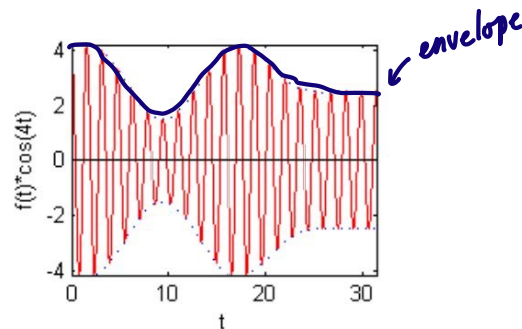
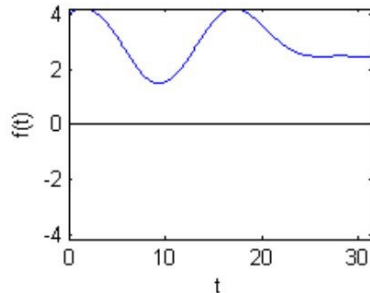


- Envelope detection of AM signals

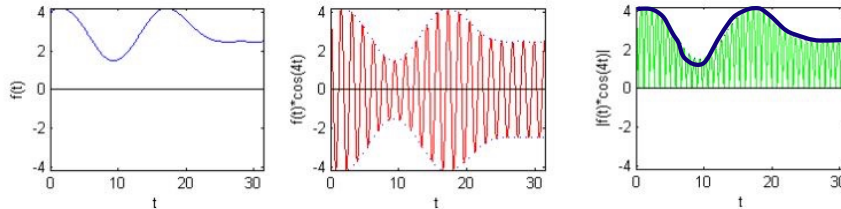


- How to recover the envelope?

full-wave rectifier

$$x(t) = f(t) \cos(\omega_c t) \rightarrow \boxed{|\cdot|} \rightarrow |x(t)|$$

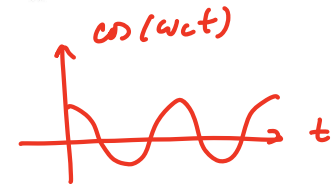
• Envelope detection of AM signals-cont



$|a+b| \neq |a|+|b|$
not linear!

- How to recover the envelope?

$$|x(t)| = \underbrace{f(t)}_{>0} \underbrace{\cos(\omega_c t)}_{\text{assume for now}} = f(t) |\cos(\omega_c t)|$$



$$= \frac{\omega_c}{2} f(t) + \sum_{n=1}^{\infty} c_n f(t) \cos(2n\omega_c t + \theta_n)$$



periodic
 $\omega_0 = 2\omega_c$

$$= \frac{\omega_c}{2} f(t) + \sum_{n=1}^{\infty} c_n f(t) \cos(2n\omega_c t + \theta_n)$$

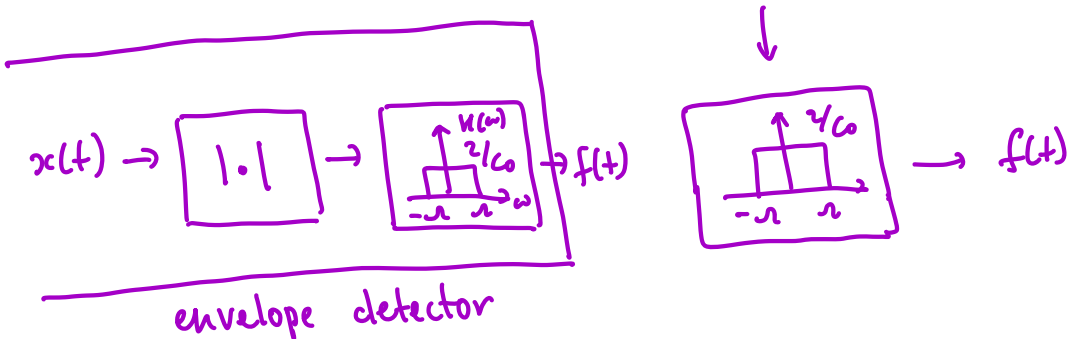
will be filtered out

$$\frac{\omega_c}{2} F(\omega) + \sum_{n=1}^{\infty} c_n \left[\frac{F(\omega - 2n\omega_c) e^{j\theta_n} + F(\omega + 2n\omega_c) e^{-j\theta_n}}{2} \right]$$

• Envelope detection of AM signals-cont

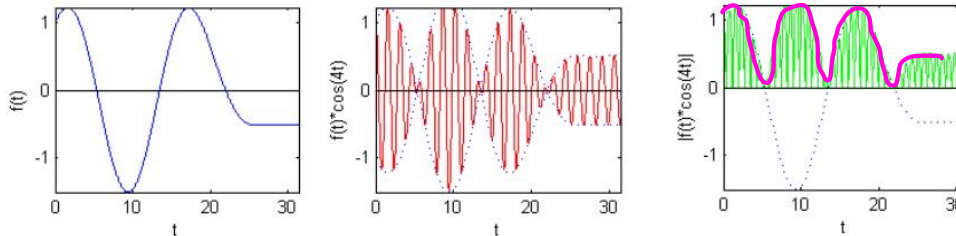
- How to recover the envelope?

$$|x(t)| = g(t) = f(t)|\cos(\omega_c t)| = \frac{c_0}{2} f(t) + \sum_{n=1}^{\infty} c_n f(t) \cos(n2\omega_c t + \theta_n)$$



- Envelope detection of AM signals-cont

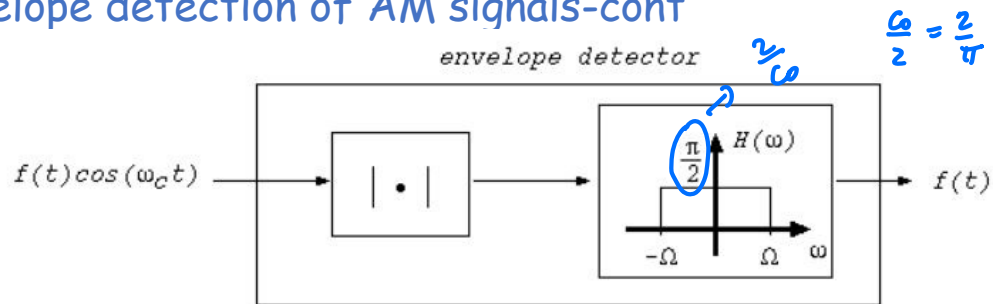
- What if $f(t) \neq 0$?



$$f(t) \rightarrow \begin{matrix} \text{⊕} \\ \uparrow \\ \text{DC} \end{matrix} \rightarrow \begin{matrix} \text{⊗} \\ \uparrow \\ \omega_c t \end{matrix} \rightarrow \dots$$

- Envelope detection of AM signals-cont
 - What if the channel is not ideal, e.g. time delay?

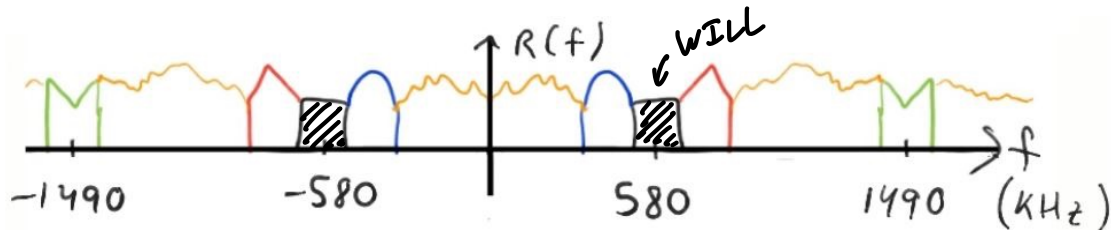
- Envelope detection of AM signals-cont



- It is not linear!

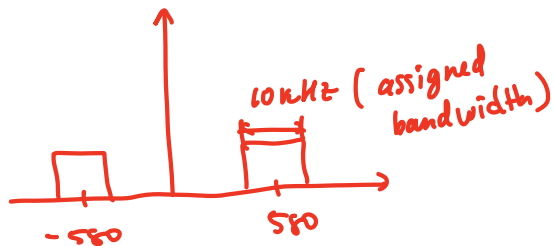
- Superheterodyne AM receiver with envelope detection

- Real wireless transmission has signals across a broad frequency spectrum:



- For envelope detection to work, need to isolate signal, how?

Need to get our signal by itself, so that envelope detection works.



A BPF would achieve this, but needs to be selective and tunable \Rightarrow expensive!

We will do it in 3 cheaper steps \smile

• Superheterodyne AM receiver with envelope detection-cont

- Heterodyne: demodulate to a lower carrier frequency

- Typically, $f_{IF} = 455\text{KHz}$ (commercial AM in U.S.)

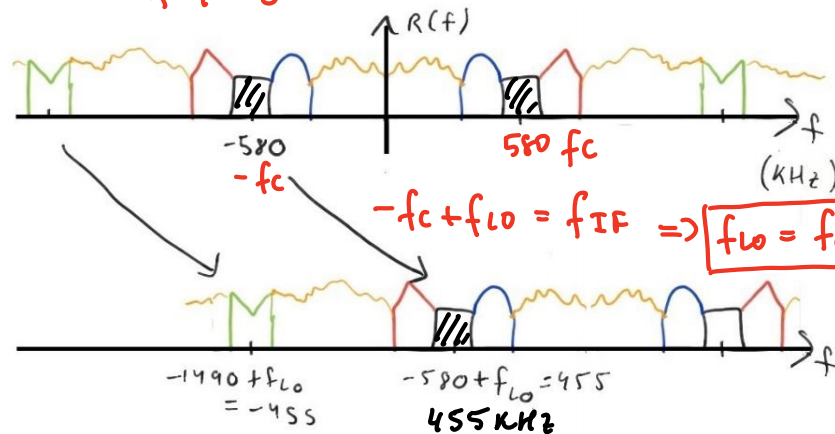
- Problem?

↑ intermediate frequency

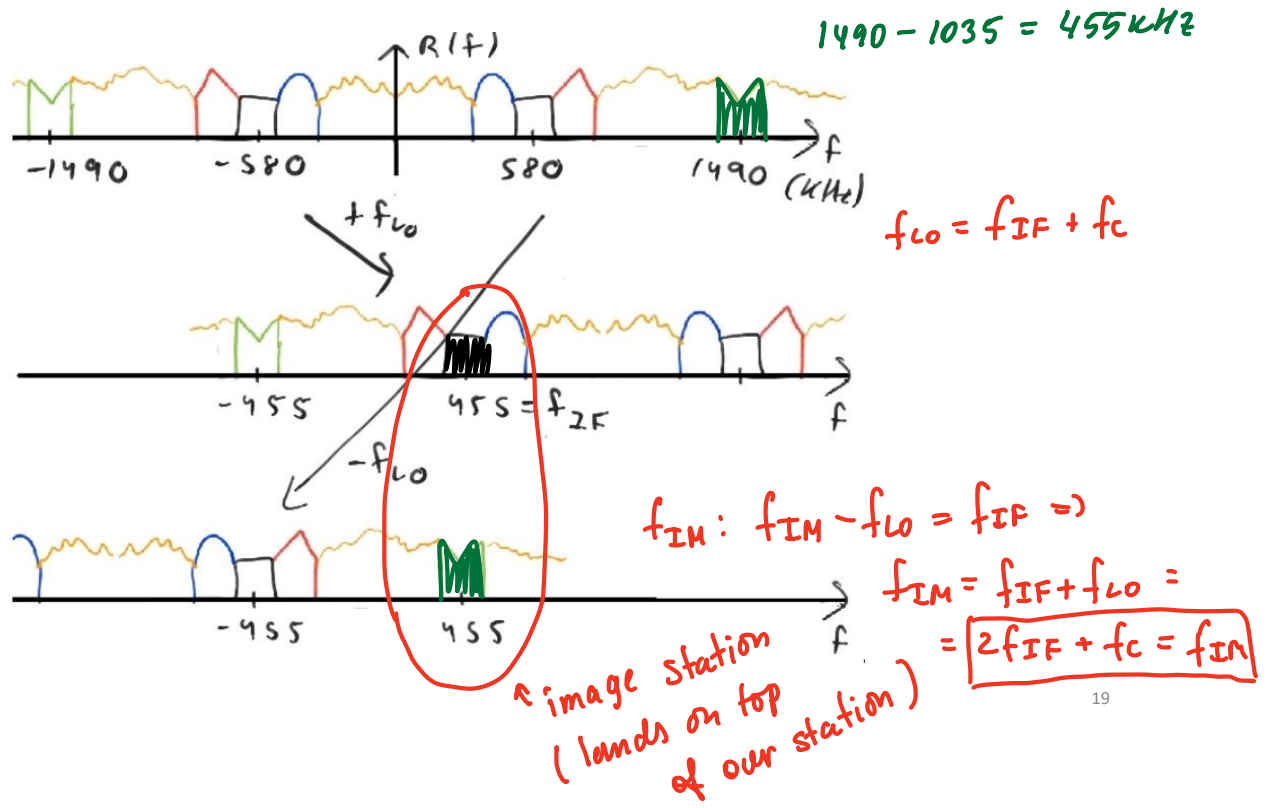
$r(t) \rightarrow \otimes$

↑ $\omega(\omega_{LO}t)$

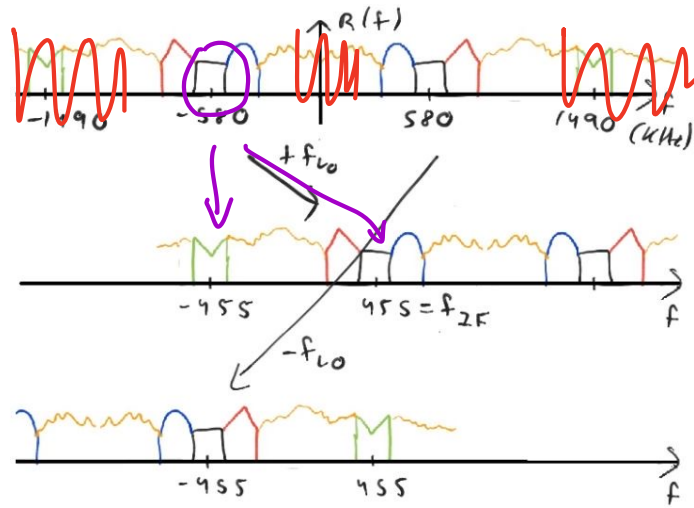
↑ local oscillator



- Superheterodyne AM receiver with envelope detection-cont



- Superheterodyne AM receiver with envelope detection-cont

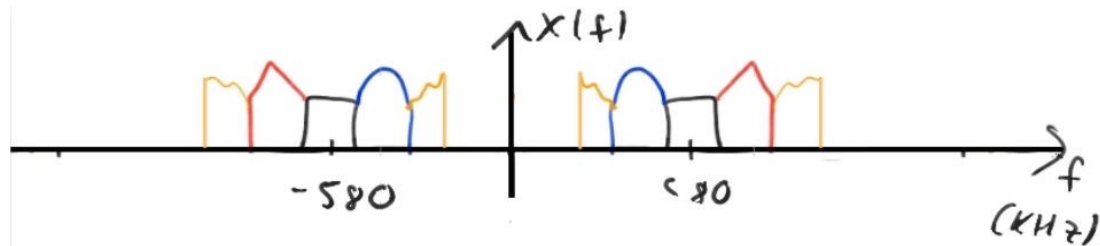


- Image station problem

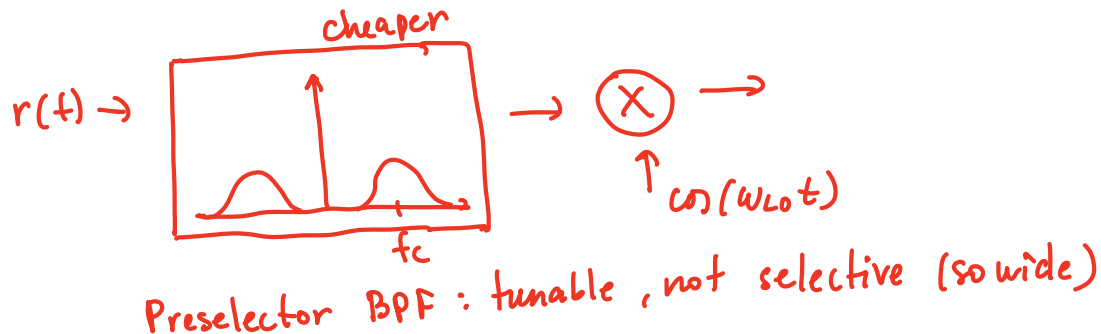
How to fix it? **Preselector BPF**

- Superheterodyne AM receiver with envelope detection-cont

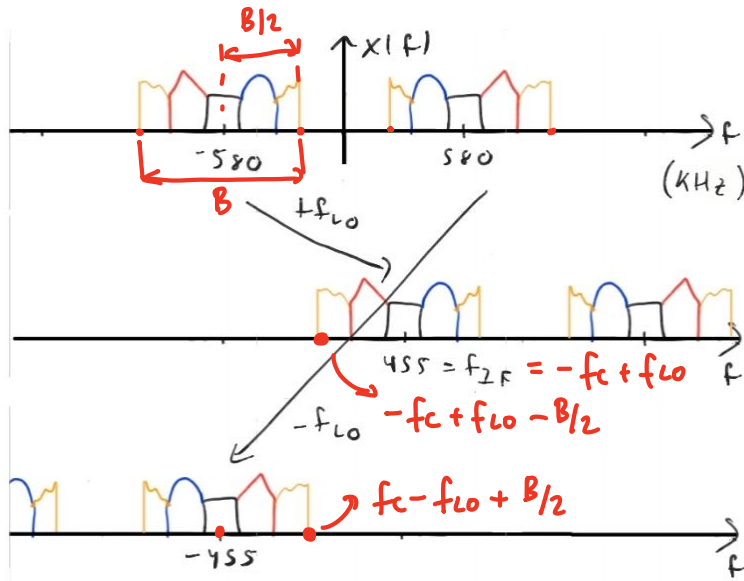
- Real wireless transmission has signals across a broad frequency spectrum:



- Bandwidth of filter?



- Superheterodyne AM receiver with envelope detection-cont



$$f_c - f_{LO} \quad f_c - f_{LO} + \frac{B}{2} < -f_c + f_{LO} - \frac{B}{2} \Rightarrow B < 2 \underbrace{(f_{LO} - f_c)}_{f_{IF}} =$$

$$= 2f_{IF}$$

$$B \approx 1 \text{ MHz} \gg 10 \text{ kHz}$$

• Superheterodyne AM receiver with envelope detection-cont

- Should we use $f_{LO} = f_c + f_{IF}$ or $f_{LO} = f_c - f_{IF}$? high-LO standard

- If we use $f_{LO} = f_c + f_{IF}$ cheaper!

$$f_{LO} \in [995, 2155] \text{ KHz}$$

$$\frac{f_{LO, \max}}{f_{LO, \min}} \approx 2$$

- If we use $f_{LO} = f_c - f_{IF}$

$$f_{LO} \in [85, 1245] \text{ KHz}$$

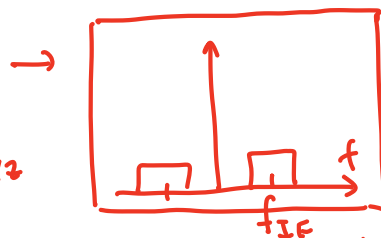
$$\frac{f_{LO, \max}}{f_{LO, \min}} \approx 15$$

↑ more demanding design

Now, signal is at 455 KHz



IF filter



BPF: not tunable,
but very selective

→ ready for
the envelope
detector :