

Linear Phase FIR Filter Window method

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Methods for design of FIR filters:

- 1) using window functions
- 2) using frequency sampling technique.

$H_d(\omega)$ is the desired freq resp.

↓ IDTFT

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) e^{j\omega n} d\omega, \text{ is the desired sample response.}$$

To make it finite, (FIR)
truncate at $n = M-1$

$$h(n) = h_d(n) \cdot w(n) \quad \begin{matrix} \text{window function } (0, \dots, M-1) \\ \text{eg. Rectangular window:} \end{matrix}$$

$$\begin{cases} h_d(n) & , n = 0, \dots, M-1 \\ 0 & \text{otherwise} \end{cases}$$

↓ $H(\omega)$ is the designed filter freq response

$$H(\omega), H_d(\omega), W(\omega)$$

$$\begin{aligned} H(\omega) &= H_d(\omega) * W(\omega) \\ &= \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\vartheta) \cdot W(\omega - \vartheta) d\vartheta \end{aligned}$$

Rectangular window function:

$$w(\omega) = \sum_{n=0}^{M-1} w(n) e^{-j\omega n}$$

$$= \sum_{n=0}^{M-1} e^{-j\omega n}$$

$$= \frac{1 - e^{-j\omega M}}{1 - e^{-j\omega}}$$

$$= \frac{e^{-j\omega M/2} (e^{j\omega M/2} - e^{-j\omega M/2})}{e^{-j\omega/2} (e^{j\omega/2} - e^{-j\omega/2})}$$

$$= \frac{e^{-j\omega M/2} (\cancel{2} \sin(\omega M/2))}{e^{-j\omega/2} (\cancel{2} \sin(\omega/2))}$$

$$w(\omega) = e^{-j\omega(\frac{M-1}{2})} \cdot \frac{\sin(\omega M/2)}{\sin(\omega/2)} //$$



$$W(\omega) = e^{-j\omega(\frac{M-1}{2})} \cdot \frac{\sin(\omega M/2)}{\sin(\omega/2)}$$

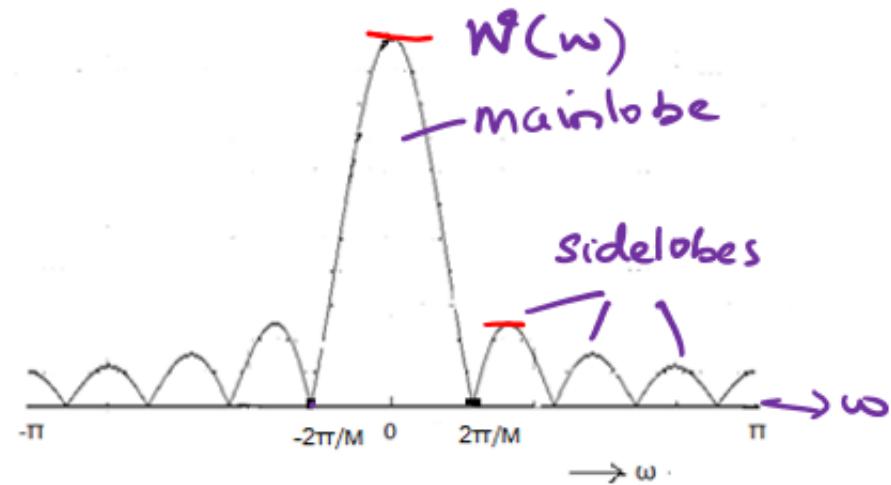
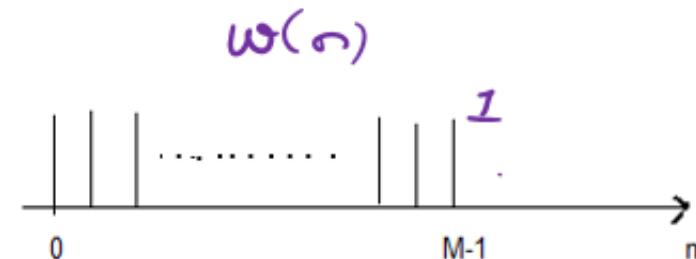
Rectangular window fn:

- width of mainlobe = $\frac{4\pi}{M}$

$M \uparrow$, width of mainlobe \downarrow
height " \uparrow

sidelobe freq \uparrow

- No. of sidelobes depends on M



- 13dB

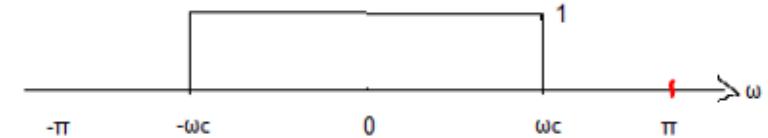
e.g. LPF with cut-off freq at ω_c :

$$H_d(\omega) = \begin{cases} 1 \cdot e^{-j\omega(\frac{M-1}{2})}, & 0 \leq \omega \leq \omega_c \\ 0 & \text{otherwise} \end{cases}$$

↓ IDFT

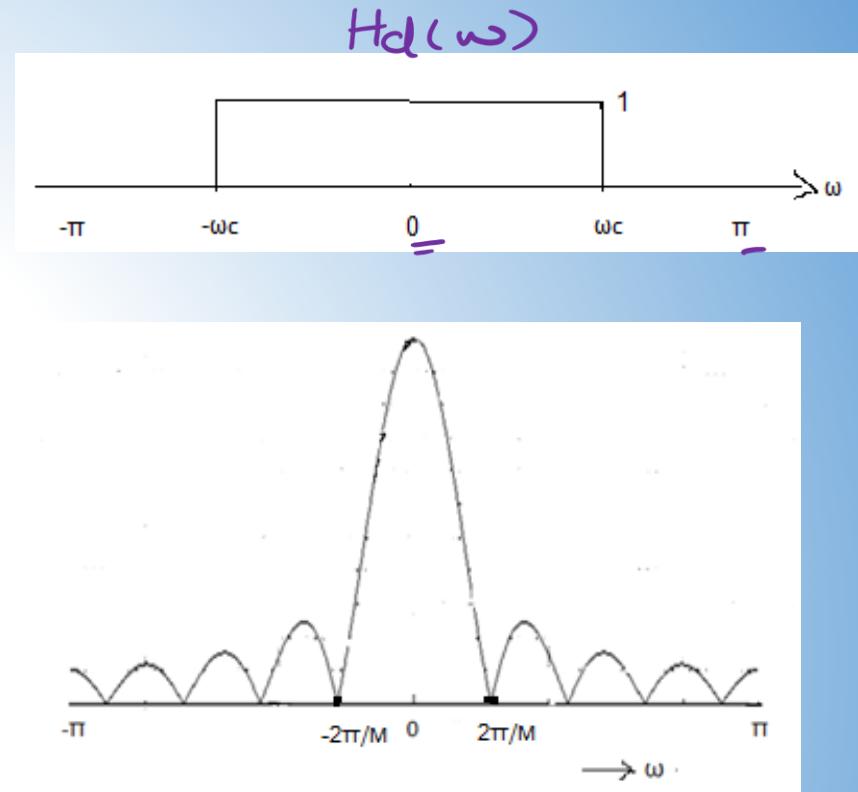
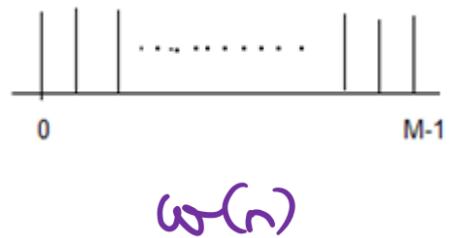
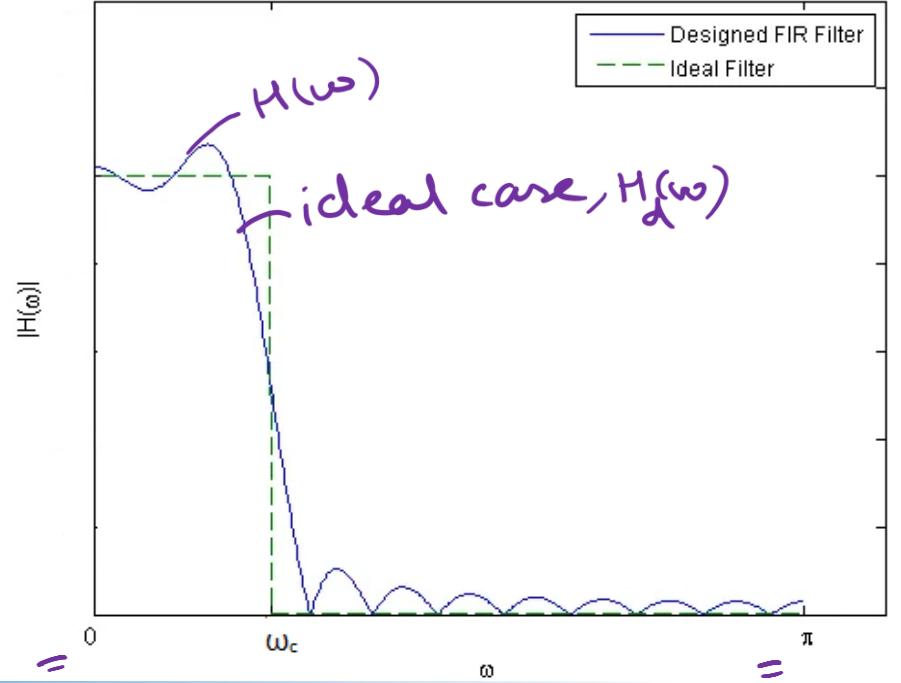
$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) e^{j\omega n} d\omega.$$

$$= \begin{cases} \frac{\sin \omega_c (n - \frac{M-1}{2})}{\pi (n - \frac{M-1}{2})} & \text{for } n \neq \frac{M-1}{2} \\ \frac{\omega_c}{\pi} & \text{for } n = \frac{M-1}{2} \quad \& M = \text{odd} \end{cases}$$



Ideal case.

This function has infinite duration. To make it finite, multiply with rectangular window function.

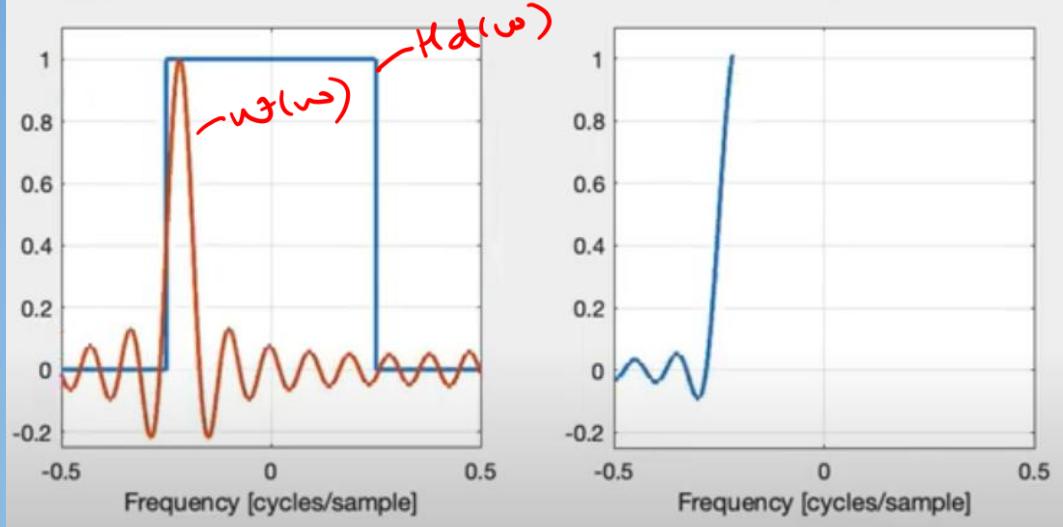


$W(\omega)$

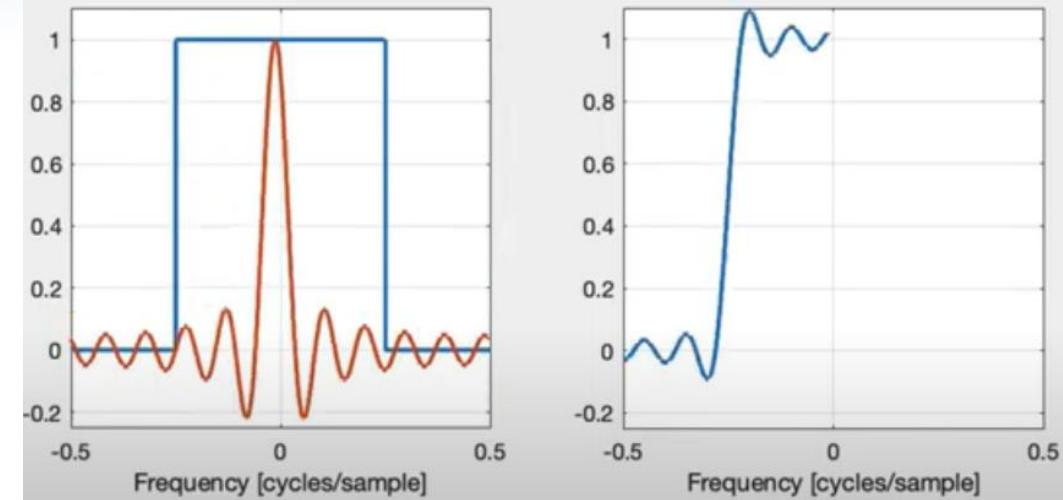
$$h(n) = h_d(n) \cdot w(n)$$

$$H(\omega) = H_d(\omega) * W(\omega)$$

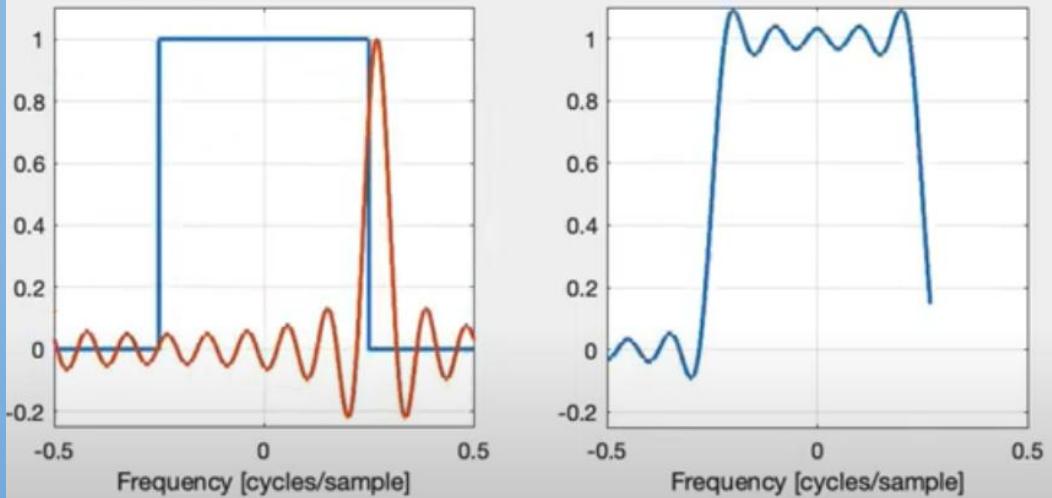
$$h[n] = h_i[n] \cdot w[n] \quad \xleftrightarrow{\text{DTFT}} \quad H(f) = H_i(f) \circledast W(f)$$



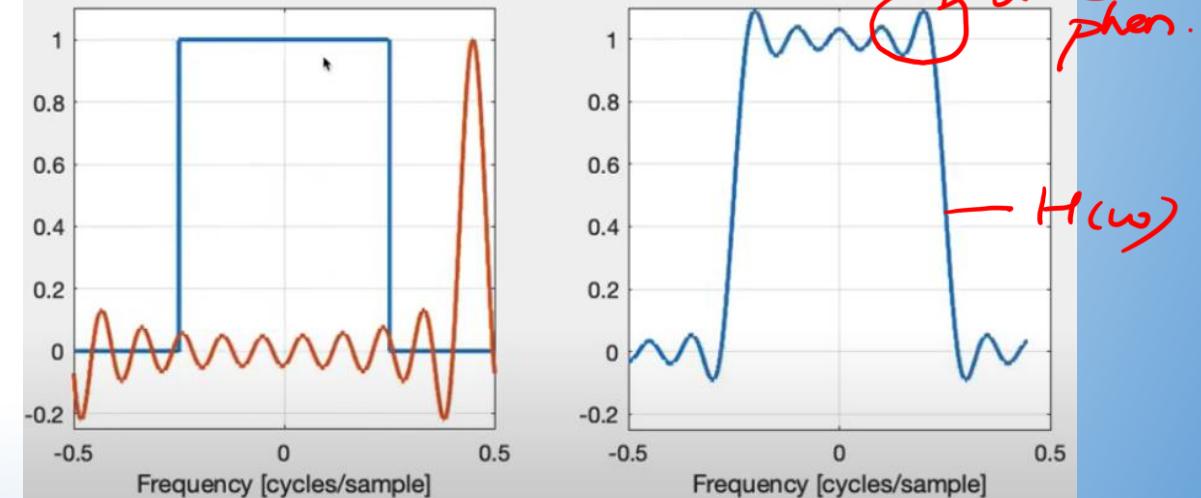
$$h[n] = h_i[n] \cdot w[n] \quad \xleftrightarrow{\text{DTFT}} \quad H(f) = H_i(f) \circledast W(f)$$



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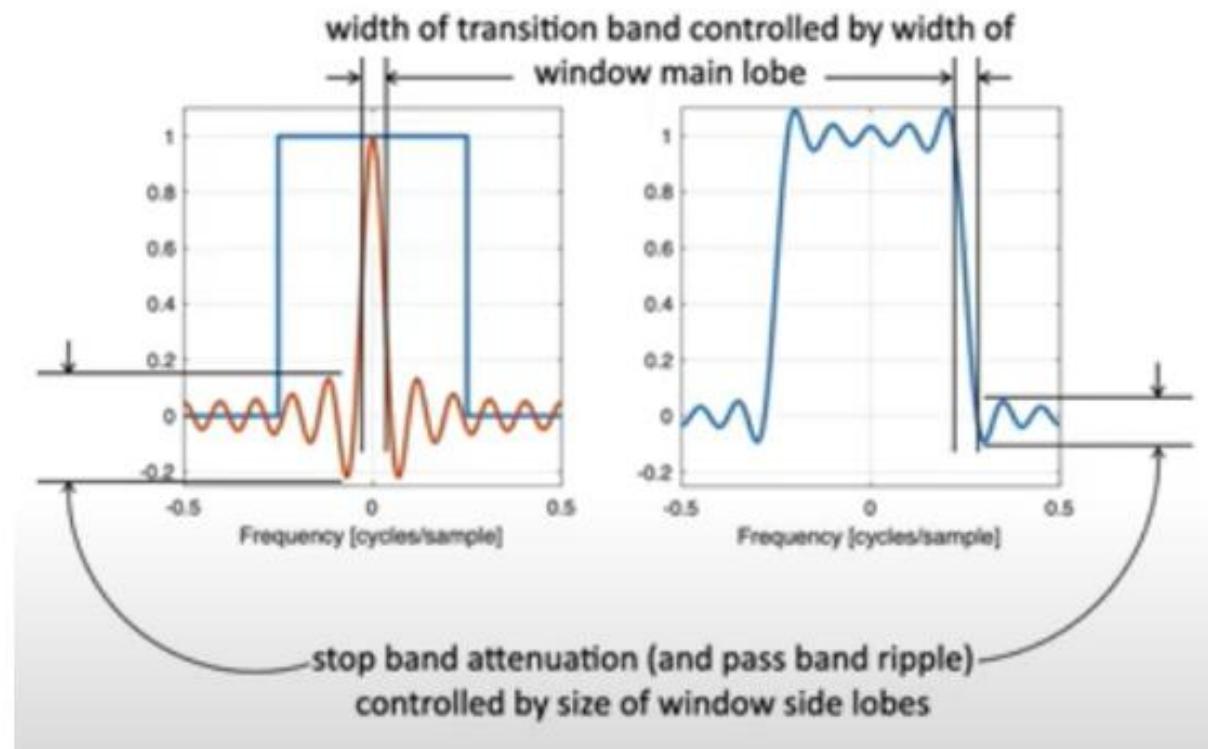


$$h[n] = h_i[n] \cdot w[n] \quad \xleftrightarrow{\text{DTFT}} \quad H(f) = H_i(f) \circledast W(f)$$

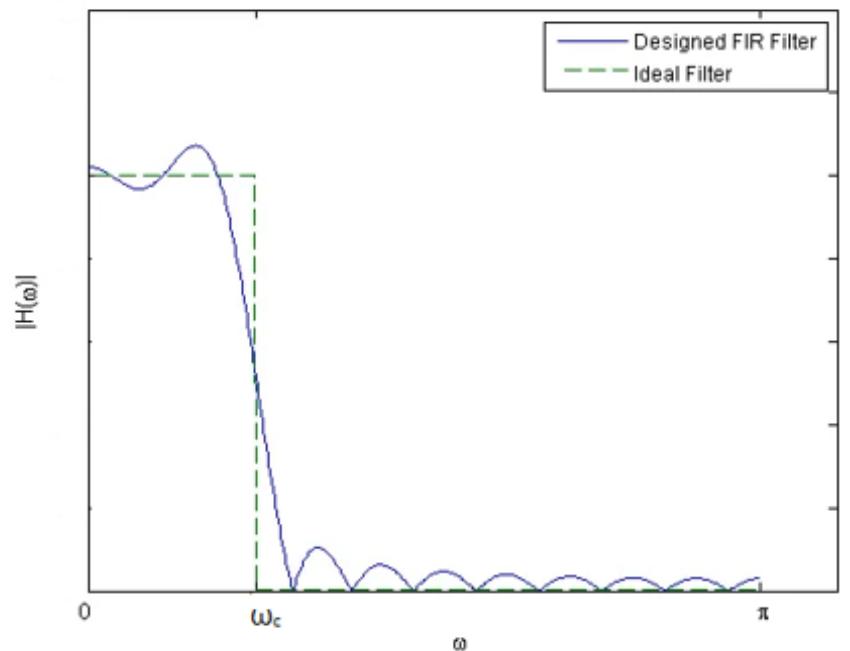


- Width of mainlobe causes the transition band in the designed filter response $H(\omega)$

- Transition bandwidth depends on M
 $M \uparrow \text{TB} \downarrow$

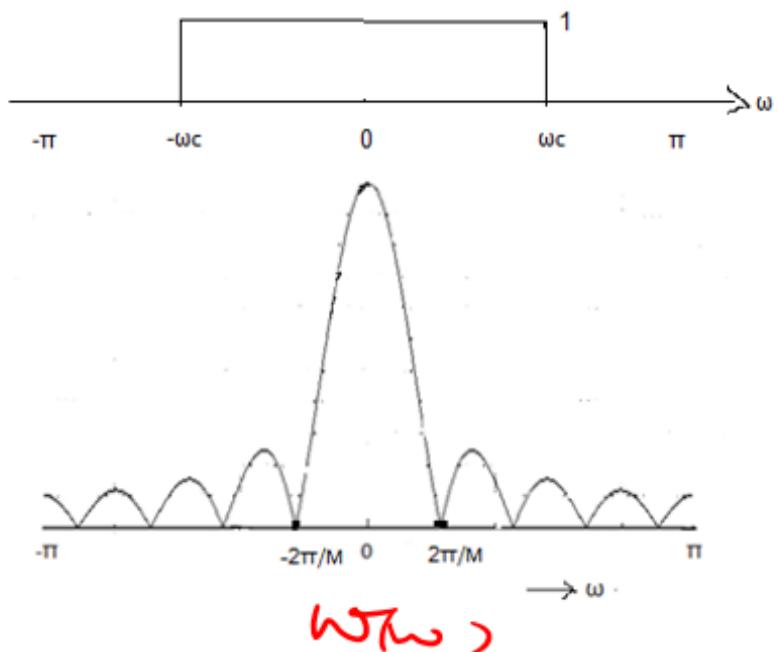


- Ripples in passband \Leftrightarrow stopband are due to significant sidelobes in $W(\omega)$
- Relatively large oscillations occur near the transition band edge. This is called Gibbs' phenomenon.



$$\omega(n) = \frac{2\pi n}{M}$$

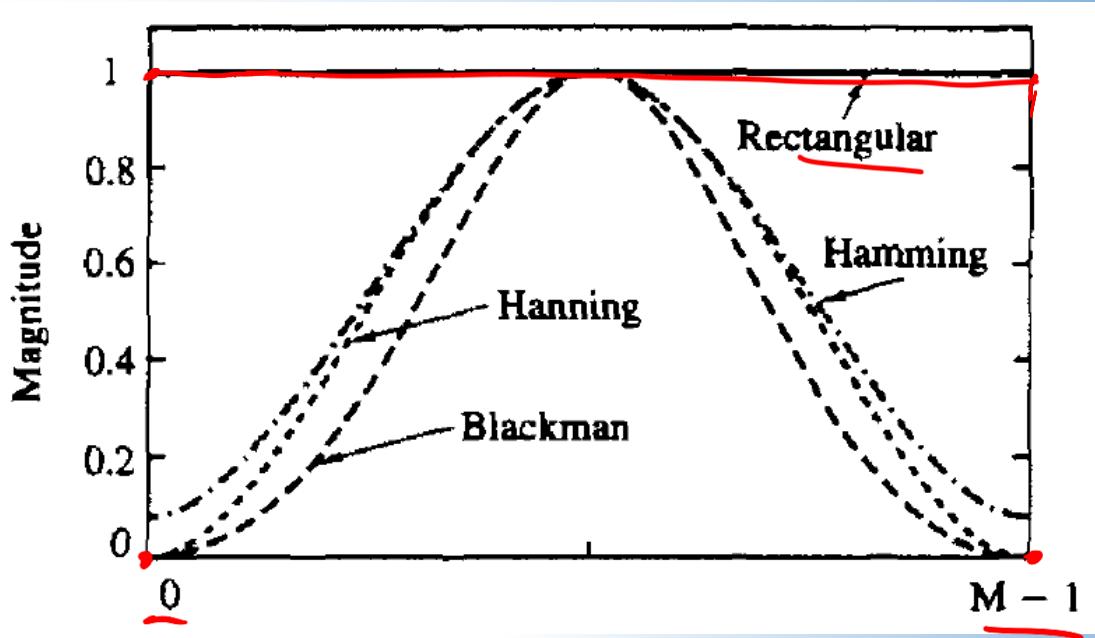
(Handwritten note: $\omega(n)$)



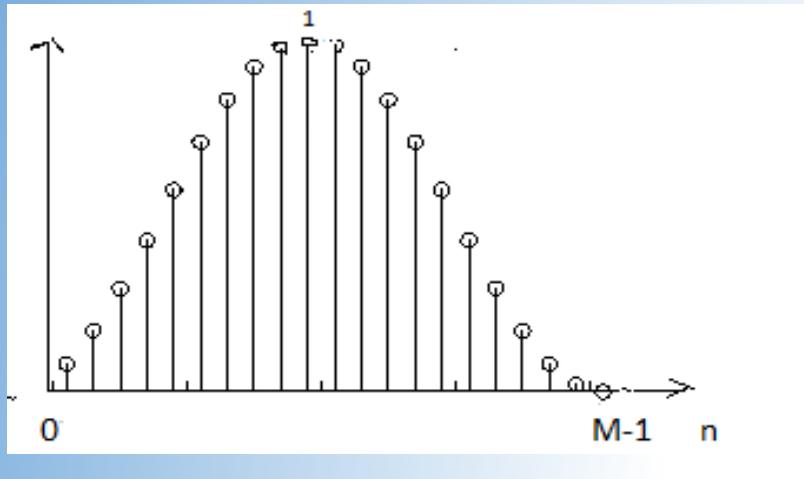
- We desire the mainlobe width to be narrow and amplitude of sidelobe to be small.
- Sidelobes must be suppressed to reduce the ripples in passband & stopband
- Sidelobes are significant in rectangular window due to sharp transitions at $n=0 \leq M-1$.

- Sidelobes can be suppressed by tapering the edges of the window function.
- Different window functions exist, depending on the way in which band edges are tapered.

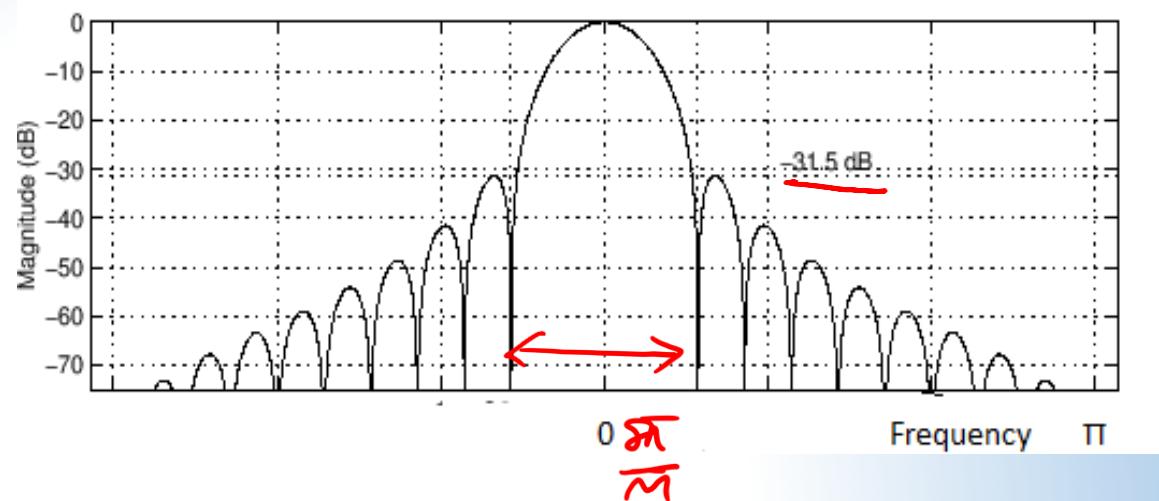
- 1) Hanning window
 - 2) Hamming window
 - 3) Blackman window
- etc.



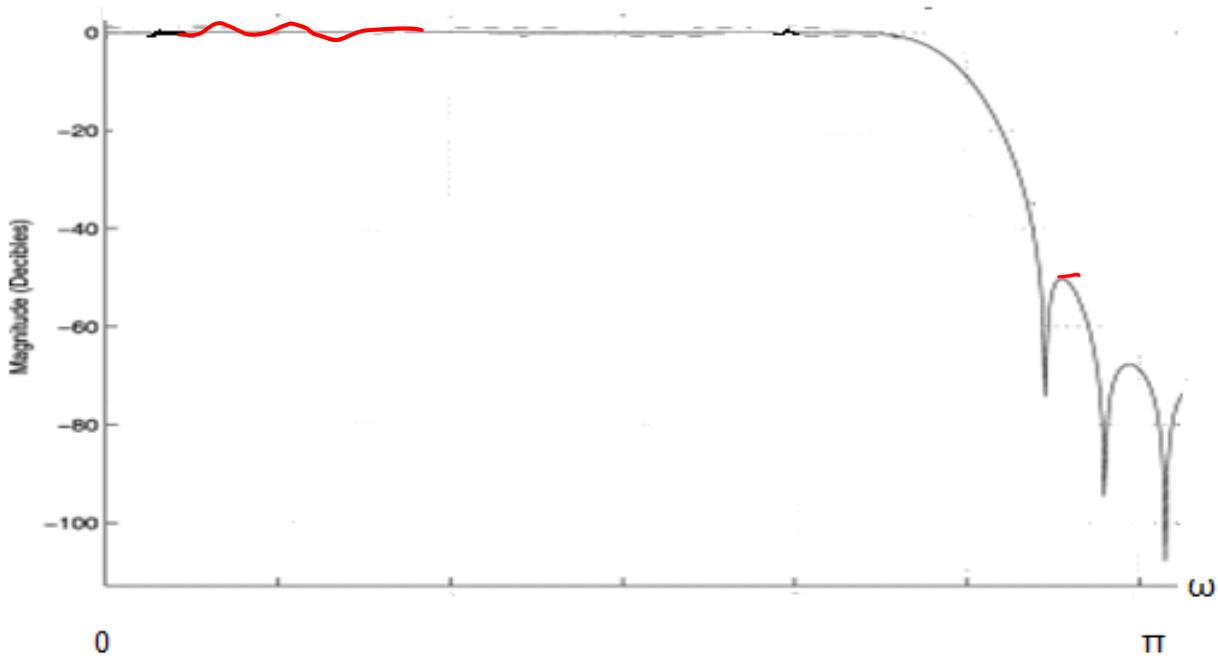
Hanning window, $w(n)$



$w(\omega)$



Sidelobes -32dB .



- Ripples in the passband and Gibbs' phenomenon has reduced.
- Stopband attenuation has increased.

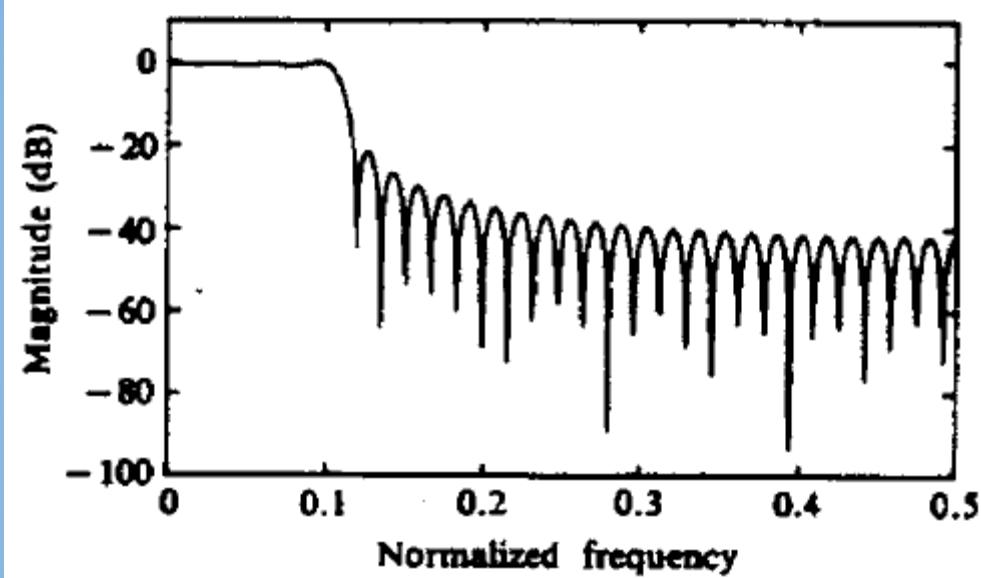
Some of the commonly used window functions are given below

Name of the window	Window function $0 \leq n \leq M-1$	Main lobe width	Peak side lobe (dB)	Normalised transition width #	Stop band attenuation (dB)
Rectangular	1	$4\pi/M$ ✓	-13 ✓	$0.9/(M-1)$	21 ✓
Hanning	$0.5 - 0.5\cos\left(\frac{2\pi n}{M-1}\right)$	$8\pi/M$ ✓	-32 ✓	$3.1/(M-1)$	44 ✓
Hamming	$0.54 - 0.46\cos\left(\frac{2\pi n}{M-1}\right)$	$8\pi/M$	-43	$3.3/(M-1)$	53
Blackman	$0.42 - 0.5\cos\left(\frac{2\pi n}{M-1}\right) + 0.08\cos\left(\frac{4\pi n}{M-1}\right)$	$12\pi/M$ ==	-58 ==	$5.5/(M-1)$	75 ==
Keiser*	$\frac{I_0\left[\beta\sqrt{\left(\frac{M-1}{2}\right)^2 - \left(n - \frac{M-1}{2}\right)^2}\right]}{I_0\left[\beta\left(\frac{M-1}{2}\right)\right]}$				> 70

*Keiser window parameters can be controlled by β . $I_0[.]$ is modified Bessel function of first kind and order 0.

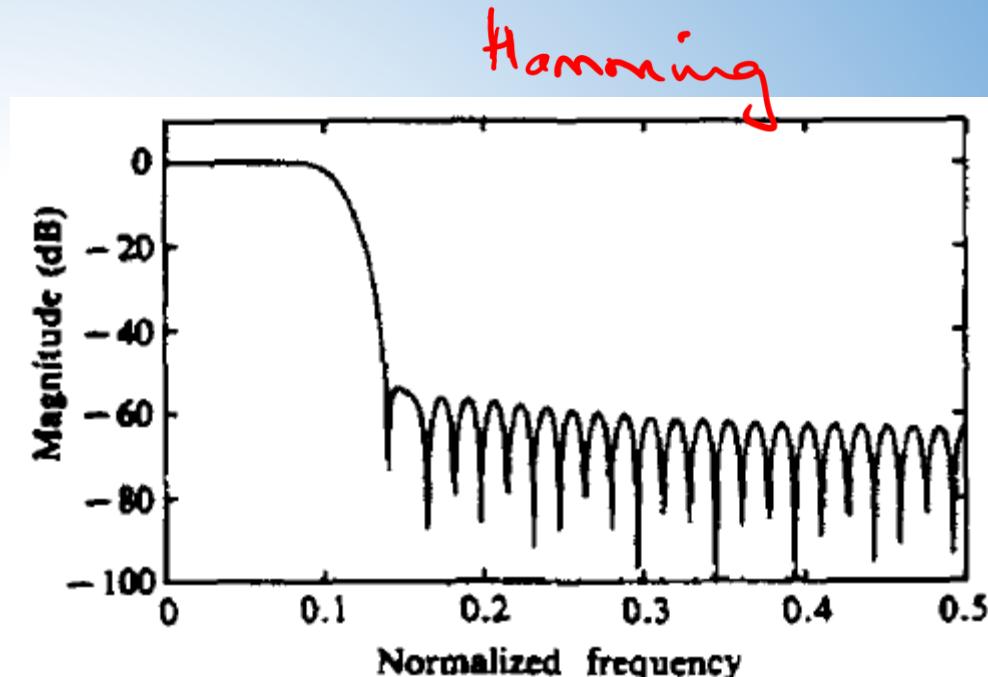
Transition width is normalised to 2π or equivalently to sampling frequency F_s

FIR LPF designed using rectangular window,
Hamming window and Blackman window ($M=61$)

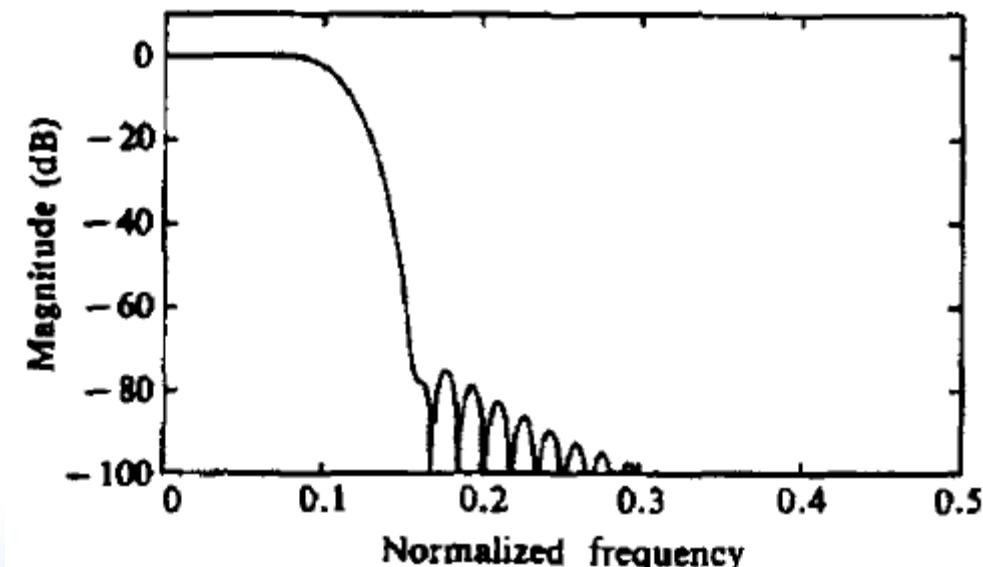


Rectangular

- Move the tapering, wider is the normalized TB and better the stopband attenuation



Hamming



Blackman

Q. Design a symmetric FIR LPF with the desired freq resp

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\alpha}, & |\omega| \leq \omega_c \\ 0 & \text{otherwise} \end{cases}$$

The length of the FIR filter is to be 7, cutoff freq $\omega_c = 1$,
use rectangular window function.

$$\alpha = \frac{M-1}{2}$$

Soln:

$H_d(\omega)$ - given

$$\downarrow h_d(n)$$

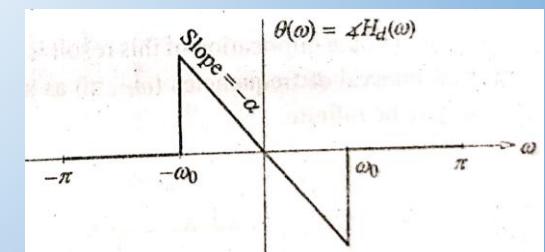
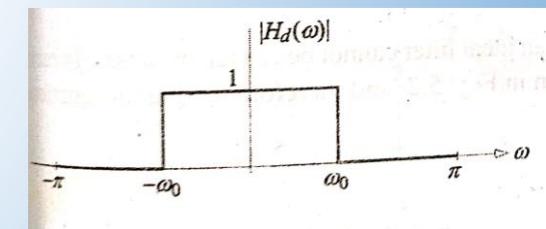
$$\downarrow$$

$$h(n) = h_d(n) \cdot w(n) \leftarrow \text{rect}$$

$$\downarrow$$

$H(\omega)$ - freq resp of designed ^{FIR} filter

$$H_d(\omega) = \begin{cases} e^{-j\omega\alpha}, & |\omega| < \omega_0 \\ 0, & \omega_0 < |\omega| < \pi \end{cases}$$



$$H_d(\omega) = \begin{cases} e^{-j\omega\alpha} & |\omega| \leq \omega_c \\ 0 & \text{otherwise} \end{cases}$$

$$\omega_c = 1$$

$$M = 7$$

$$h_d(n) = \begin{cases} \frac{\sin \omega_c (n - \frac{M-1}{2})}{\pi (n - \frac{M-1}{2})} & \text{for } n \neq \frac{M-1}{2} \\ \frac{\omega_c}{\pi} & \text{for } n = \frac{M-1}{2} \end{cases}$$

$$= \begin{cases} \frac{\sin (n-3)}{\pi (n-3)} & , \quad n \neq 3 \\ \frac{1}{\pi} & , \quad n = 3 \end{cases}$$

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\tau} & -\omega_c \leq \omega \leq \omega_c \\ 0 & \text{Otherwise} \end{cases}$$

By taking inverse Fourier transform

$$\begin{aligned} h_d(n) &= \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega \\ &= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{-j\omega\tau} e^{j\omega n} d\omega \\ &= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega(n-\tau)} d\omega \end{aligned}$$

$$\begin{aligned} h_d(n) &= \frac{1}{2\pi} \left[\frac{e^{j\omega(n-\tau)}}{j(n-\tau)} \right]_{-\omega_c}^{\omega_c} \\ &= \frac{1}{2j\pi(n-\tau)} [e^{j\omega_c(n-\tau)} - e^{-j\omega_c(n-\tau)}] \\ &= \frac{1}{\pi(n-\tau)} \left[\frac{e^{j\omega_c(n-\tau)} - e^{-j\omega_c(n-\tau)}}{2j} \right] \end{aligned}$$

$$h(n) = h_d(n) \cdot w(n)$$

$M=7$, $h(6)=h(6)$, $h(1)=h(5)$, $h(2)=h(4) \Rightarrow$ symmetric

n	$h_d(n)$	$w(n)$	$h(n) = h_d(n) \cdot w(n)$
0, 6	0.0149	1	0.0149
1, 5	0.1447	1	0.1447
2, 4	0.2678	1	0.2678
3	0.3183	1	0.3183 .

$$\begin{aligned} H(z) &= \sum_{n=0}^6 h(n) z^{-n} \\ &= 0.0149(z^0 + z^6) + 0.1447(z^{-1} + z^{-5}) + \\ &\quad 0.2678(z^{-2} + z^{-4}) + 0.3183 z^{-3} . \end{aligned}$$

Linear phase
FIR filter
frequency
response

i) Symmetric impulse response, odd length

$$H(\omega) = e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \cos\left\{\omega\left(\frac{M-1}{2} - n\right)\right\} \right]$$

ii) Symmetric impulse response, even length

$$H(\omega) = e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M}{2}-1} h(n) \cos\left\{\omega\left(\frac{M-1}{2} - n\right)\right\} \right]$$

iii) Anti-symmetric impulse response, odd length

$$H(\omega) = j e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \sin\left\{\omega\left(\frac{M-1}{2} - n\right)\right\} \right]$$

iv) Anti-symmetric impulse response, even length

$$H(\omega) = j e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M}{2}-1} h(n) \sin\left\{\omega\left(\frac{M-1}{2} - n\right)\right\} \right]$$

$$H(\omega) = e^{-j\omega \left(\frac{M-1}{2}\right)} \cdot H_R(\omega)$$

Given, $M=7$ (odd), $h(n)$ - symmetric

$$H_R(\omega) = h\left(\frac{M-1}{2}\right) + 2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \cos \omega \left(\frac{M-1}{2} - n\right)$$

$$= h(3) + 2 \sum_{n=0}^2 h(n) \cos \omega (3-n)$$

$$= 0.3183 + 2 [0.0149 \cos 3\omega + 0.1447 \cos 2\omega \\ + 0.2678 \cos \omega]$$

$$H(e^{j\omega}) = e^{-j3\omega} \cdot [0.3183 + 0.0298 \cos 3\omega + 0.2894 \cos 2\omega \\ + 0.5356 \cos \omega]$$

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Q. Use Hanning windows for previous qn.

$$w(n) = 0.5 - 0.5 \cos\left(\frac{2\pi n}{M-1}\right)$$

<u>n</u>	<u>hd(n)</u>	<u>w(n)</u>	<u>$h(n) = hd(n) - w(n)$</u>
0, 6	0.0149	0	0
1, 5	0.1447	0.25	0.0361
2, 4	0.2678	0.75	0.2008
3	0.3183	1	0.3183

odd symm, $H_2(\omega) = h\left(\frac{M-1}{2}\right) + 2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \cos \omega\left(\frac{M-1}{2}-n\right)$

$$H(e^{j\omega}) = e^{j3\omega} \left[0.3183 + 0.0722 \cos 2\omega + 0.4016 \cos \omega \right]$$

Obtain the ω_{eff} of FIR LPF to meet the specification given below. use suitable window.

Passband edge frequency = 1.5 kHz

Transition width = 0.5 kHz

Stop band attenuation ≥ 50 dB

Sampling frequency = 8 kHz.

Name of the window	Window function $0 \leq n \leq M-1$	Main lobe width	Peak side lobe (dB)	Normalised transition width #	Stop band attenuation (dB)
Rectangular	1	$4\pi/M$	-13	$0.9/(M-1)$	21
Hanning	$0.5 - 0.5\cos\left(\frac{2\pi n}{M-1}\right)$	$8\pi/M$	-32	$3.1/(M-1)$	44
Hamming	$0.54 - 0.46\cos\left(\frac{2\pi n}{M-1}\right)$	$8\pi/M$	-43	$3.3/(M-1)$	53
Blackman	$0.42 - 0.5\cos\left(\frac{2\pi n}{M-1}\right) + 0.08\cos\left(\frac{4\pi n}{M-1}\right)$	$12\pi/M$	-58	$5.5/(M-1)$	75
Keiser*	$\frac{I_0\left[\beta\sqrt{\left(\frac{M-1}{2}\right)^2 - \left(n - \frac{M-1}{2}\right)^2}\right]}{I_0\left[\beta\left(\frac{M-1}{2}\right)\right]}$				> 70

The window to be selected is hamming since the stopband attn is 53 dB.

$$\Delta f = 0.5 \text{ kHz}$$

$$f_{se} = 8 \text{ kHz}$$

$$\Delta F = \frac{3.3}{M}$$

$$\frac{\Delta f}{f_{se}} = \frac{0.5 \text{ kHz}}{8 \text{ kHz}} = \frac{3.3}{M}$$

$$M = 52.8 \approx 53$$

$$\alpha = \frac{M-1}{2}$$

$$\boxed{\alpha = \underline{\underline{26}}}$$

cutoff freq = Passband edge + $\frac{\text{Transition freq}}{2}$

$$f_c = 1.5 \text{ kHz} + \frac{0.5 \text{ kHz}}{2}$$

$$\boxed{f_c = 1.75 \text{ kHz}}$$

$$F_c = \frac{1.75 \text{ kHz}}{8 \text{ kHz}} = 0.21875$$

$$\omega_c = 2\pi F_c = 1.37744 \text{ rad/s}$$

$$H_d(e^{j\omega}) = \begin{cases} 1 e^{-j26\omega} & -1.3744 \leq \omega \leq 1.3744 \\ 0 & \text{otherwise.} \end{cases}$$

$$\boxed{h_d(n) = \frac{1}{\pi(n-26)} [\sin(1.3744)(n-26)]} \rightarrow \text{Infinite}$$

Step 4 :- $h'(n) = h_d(n) \omega(n)$

$$0.54 - 0.46 \cos\left(\frac{2\pi n}{M-1}\right) \quad 0 \leq n \leq M-1$$

$$M = 53$$

$$0.54 - 0.46 \cos\left(\frac{2\pi n}{52}\right) \quad 0 \leq n \leq 52$$

<u>n</u>	<u>$h_d(n)$</u>	<u>$\omega(n)$</u>	<u>$h(n) = h_d(n) - \omega(n)$</u>
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Reference

- Proakis J. G, Manolakis D. G. Mimitris D., “Introduction to Digital Signal Processing” Prentice Hall, India, 2007.

*Thank
you*

