

Interaction of matrix cracking and diffuse delamination in cross-ply composites

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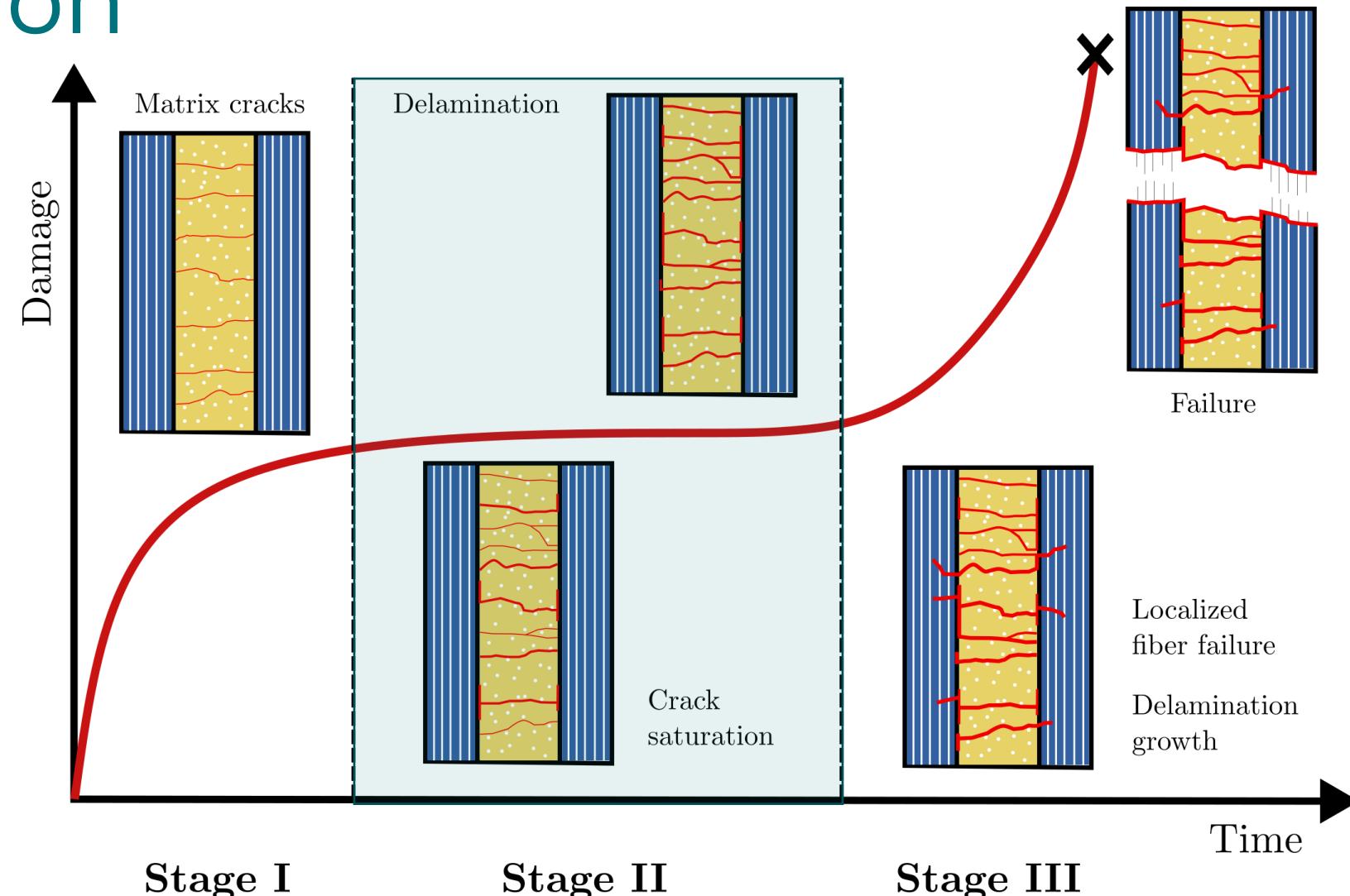


Composites 2025

Move mountains

Motivation

- The damage history from Stage I also influences Stage II, so both stages need to be modelled.

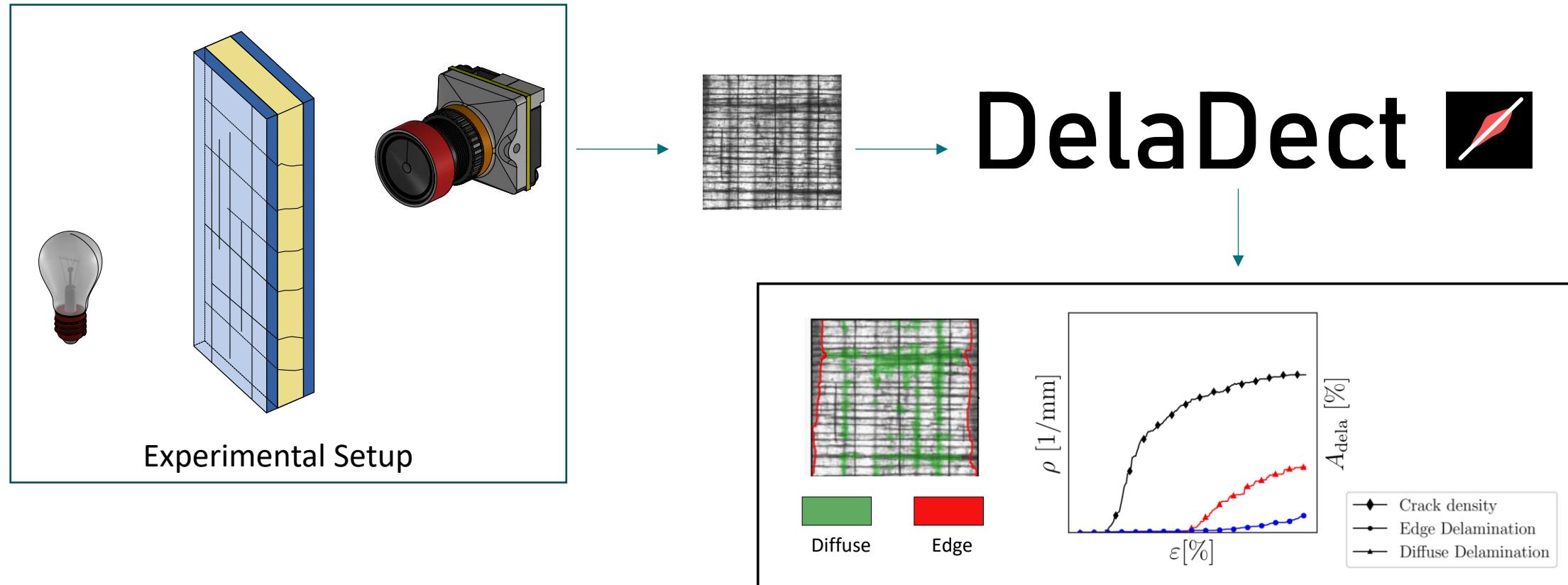


Motivation

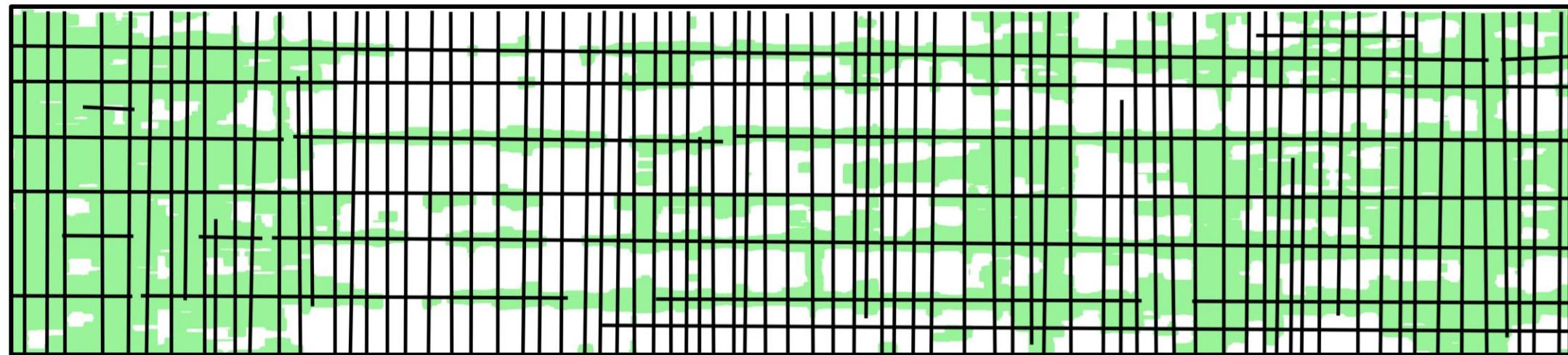
How does matrix cracking influence the onset and progression of delamination in laminates?

- Qualitatively
- Quantitatively (?)

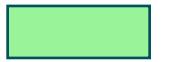
Experimentally, we observed...



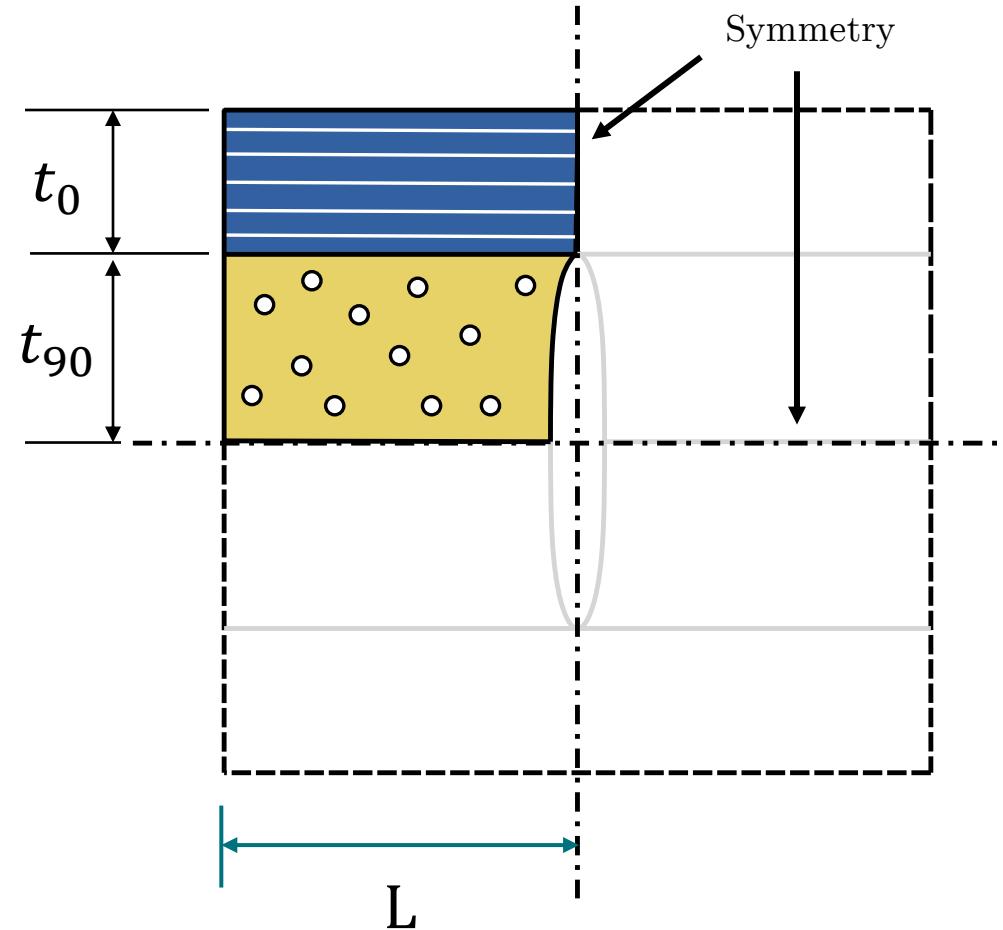
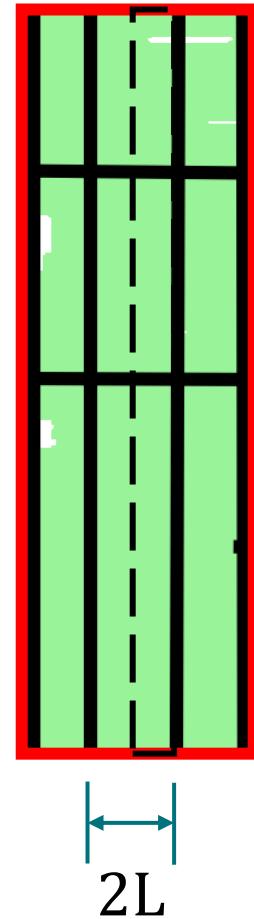
Modelling approach



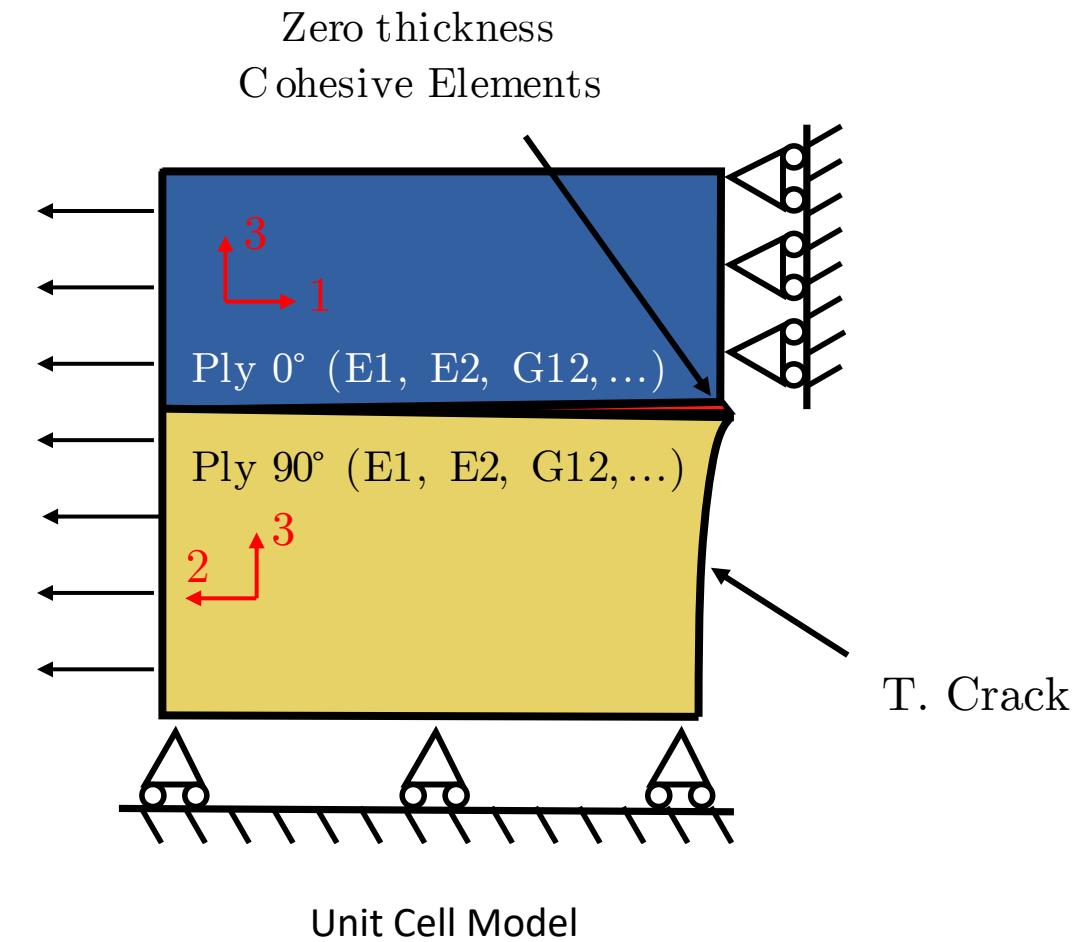
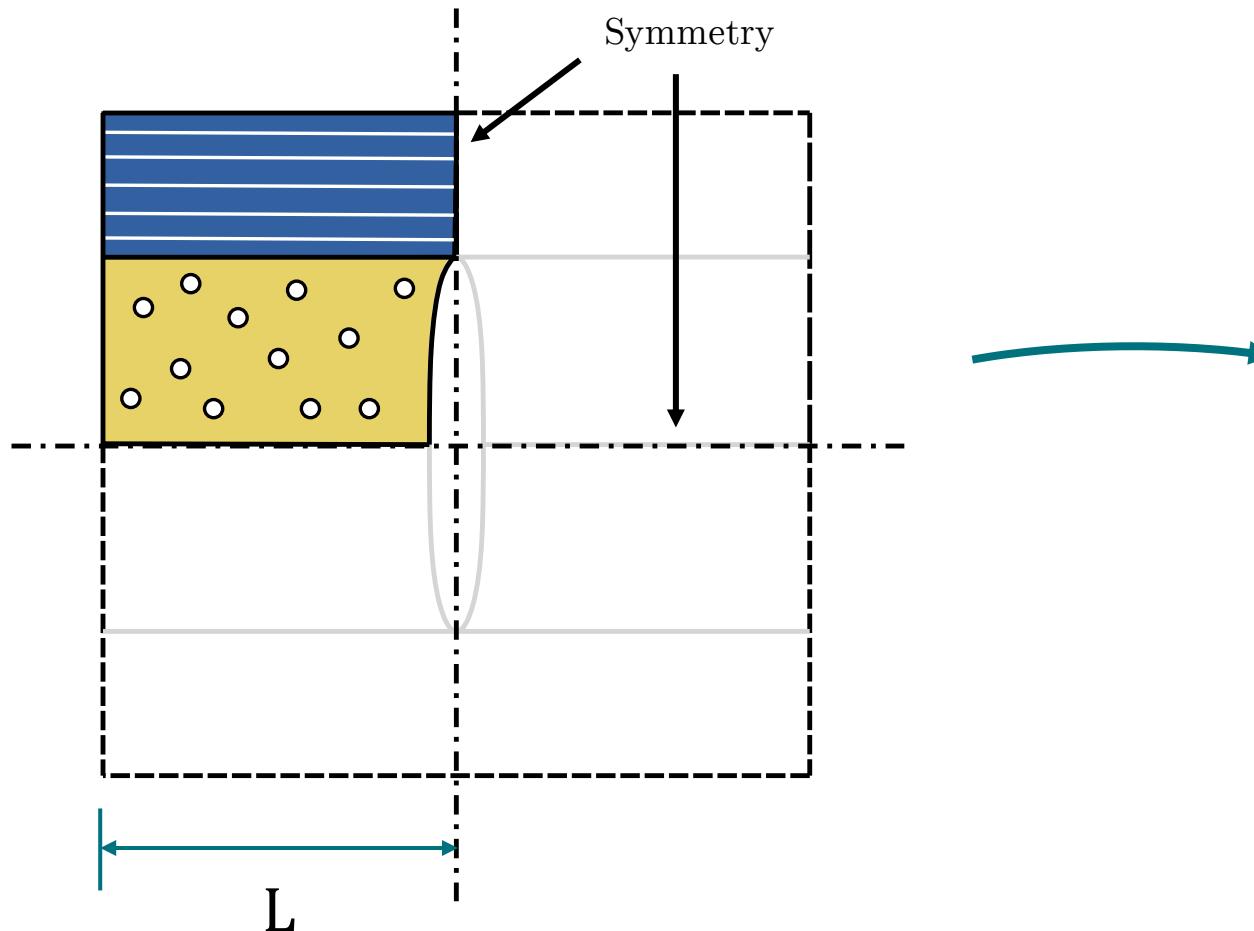
Glass/Epoxy
Cross-ply [0/90₃/0]
Ply thickness = 0.8 mm

 Delamination
 Matrix cracks

Modelling approach



Modelling approach



Modelling approach

Cohesive Settings

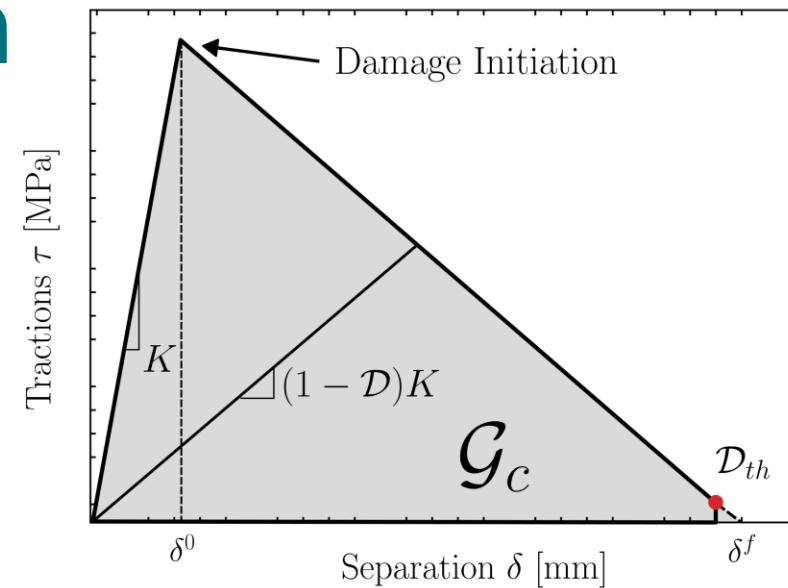
Damage Initiation:

$$\left\{ \frac{\langle \tau_n \rangle}{\tau_n^0} \right\}^2 + \left\{ \frac{\tau_s}{\tau_s^0} \right\}^2 = 1$$

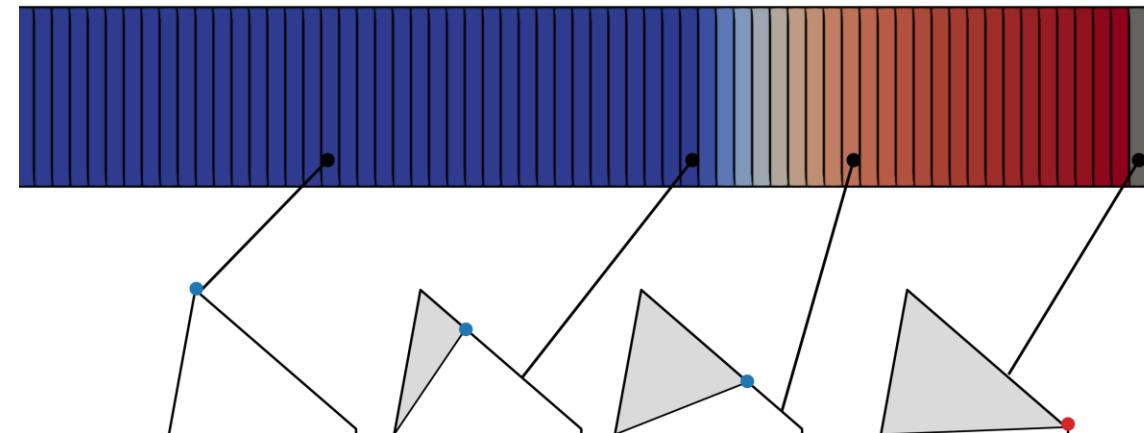
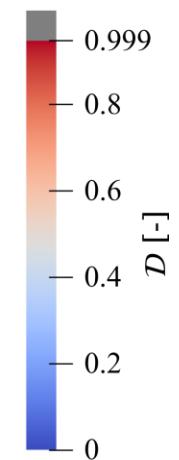
Damage Evolution: Linear

Mixed mode behavior: B-K Law

$$\mathcal{G}_C = \mathcal{G}_{IC} + (\mathcal{G}_{IIC} - \mathcal{G}_{IC}) \left(\frac{\mathcal{G}_{II}}{\mathcal{G}_T} \right)^\eta$$

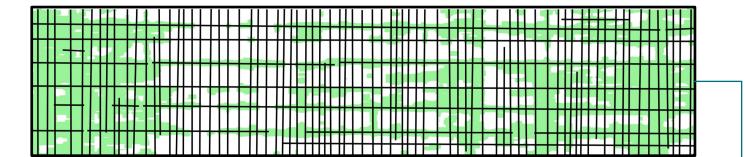
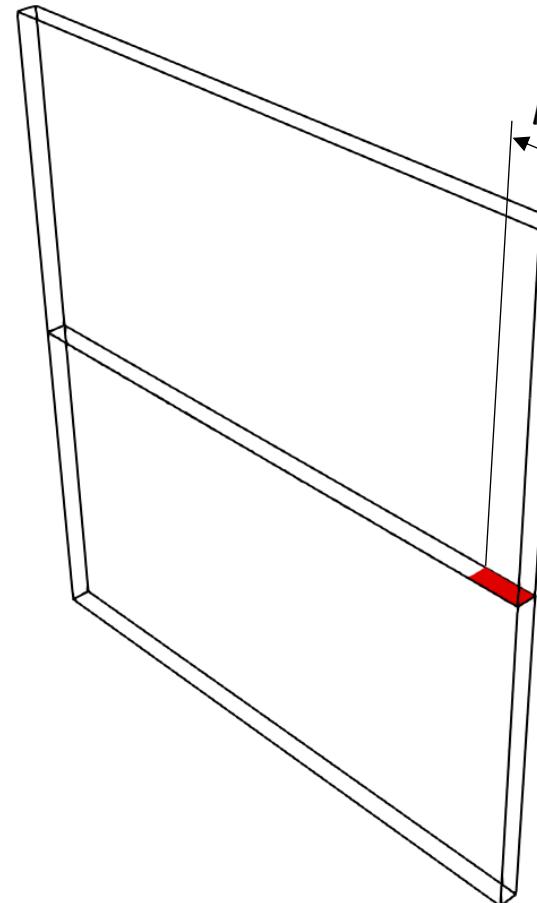


\mathcal{D} corresponds to the degradation of the element



Modelling approach

Once the element reaches the damage threshold \mathcal{D}_{th} , it is considered to be delaminated.



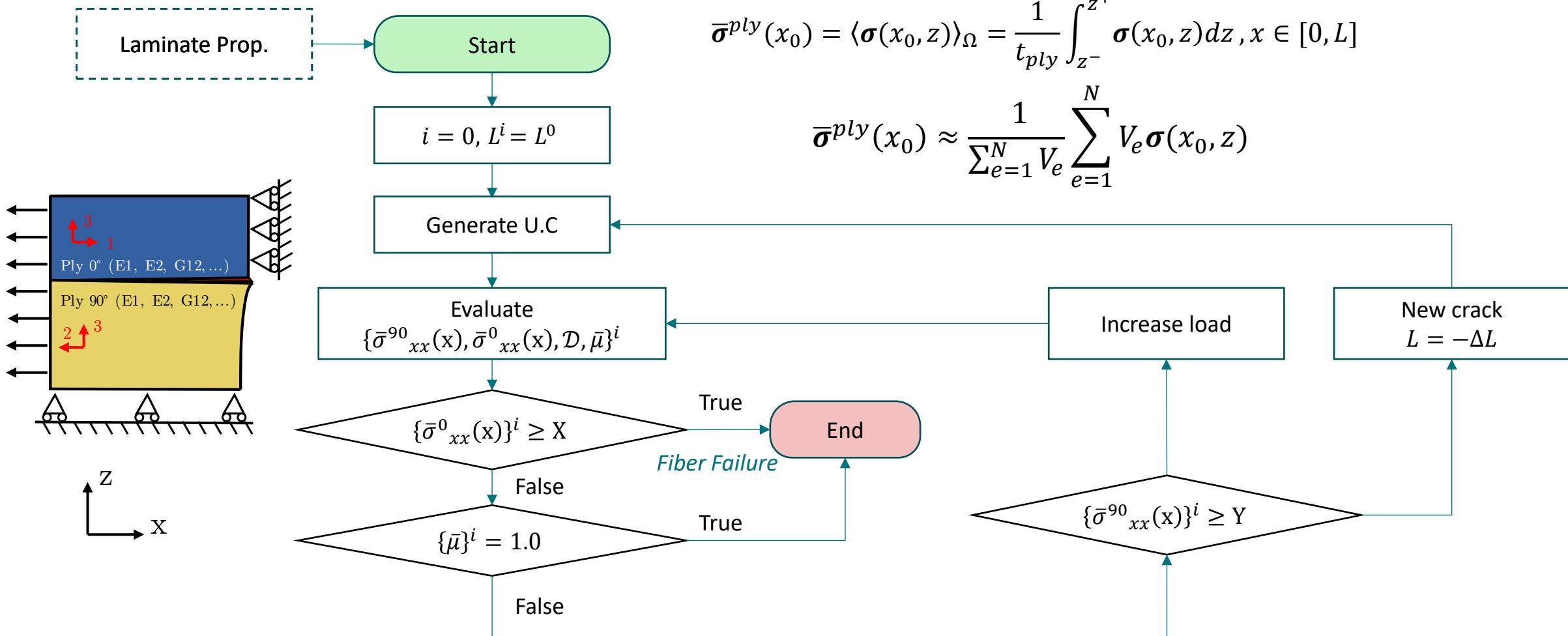
Relative Delamination:

$$\bar{\mu} = \frac{\mu}{L} \Leftrightarrow \bar{\mu} = \frac{A_{del}}{A_{specimen}}$$

Crack Density:

$$\rho = \frac{1}{2L}$$

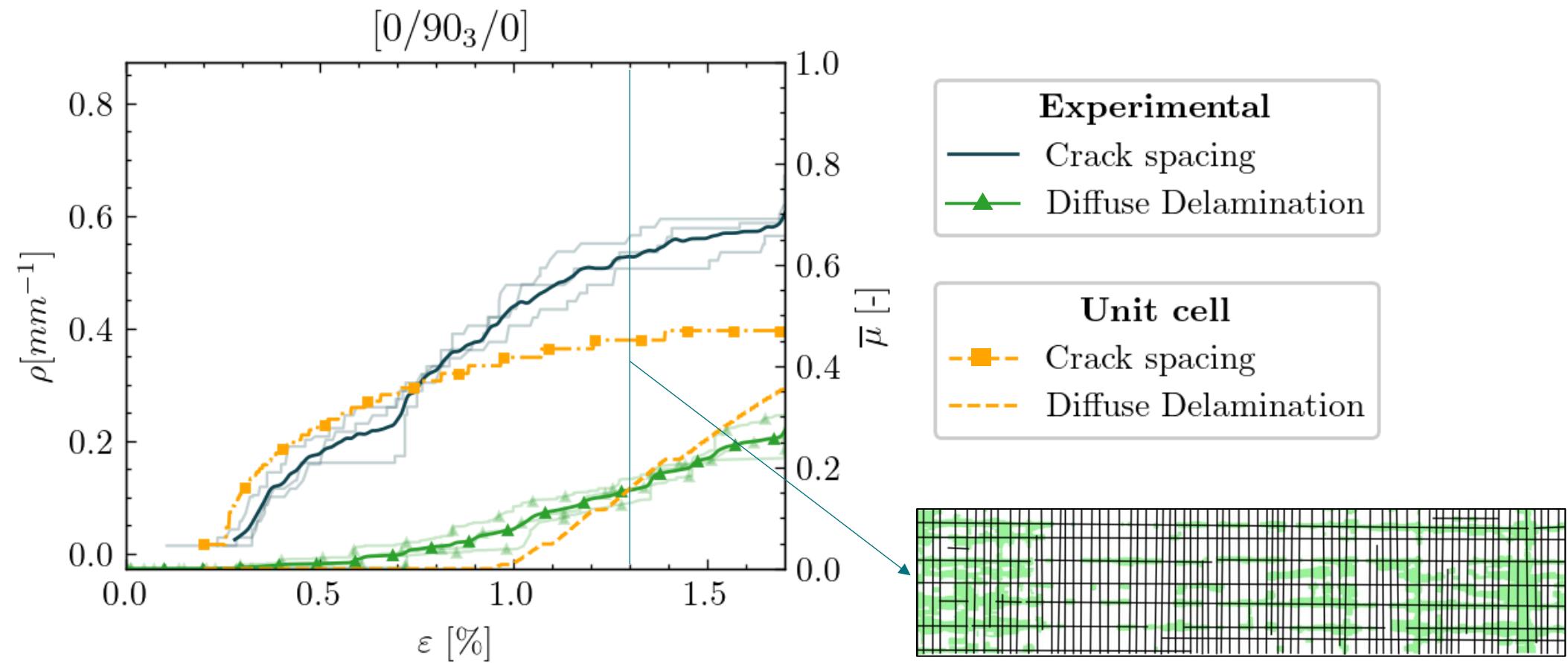
Methodology – Crack evolution



$$\bar{\sigma}^{ply}(x_0) = \langle \sigma(x_0, z) \rangle_{\Omega} = \frac{1}{t_{ply}} \int_{z^-}^{z^+} \sigma(x_0, z) dz, x \in [0, L]$$

$$\bar{\sigma}^{ply}(x_0) \approx \frac{1}{\sum_{e=1}^N V_e} \sum_{e=1}^N V_e \sigma(x_0, z)$$

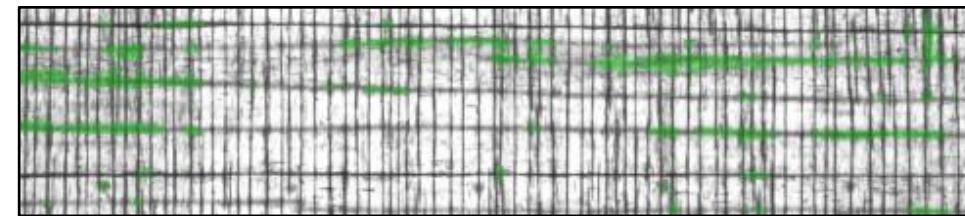
Results – Damage progression



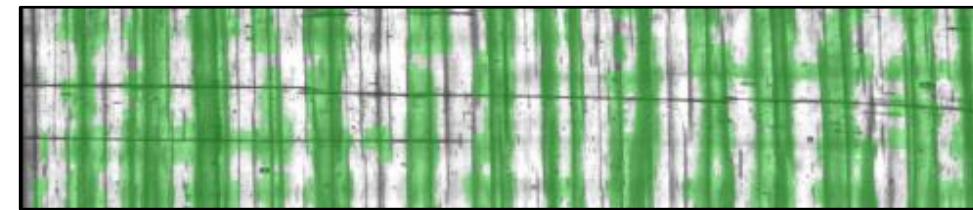
Results – Effect of t_{90}

 Delamination
 Matrix cracks

$[0/90/0]$, $t_{90} = 0.8 \text{ mm}$



$[0/90_4/0]$, $t_{90} = 3.6 \text{ mm}$

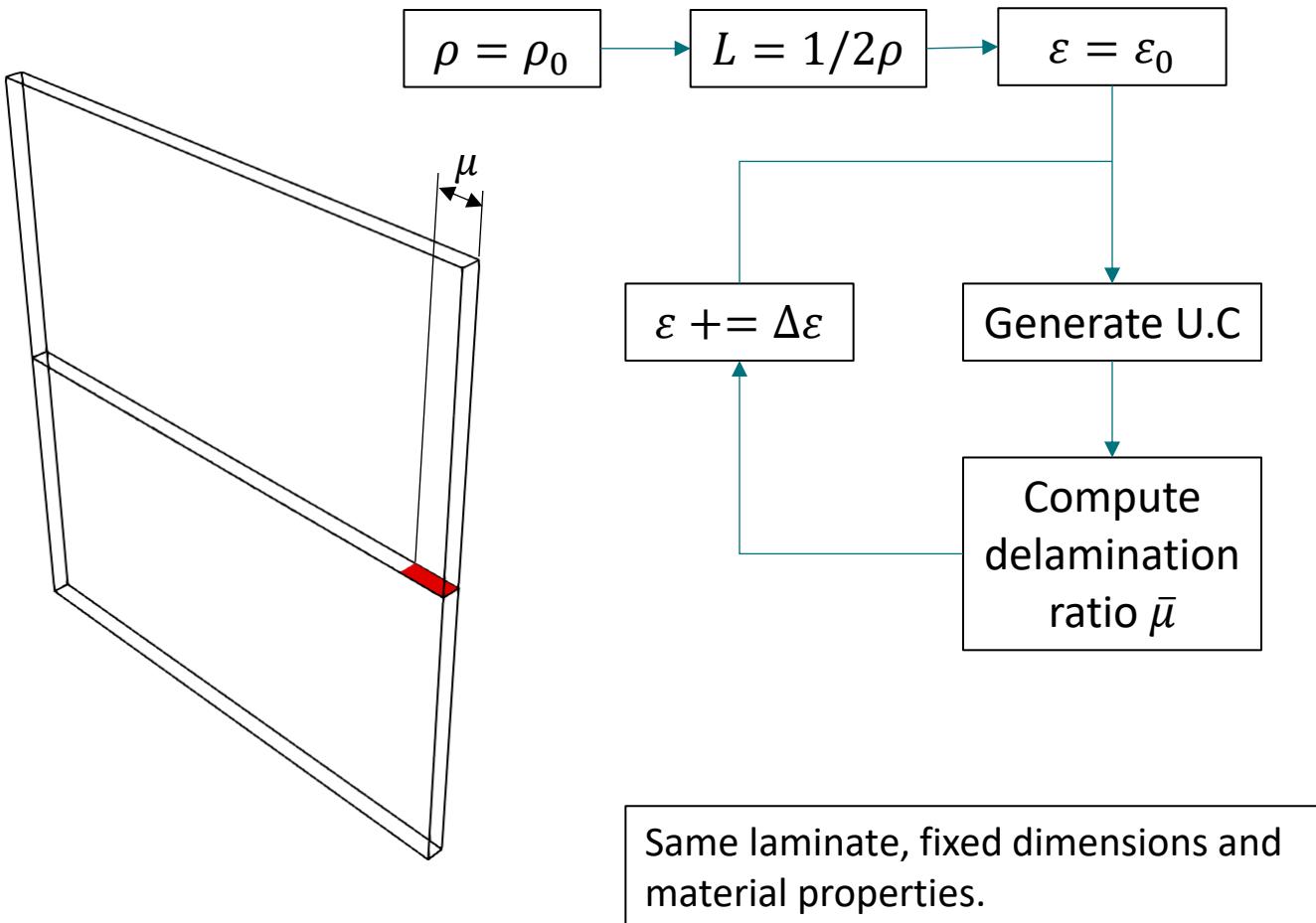


$$t_{90} \rightarrow \rho \rightarrow \mu$$

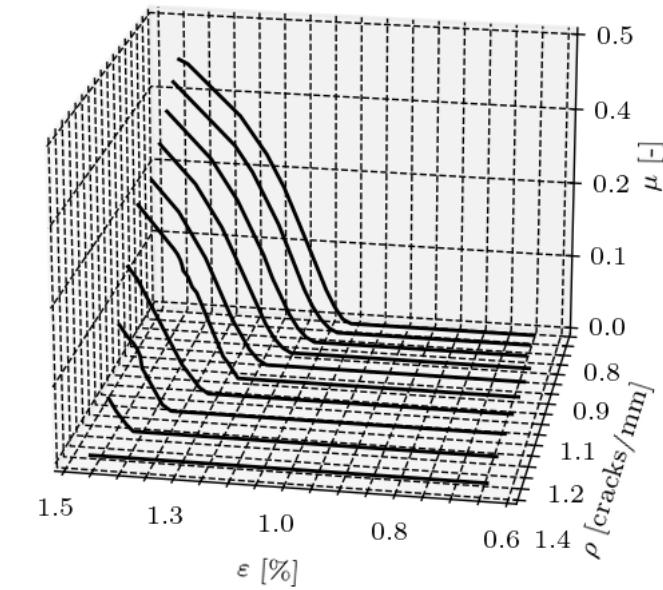
$$t_{90} \rightarrow \begin{cases} \rho \\ \mu \end{cases} \quad ?$$

Experimentally, we cannot decouple all these parameters

Parametric study

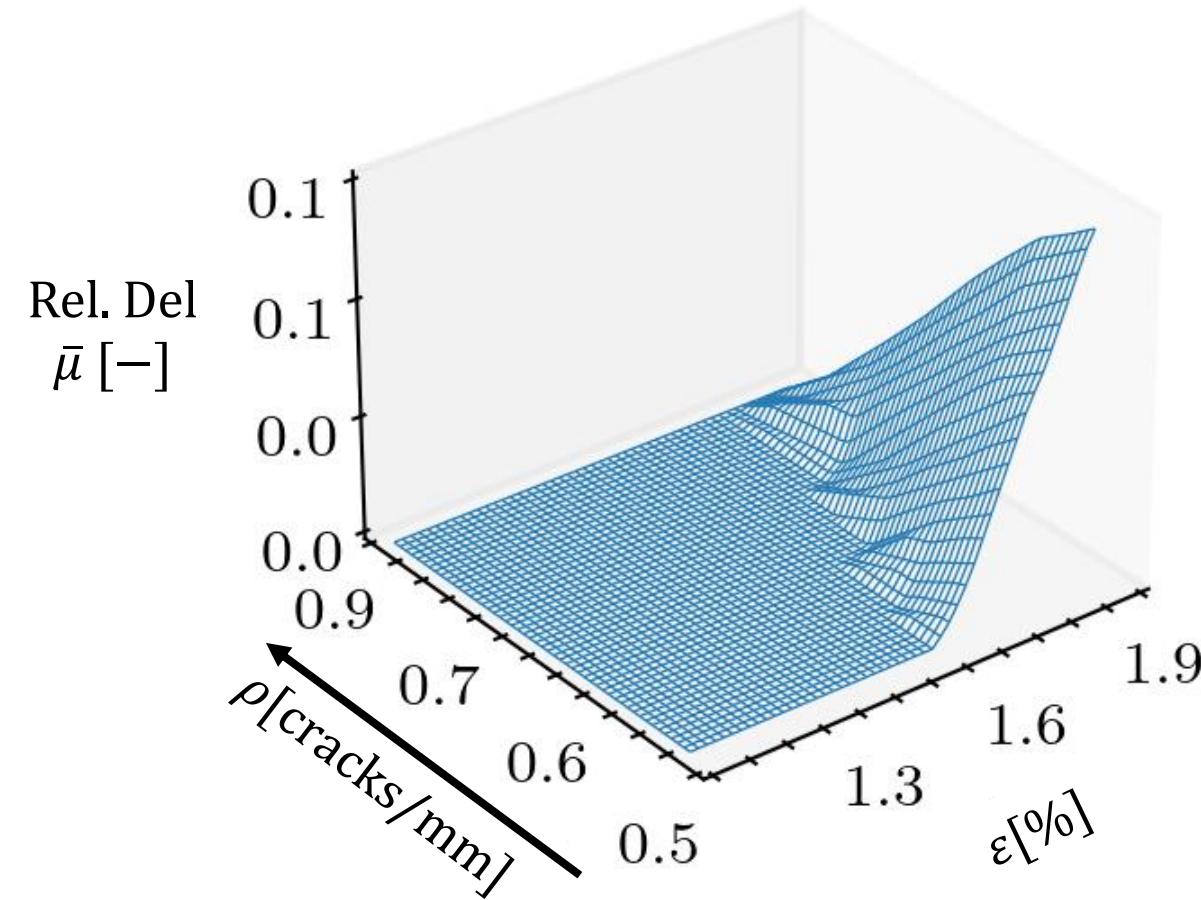


Unit Cell for a fixed crack spacing/density



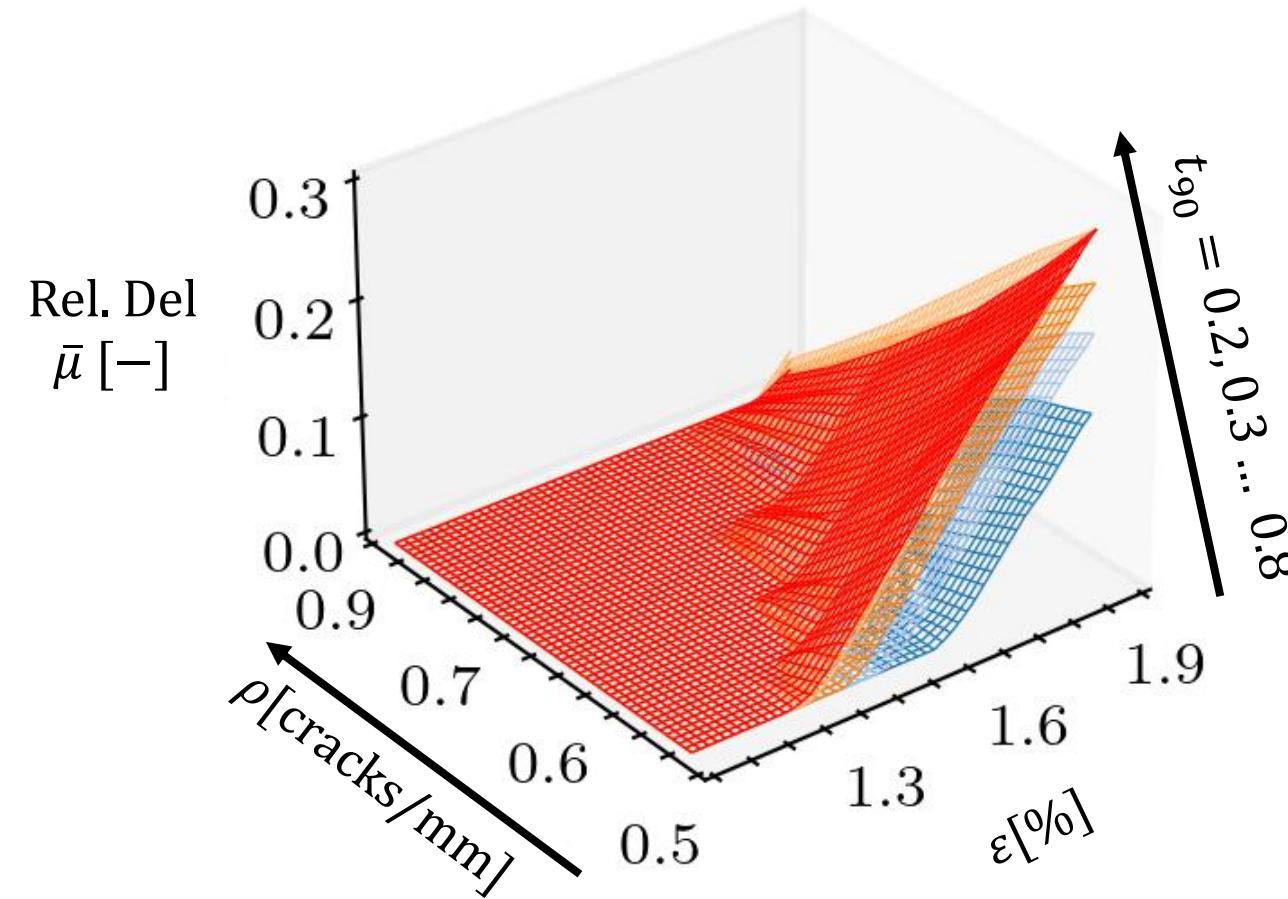
Results

Layup: $[0/90_n/0]$



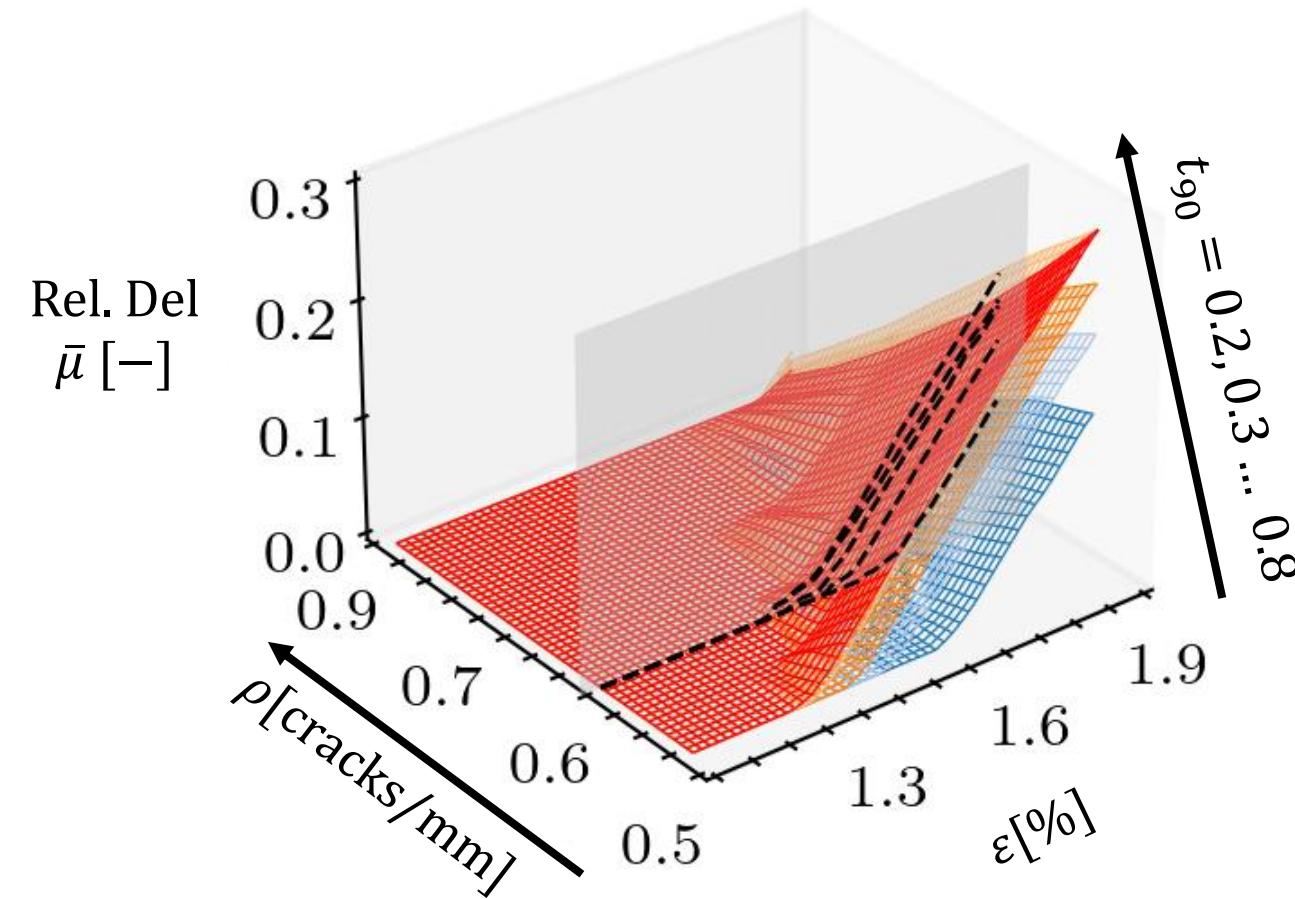
Results

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Results

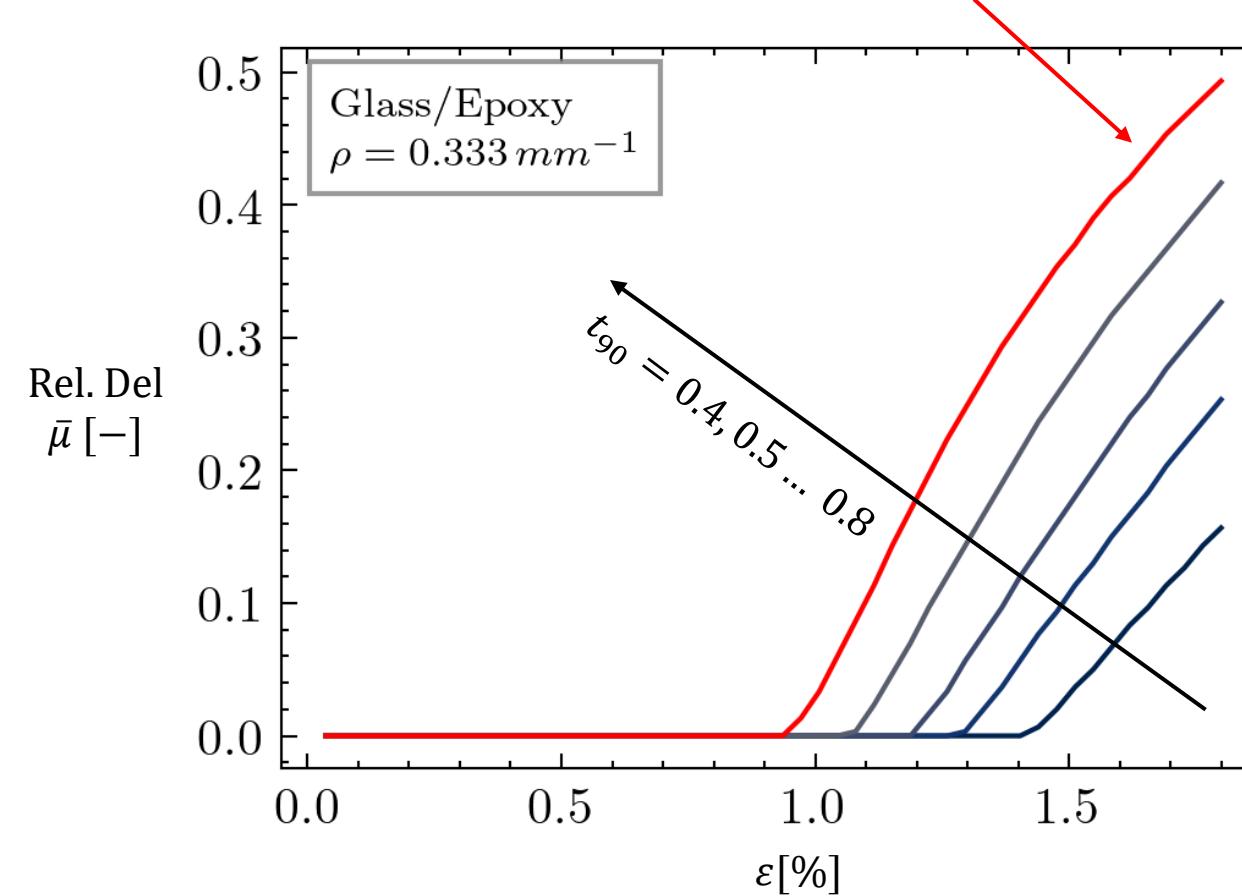
Layup: $[0/90_n/0]$



Results

$\rho = \text{Const}$
 $t_{90} \uparrow \rightarrow \bar{\mu} \uparrow$

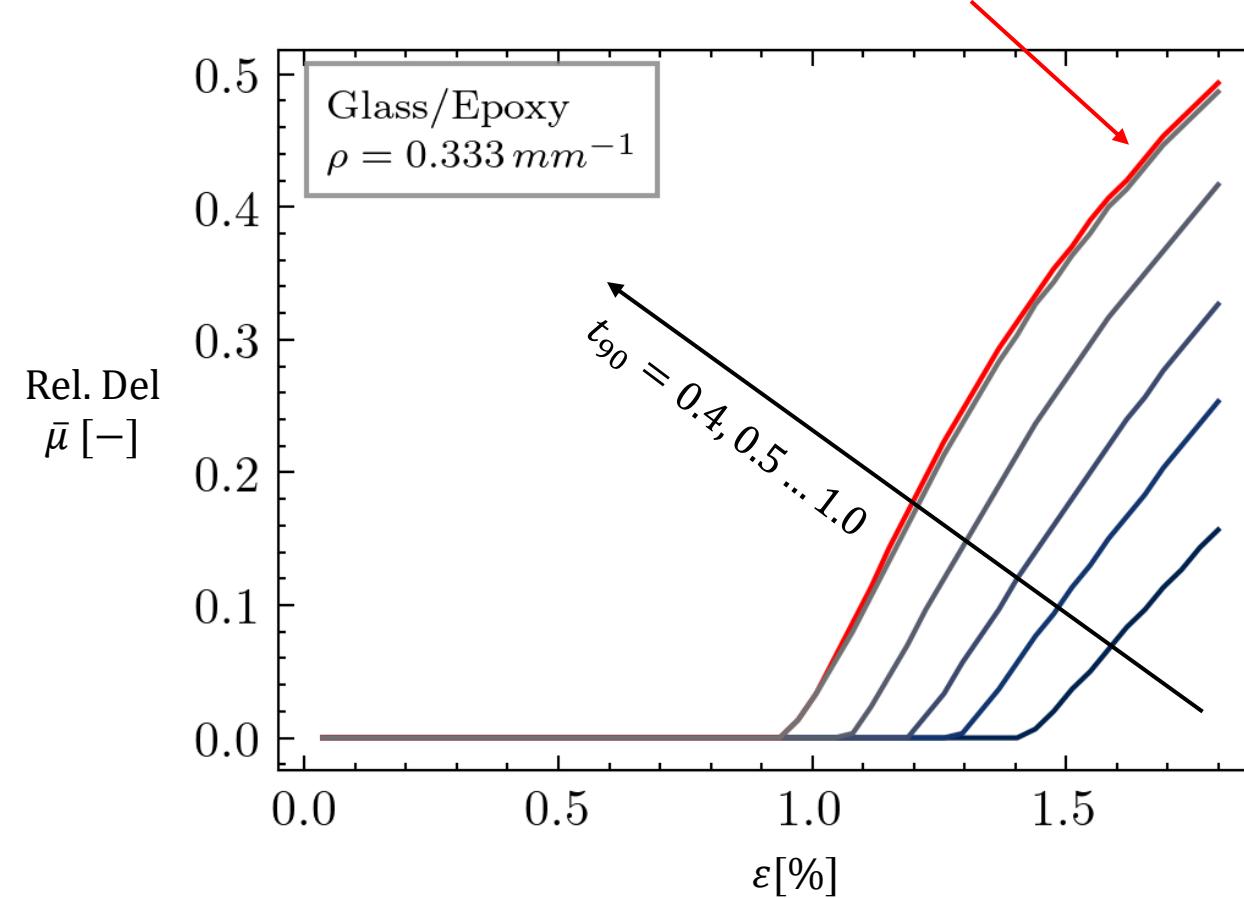
Glass/Epoxy
Cross-ply [0/90_n/0]
Outer Ply thickness = 0.8 mm



Results

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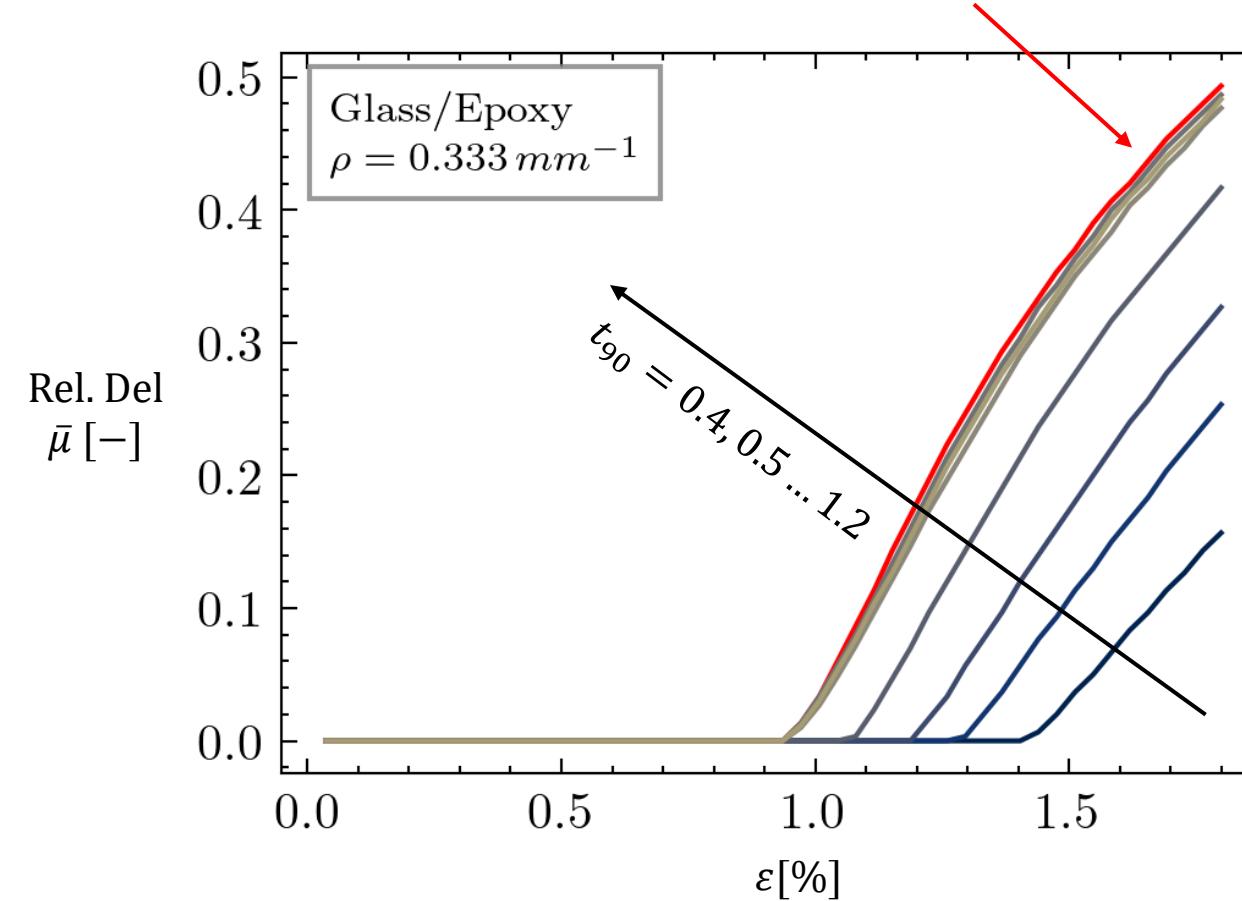


Results

?

$$\begin{aligned} \rho &= \text{Const} \\ t_{90} \uparrow &\rightarrow \bar{\mu} \uparrow \end{aligned}$$

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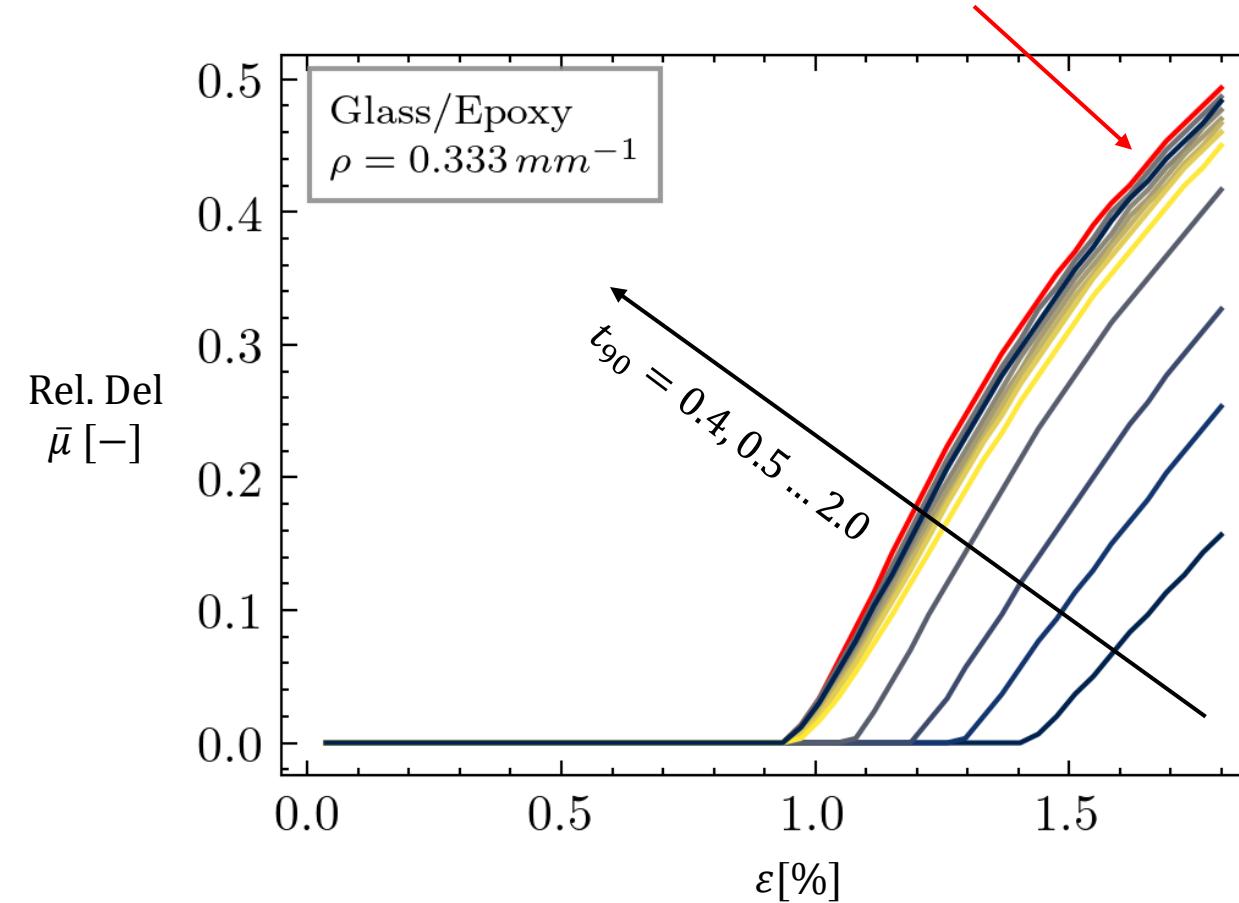


Results

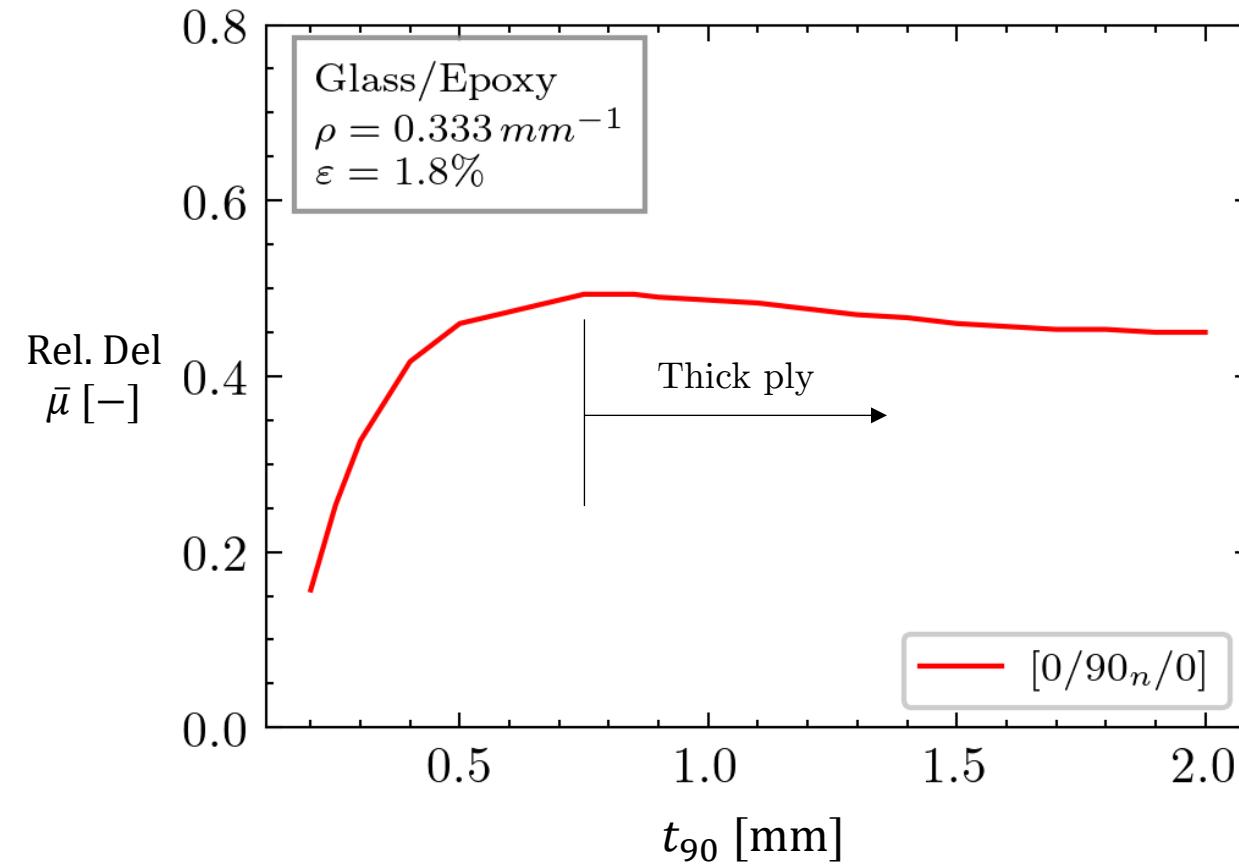
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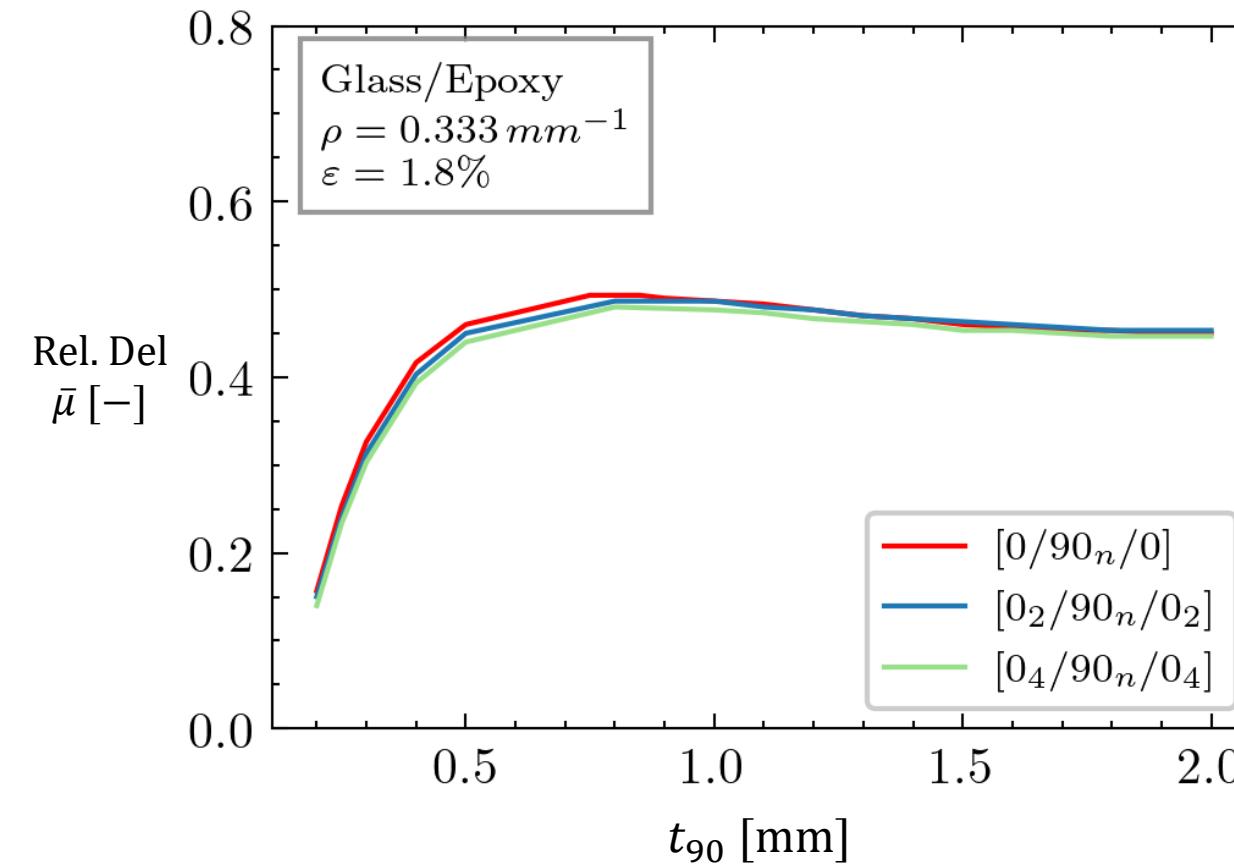
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Results



Results



Conclusions

How does matrix cracking influence the onset and progression of delamination in laminates?

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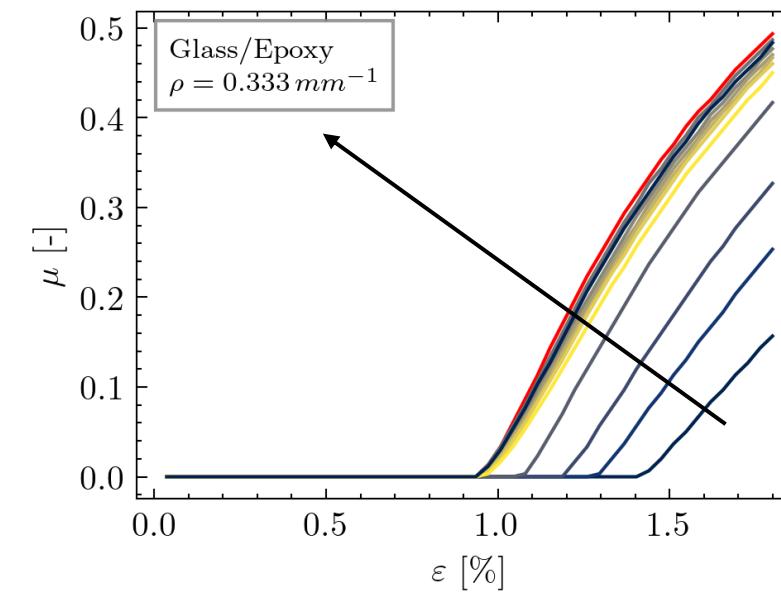
How does matrix cracking influence the onset and progression of delamination in laminates?

- Experimentally there's a link between cracking, inner ply thickness and delamination
- However, we cannot separate individual contributions

Conclusions

How does matrix cracking influence the onset and progression of delamination in laminates?

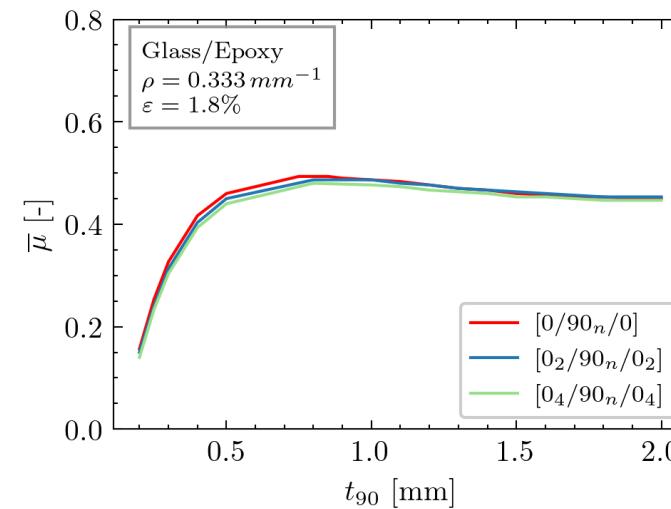
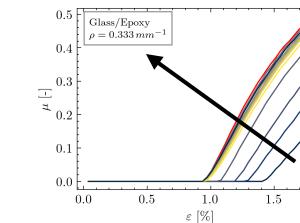
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- There's a “**thin/thick ply concept**” for diffuse delamination



Conclusions

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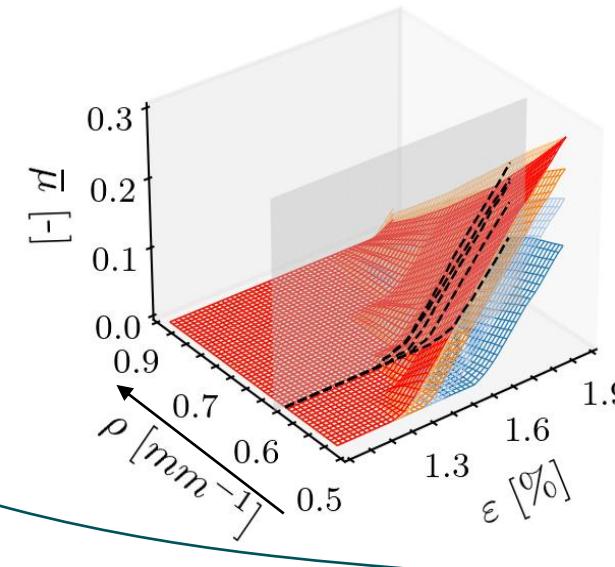
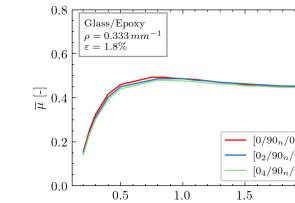
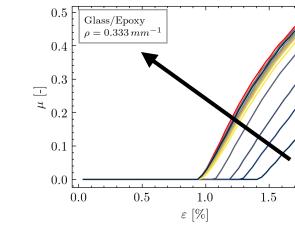
- Experimentally there's a link between cracking, inner ply thickness and delamination
- There's a “**thin/thick ply concept**” for diffuse delamination
- The **outer ply** thickness seems to play no role for diffuse delamination



Conclusions

How does matrix cracking influence the onset and progression of delamination in laminates?

- Experimentally there's a link between cracking, inner ply thickness and delamination
- There's a “**thin/thick ply concept**” for diffuse delamination
- The **outer ply** thickness seems to play no role for diffuse delamination
- $\rho \downarrow \rightarrow \bar{\mu} \uparrow$



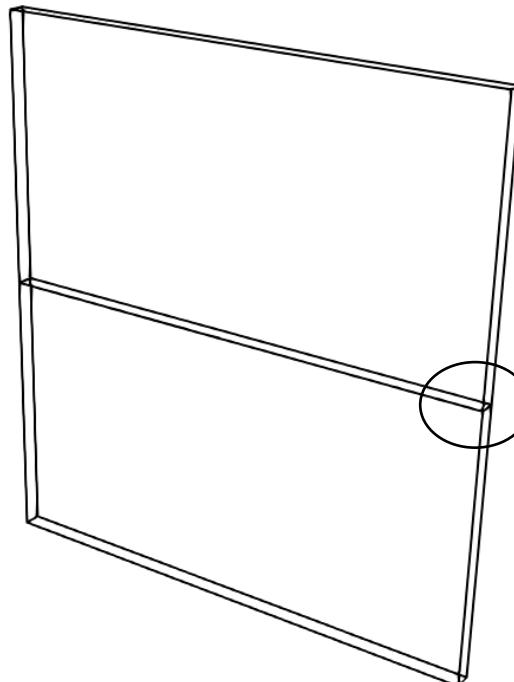
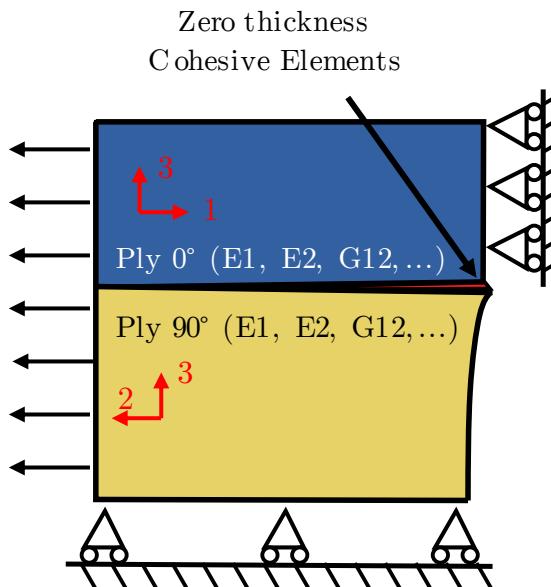
vasco.castro-pires@unileoben.ac.at



Thanks for your attention!

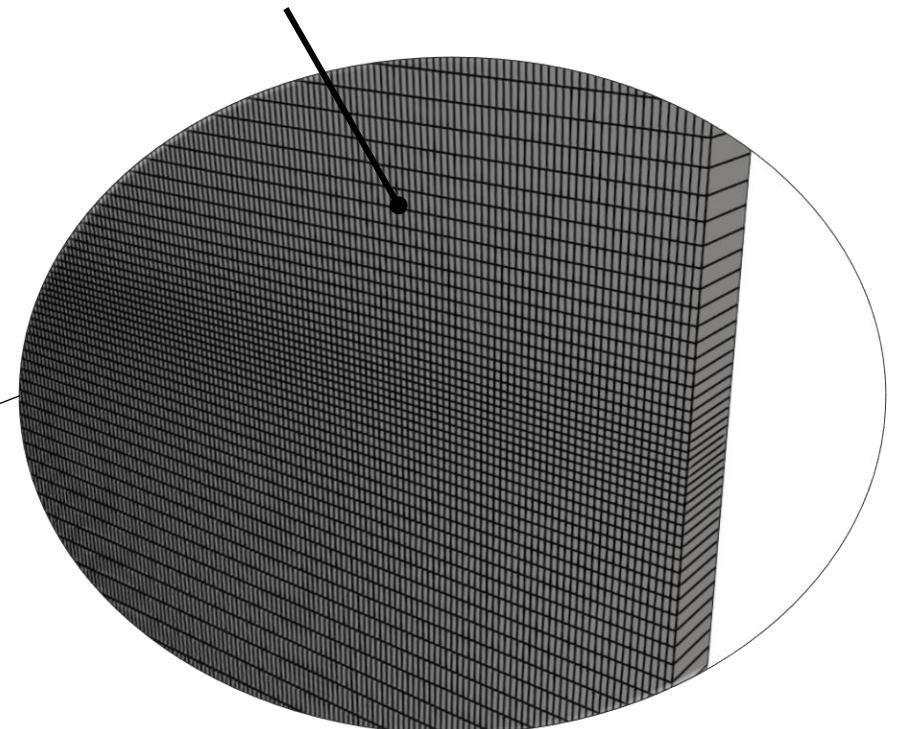
Backup Slides

Modelling approach

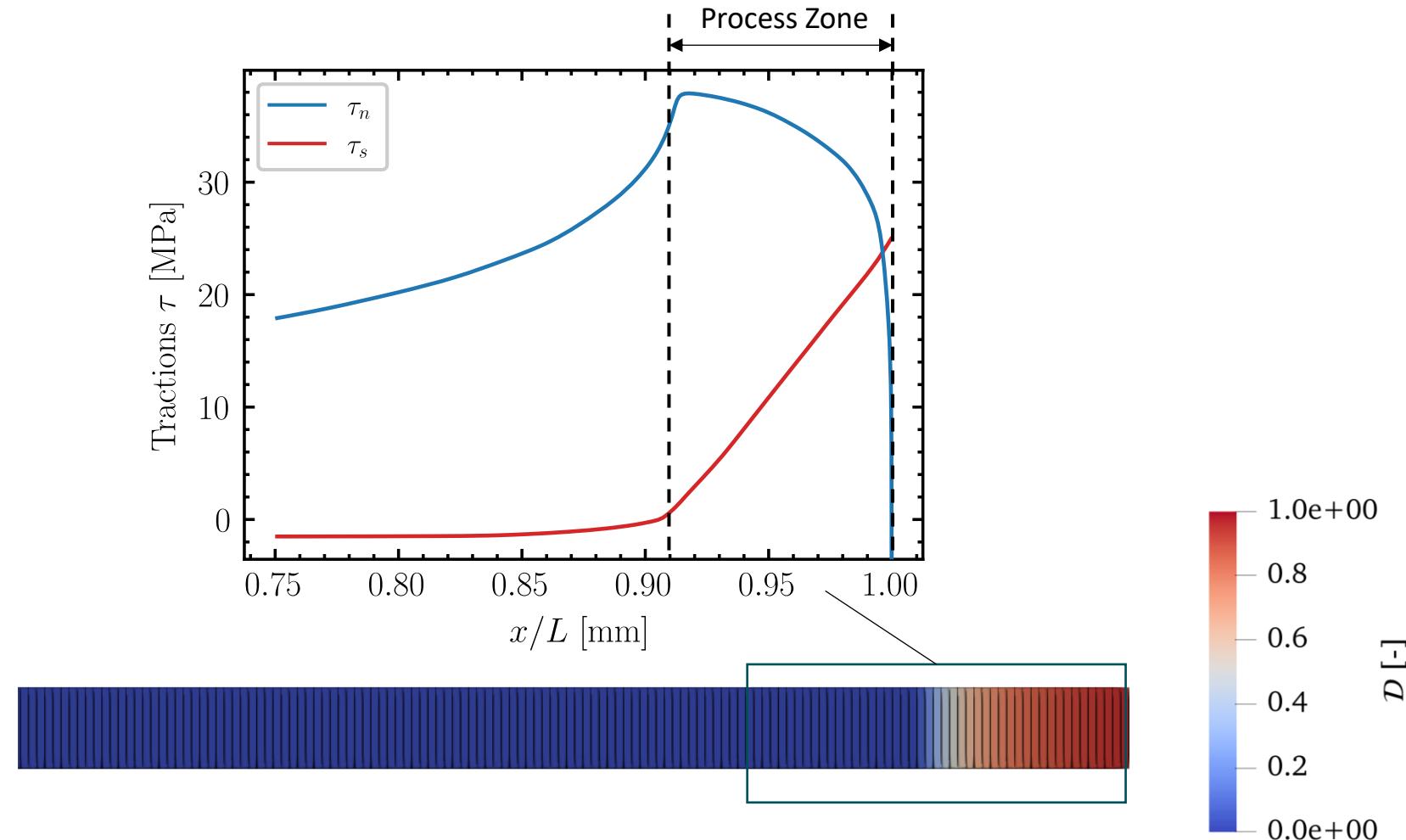


Generalized plane strain model

ABAQUS/Standard
3D Continuum linear solid elements



Process Zone and Traction



Material Properties - Elastic

GFRP:

E_1 [GPa]	E_2 [GPa]	ν_{12} [-]	G_{12} [GPa]
50.4	14.3	0.296	3.2
X_T [MPa]	X_C [MPa]	Y_T [MPa]	Y_C [MPa]
1490	973	36	127
S_{12} [MPa]			38

CFRP:

E_1 [Gpa]	E_2 [GPa]	ν_{12} [-]	G_{12} [GPa]
123.5	7.3	0.351	3.3
X_T [MPa]	X_C [MPa]	Y_T [MPa]	Y_C [MPa]
1858	874	38	131
S_{12} [MPa]			52



Material Properties - Cohesive

GFRP:

t_n [MPa]	t_s [MPa]	G_{Ic} [N/mm]	G_{IIc} [N/mm]
36	38	0.202	2.566

CFRP:

t_n [MPa]	t_s [MPa]	G_{Ic} [N/mm]	G_{IIc} [N/mm]
38	52	0.186	0.786

Interface Stiffness:

K_{nn} [N/mm]	K_{ss} [N/mm]	K_{ss} [N/mm]
1E6	1E6	1E6

Material Properties – BK Law fit

