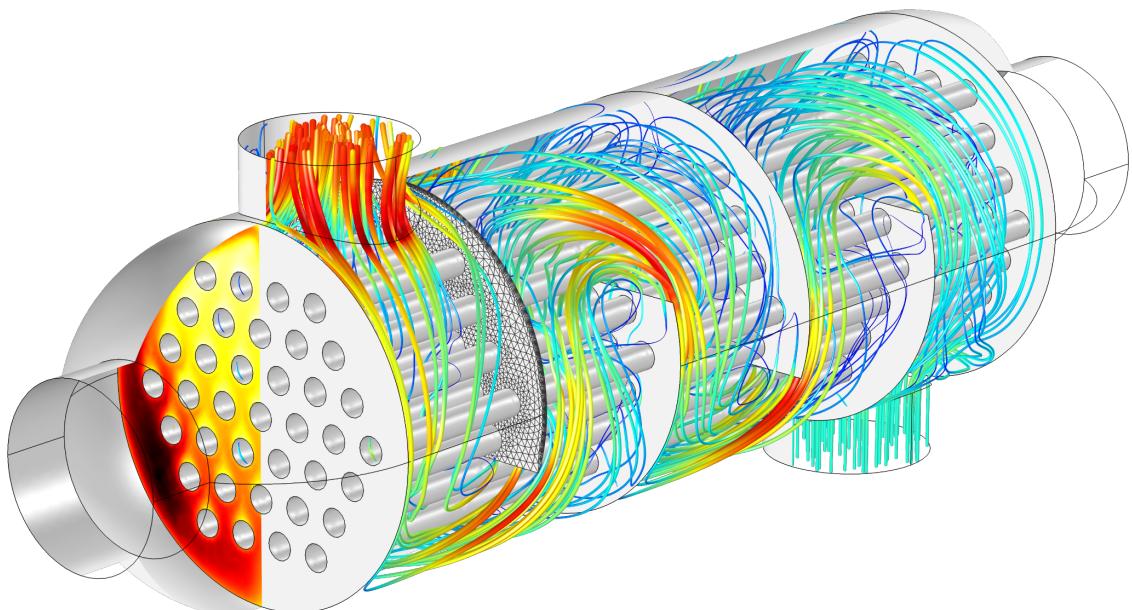


Heat Exchanger Network



Group - 29
S.S.S.Vardhan
19CH30018

Heat Exchanger Network

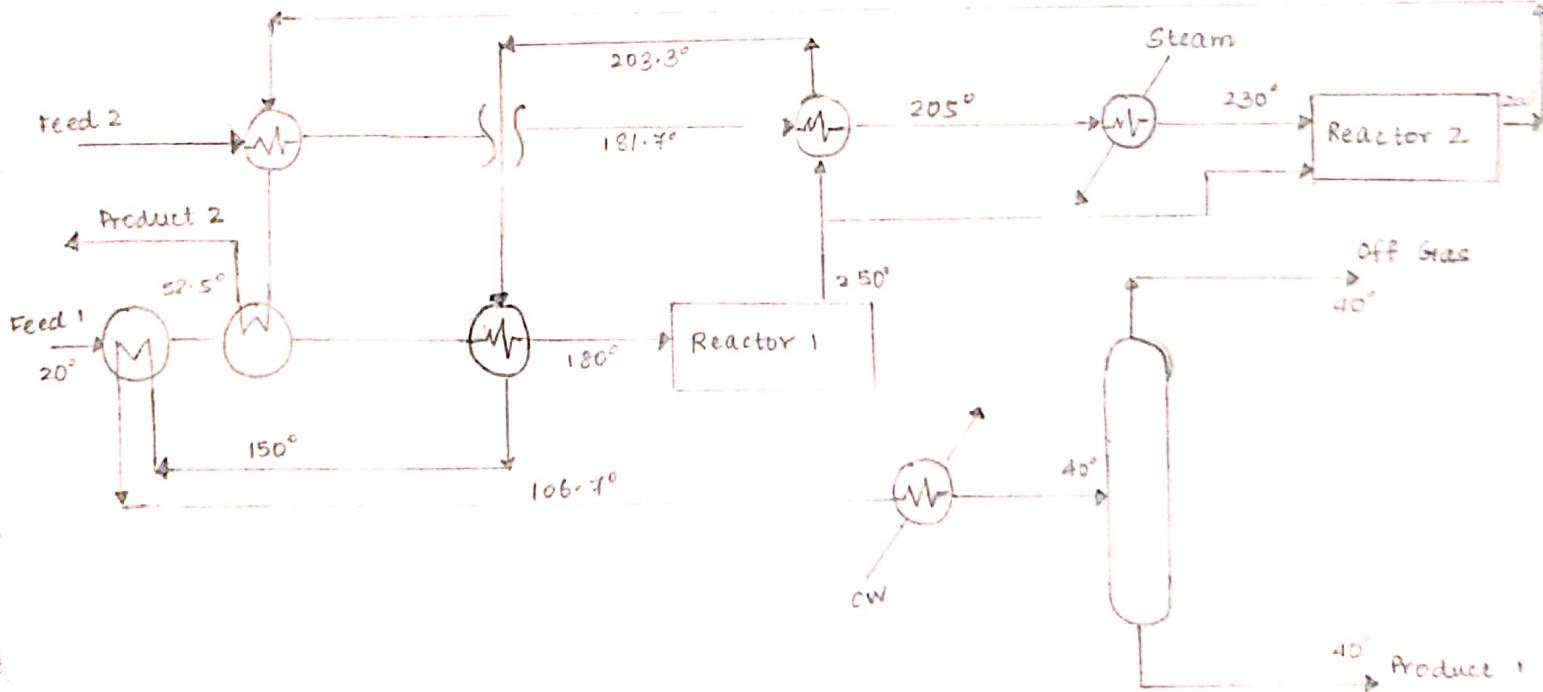
Stream	Type	Supply Temp. (T_s)	Target Temp. (T_t)	ΔH (HW)	c_p (MW °C ⁻¹)
Reactor 1 (Feed)	Cold	20 °C	180 °C	33.7	0.211
Reactor 1 (Product)	Hot	250 °C	40 °C	-31.7	0.151
Reactor 2 (Feed)	Cold	140 °C	230 °C	28.7	0.319
Reactor 2 (Product)	Hot	200 °C	80 °C	-34.7	0.289

For heating feed 2 from 140 °C to 230 °C , $\Delta H = 28.7 \text{ MW } ^\circ\text{C}^{-1}$

For heating feed 1 from 20 °C to 180 °C , $\Delta H = 33.7 \text{ MW } ^\circ\text{C}^{-1}$

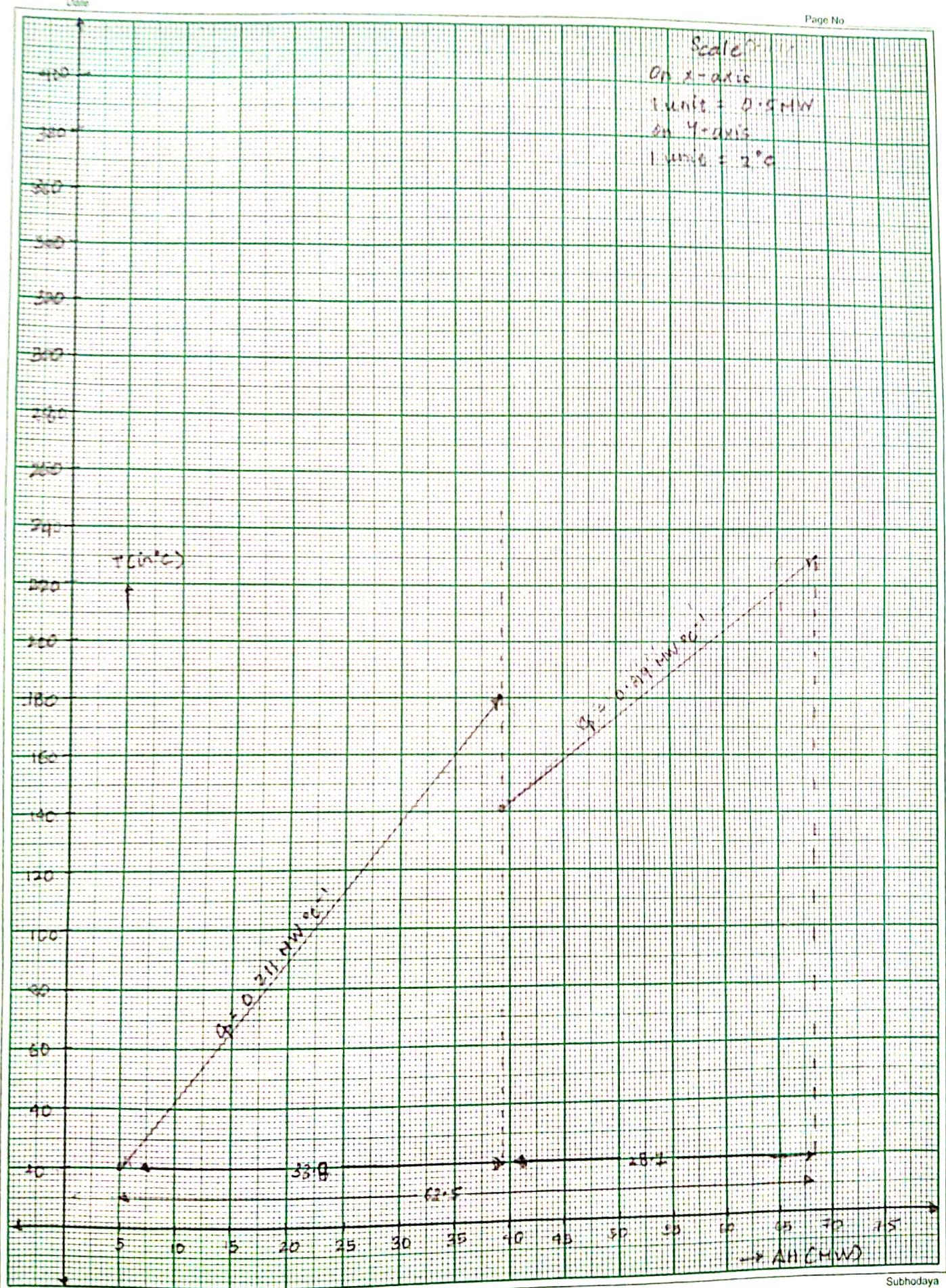
For cooling reactor 2 outlet stream from 200 °C to 80 °C , $\Delta H = -34.7 \text{ MW } ^\circ\text{C}^{-1}$

For cooling reactor 2 outlet stream from 250 °C to 40 °C , $\Delta H = -31.7 \text{ MW } ^\circ\text{C}^{-1}$



Scale
On X-axis
1 unit = 0.5 MW
On Y-axis
1 unit = 2°C

$T(^{\circ}\text{C})$



Scale:

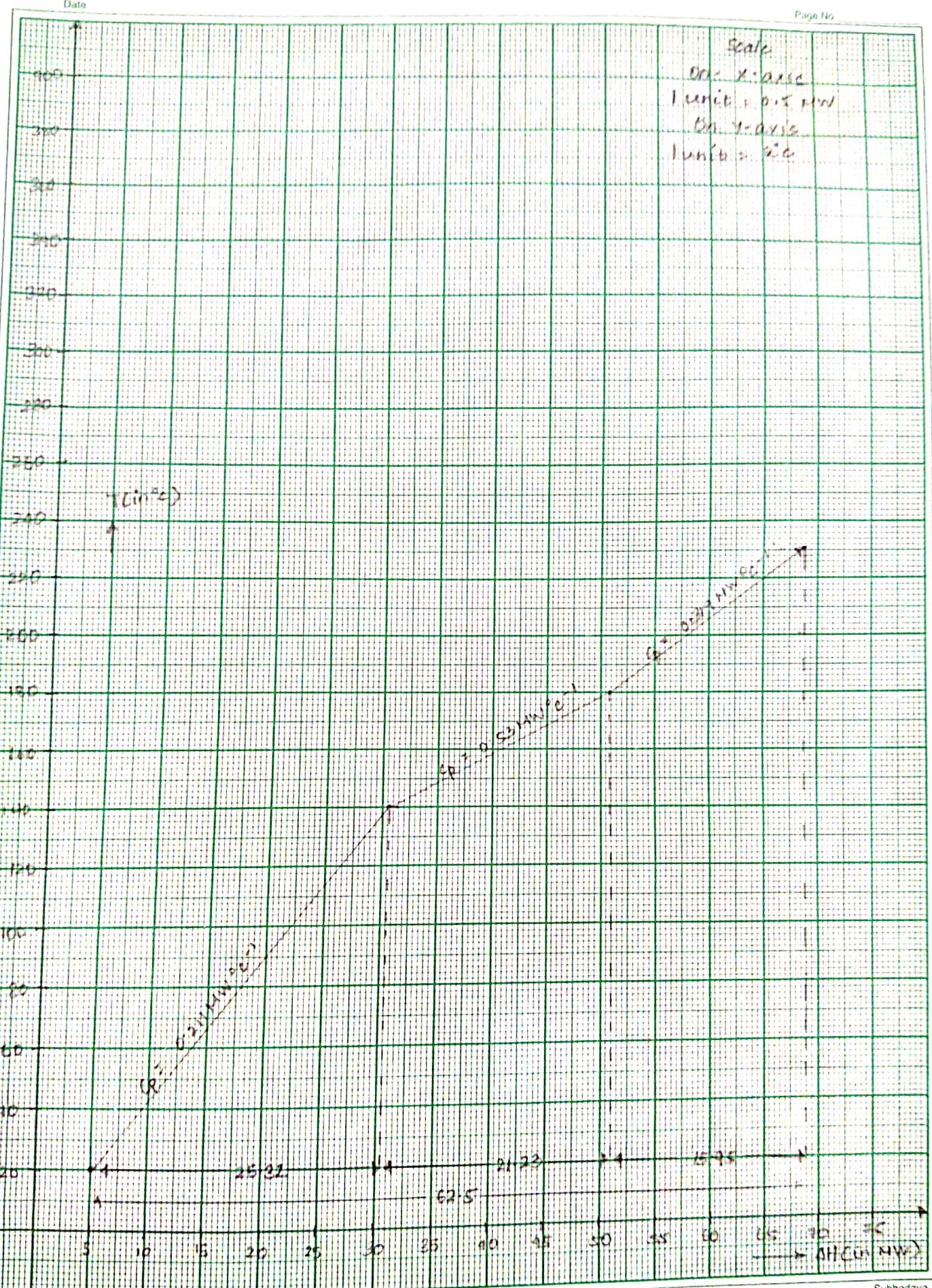
One X-axis

1 unit = 10 mm

One Y-axis

1 unit = 50

(in cm)

25.37
11.75

Scale 1:10
On X-axis
1 unit = 0.01W
On Y-axis
1 unit = 2°C

T(°C)

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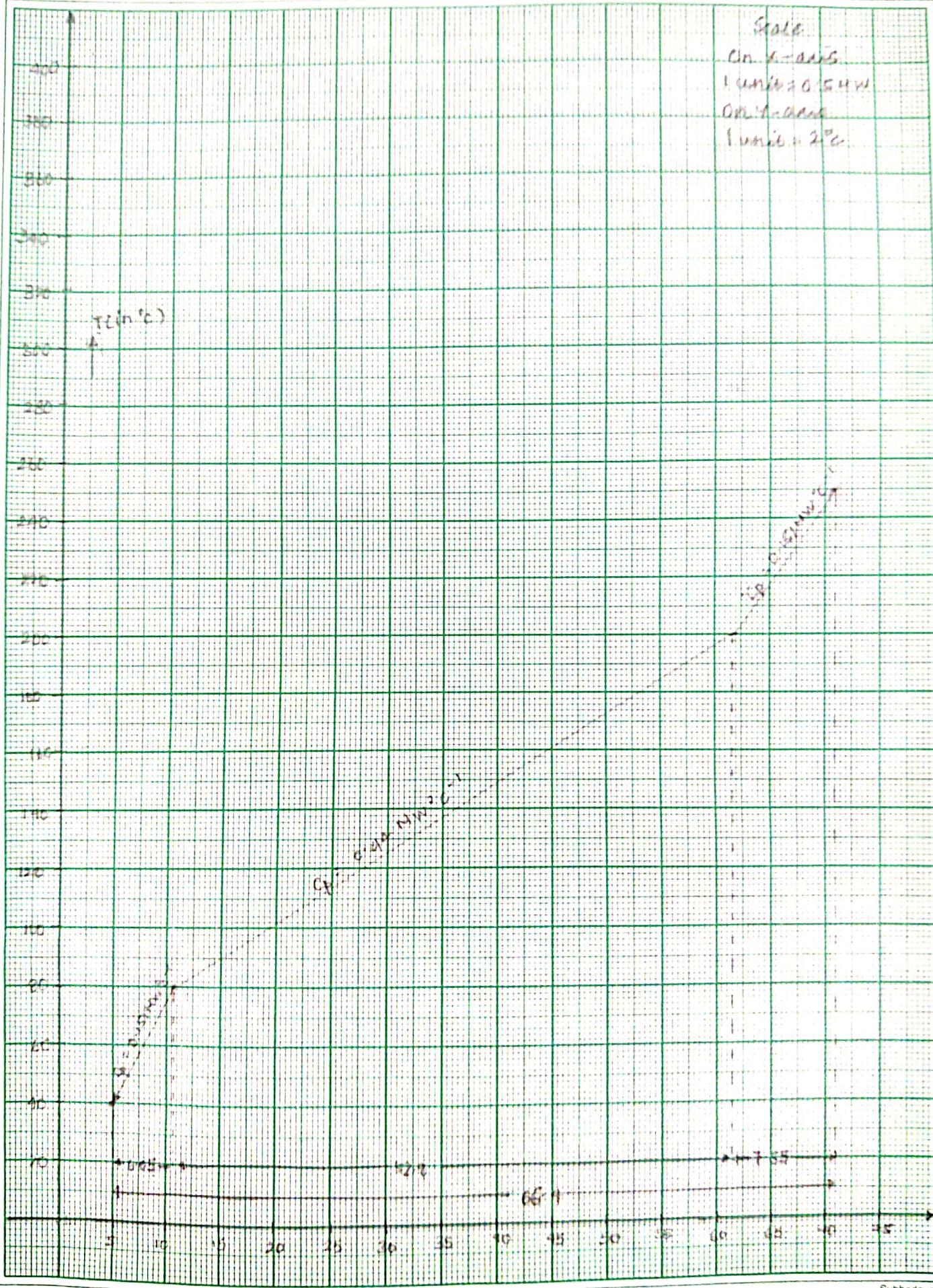
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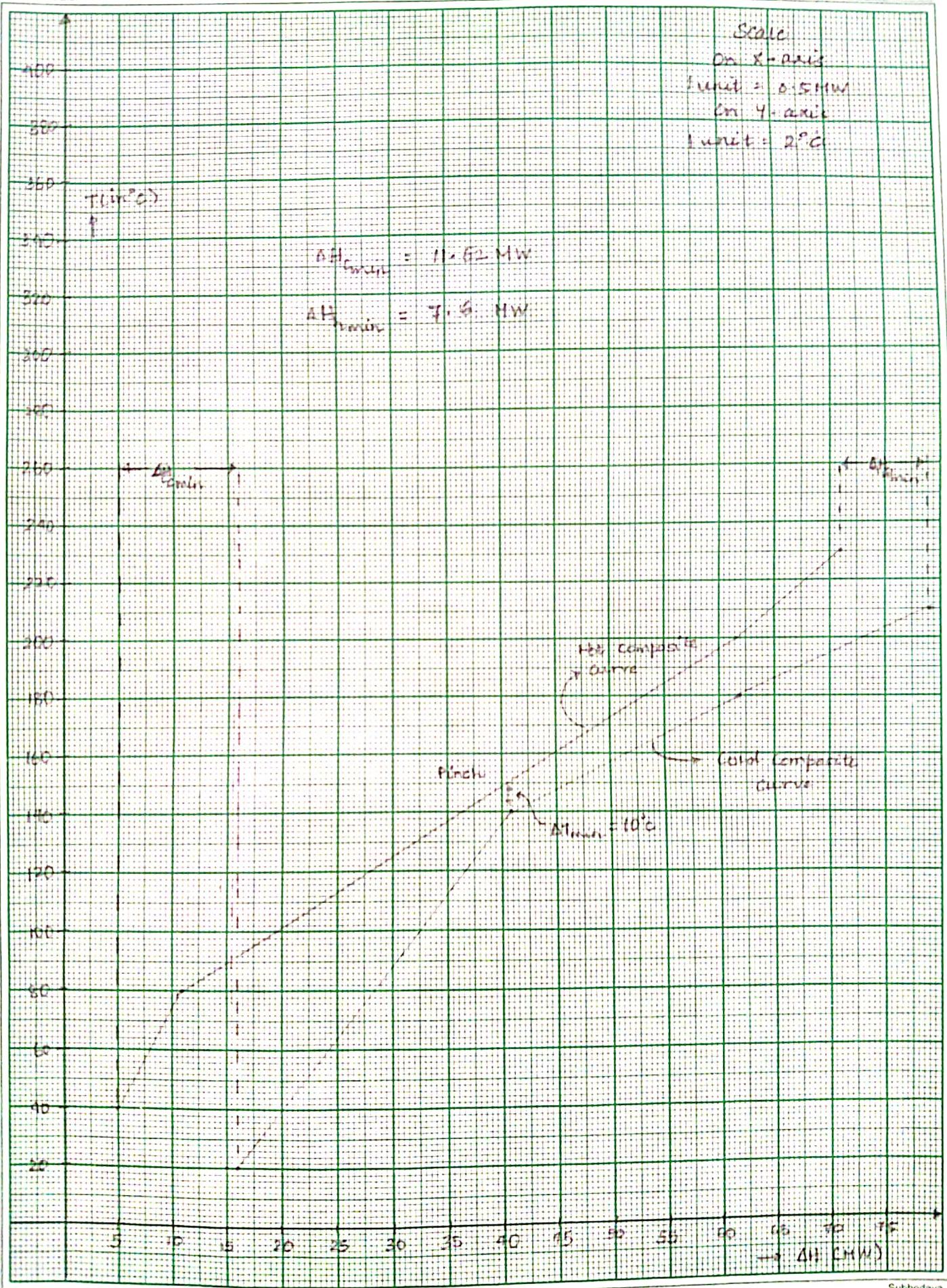
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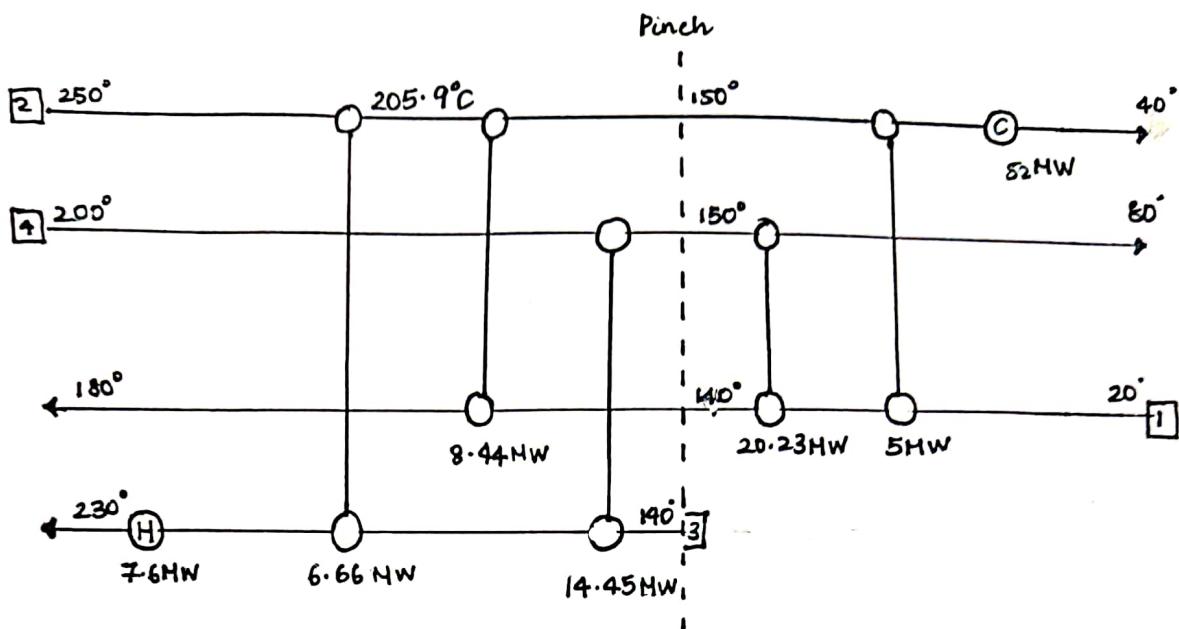
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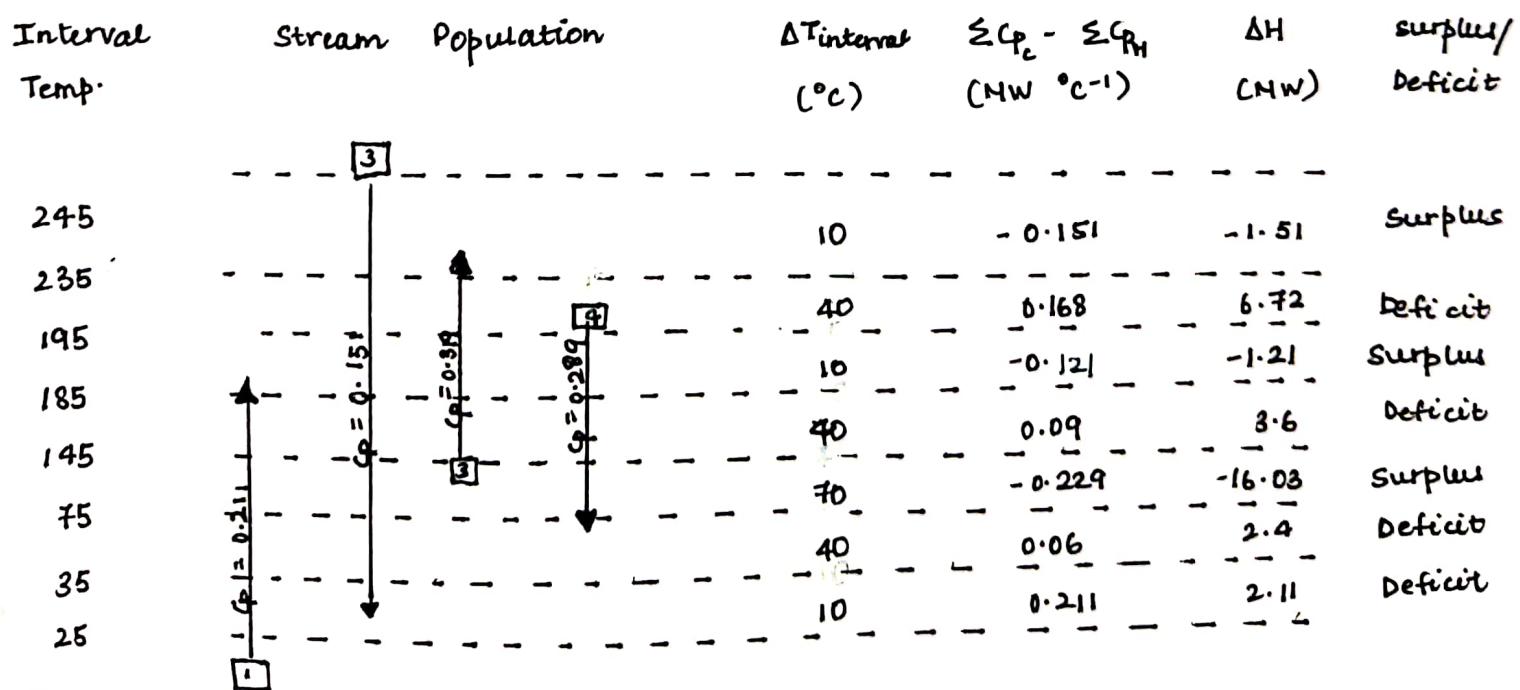


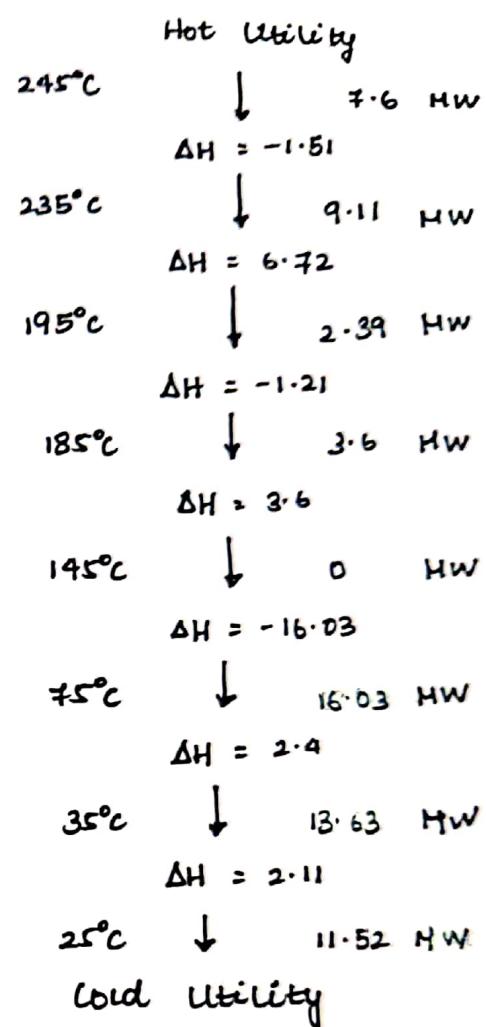
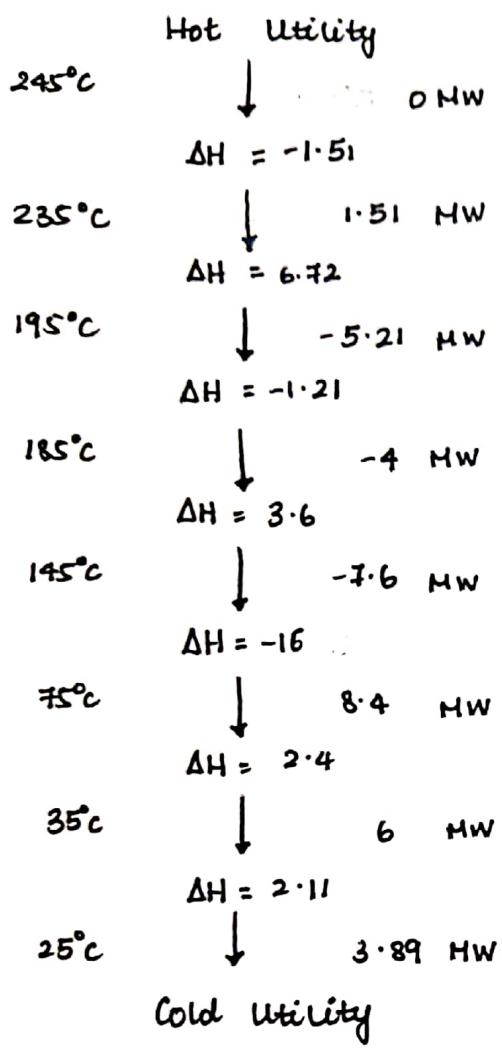




Shifting the curve by $\Delta T_{min}/2$ (5°C)

Stream	Type	T_s	T_t	T_s'	T_t'	
1	cold	20	180	25	185	All the
2	Hot	250	40	245	35	temperatures
3	Cold	140	230	145	235	are in 'c'
4	Hot	200	80	195	75	





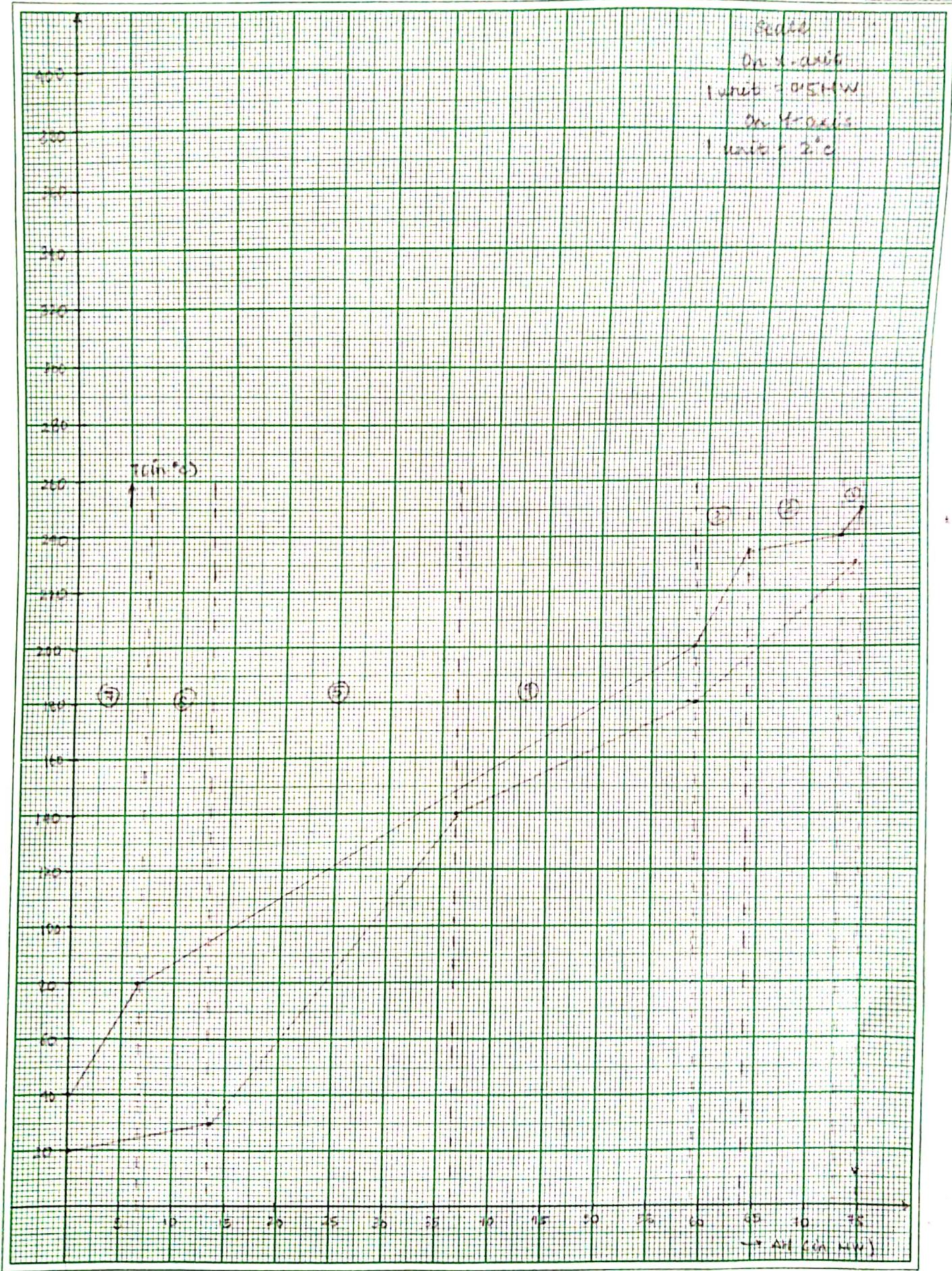
Stream	Supply Temp (°c)	Target Temp (°c)	ΔH (MW)	q_f (MW °c ⁻¹)	Film heat transfer co-eff (MW m ⁻² K ⁻¹)
Reactor 1 feed	20	180	33.7	0.211	0.0006
Reactor 1 pdt.	250	40	-31.7	0.151	0.0010
Reactor 2 feed	140	230	28.7	0.319	0.0008
Reactor 2 pdt.	200	80	28.7	0.289	0.0008
Stream	240	239	7.6	7.6	0.030
Cooling Water	20	30	11.52	1.152	0.0010

Balanced Hot Composite Data

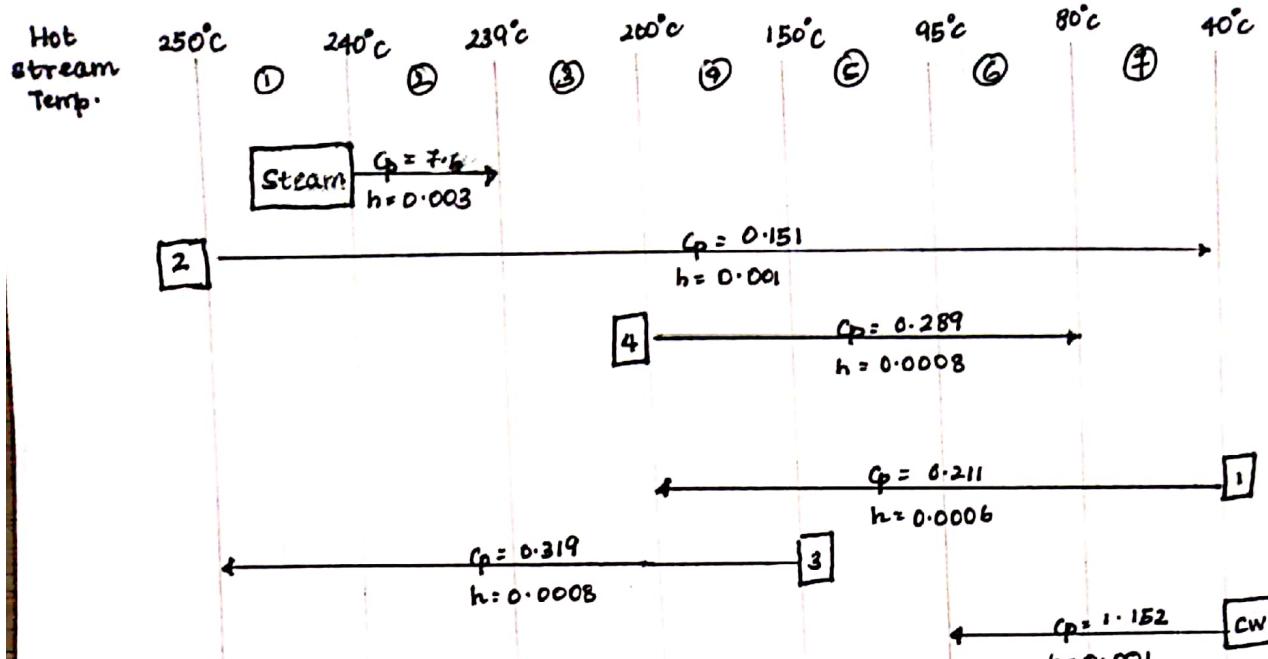
Temperature	Stream	Population	$\Delta T_{int.}$	ΣC_p	ΔH	$\Sigma \Delta H$	v
40	- - -	- - -	- - -	40	0.151	6.04	6.04
80	- - -	- - -	- - -	120	0.44	52.3	58.89
200	- - -	4	- - -	39	0.151	5.39	64.73
239	- - -	- - -	- - -	1	7.751	7.75	72.48
240	- - -	0.000	- - -	10	0.151	1.51	74
250	- - -	2	- - -	- - -	- - -	- - -	- - -

Balanced Cold Composite Data

Temperature	Stream	Population	$\Delta T_{int.}$	ΣC_p	ΔH	$\Sigma \Delta H$
20	1	10	10	1.363	13.63	13.63
30	- - -	- - -	- - -	- - -	- - -	- - -
140	- - -	3	110	0.211	23.21	36.84
180	- - -	- - -	40	0.53	21.2	58.04
230	- - -	- - -	50	0.319	15.95	74



Subhodaya



Cold Stream Temp.	230°C	225°C	199.5°C	180°C	140°C	30°C	25°C	20°C
Enthalpy	74	72.48	64.73	58.84	36.84	13.63	6.04	0

Enthalpy Interval	ΔT_{LMTD}	$\sum \left(q_i / n_i \right)_{\text{Hot streams}}$	$\sum \left(q_i / n_i \right)_{\text{cold streams}}$	A_k
1	17.38	1510	1993.75	201.60
2	25.30	2684.83	10168.125	508.00
3	28.65	5889	7775.625	476.95
4	14.43	25612.5	30016.67	3855.11
5	29.38	28143.75	38683.33	2275.51
6	59.86	2561.25	4518.33	168.39
7	34.60	6040	4518.33	391.86
$\sum A_k = 7877.509$				

$$\text{Area} = \frac{1}{\Delta T_{LMTD}} \left(\sum_n q/n + \sum_c q/n \right)$$

Price of steam = Rs 1.58 / kg

Price of cooling water = Rs 11.1 / 1000 kg

Steam (MJ/kg) = 2.26

water (MJ/kg) = 4.187×10^{-2}

Assuming that there are total 300 working days and 10 hrs use of heat exchanger network per day

Total running time = $300 \times 10 \times 3600 = 1.08 \times 10^7$ sec

Steam utility = Steam Price / steam Energy * Running Time
= Rs 750442.48 / MW/year

Water utility = Water Price / water Energy * Running Time
= Rs 2863147.84 / MW year

Steam Utility price = 750442.48 * 7.6 = Rs 57003362.85 / year

Water Utility price = 2863147.84 * 11.52 = Rs 32983462.66 / year

Annualized Capital Cost

$$a = 3012799.99, b = 37660, c = 1$$

$$\text{Number of units} = (\text{Streams above pinch} + \text{Streams below pinch} - 2) \\ = 5+4-2 = 7$$

$$\text{Raw cost} = N (a + b(\text{area}/N)^c) \\ = 7 (3012799.99 + 37660 (7877.51)^{1/7}) \\ = \text{Rs } 817756626.6 \text{ /year}$$

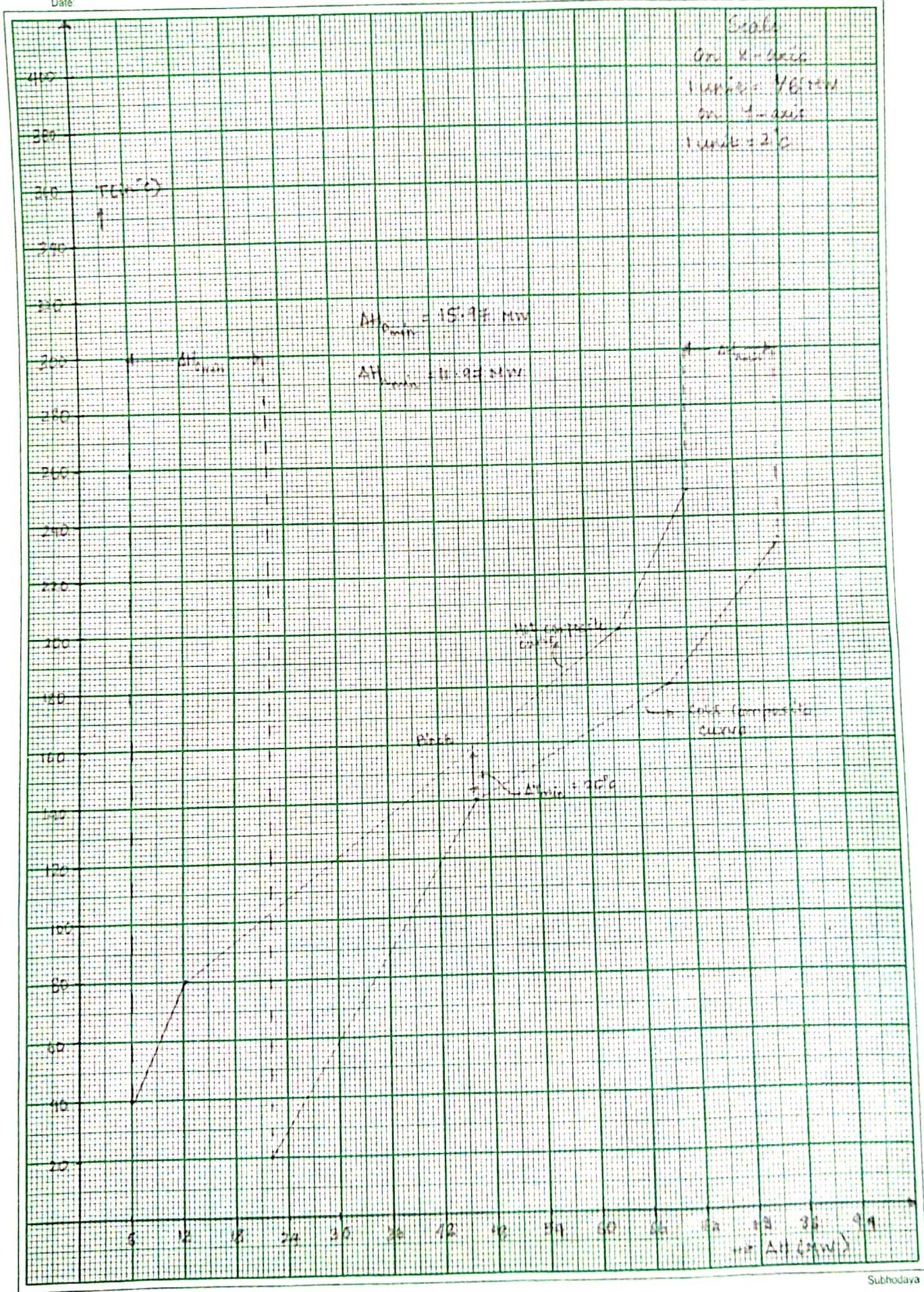
Interest (i) = 10% Time period (n) = 5 years

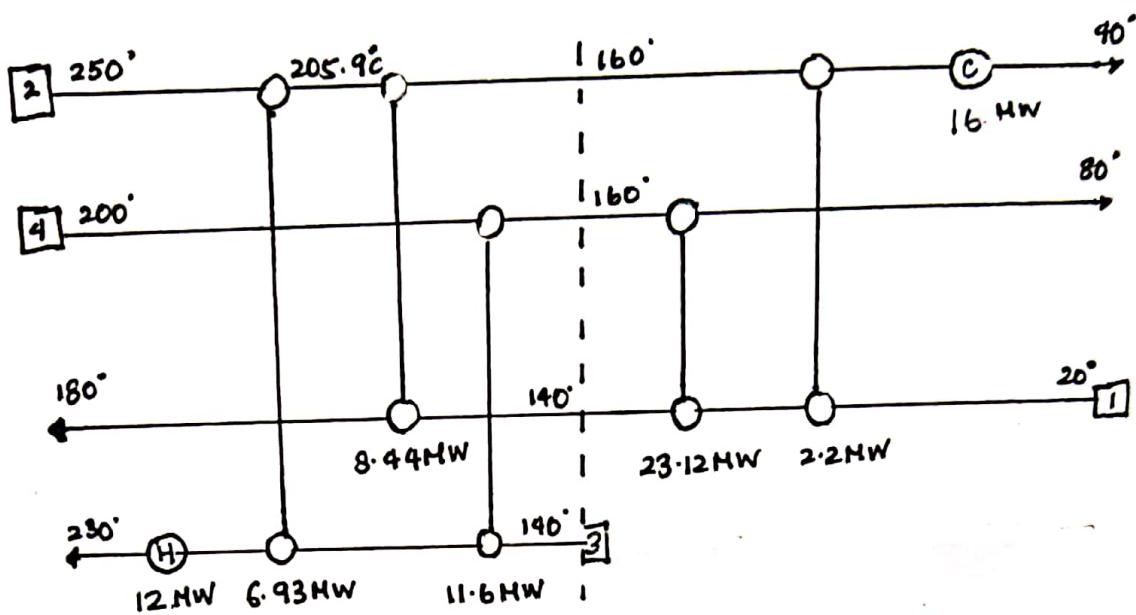
$$\text{Annunity factor} = 1 - (1+i)^n / I = 3.791$$

$$\text{Cost} = \text{Raw cost} * \text{Annunity factor} \\ = \text{Rs } 1204615371 \text{ /year}$$

$$\text{Total cost} = \text{Rs } 1294602197 \text{ /year}$$

Date





Shifting the curve by $\Delta T_{min}/2$ (10°C)

Stream	Type	T_S	T_T	T_S^*	T_T^*	
1	Cold	20	180	30	190	All the
2	Hot	250	40	240	30	temperatures
3	Cold	140	280	150	240	are in $^\circ\text{C}$
4	Hot	200	80	190	70	

Interval Temp	Stream	Population	$\Delta T_{interval}$	Σp	ΔH	Surplus/Deficit
240	1	50	50	0.168	8.4	Deficit
190	2	40	50	0.09	3.6	Deficit
150	3	80	50	-0.229	-18.32	Surplus
70	4	40	50	0.06	2.4	Deficit
30						

$$\begin{aligned}
 & \text{Hot Utility} \\
 & \downarrow \quad 0 \text{ MW} \\
 & \Delta H = +8.4 \\
 & \downarrow \quad -8.4 \text{ MW} \\
 & \Delta H = 3.6 \\
 & \downarrow \quad -12 \text{ MW} \\
 & \Delta H = -18.82 \\
 & \downarrow \quad 6.32 \text{ MW} \\
 & \Delta H = 2.4 \\
 & \downarrow \quad 3.92 \text{ MW}
 \end{aligned}$$

cold utility

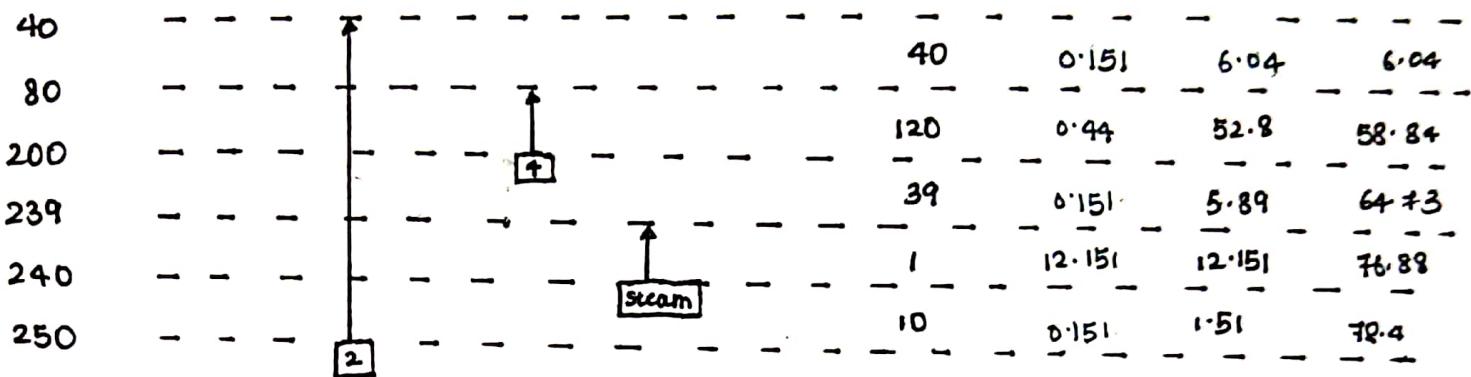
$$\begin{aligned}
 & \text{Hot utility} \\
 & \downarrow \quad 12 \text{ MW} \\
 & \Delta H = 8.4 \\
 & \downarrow \quad 3.6 \text{ MW} \\
 & \Delta H = 3.6 \\
 & \downarrow \quad 0 \text{ MW} \\
 & \Delta H = -18.82 \\
 & \downarrow \quad 18.82 \text{ MW} \\
 & \Delta H = 2.4 \\
 & \downarrow \quad 16 \text{ MW}
 \end{aligned}$$

Cold utility

Stream	Supply Temp (°C)	Target Temp (°C)	ΔH (MW)	C_p (MW °C⁻¹)	Film heat transfer co-eff (MW m⁻² °C⁻¹)
Reactor 1 feed	20	180	33.7	0.211	0.0006
Reactor 1 bolt.	250	40	-31.7	0.151	0.0010
Reactor 2 feed	140	230	28.7	0.319	0.0008
Reactor 2 bolt.	200	80	-34.7	0.289	0.0008
Stream	240	239	12	12	0.0030
cooling water	20	30	16	1.6	0.0010

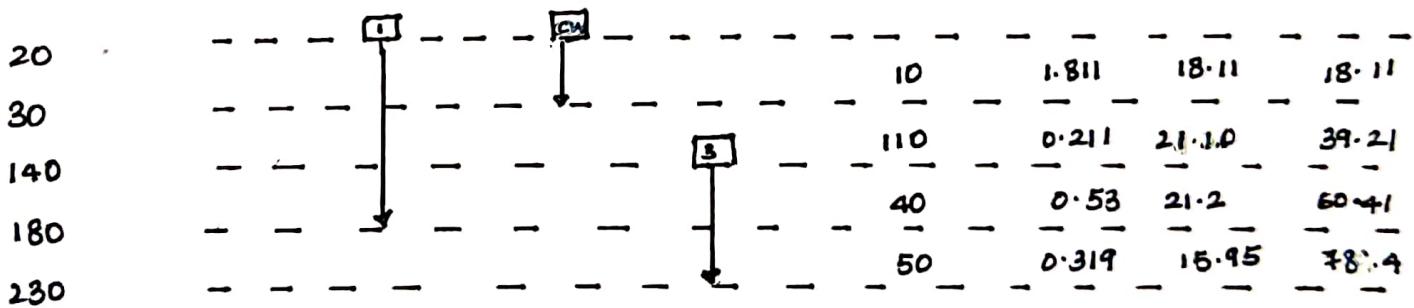
Balanced Hot Composite Data

Temperature	stream	Population	ΔT_{int}	ΣQ_p	ΔH	$\Sigma \Delta H$
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Balanced Cold Composite Data

Temperature	stream	Population	ΔT_{int}	ΣQ_p	ΔH	$\Sigma \Delta H$
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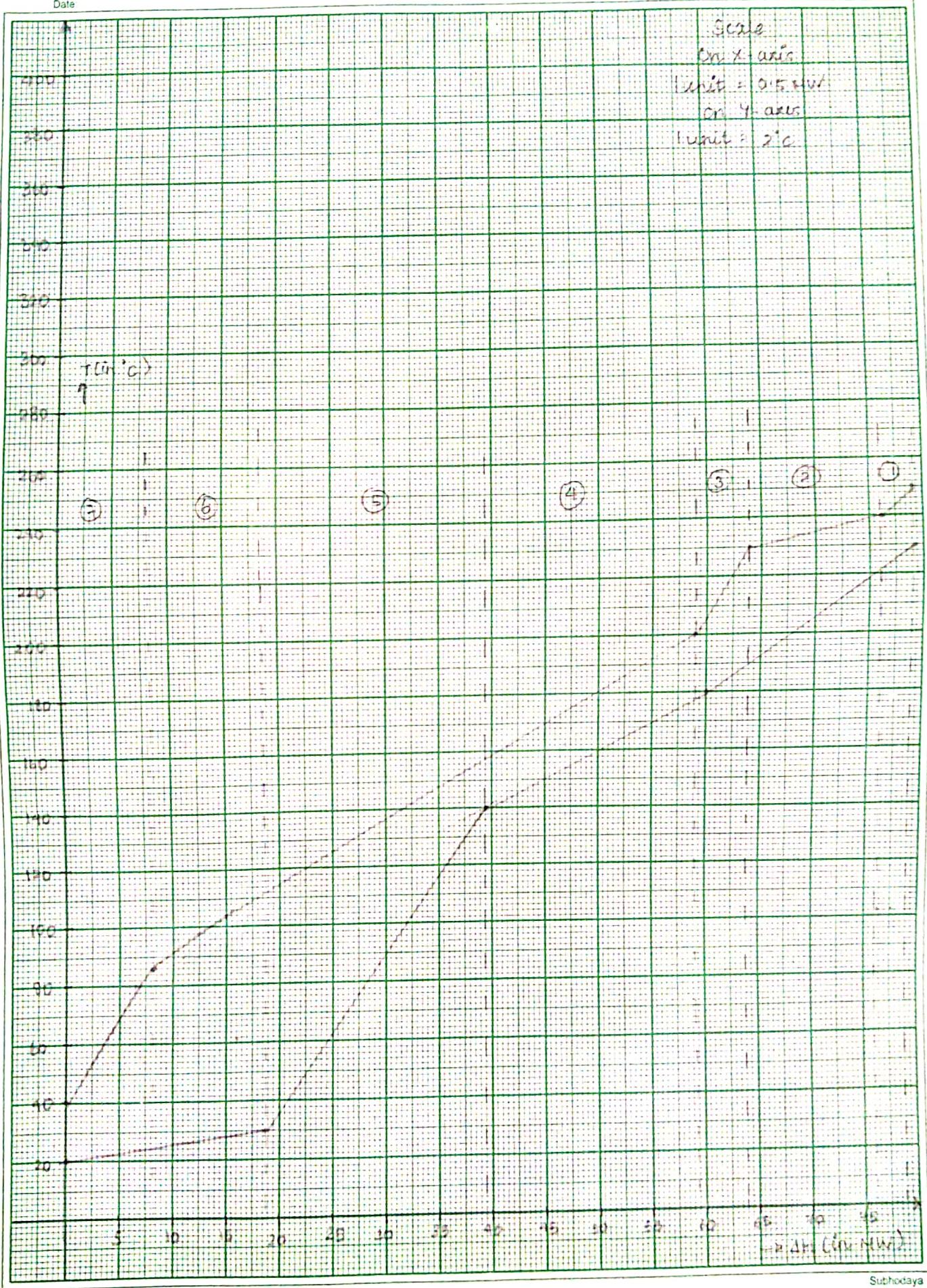
Scale

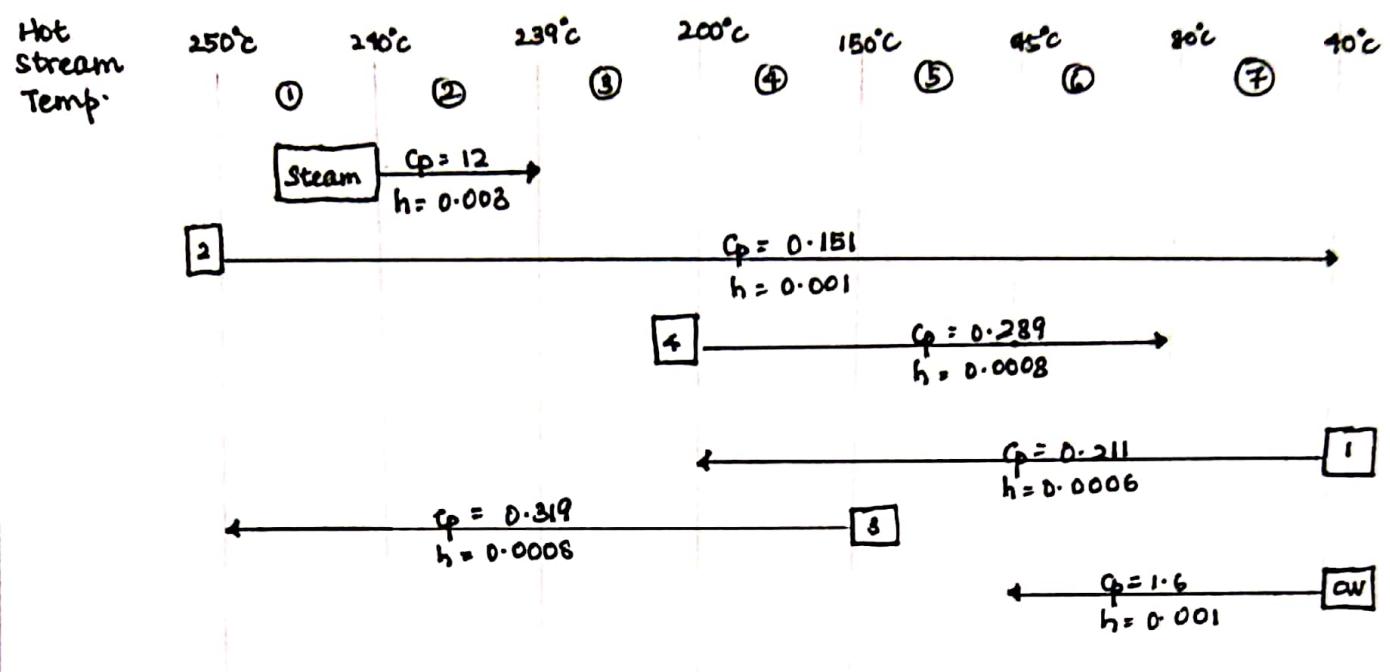
On X-axis

Unit = 0.5 mm

On Y-axis

1 unit = 2°C





Cold Stream Temp.

	230°C	225°C	199.5°C	180°C	140°C	30°C	25°C	20°C
Enthalpy	78.4	76.88	64.73	60.41	39.21	18.11	6.04	0

Enthalpy Interval	ΔT_{LMTD}	$\sum \left(q_i / h_i \right)_h$ (Hot streams)	$\sum \left(q_i / h_i \right)_c$ (Cold streams)	A_k
1	17.38	1510	1993.75	201.60
2	25.30	4151	10168.125	565.97
3	28.65	5889	7775.625	476.95
4	14.43	25612.5	30016.67	3855.11
5	29.38	28173.75	38683.33	2275.60
6	59.86	2561.25	9758.33	205.81
7	34.60	6040	9758.33	456.60
$\sum A_k = 8037.64$				

Price of steam = Rs 1.53 / kg

Price of cooling water = Rs 11.1 / 1000 kg

Steam (MJ/kg) = 2.26

Water (MJ/kg) = 4.187×10^{-2}

Assuming that there are total 300 working days and 10 hrs of use of heat exchanger network per day.

$$\text{Total running time} = 300 \times 10 \times 3600 = 1.08 \times 10^7 \text{ sec}$$

$$\begin{aligned}\text{Steam Utility} &= \text{Steam Price} / \text{Steam Energy} \cdot \text{Running Time} \\ &= \text{Rs } 7550442.48 / \text{MW year}\end{aligned}$$

$$\begin{aligned}\text{Water Utility} &= \text{Water Price} / \text{Water Energy} \cdot \text{Running Time} \\ &= \text{Rs } 2863147.84 / \text{MW year}\end{aligned}$$

$$\text{Steam Utility price} = 7550442.48 \times 12 = \text{Rs } 90605309.76 / \text{year}$$

$$\text{Water Utility price} = 2863147.84 \times 16 = \text{Rs } 45810365.48 / \text{year}$$

Annualized Capital Cost

$$a = 3012799.99, b = 37660, c = 1$$

$$\begin{aligned}\text{Number of unit} &= (\text{Streams above pinch} + \text{streams below pinch} - 2) \\ &= 5 + 4 - 2 = 7\end{aligned}$$

$$\begin{aligned}\text{Raw cost} &= N(a + b(\text{area}/N)^c) \\ &= 7(3012799.99 + 37660(5571.19/7)) \\ &\Rightarrow \text{Rs } 230900615.3 / \text{year}\end{aligned}$$

$$\text{Interest (i)} = 10\% \quad \text{Time period (n)} = 5 \text{ years}$$

$$\text{Annuity factor} = 1 - (1+i)^{-n} / i = 3.791$$

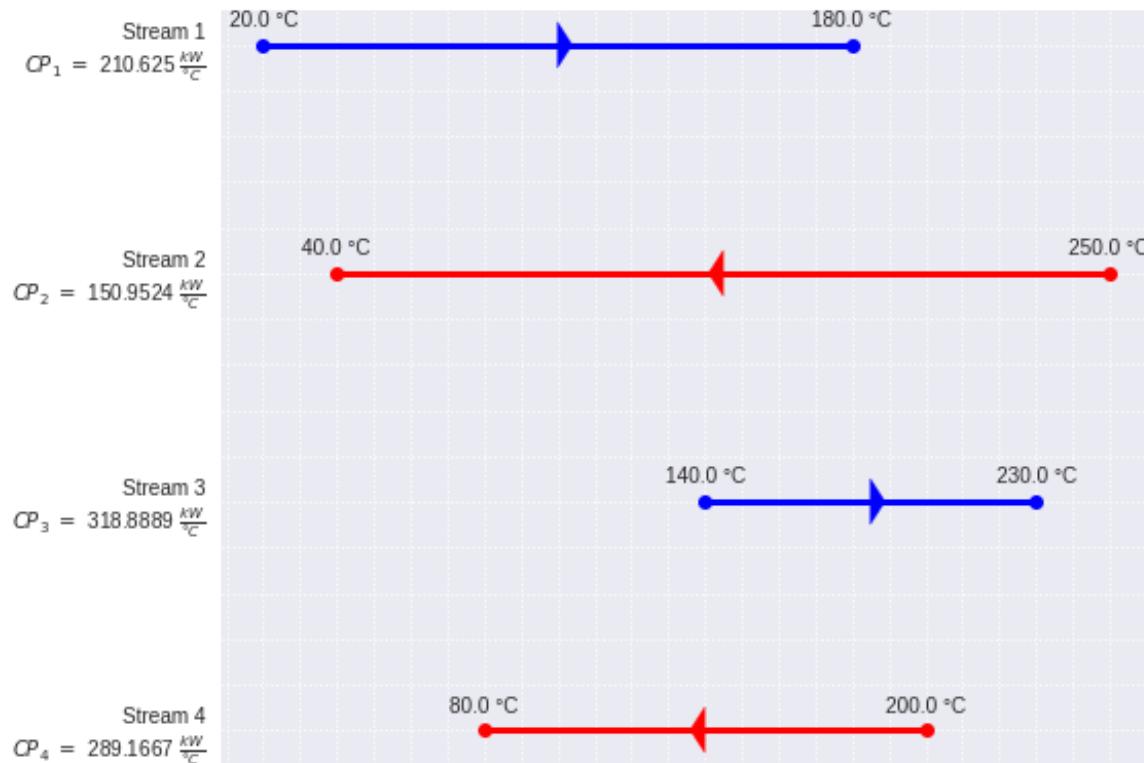
$$\text{Cost} = \text{Raw cost} \times \text{Annuity factor}$$

$$\Rightarrow 230900615.3 \times 3.791 = \text{Rs } 87534232.71 / \text{year}$$

$$\text{Total Cost} = \text{Rs } 1011759908$$

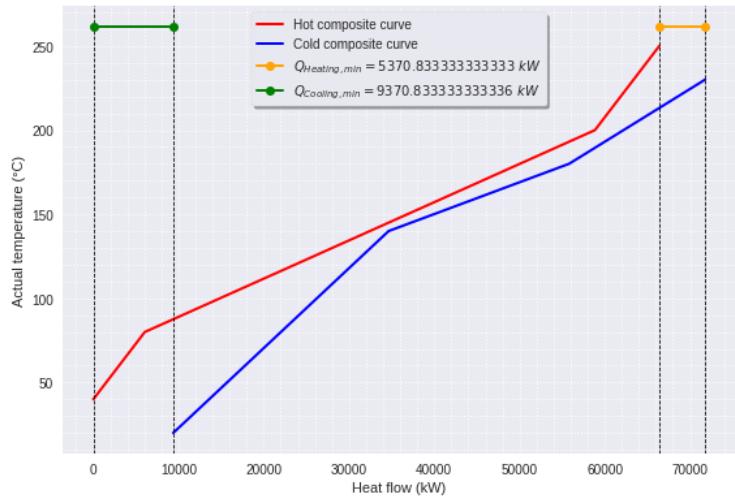
∴ The cost when $\Delta T_{min} = 10^\circ\text{C}$ is more compared to when $\Delta T_{min} = 20^\circ\text{C}$

Stream Information	Supply Temperature (°C)	Target Temperature (°C)	Heat Load (MW)
Stream 1	20	180	33.7
Stream 2	250	40	-31.7
Stream 3	140	230	28.7
Stream 4	200	80	-34.7

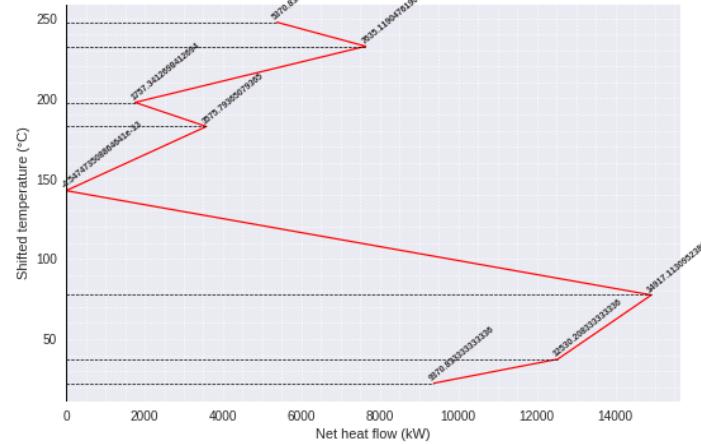


For $\Delta T_{\min} = 5^{\circ}\text{C}$

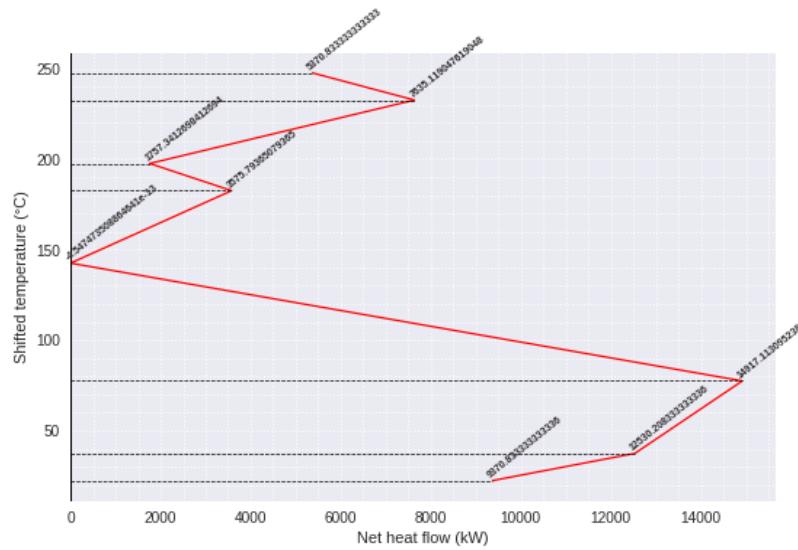
Composite Curve



Grand Composite Curve

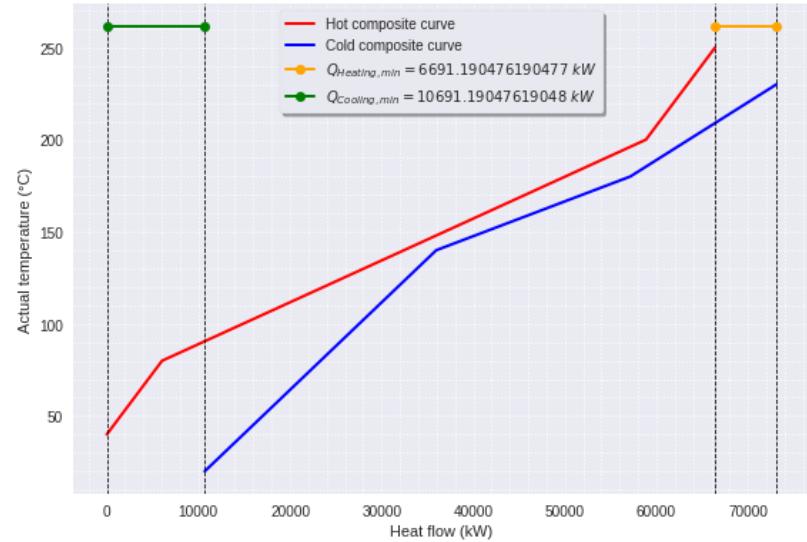


Intervals

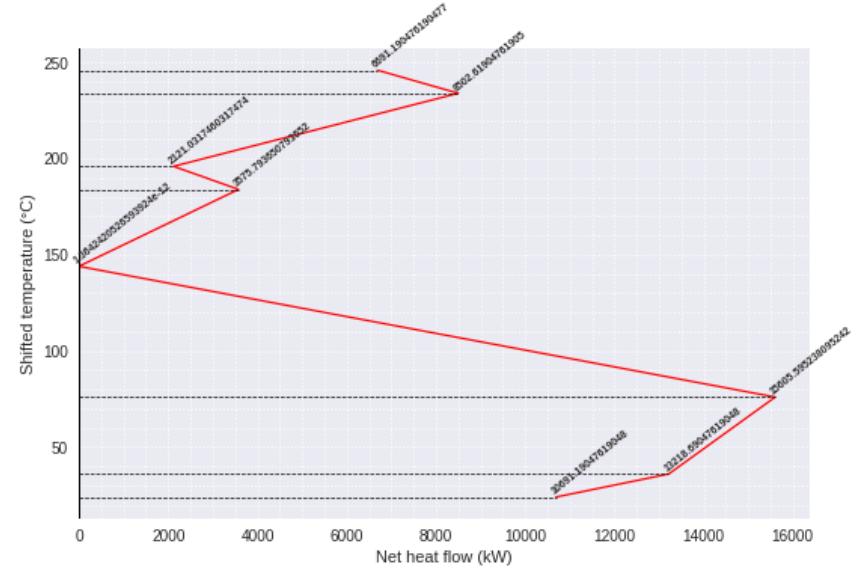


For $\Delta T_{\min} = 8^{\circ}\text{C}$

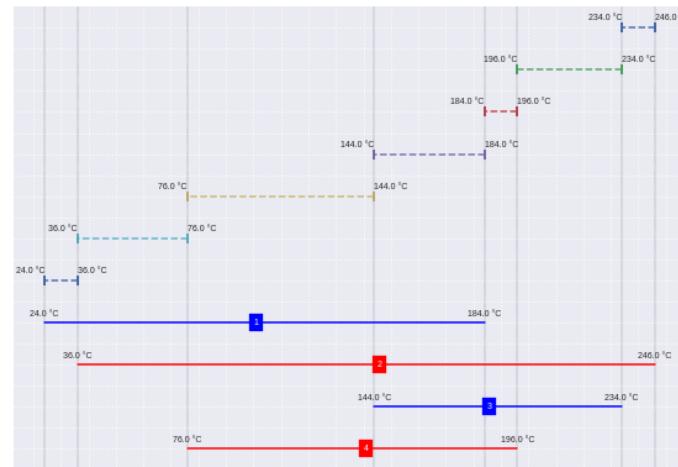
Composite Curve



Grand Composite Curve

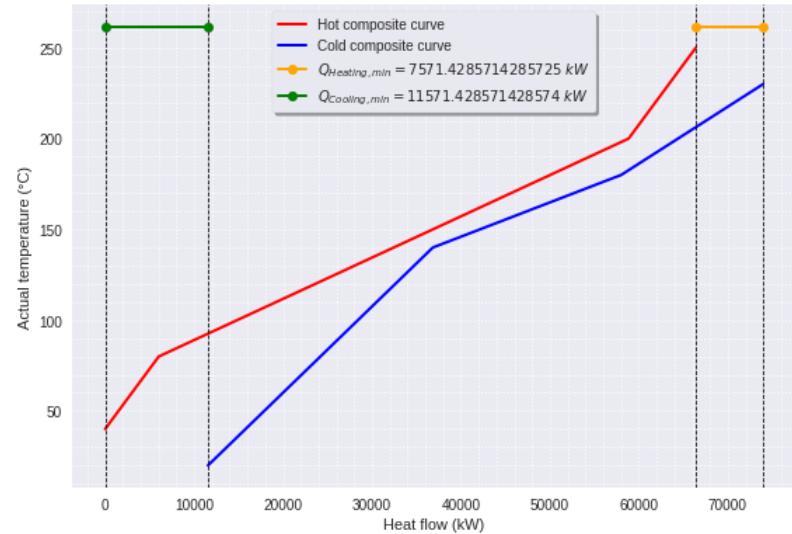


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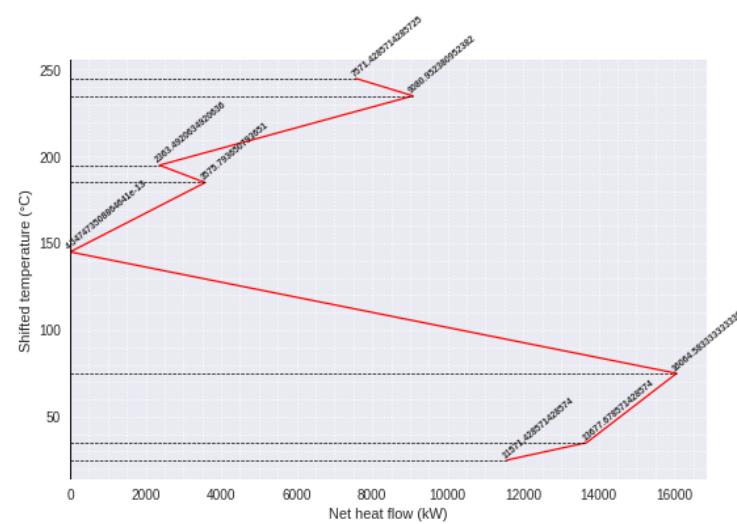


For $\Delta T_{min} = 10^{\circ}\text{C}$

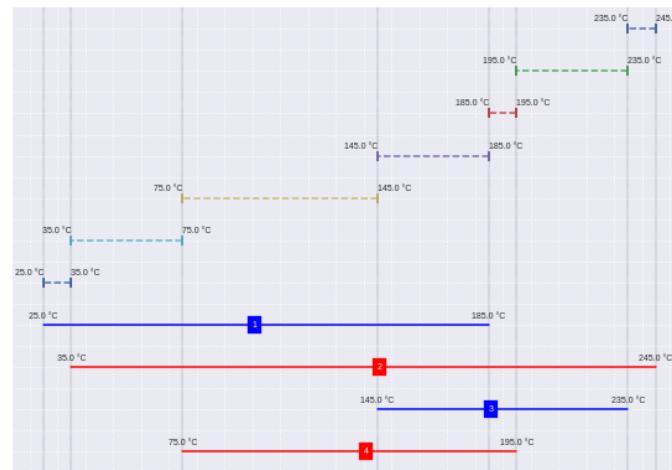
Composite Curve



Grand Composite Curve

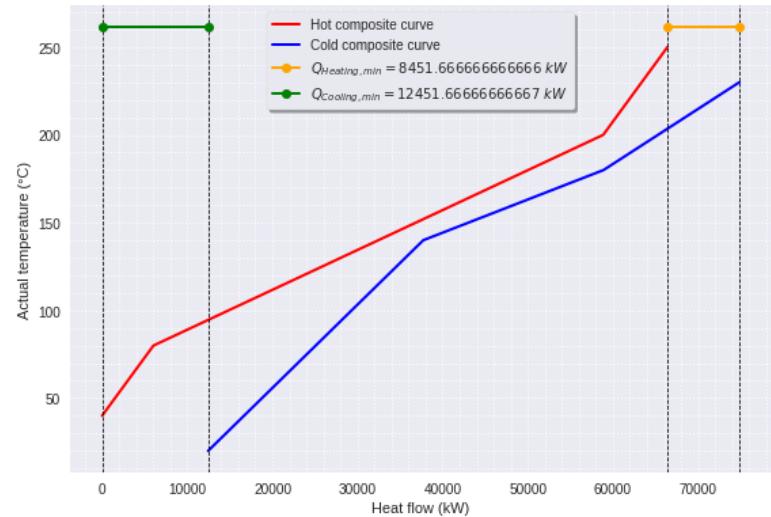


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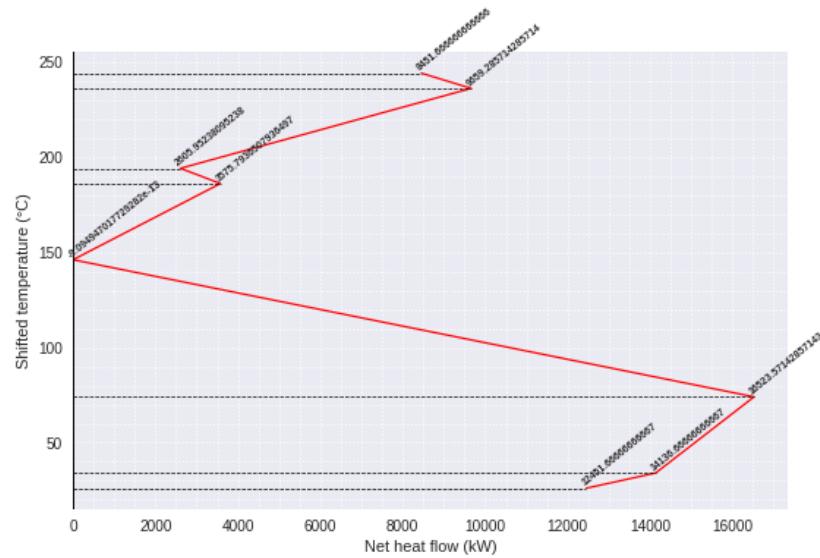


For $\Delta T_{\min} = 12^\circ\text{C}$

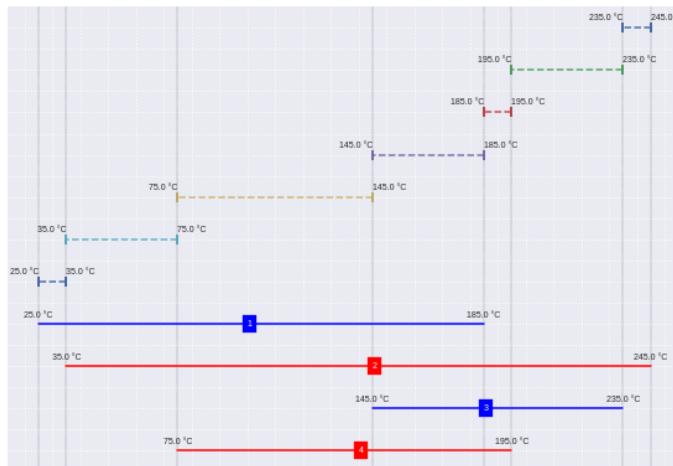
Composite Curve



Grand Composite Curve

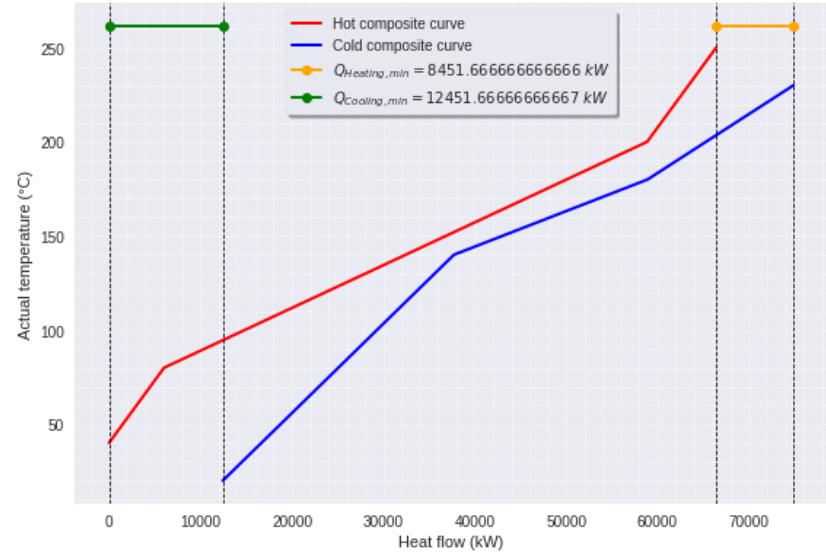


Intervals

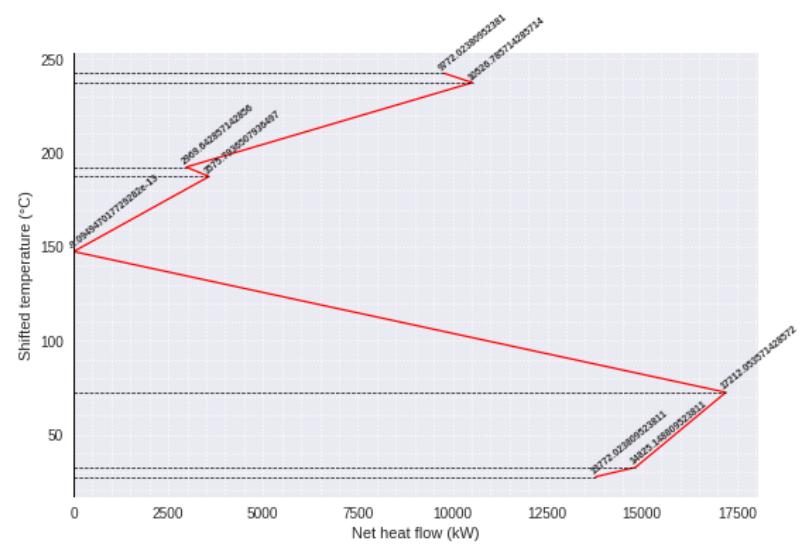


For $\Delta T_{min} = 15^{\circ}\text{C}$

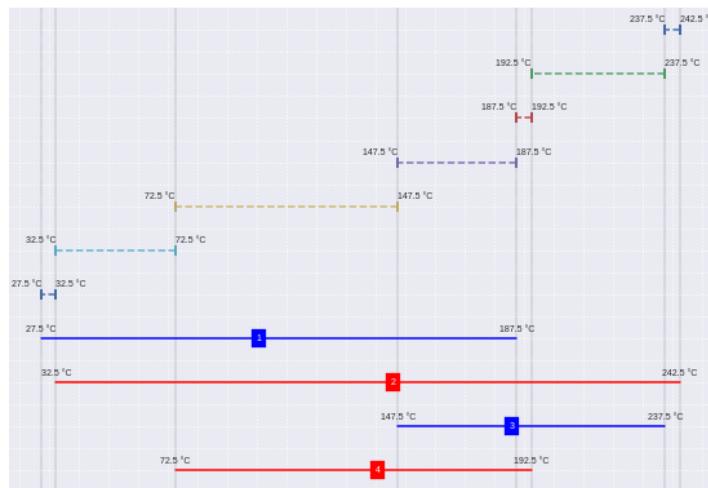
Composite Curve



Grand Composite Curve

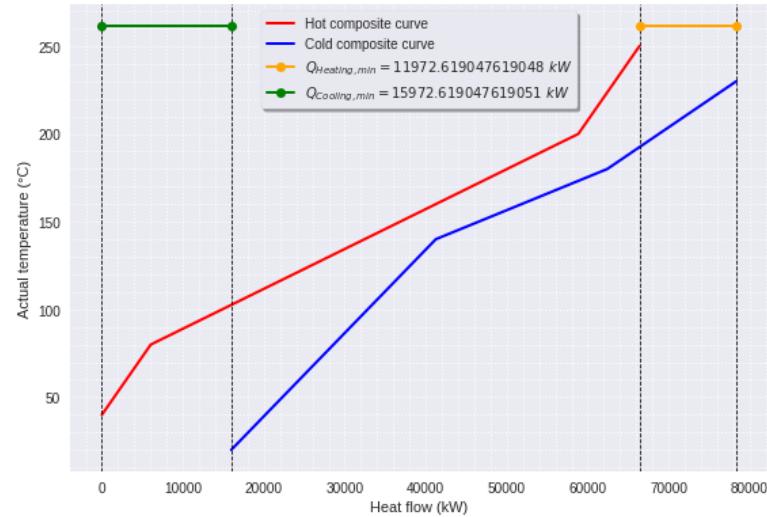


Intervals

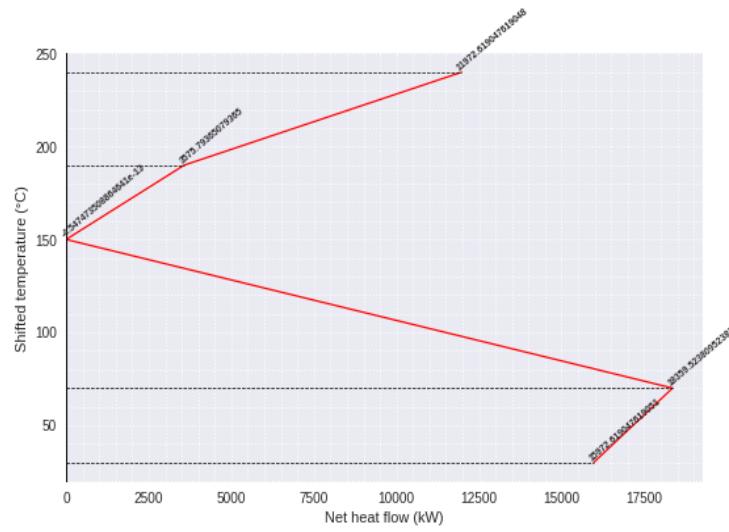


For $\Delta T_{min} = 20^{\circ}\text{C}$

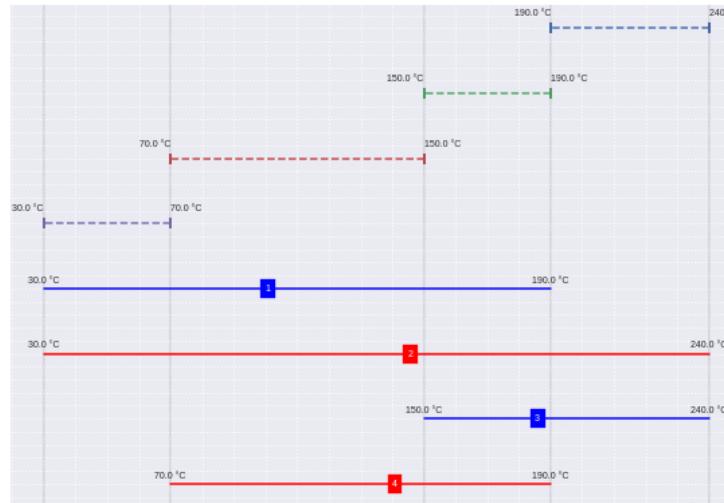
Composite Curve



Grand Composite Curve



Intervals



	$\Delta T_{min} = 10^{\circ}\text{C}$	$\Delta T_{min} = 20^{\circ}\text{C}$
Hot Utility target	7.6	12
Cold Utility target	11.52	16
Area Target	7877.51	8037.64
Amount for Steam Utility	7550442.48	90605309.76
Amount for Water Utility	2863147.84	4581036548
Annuity Cost	1204615371	875344232.7
Total Cost	1294602197	1011759908

Discussion

As we can see that the hot and cold utility requirement are less for $\Delta T_{min} = 10^{\circ}\text{C}$ as compared to $\Delta T_{min} = 20^{\circ}\text{C}$ this is because the overlap of the cold and hot composite curve is more for $\Delta T_{min} = 10^{\circ}\text{C}$ on temperature vs ΔH plot as shown earlier. So we can conclude that as T_{min} increases, effective heat transfer through the heat exchanger decreases, hot and cold utility requirements increases.

As we can see that the area required for constructing the heat exchanger is less for $\Delta T_{min} = 20^{\circ}\text{C}$ as compared to $\Delta T_{min} = 10^{\circ}\text{C}$ this is because the fact that area required is inversely proportional to the temperature difference in a given heat exchanger.

Out of the two choices of $\Delta T_{min} = 10^{\circ}\text{C}$ and $\Delta T_{min} = 20^{\circ}\text{C}$, we would prefer $\Delta T_{min} = 20^{\circ}\text{C}$ because the total annualized cost is less for $\Delta T_{min} = 20^{\circ}\text{C}$ and for the effective heat transfer through the heat exchanger the hot stream should be hotter by at least 10 degrees than the cold stream and for our choice it is valid.

Resources

- 1) Process Heat Transfer Principles and Applications by Robert. W. Sarat
- 2) Process Heat Transfer by D.Q.Kern
- 3) Equipment Sizing and Capital Cost Estimation by Warren D. Seider, University of Pennsylvania
- 4) Chemical Technology An Indian Journal Vol. 11 Issue 2 (2016)
- 5) General Process Plant Cost Estimating (ENGINEERING DESIGN GUIDELINE)
 - a) www.klmtechgroup.com
- 6) Process Equipment Cost Estimation by H.P. Loh, Jennifer Lyons and Charles W. White
- 7) Code Reference - <https://github.com/LuisEduardoCorreaGallego/PinchAnalysis-Console>