuclear Fusion. *Fusion Technology*. 1984 Nov; 6:584–96. DOI: 10.13182/FST84-A23140. Available from: <https://www.tandfonline.com/doi/full/10.13182/FST84-A23140> [Accessed on: 2025 Oct 14]
19. Wang X, Feng K, Chen Y, Zhang L, Feng Y, Wu X, et al. Current design and R&D progress of the Chinese helium cooled ceramic breeder test blanket system. *Nuclear Fusion*. 2019 Jul 1; 59:1–8. DOI: 10.1088/1741-4326/ab0c32. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/ab0c32> [Accessed on: 2025 Oct 7]
20. Liu S, Chen L, Ma X, Cheng X, Lu P, Lei M, et al. Design of the Water-Cooled Ceramic Breeder blanket for CFETR. *Fusion Engineering and Design*. 2022 Apr; 177:1–8. DOI: 10.1016/j.fusengdes.2022.113059. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S092037962200059X> [Accessed on: 2025 Oct 7]
21. Tas H, Malang S, Reiter F, and Sannier J. Liquid breeder materials. *Journal of Nuclear Materials*. 1988 Jul; 155-157:178–87. DOI: 10.1016/0022-3115(88)90239-5. Available from: <https://linkinghub.elsevier.com/retrieve/pii/0022311588902395> [Accessed on: 2025 Oct 8]
22. Sorbom B, Ball J, Palmer T, Mangiarotti F, Sierchio J, Bonoli P, et al. ARC: A compact, high-field, fusion nuclear science facility and demonstration power plant with demountable magnets. *Fusion Engineering and Design*. 2015 Nov; 100:378–405. DOI: 10.1016/j.fusengdes.2015.07.008. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379615302337> [Accessed on: 2025 Oct 8]
23. Shimwell J, Lilley S, Morgan L, Packer L, Kovari M, Zheng S, et al. Reducing beryllium content in mixed bed solid-type breeder blankets. *Fusion Engineering and Design*. 2016 Nov; 109-111:1564–8. DOI: 10.1016/j.fusengdes.2015.11.021. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379615303458> [Accessed on: 2025 Oct 7]
24. Wu Y. Overview of liquid lithium lead breeder blanket program in China. *Fusion Engineering and Design*. 2011 Oct; 86:2343–6. DOI: 10.1016/j.fusengdes.2010.12.046. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379610005818> [Accessed on: 2025 Oct 7]
25. Bocci B, Hartwig Z, Segantin S, Testoni R, Whyte D, and Zucchetti M. ARC reactor materials: Activation analysis and optimization. *Fusion Engineering and Design*. 2020 May 1; 154:1–8. DOI: 10.1016/j.fusengdes.2020.111539. Available from: <https://www.sciencedirect.com/science/article/pii/S0920379620300879> [Accessed on: 2025 Oct 9]
26. Mas de les Valls E, Sedano LA, Batet L, Ricapito I, Aiello A, Gastaldi O, et al. Lead-lithium eutectic material database for nuclear fusion technology. *Journal of Nuclear Materials. Heavy Liquid Metal Cooled Reactors and Related Technologies*. 2008 Jun 15; 376:353–7. DOI: 10.1016/j.jnucmat.2008.02.016. Available from: <https://www.sciencedirect.com/science/article/pii/S0022311508000809> [Accessed on: 2025 Oct 8]
27. Fernández-Berceruelo I, Palermo I, Urgorri F, Rapisarda D, González M, Alguacil J, et al. Progress in design and experimental activities for the development of an advanced breeding blanket. *Nuclear Fusion*. 2024 May 1; 64:1–16. DOI: 10.1088/1741-4326/ad37ca. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/ad37ca> [Accessed on: 2025 Oct 7]
28. Segantin S, Testoni R, Hartwig Z, Whyte D, and Zucchetti M. Optimization of tritium breeding ratio in ARC reactor. *Fusion Engineering and Design*. 2020 May; 154:1–5. DOI: 10.1016/j.fusengdes.2020.111531. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S092037962030079X> [Accessed on: 2025 Oct 8]
29. Segantin S, Testoni R, and Zucchetti M. Neutronic comparison of liquid breeders for ARC-like reactor blankets. *Fusion Engineering and Design*. 2020 Nov; 160:1–10. DOI: 10.1016/j.fusengdes.2020.112013. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379620305615> [Accessed on: 2025 Oct 8]

30. Bohm TD and Lindley BA. Initial Neutronics Investigation of a Chlorine Salt-Based Breeder Blanket. *Fusion Science and Technology*. 2023 Nov 17; 79:995–1007. DOI: 10.1080/15361055.2022.2136923. Available from: <https://www.tandfonline.com/doi/full/10.1080/15361055.2022.2136923> [Accessed on: 2025 Oct 8]
31. Proust E, Anzidei L, Dalle Donne M, Fischer U, and Kuroda T. Solid breeder blanket design and tritium breeding. *Fusion Engineering and Design*. 1991 Dec; 16:73–84. DOI: 10.1016/0920-3796(91)90184-R. Available from: <https://linkinghub.elsevier.com/retrieve/pii/092037969190184R> [Accessed on: 2025 Oct 14]
32. Knitter R, Chaudhuri P, Feng Y, Hoshino T, and Yu IK. Recent developments of solid breeder fabrication. *Journal of Nuclear Materials*. 2013 Nov; 442:S420–S424. DOI: 10.1016/j.jnucmat.2013.02.060. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0022311513004662> [Accessed on: 2025 Oct 14]
33. Hernández FA, Gaisin R, Ghidersa BE, Knitter R, Neuberger H, Spagnuolo GA, et al. Chapter 7.5 - Ceramic breeder blankets. *Fusion Energy Technology R&D Priorities*. Ed. by El-Guebaly LA. Elsevier, 2025 Jan 1:225–34. DOI: 10.1016/B978-0-443-13629-0.00029-0. Available from: <https://www.sciencedirect.com/science/article/pii/B9780443136290000290> [Accessed on: 2025 Oct 8]
34. Lei M, Wu Q, Xu S, Xu K, Ma X, and Liu S. Design and analysis of the equatorial inboard WCCB blanket module for CFETR. *Fusion Engineering and Design*. 2020 Dec; 161:1–9. DOI: 10.1016/j.fusengdes.2020.111889. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379620304373> [Accessed on: 2025 Oct 7]
35. Federici G, Biel W, Gilbert M, Kemp R, Taylor N, and Wenninger R. European DEMO design strategy and consequences for materials. *Nuclear Fusion*. 2017 Sep 1; 57:1–26. DOI: 10.1088/1741-4326/57/9/092002. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/57/9/092002> [Accessed on: 2025 Oct 7]
36. Kawamura Y, Hirose T, Guan W, Miyoshi Y, Katagiri T, Wakasa A, et al. Overview of progress on water cooled ceramic breeder blanket in Japan. *Fusion Engineering and Design*. 2024 Apr; 201:1–7. DOI: 10.1016/j.fusengdes.2024.114260. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379624001133> [Accessed on: 2025 Oct 7]
37. Shi Y, Lu T, Gao T, Xiang X, Zhang Q, Yu X, et al. Density functional study of lithium vacancy in Li₄SiO₄: Trapping of tritium and helium. *Journal of Nuclear Materials*. 2015 Dec; 467:519–26. DOI: 10.1016/j.jnucmat.2015.09.017. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0022311515302063> [Accessed on: 2025 Oct 7]
38. Delaporte-Mathurin R, Goles N, Ball J, Dunn C, Edwards E, Ferry S, et al. Advancing tritium self-sufficiency in fusion power plants: insights from the BABY experiment. *Nuclear Fusion*. 2025 Feb 1; 65:1–11. DOI: 10.1088/1741-4326/ada2ab. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/ada2ab> [Accessed on: 2025 Oct 8]
39. Hirose T, Guan W, Katagiri T, Wakasa A, Someya Y, Nakajima M, et al. Functional tests for water cooled ceramic breeder blanket system using full-scale mockups. *Fusion Engineering and Design*. 2024 Mar; 200:1–6. DOI: 10.1016/j.fusengdes.2024.114227. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379624000802> [Accessed on: 2025 Oct 8]
40. Kalos MH and Whitlock PA. Monte Carlo Methods. 1st ed. Wiley, 2008 Sep 17. DOI: 10.1002/9783527626212. Available from: <https://onlinelibrary.wiley.com/doi/book/10.1002/9783527626212> [Accessed on: 2025 Oct 7]
41. Romano PK, Horelik NE, Herman BR, Nelson AG, Forget B, and Smith K. OpenMC: A state-of-the-art Monte Carlo code for research and development. *Annals of Nuclear Energy*. 2015 Aug; 82:90–7. DOI: 10.1016/j.anucene.2014.07.048. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S030645491400379X> [Accessed on: 2025 Oct 19]

42. Bae JW, Peterson E, and Shimwell J. ARC reactor neutronics multi-code validation*. Nuclear Fusion. 2022 Jun 1; 62:1–17. DOI: 10.1088/1741-4326/ac5450. Available from: <https://iopscience.iop.org/article/10.1088/1741-4326/ac5450> [Accessed on: 2025 Oct 7]
43. Fradera J, Sádaba S, Calvo F, Ha S, Merriman S, Gordillo P, et al. Pre-conceptual design of an encapsulated breeder commercial blanket for the STEP fusion reactor. Fusion Engineering and Design. 2021 Nov; 172:1–15. DOI: 10.1016/j.fusengdes.2021.112909. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0920379621006852> [Accessed on: 2025 Oct 8]
44. King D, Knowles A, Bowden D, Wenman M, Capp S, Gorley M, et al. High temperature zirconium alloys for fusion energy. Journal of Nuclear Materials. 2022 Feb; 559:1–27. DOI: 10.1016/j.jnucmat.2021.153431. Available from: <https://linkinghub.elsevier.com/retrieve/pii/S0022311521006516> [Accessed on: 2025 Oct 7]
45. Shimwell J, Billingsley J, Delaporte-Mathurin R, Morbey D, Bluteau M, Shriwise P, et al. The Paramak: automated parametric geometry construction for fusion reactor designs. F1000Research. 2021 Jan 18; 10:27. DOI: 10.12688/f1000research.28224.1. Available from: <https://f1000research.com/articles/10-27/v1> [Accessed on: 2025 Oct 7]
46. Bouillon R, Jaboulay JC, and Aubert J. Molten salt breeding blanket: Investigations and proposals of pre-conceptual design options for testing in DEMO. Fusion Engineering and Design. 2021 Oct 1; 171:1–9. DOI: 10.1016/j.fusengdes.2021.112707. Available from: <https://www.sciencedirect.com/science/article/pii/S092037962100483X> [Accessed on: 2025 Oct 14]
47. Goel V, Aslam S, and Dua S. Optimization of Tritium Breeding Ratio in a DT and DD Submersion Tokamak Fusion Reactor. 2023 Sep 30. DOI: 10.48550/arXiv.2310.00220. arXiv: 2310.00220[physics]. Available from: <http://arxiv.org/abs/2310.00220> [Accessed on: 2025 Oct 8]