

• Example #1-cont

- Recall

$$|H(\omega)| = \frac{1}{\sqrt{1+(\omega RC)^2}} \quad \angle H(\omega) = -\tan^{-1}(\omega RC)$$

- Determine $v_o(t)$ if $v_i(t) = 2 \cos(3t + \frac{\pi}{3})$

$$v_o(t) = 2 \cdot |H(3)| \cos\left(3t + \pi/3 + \arg(H(3))\right) = 2 \cdot \frac{1}{\sqrt{1+9R^2C^2}} \cos\left(3t + \pi/3 - \tan^{-1}(3RC)\right)$$

- Determine $v_o(t)$ if $v_i(t) = 3 \sin(6t + \frac{\pi}{6}) = 3 \cos(6t + \pi/6 - \pi/2)$

$$v_o(t) = 3 \cdot |H(6)| \cos\left(6t + \pi/6 - \pi/2 + \arg(H(6))\right) =$$

$$= 3 \cdot |H(6)| \sin\left(6t + \pi/6 + \arg(H(6))\right)$$

$$v_o(t) = 3 \cdot |H(6)| \sin\left(6t + \pi/6 + \arg(H(6))\right)$$

- Frequency response of LTI systems-cont

- More generally, for LTI systems with

~~input $f(t) = \operatorname{Re} \{F e^{j\omega t}\}$~~
~~output $y(t) = \operatorname{Re} \{Y e^{j\omega t}\}$~~

We have:

$$Y = FH(\omega)$$

output phasor *input phasor*

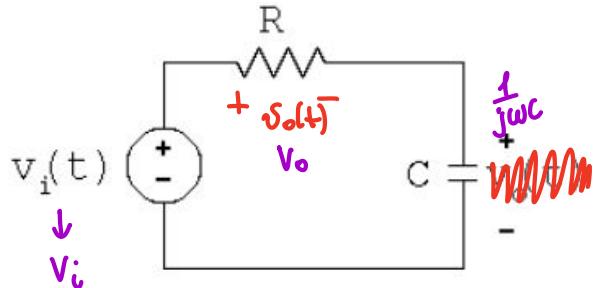
$$F = |F|e^{j(\angle F)}$$

$$Y = |F||H(\omega)|e^{j(\angle F + \angle H(\omega))}$$

$$\begin{aligned} f(t) &\rightarrow \boxed{\text{LTI}} \rightarrow y(t) \\ \downarrow \\ F &\rightarrow \boxed{H(\omega)} \rightarrow Y = F \cdot H(\omega) \\ \downarrow \\ H(\omega) &= \frac{Y}{F} \end{aligned}$$

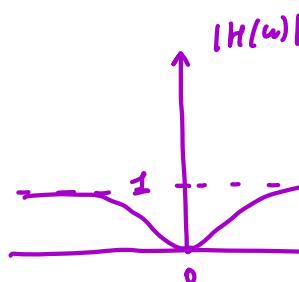
$$\begin{aligned} f(t) &= |F| \cos(\omega t + \angle F) \\ y(t) &= |F||H(\omega)| \cos(\omega t + \angle F + \angle H(\omega)) \end{aligned}$$

• Example #2



$$V_o = V_i \cdot \frac{R}{R + \frac{1}{j\omega C}} = V_i \cdot \frac{j\omega RC}{j\omega RC + 1} \quad H(\omega)$$

$$Y = F \cdot H(\omega)$$

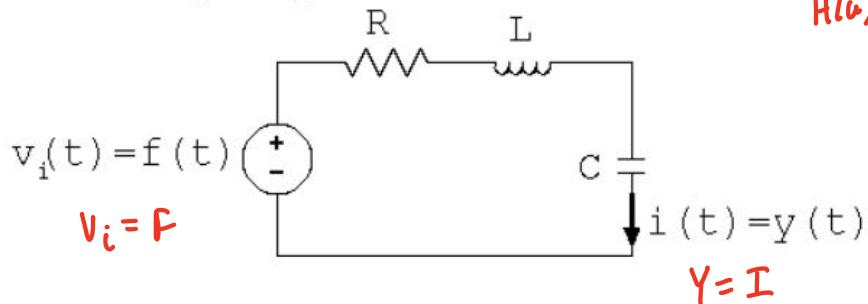


↑
high frequencies
pass through almost
untouched

↓
high-pass
filter

$$H(\omega) = \begin{cases} \pi/2 - \tan^{-1}(wRC) & \text{if } \omega > 0 \\ -\pi/2 - \tan^{-1}(wRC) & \text{if } \omega < 0 \\ 0 & \text{if } \omega = 0 \end{cases}$$

• Example #3



$$H(\omega) = \frac{V}{F} = \frac{I}{V_i}$$

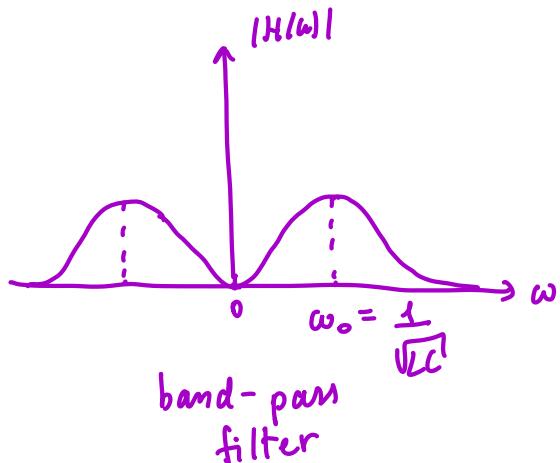
$$I = \frac{V_i}{R + j\omega L + \frac{1}{j\omega C}} =$$

$$= \frac{j\omega C V_i}{j\omega RC - \omega^2 LC + 1}$$

$H(\omega)$

- Let $v_i(t) = A \cos(\omega t + \theta)$
- Determine $H(\omega)$, $|H(\omega)|$ and $\angle H(\omega)$

$$|H(\omega)| = \frac{\omega C}{\sqrt{(1 - \omega^2 LC)^2 + (\omega RC)^2}}$$



• Example #4

- Consider the ODE

$$\frac{dy}{dt} + y = 3f(t)$$

↓ phasors

- Let $f(t) = A \cos(\omega t + \theta)$

- Determine $H(\omega)$, $|H(\omega)|$ and $\angle H(\omega)$

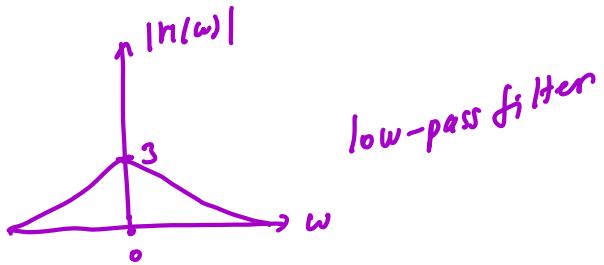
$$H(\omega) = \frac{Y}{F} = \frac{3}{1+j\omega}$$

$$j\omega Y + Y = 3F$$

$$Y = \frac{3F}{j\omega + 1}$$

$$|H(\omega)| = \sqrt{\frac{3^2}{1+\omega^2}}$$

$$\angle H(\omega) = 0 - \tan^{-1}(\omega) = -\tan^{-1}(\omega)$$



- General first-order filters
and second

- Low-pass

$$|H(0)| = 1 \quad |H(\omega)| \approx \frac{1}{\sqrt{1+\omega^2}}$$
$$|H(\infty)| = 0$$

- High-pass

$$|H(0)| = 0 \quad |H(\omega)| \approx \frac{\omega}{\sqrt{1+\omega^2}}$$
$$|H(\infty)| = 1$$

- Band-pass

$$|H(0)| = 0$$
$$|H(\infty)| = 0$$
$$\text{in between } \neq 0$$
$$|H(\omega)| \approx \frac{\omega}{\sqrt{\omega^2 + (1-\omega^2)^2}}$$

- $H(\omega)$ is only meaningful for dissipative LTI systems

- Properties of $H(\omega)$ for real-valued LTI systems

- Conjugate symmetry

$$H(\omega) = H^*(-\omega)$$

$$j\omega L \quad (j(-\omega)L)^* = -j \cdot (-\omega)L = j\omega L$$

- Even amplitude response

$$|H(\omega)| = |H(-\omega)|$$

- Odd phase response

$$\angle H(\omega) = -\angle H(-\omega)$$

$$-\angle H(\omega) = \angle H(-\omega)$$

- Properties of $H(\omega)$ -cont

- Real-valued DC response

$$H(0) \in \mathbb{R}$$

- Steady-state response to complex exponential

$$f(t) = A e^{j(\omega t + \theta)}$$

$\xrightarrow{\quad H(\omega) \quad}$

$$A e^{j(\omega t + \theta)} = y(t)$$