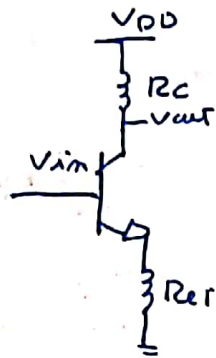
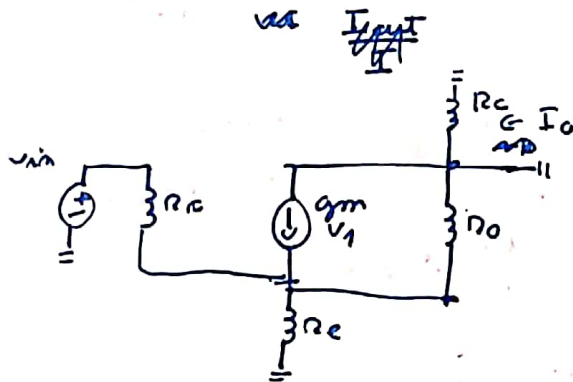


# common emitter degeneration



Transconductance



output node is loaded

$$\frac{I_o}{v_{in}}$$

$$I_o = +g_m v_1$$

$$v_1 = v_{in} - v_A$$

$$I_o = -g_m v_A$$

$$v_A = g_m v_1 R_E$$

$$v_A = g_m v_{in} R_E - g_m v_A R_E$$

$$v_A (1 + g_m R_E)$$

$$v_A = \frac{g_m v_{in} R_E}{(1 + g_m R_E)}$$

$$v_A = \frac{v_A}{g_m R_E}$$

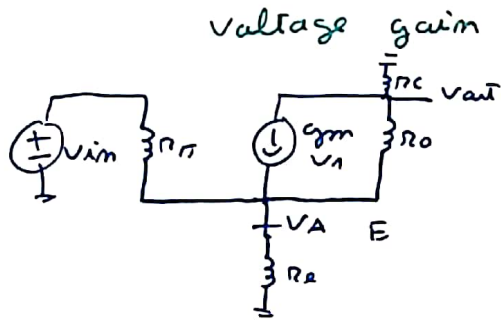
$$I_o = g_m \times \frac{v_A}{g_m R_E} \times g_m$$

$$I_o = g_m \times \frac{v_A}{g_m R_E} \times \frac{g_m v_{in} R_E}{(1 + g_m R_E)}$$

$$\frac{I_o}{v_{in}} \approx \frac{g_m}{(1 + g_m R_E)}$$

Base current is neglected

$$I_B \ll I_C$$



$$-\frac{v_{out}}{R_C} + \frac{v_{in} - v_{out}}{R_E} = \frac{v_A}{R_E}$$

$$-\frac{v_{out}}{R_C} + \frac{v_{in}}{R_E} = v_A \left( \frac{R_E + R_C}{R_E R_C} \right)$$

$$\frac{-v_{out} R_C + v_{in} R_C}{R_C R_E} = v_A \left( \frac{R_E + R_C}{R_E R_C} \right)$$

$$v_A = \frac{-v_{out} R_C R_E + v_{in} R_C R_E}{R_C (R_E + R_C)}$$

sum of currents at  $v_{out}$

$$-g_m v_1 - g_m v_{in} + g_m v_A - \frac{v_{out}}{R_C} + \frac{v_A}{R_E} - \frac{v_{out}}{R_C} = 0$$

$$-v_{out} \left( \frac{1}{R_C} + \frac{1}{R_C} \right) - g_m v_{in} + v_A \left( g_m + \frac{1}{R_E} \right)$$

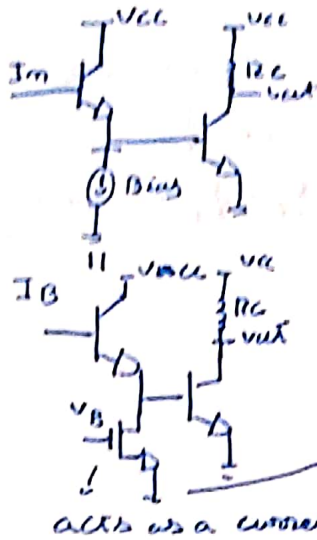
$$-v_{out} \left( \frac{1}{R_C} + \frac{1}{R_C} + \left( g_m + \frac{1}{R_E} \right) \frac{R_C R_E}{R_C (R_E + R_C)} \right) - v_{in} \left( g_m - \left( \frac{1}{R_C} + g_m \right) \frac{R_C R_E}{R_C (R_E + R_C)} \right) = 0$$

$$* \quad A_V = \frac{-g_m R_C (R_E + R_C) + \frac{1}{R_C} + g_m}{\left( \frac{1}{R_C} + \frac{1}{R_C} \right) (R_C (R_E + R_C)) + \frac{1}{R_C} + g_m} \quad \times R_C$$

$$A_V = \frac{-g_m R_C (R_E + R_C) + 1 + g_m R_C}{(R_C + R_C) (R_E + R_C) + 1 + g_m R_C}$$

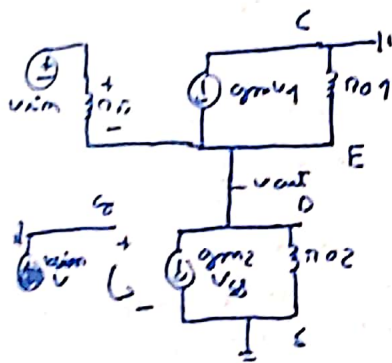
gain equation

Common collector - common emitter



I don't like to use perfect current sources for calculations

1st stage



=

current at  $v_{out}$

$$v_1 = v_{in} - v_{out}$$

$$-\frac{v_{out}}{r_{o2}} + \frac{-v_{out}}{r_{o1}} + g_{m1}v_1 - \frac{v_{out} - v_{in}}{r_{\pi}}$$

$$-\frac{v_{out}}{r_{o2}} - \frac{v_{out}}{r_{o1}} + g_{m1}v_{in} - g_{m1}v_{out}$$

$$-\frac{v_{out}}{r_{\pi}} + \frac{v_{in}}{r_{\pi}} = 0$$

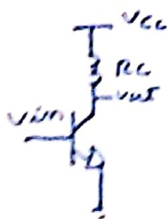
$$v_{in}\left(g_{m1} + \frac{1}{r_{\pi}}\right) = v_{out}\left(\frac{1}{r_{o2}} + \frac{1}{r_{o1}} + g_{m1} + \frac{1}{r_{\pi}}\right)$$

$$\frac{v_{out}}{v_{in}} = \frac{g_{m1} + \frac{1}{r_{\pi}}}{\left(\frac{1}{r_{o2}} + \frac{1}{r_{o1}} + g_{m1} + \frac{1}{r_{\pi}}\right)} = A_{v1}$$

2nd stage

$$\frac{v_{in}}{v_{out1}} = v_{in} A_{v1}$$

$$\frac{v_{out2}}{v_{in}} = A_{v1} \times A_{v2}$$



$$A_{v2} = -g_{m3} \times R_C || R_{o3}$$

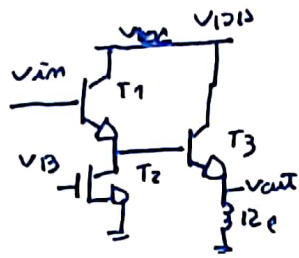
$$A_{v2} = -\frac{g_{m3} R_C R_{o3}}{R_C || R_{o3}}$$

higher Input Resistance

- higher gain
- more complex
- less Bandwidth

$$A_v = \frac{-\left(g_{m1} + \frac{1}{r_{\pi}}\right) g_{m3} R_C R_{o3}}{\left(\frac{1}{r_{o2}} + \frac{1}{r_{o1}} + g_{m1} + \frac{1}{r_{\pi}}\right) (r_{\pi} + r_{o3})}$$

common collector - common collector



1<sup>st</sup> stage analysis

$$A_{V1} = \frac{g_{m1} + \frac{1}{r_{\pi}}}{\left(\frac{1}{r_{\pi}} + \frac{1}{r_{o1}} + g_{m1} + \frac{1}{r_{o2}}\right)}$$

2<sup>nd</sup> stage analysis

$$A_{V2} = \frac{\left(\frac{1}{r_{\pi23}} + g_{m3}\right)}{\left(\frac{1}{r_{L}} + \frac{1}{r_{\pi23}} + \frac{1}{r_{o3}} + g_{m3}\right)}$$

$$A_{V1} \times A_{V2} = \frac{\left(g_{m1} \frac{1}{r_{\pi}}\right) \left(\frac{1}{r_{L}} + g_{m3}\right)}{\left(\frac{1}{r_{\pi}} + \frac{1}{r_{o1}} + g_{m1} + \frac{1}{r_{o2}}\right) \left(\frac{1}{r_{L}} + \frac{1}{r_{\pi23}} + \frac{1}{r_{o3}} + g_{m3}\right)}$$

↓  
Total circuit gain

→ It can be easily observed

That  $A_{V1} \times A_{V2} < 1$

↓  
super Buffer stage  
with high input Impedance  
good to drive loads