

## • Example #1-cont

- Recall

$$|H(\omega)| = \frac{1}{\sqrt{1+(\omega RC)^2}}$$

$$\angle H(\omega) = -\tan^{-1}(\omega RC)$$

- Determine  $v_o(t)$  if  $v_i(t) = 2 \cos(3t + \frac{\pi}{3})$

$$v_o(t) = 2 \cdot |H(3)| \cos(3t + \frac{\pi}{3} + \angle H(3)) = 2 \frac{1}{\sqrt{1+9R^2C^2}} \cos(3t + \frac{\pi}{3} - \tan^{-1}(3RC)) \text{ V}$$

- Determine  $v_o(t)$  if  $v_i(t) = 3 \sin(6t + \frac{\pi}{6}) = 3 \cos(6t + \frac{\pi}{6} - \frac{\pi}{2})$

$$v_o(t) = 3 \cdot |H(6)| \cos(6t + \frac{\pi}{6} - \frac{\pi}{2} + \angle H(6)) =$$

$$= 3 \cdot |H(6)| \sin(6t + \frac{\pi}{6} + \angle H(6))$$

$$v_o(t) = 3 \cdot |H(6)| \sin(6t + \frac{\pi}{6} + \angle H(6))$$

## • Frequency response of LTI systems-cont

- More generally, for LTI systems with

input  $f(t) = \text{Re} \{ F e^{j\omega t} \}$   
 output  $y(t) = \text{Re} \{ Y e^{j\omega t} \}$

We have:

*output phasor*  
*input phasor*

$$Y = FH(\omega)$$

$$F = |F|e^{j(\angle F)}$$

$$Y = |F||H(\omega)|e^{j(\angle F + \angle H(\omega))}$$

$$f(t) \rightarrow \boxed{\text{LTI}} \rightarrow y(t)$$

$$\downarrow$$

$$F \rightarrow \boxed{H(\omega)} \rightarrow Y = F \cdot H(\omega)$$

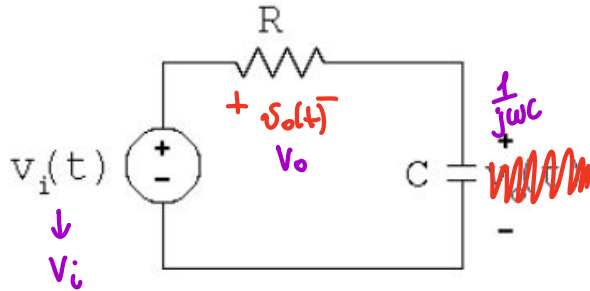
$$\Downarrow$$

$$\boxed{H(\omega) = \frac{Y}{F}}$$

$$f(t) = |F| \cos(\omega t + \angle F)$$

$$y(t) = |F||H(\omega)| \cos(\omega t + \angle F + \angle H(\omega))$$

## • Example #2



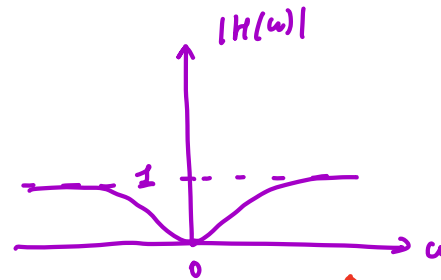
$$V_o = V_i \frac{R}{R + \frac{1}{j\omega C}} = V_i \frac{j\omega RC}{j\omega RC + 1} H(\omega)$$

$$Y = F \cdot H(\omega)$$

- Let  $v_i(t) = A \cos(\omega t + \theta)$
- Determine  $H(\omega)$ ,  $|H(\omega)|$  and  $\angle H(\omega)$

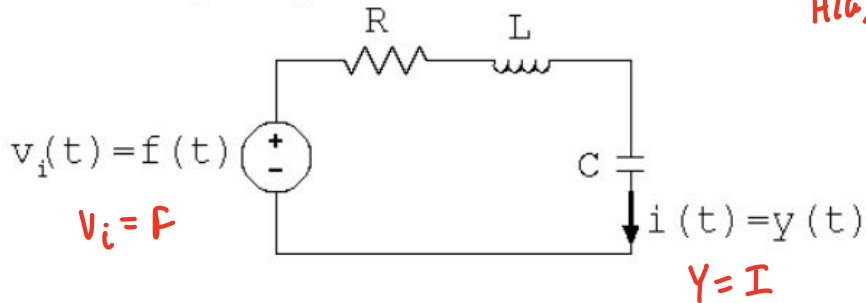
$$|H(\omega)| = \frac{|\omega| RC}{\sqrt{1 + \omega^2 R^2 C^2}}$$

$$\angle H(\omega) = \begin{cases} \pi/2 - \tan^{-1}(\omega RC) & \text{if } \omega > 0 \\ -\pi/2 - \tan^{-1}(\omega RC) & \text{if } \omega < 0 \\ 0 & \text{if } \omega = 0 \end{cases}$$



↑ high frequencies pass through almost untouched  
 ↓ high-pass filter

### • Example #3



$$H(\omega) = \frac{Y}{F} = \frac{I}{V_i}$$

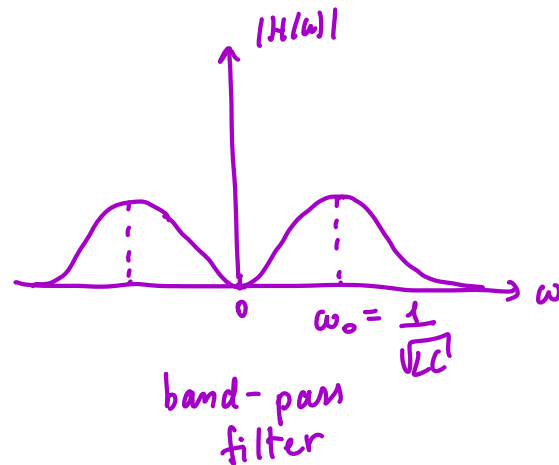
$$I = \frac{V_i}{R + j\omega L + \frac{1}{j\omega C}} =$$

$$= \frac{j\omega C V_i}{j\omega RC - \omega^2 LC + 1}$$

$H(\omega)$

- Let  $v_i(t) = A \cos(\omega t + \theta)$
- Determine  $H(\omega)$ ,  $|H(\omega)|$  and  $\angle H(\omega)$

$$|H(\omega)| = \frac{|\omega| C}{\sqrt{(1 - \omega^2 LC)^2 + (\omega RC)^2}}$$



## • Example #4

- Consider the ODE

$$\frac{dy}{dt} + y = 3f(t)$$

- Let  $f(t) = A \cos(\omega t + \theta)$
- Determine  $H(\omega)$ ,  $|H(\omega)|$  and  $\angle H(\omega)$

$$H(\omega) = \frac{Y}{F} = \frac{3}{1+j\omega}$$

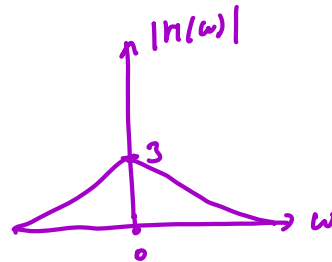
$$|H(\omega)| = \frac{3}{\sqrt{1+\omega^2}}$$

$$\angle H(\omega) = 0 - \tan^{-1}(\omega) = -\tan^{-1}(\omega)$$

↓ phasors

$$j\omega Y + Y = 3F$$

$$Y = \frac{3F}{j\omega + 1}$$



low-pass filter

## • General first-order filters

- Low-pass *and second*

$$|H(0)| = 1$$

$$|H(\infty)| = 0$$

$$|H(\omega)| \approx \frac{1}{\sqrt{1+\omega^2}}$$

- High-pass

$$|H(0)| = 0$$

$$|H(\infty)| = 1$$

$$|H(\omega)| \approx \frac{\omega}{\sqrt{1+\omega^2}}$$

- Band-pass

$$|H(0)| = 0$$

$$|H(\infty)| = 0$$

*in between  $\neq 0$*

$$|H(\omega)| \approx \frac{\omega}{\sqrt{\omega^2 + (1-\omega^2)^2}}$$

- $H(\omega)$  is only meaningful for **dissipative** LTI systems

- Properties of  $H(\omega)$  for real-valued LTI systems

- Conjugate symmetry

$$H(\omega) = H^*(-\omega)$$

$$j\omega L \quad (j(-\omega)L)^* = -j \cdot (-\omega)L = j\omega L$$

- Even amplitude response

$$|H(\omega)| = |H(-\omega)|$$

- Odd phase response

$$\angle H(\omega) = -\angle H(-\omega)$$

$$-\angle H(\omega) = \angle H(-\omega)$$

- Properties of  $H(\omega)$ -cont

- Real-valued DC response

$$H(0) \in \mathbb{R}$$

- Steady-state response to complex exponential

