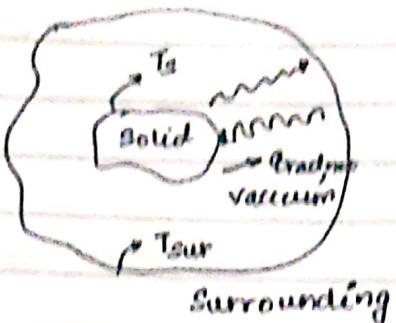
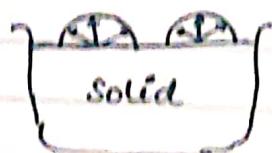


Radiation Heat Transfer

Body at high temp. radiates energy. (Sun \rightarrow Earth)
This heat transfer can be done via space.



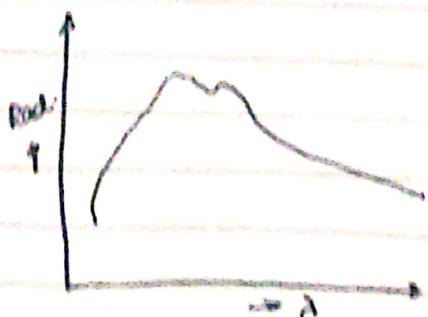
For gases, radiation comes from the volume of gas, while for solids it comes from the surface, as the radiation of the particles inside, gets absorbed by other particles in solid itself.

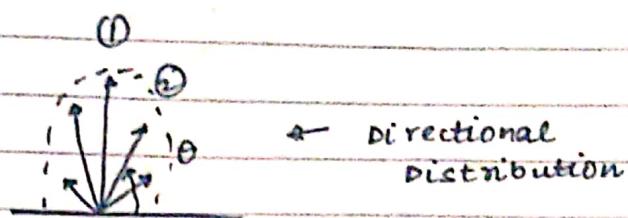


All EMR doesn't cause thermal effect, only those EMR that can cause vibration of molecules.

Distribution of radiation

Spectral Distribution





Intensity of radiation depends on θ , the intensity at ① > intensity at ②, it also depends on λ

Colour depends on which direction we see.

$$\rightarrow I(\theta, \phi, \lambda)$$

Emissive power (E) - Rate at which radiation is emitted from a surface per unit area.

$$E = E_0 \sigma T_e^4$$

→ Stefan Boltzmann const
↳ emissivity

Irradiation (G_i) - Rate at which radiation is incident upon a surface per unit area

$$G_i \leq E$$

Radiosity (J) - Rate at which radiation leaves a surface per unit area

$$J = E + \rho G_i \quad (\text{opaque surface})$$

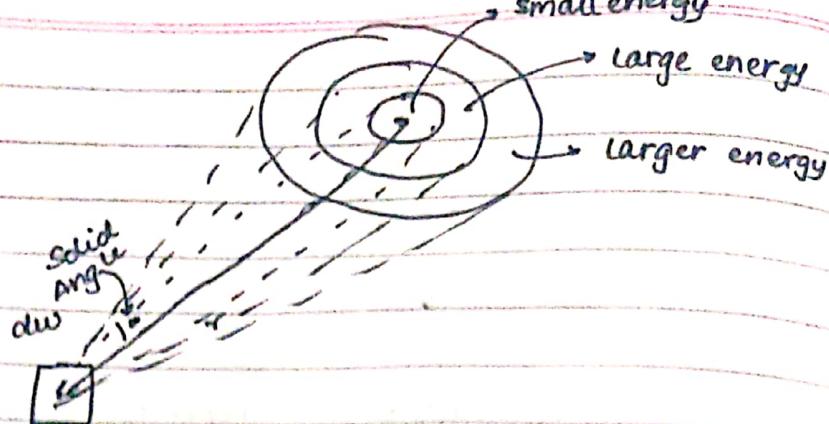
Net radiative Flux ($q_{rad}^{''}$) - Net rate of radiation leaving a surface per unit area.

$$q_{rad}^{''} = \epsilon \sigma T_e^4 - \alpha G$$

$\rho \rightarrow$ reflected
 $\tau \rightarrow$ Transmitted
 $\alpha \rightarrow$ Absorbed

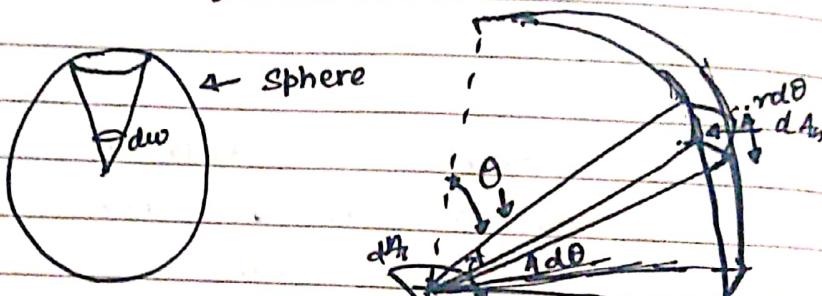
$$\boxed{\tau + \alpha + \rho = 1}$$

classmate
Date _____
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Amount of heat energy received is prop. to the solid angle.

$$dq \propto d\omega$$



$$d\omega = dA/r^2$$

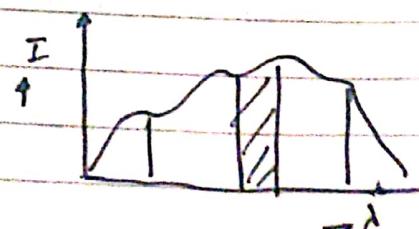
$$d\omega = \frac{dA_n}{r^2}$$

$$+ d\omega = \sin \theta \, d\theta \, d\phi$$

Consider a surface dA_i
Radiation increases with
increase in



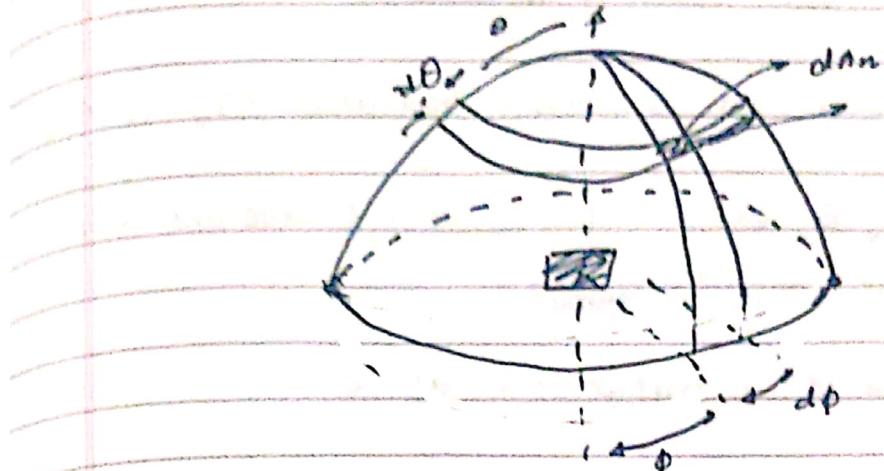
- ① Solid Angle
- ② Area of sheet
- ③ (Projection of Area in the direction of view)
- ④ Range of λ



Projection of
area

 $d\omega_{sr}$

$$d\omega = I_{sr}(\lambda, \theta, \phi) d\omega A_i \cos\theta d\lambda$$



$$d\omega = I_{sr}(\lambda, \theta, \phi) dA_i \cos\theta d\omega d\lambda$$

$$dq_s = \frac{d\omega}{d\lambda} = I_{sr}(\lambda, \theta, \phi) dA_i \cos\theta d\omega$$

$$dq'' = \frac{dq_s}{dA_i} = I_{sr}(\lambda, \theta, \phi) \cos\theta \sin\theta d\theta d\phi$$

Emissive Power

$$E_\lambda(\lambda) = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi/2} I_{sr}(\lambda, \theta, \phi) \cos\theta \sin\theta d\theta d\phi$$

$$E_T = \int_0^\infty E_\lambda(\lambda) d\lambda$$

If emitter is diffused, $I_s(\lambda)$ only

$$E_\lambda(\lambda) = I_s(\lambda) \int_{2\pi}^{\pi/2} \int_0^{\pi} \cos\theta \sin\theta d\theta d\phi$$

$$\Rightarrow \frac{I_s(\lambda)}{2} \int_0^{\pi/2} \int_0^\pi \sin 2\theta d\theta d\phi$$

$$\therefore E = \pi \int I_{\lambda,e}(\lambda) d\lambda \quad \leftarrow \text{Diffused emission}$$

Only for emitted radiation

Intensity of Incident Radiation, $(I_{\lambda,i}(\lambda, \theta, \phi))$

$$G_{\lambda}(\lambda) = \iint_{\text{Hemi}} I_{\lambda,i}(\lambda; \theta, \phi) \cos\theta \sin\theta d\theta d\phi$$

Global

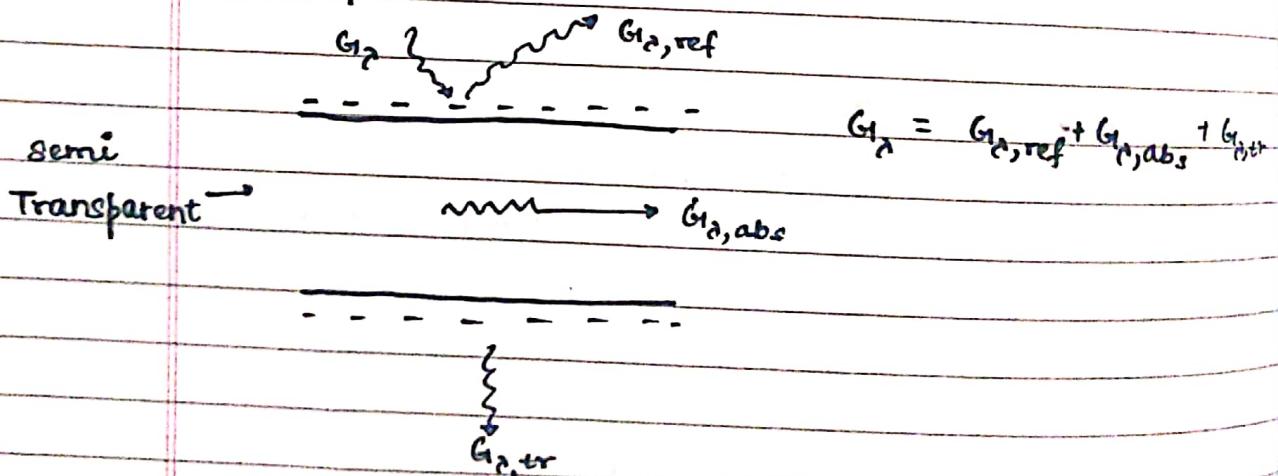
G_{λ} is integrated over all λ

Radio city \rightarrow Combined emitted and reflected radiation observer

$$I_{\lambda,\text{err}}(\lambda, \theta, \phi)$$

$$J_{\lambda}(\lambda) = \iint_{\text{Hemi}} I_{\lambda,\text{err}}(\lambda, \theta, \phi) \cos\theta \sin\theta d\theta d\phi$$

Absorption



$$\text{Absorptivity} = \frac{\underbrace{I_{\lambda,i,\text{abs}}(\lambda, \theta, \phi)}_{\alpha_{\lambda,\theta}(\lambda, \theta, \phi)}}{I_{\lambda,i}(\lambda, \theta, \phi)} = \alpha$$

$$\text{Spectral hemispherical} = \frac{G_{hi,abs}(\lambda)}{G_{hi,i}(\lambda)}$$

Absorptivity
 $(\alpha_i(\lambda))$

Total hemispherical
absorptivity

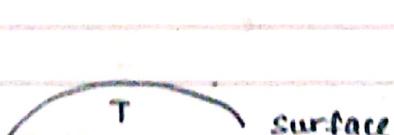
$$\alpha = \frac{\int G_{hi,abs}(\lambda)}{\int G_{hi,i}(\lambda)} = \frac{G_{abs}}{G_{hi}}$$

Similarly we have Transmittivity (τ)
Reflectivity (ρ)

$$\tau + \rho + \alpha = 1$$

$$(\tau_\lambda + \rho_\lambda + \alpha_\lambda = 1)$$

\rightarrow (Medium shouldn't
transmit energy).



$$I_e(0, \lambda, \phi, T)$$

T

If temp isn't const.

Black Body

- > Absorb all incident radiation, irrespective of λ, θ, ϕ
- > For a given λ, T , no surface can emit more radiation than
- > Black body is a diffused emitter

$$I_{\lambda,b}(\lambda, T) = \frac{2h c^2 d^{-5}}{\exp\left(\frac{hc}{kT\lambda}\right) - 1}$$

$h \rightarrow$ Plank's const.

$c \rightarrow$ speed of light

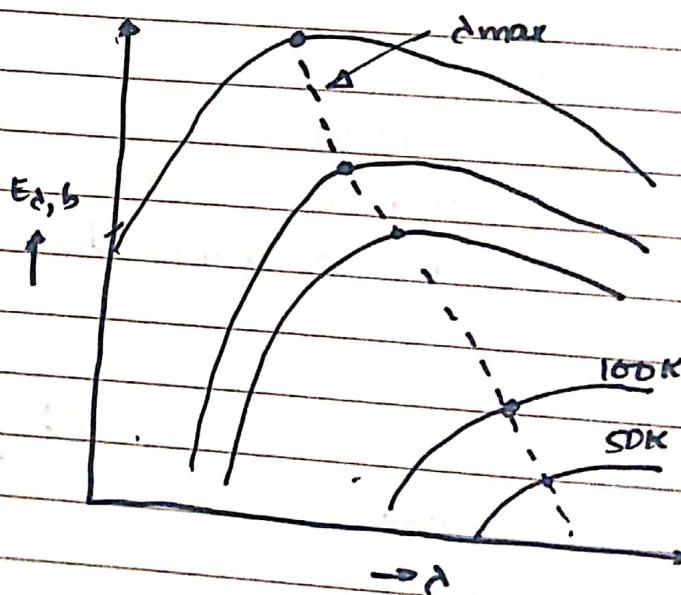
$k \rightarrow$ Boltzmann const.

$$F_{\lambda,b}(\lambda, T) = \pi I_{\lambda,b}$$

$$\text{Emission/Area} = \sigma T^4$$

\hookrightarrow Stephan's boltzmann constant

$$\sigma = 5.67 \times 10^{-8} \text{ W/m}^2\text{K}^4$$



Wein's Displacement law

$$T\lambda_{\max} = c = 2898 \text{ } \mu\text{m K}$$

Emissivity (Real Body)

$$E_{\lambda,\theta}(\lambda, \theta, \phi; T) = \frac{I_{\text{re}}(\lambda, \theta, \phi, T)}{I_{\text{rb}}(\lambda, T)}$$

Spectral directional
Emissivity

Total directional Emissivity

$$\epsilon_{\theta,\lambda}(\theta, \phi, T) = \frac{I_e(\theta, \phi, T)}{I_b(T)}$$

Spectral hemispherical emissivity

$$\epsilon_\lambda(\lambda, T) = \frac{E_a(\lambda, T)}{E_{\lambda,b}(\lambda, T)}$$

Total Hemispherical Emissivity

$$\epsilon(T) = \frac{\epsilon(T)}{E_b(T)}$$

Compare radiative and neutral convective
flux from a horizontal flat plate 1m^2 once
when the plate is at temp 350K and then
for 700K. The emissivity is 0.8, Ambient
temp. 300K

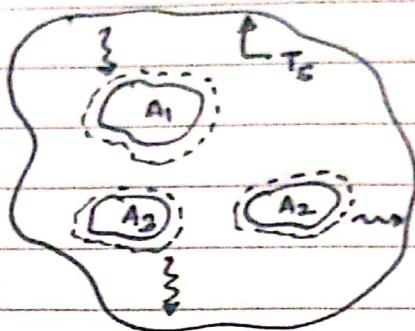
A)

$$\begin{aligned} E_{\lambda,b} &= \sigma A T^4 & q_s &= h (T_s - T_a) \\ &= 5.67 \times 10^{-8} \times 1 \times 350^4 & &= 290 \text{ W/m}^2 \\ &= 255.26 \text{ W/m}^2 \end{aligned}$$

$$\text{At } 700\text{K}, E_{\lambda,b} = 4084 \text{ W/m}^2 \quad q_s = 3389 \text{ W/m}^2$$

Kirchoff's Law

Consider large, isothermal enclosure of surface temperature T_s :



$$G = E_b(T_s)$$

Applying energy balance,

$$\alpha_1 G A_1 - \sigma E_b(T_s) A_1 = 0$$

$$\frac{E_b(T_s)}{\alpha_1} = E_b(T_s)$$

$$\text{Similarly, } \frac{E_b(T_s)}{\alpha_1} = \frac{E_b(T_s)}{\alpha_2} = \dots = E_b(T_s)$$

Major implication from this law, since $\alpha \leq 1$, $E(T_s) \leq E_b(T_s)$. Hence no real surface can have emissive power exceeding that of a black surface at same temperature

$$\frac{E_1}{\alpha_1} = \frac{E_2}{\alpha_2} = \dots = 1$$

Hence, for any surface enclosure,
 $\alpha = E$

For spectral cond.^{diff.}, $\alpha_{\lambda} = E_{\lambda}$

For diff spectral cond. and directions,

$$\alpha_{\lambda, \theta} = \epsilon_{\lambda, \theta}$$

$\epsilon_{\lambda, \theta}$, $\alpha_{\lambda, \theta}$ are inherent surface properties

Gray Surface

$$\epsilon_{\lambda} = \frac{\iint \epsilon_{\lambda, \theta} \cos \theta \sin \theta d\theta d\phi}{\iint \cos \theta \sin \theta d\theta d\phi}$$

$$= \frac{\iint \alpha_{\lambda, \theta} I_{\lambda, i} \cos \theta \sin \theta d\theta d\phi}{\iint I_{\lambda, i} \cos \theta \sin \theta d\theta d\phi} = \alpha_{\lambda}$$

The above is satisfied when

- ① Irradiation ($I_{\lambda, i}$) is independent of θ, ϕ)
- ② $\epsilon_{\lambda, \theta}, \alpha_{\lambda, \theta}$ is independent of θ and ϕ

$$\epsilon = \frac{\int_0^{\infty} \epsilon_{\lambda} E_{\lambda, b} d\lambda}{E_b(T)} = \frac{\int_0^{\infty} \alpha_{\lambda} G_{\lambda}(T) d\lambda}{G_1} = \alpha$$

$$\rightarrow G_{\lambda}(T) = \epsilon_{\lambda, b}(\lambda, T) \quad \text{and} \quad G_1 = E_b(T)$$

$\alpha_{\lambda}, \epsilon_{\lambda}$ are independent of λ (Gray surface)

$$\therefore \varepsilon = \frac{\varepsilon_{\lambda,0} \int_{\lambda_1}^{\lambda_2} E(\lambda, T) d\lambda}{G} = \varepsilon_{\lambda,0}$$

$$\alpha = \frac{\alpha_{\lambda,0} \int_{\lambda_1}^{\lambda_2} G_p(\lambda) d\lambda}{G} = \alpha_{\lambda,0}$$

Solar Radiation

At the top outer edge of earth's atmosphere, the flux of solar energy is decreased by a factor $(r_s/r_d)^2$

Solar const. → It is defined as flux of solar energy incident on a surface oriented normal to the sun's rays.

$$G_{s,0} = S_c \cdot f \cdot \cos\theta$$

↑
Correction
factor

$$0.97 \leq f \leq 1.03$$

$$d_e = 2r_e = 1.27 \times 10^7 \quad , \quad S_c = 342 \times 4 \text{ W/m}^2$$

$$G_{atm} = \sigma T_{sky}^4$$

↑
effective sky
temp.

$$G_{atm} = 324 \text{ W/m}^2$$

$$T_{sky} = 275 \text{ K}$$

Kirchoff's law

$$\epsilon_{\lambda,\theta} = \frac{I_{\lambda,\theta}(\lambda, \theta, \phi, T)}{I_{\lambda}(\lambda, T)}$$

$$\epsilon_p = \frac{\iint I_{\lambda,\theta}(\lambda, \theta, \phi, T) \cos\theta d\theta \sin\theta d\phi}{\iint I_{\lambda}(\lambda, T) \cos\theta d\theta \sin\theta d\phi}$$

$$\epsilon_T = \frac{E(T)}{E_b(T)}$$

$$\alpha_{\lambda,\theta} = \frac{I_{\lambda,i,abs}(\lambda, \theta, \phi)}{I_{\lambda,i}(\lambda, \theta, \phi)}$$

After solving, we see that,

$$\alpha_{\lambda,\theta} = \epsilon_{\lambda,\theta} \quad \text{Surface need not be diffused}$$

For this course, we consider, $\alpha = E$

(under such
certain assumptions)

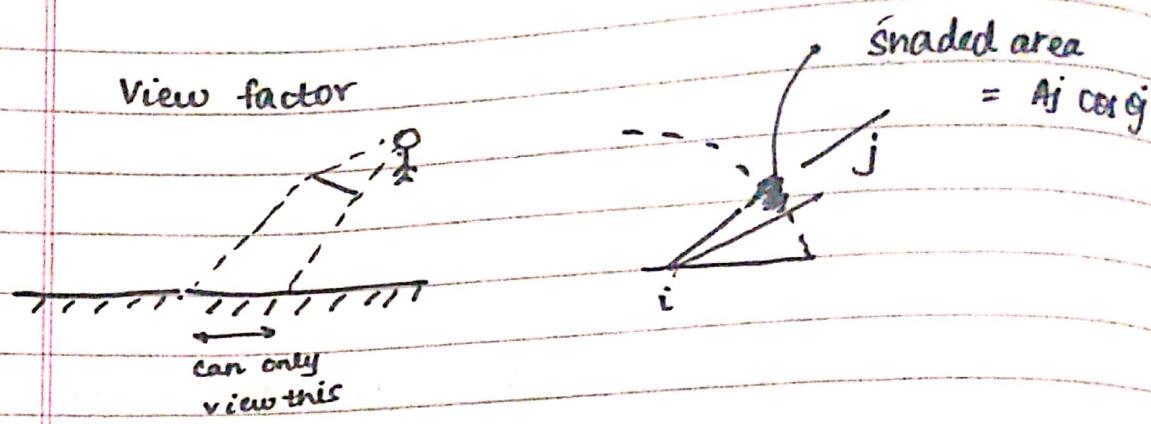
If the incident radiation is diffused,

then also $\epsilon_p = \alpha$

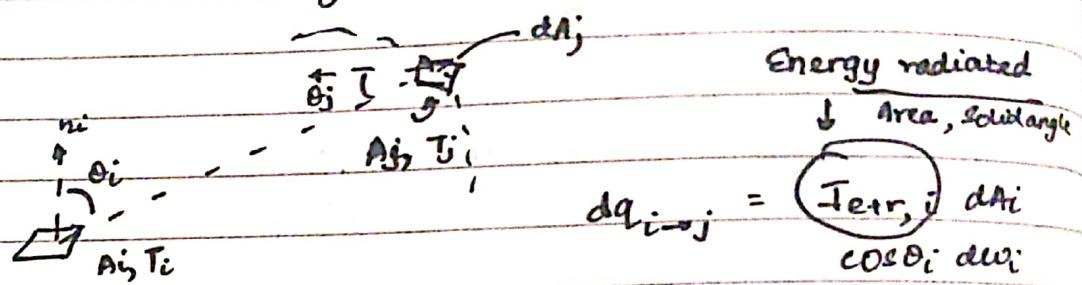
Gray surface - $E = \alpha$ & diffused gray surface

\hookrightarrow Surfaces independent of λ

View factor



Fraction of radiation from i^{th} surface that reaches j^{th} surface



Thus, this depends on $dW = \frac{\text{shaded area}}{R^2}$

(1) dW

$$(2) dA \cos\theta \Rightarrow dW = \frac{\partial A_j \cos\theta_j}{R^2}$$

(3) $d\lambda$

$$\therefore dq_{i \rightarrow j} = I_{err,i} \frac{dA_i \cos\theta_i dA_j \cos\theta_j}{R^2}$$

$$dq_{i \rightarrow j} = \frac{J}{\pi} \frac{\cos\theta_i dA_i \cos\theta_j dA_j}{R^2}$$

$$dW_{i \rightarrow j} = \int \int \frac{J \cos\theta_i \cos\theta_j dA_i dA_j}{\pi R^2}$$

$$dW_{i \rightarrow j} = \frac{J}{\pi} \int \int \frac{\cos\theta_i \cos\theta_j dA_i dA_j}{R^2}$$

↳ Uniform radiosity, emitter, diffuser
(Assumption)?

$$F_{ij} = \frac{q_{ij}}{A_i A_j} = \frac{1}{A_i A_j} \frac{1}{\pi} \iint \frac{\cos \theta_i \cos \theta_j dA_i dA_j}{R^2}$$

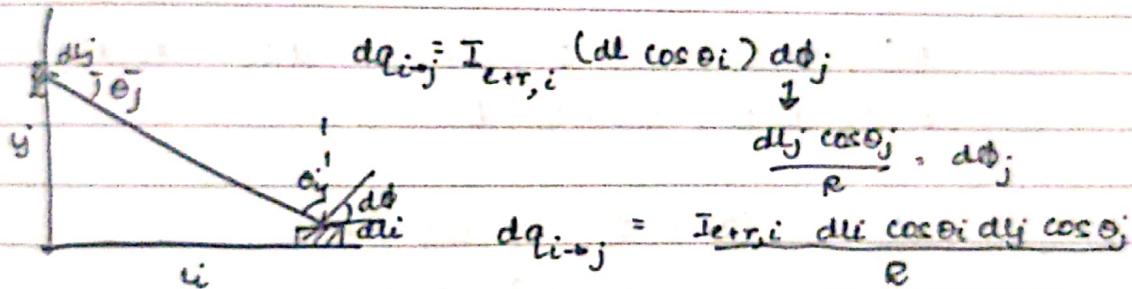
$$\therefore F_{ij} = \frac{1}{A_i \pi} \iint \frac{\cos \theta_i \cos \theta_j dA_i dA_j}{R^2}$$

→ Diffused reflector / emitter

→ Uniform radiosity

$$F_{ij} = \frac{1}{\pi} \iint \frac{\cos \theta_i \cos \theta_j dA_i dA_j}{\pi R^2}$$

$$A_i F_{ij} = A_j F_{ji}$$



$$q_{i-j} = I_{err,i} \iint \frac{\cos \theta_i \cos \theta_j du dv}{R}$$

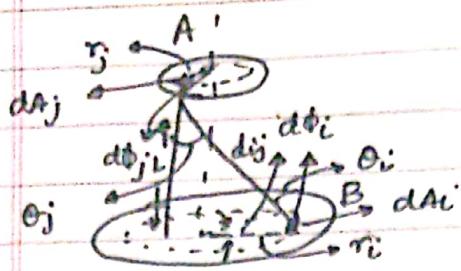
$$F_{ij} = \frac{1}{L_i} \iint \frac{\cos \theta_i \cos \theta_j dL_i dL_j}{R}$$

$$\cos \theta_i \cos \theta_j = \frac{u \cdot y}{(u^2 + y^2)}$$

$$F_{ij} = \frac{1}{L_i} \iint_0^{\pi/2} \frac{u \cdot y du dy}{(u^2 + y^2)^{3/2}}$$

$$= \frac{1}{L_i} (L_i - L_j) - \frac{1}{L_i} \sqrt{L_i^2 + L_j^2}$$

Obtaining view factor by inspection



$$r_j \cdot d\phi_j \cdot dr_j = dA_j$$

$$r_i \cdot d\phi_i \cdot dr_i = dA_i$$

$$\cos\theta = \frac{L}{dij}$$

$$\theta_i = \theta_j$$

$$F_{ij} = \frac{1}{A_i} \iint_{A_i A_j} \frac{\cos\theta_i \cos\theta_j}{\pi (dij)^2} dA_i dA_j$$

$$= \frac{1}{A_i} \iint_{A_i A_j}$$

$$A(r_j \cos\phi_j, r_j \sin\phi_j, L) \quad dA_i = r_i d\phi_i dr_i$$

$$B(r_i \cos\phi_i, r_i \sin\phi_i, 0)$$

$$dij^2 = (r_i \cos\phi_i - r_j \cos\phi_j)^2 + L^2 + (r_i \sin\phi_i - r_j \sin\phi_j)^2$$

$$\phi_j = 2\pi - \phi_i$$

$$F_{ij} = \frac{1}{\pi R_i^2} \int_0^{2\pi} \int_0^{2\pi} \int_0^L \int_0^{R_j - R_i} \frac{L^2}{\pi (dij^2)^2} d\phi_j d\phi_i dr_j dr_i$$

$$\phi_j = 0 \quad \phi_i = 0 \quad r_j = 0 \quad r_j = 0$$

$$dij^2 = r_i^2 + r_j^2 + L^2 - 2r_i r_j \cos(\phi_i - \phi_j)$$

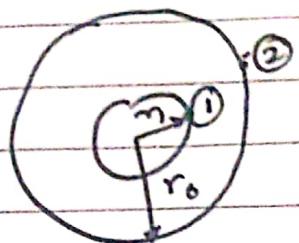
$$q_{\text{net}} = q_{1 \rightarrow 2} - q_{2 \rightarrow 1}$$

$$\text{View factor} = 0.28527$$

$$q_{\text{net}} = 0.28 \times \sigma T_1^4 \times A_1$$

$$= 0.28 \times \sigma T_2^4 \times A_2$$

$$= 18.4 \text{ kW}$$



We have four view factors, $F_{11}, F_{12}, F_{21}, F_{22}$

$$\sum_j F_{ij} = 1, \quad A_i F_{ij} = A_j F_{ji}$$

$F_{11} = 0$ (whatever radiations leaves (1), can't reach (1), it's a convex surface)

$F_{22} \neq 0$ (concave surface)

$$F_{11} + F_{12} = 0 \Rightarrow F_{12} = 1$$

$$F_{21} = \frac{r_i^2}{r_o^2} \quad F_{22} = 1 - \frac{r_i^2}{r_o^2}$$

we assume this to be an open black surface, as the radiation that

Open surface

Encloser : $q_i = \text{Net amount of energy leaving surface } i$

$$q_i = A_i (J_i - G_i)$$

$$J_i = E_i + \rho_i G_i = E_i E_{bi} + (1 - \epsilon_i) G_i$$

$$= E_i E_{bi} + (1 - E_i) G_i$$

$$\frac{J_i - \epsilon_i E_{bi}}{1 - \epsilon_i} = G_i$$

$$q_i = A_i \left(\frac{E_{bi} - J_i}{(1 - \epsilon_i) / \epsilon_i} \right)$$

$$A_i G_i = \sum F_{ji} A_j T_j$$

$$= \sum_{j=1}^N A_i F_{ij} T_j$$

$$G_i = \sum F_{ij} T_j$$

$$q_i = A_i (J_i - \sum F_{ij} T_j)$$

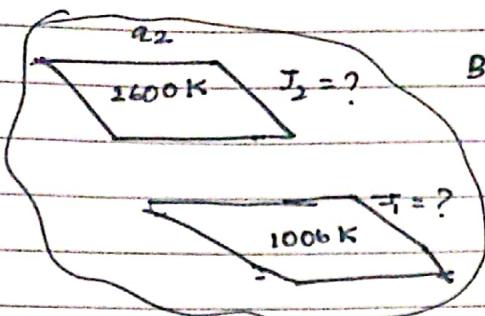
$$= A_i \left(\sum_j F_{ij} (J_i - F_{ij} T_j) \right)$$

$$= A_i \sum_j F_{ij} (J_i - T_j)$$

$$\therefore q_i = \sum A_i F_{ij} (J_i - T_j)$$

$$A_i \frac{E_{bi} - J_i}{(1 - \epsilon_i) / \epsilon_i} = \sum A_i F_{ij} (J_i - T_j) = q_i$$

Radiation exchange b/w opaque, diffuse, grey surfaces forming enclosure.



Black

$$F_{12} = F_{21} = 0.4$$

$$F_{11} + F_{12} + F_{13} = 1.0$$

$$F_{13} = 0.6$$

$$F_{23} = 0.6$$

$$10 J_1 - 0.4 J_2 = 515766$$

$$-0.4 J_1 + 2.0 J_2 = 7624$$

$$J_2 \approx 14 \text{ kW/m}^2$$

$$E_{b2} = 7.34 \text{ kW/m}^2$$

$$q_2 = 10 \left(\frac{7.34 - 14.0}{1 - \epsilon/\epsilon} \right) \approx -67 \text{ kW}$$