

Digital Signal Processing (ECE – 2222)

List of Formulae

1	DFT pair	$x(n) = \frac{1}{N} \sum_{k=0}^{N-1} X(k) e^{j\frac{2\pi}{N}kn}, \quad n = 0, 1, 2, \dots, N-1$ $X(k) = \sum_{n=0}^{N-1} x(n) e^{-j\frac{2\pi}{N}kn}, \quad k = 0, 1, 2, \dots, N-1$	<p>$x(n)$: Signal of length L $X(k)$: N-point DFT of $x(n)$ $N \geq L$</p>
2	N-point Circular convolution	$x_3(n) = x_1(n) \circledast x_2(n) = \sum_{m=0}^{N-1} x_1(m) x_2(n-m)$	<p>$x_1(n), x_2(n)$: signals of length N or less</p>
3	Pole-zero IIR system	$y(n) = -\sum_{k=1}^N a_k y(n-k) + \sum_{k=0}^M b_k x(n-k)$ $H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}}$	
4	All pole IIR system	$y(n) = \sum_{k=1}^N a_k y(n-k) + b_0 x(n)$ $H(z) = \frac{Y(z)}{X(z)} = \frac{b_0}{1 + \sum_{k=1}^N a_k z^{-k}}$	<p>$x(n)$: input $y(n)$: output $X(z)$: z-transform of $x(n)$</p>
5	All zero FIR system	$y(n) = \sum_{k=0}^M b_k x(n-k)$ $H(z) = \frac{Y(z)}{X(z)} = \sum_{k=0}^M b_k z^{-k}$	<p>$Y(z)$: z-transform of $y(n)$ $H(z)$: System function K: Integer part of $(N+1)/2$ $N \geq M$</p>
6	Cascade realization for IIR filters	$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}} = \prod_{k=1}^K H_k(z)$ $H_k(z) = \frac{b_{k0} + b_{k1} z^{-1} + b_{k2} z^{-2}}{1 + a_{k1} z^{-1} + a_{k2} z^{-2}}$	<p>$C = \frac{b_N}{a_N}$</p>

7	Parallel realization for IIR filters	$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}} = C + \sum_{k=1}^K H_k(z)$ $H_k(z) = \frac{b_{k0} + b_{k1} z^{-1}}{1 + a_{k1} z^{-1} + a_{k2} z^{-2}}$	
8	Frequency sampling realization for FIR filters	$H(z) = \frac{1}{M} (1 - z^{-M}) H_p(z)$ $H_p(z) = \frac{H(0)}{1 - z^{-1}} + \sum_{k=1}^{(M-1)/2} \frac{A(k) - B(k) z^{-1}}{1 - 2 \cos\left(\frac{2\pi k}{M}\right) z^{-1} + z^{-2}} \quad M \text{ odd}$ $H_p(z) = \frac{H(0)}{1 - z^{-1}} + \frac{H\left(\frac{M}{2}\right)}{1 + z^{-1}} + \sum_{k=1}^{\frac{M}{2}-1} \frac{A(k) - B(k) z^{-1}}{1 - 2 \cos\left(\frac{2\pi k}{M}\right) z^{-1} + z^{-2}} \quad M \text{ even}$ $A(k) = H(k) + H(M - k)$ $B(k) = H(k) e^{-j \frac{2\pi k}{M}} + H(M - k) e^{j \frac{2\pi k}{M}}$	<p>$H(\omega)$: Frequency response</p> <p>$H(k)$: $H(\omega)$ at $\omega = \omega_k = \frac{2\pi k}{M}$</p> <p>M: Length of the FIR filter</p>
9	Impulse Invariant Transformation	$z = e^{sT}$ $H(s) = \sum_{k=1}^N \frac{A_k}{s - s_k} \equiv H(z) = \sum_{k=1}^N \frac{A_k}{1 - e^{s_k T} z^{-1}}$	<p>N: Order of the analog filter</p> <p>s_k: Poles of $H(s)$</p> <p>z_k: Zeroes of $H(z)$</p>
10	Bilinear Transformation	$s = \frac{2(1 - z^{-1})}{T(1 + z^{-1})}$ $\Omega = \frac{2}{T} \tan\left(\frac{\omega}{2}\right)$	<p>T: Sampling interval</p> <p>Ω: Analog filter frequency variable</p> <p>ω: Digital filter frequency variable</p>
11	Matched z-transform	$H(s) = \frac{\prod_{k=1}^M (s - z_k)}{\prod_{k=1}^N (s - s_k)} \equiv H(z) = \frac{\prod_{k=1}^M (1 - e^{z_k T} z^{-1})}{\prod_{k=1}^N (1 - e^{s_k T} z^{-1})}$	
12	Butterworth analog low pass filter response	$ H(\Omega) ^2 = \frac{1}{1 + \left(\frac{\Omega}{\Omega_c}\right)^{2N}} = \frac{1}{1 + \epsilon^2 \left(\frac{\Omega}{\Omega_p}\right)^{2N}}$ $N = \frac{\log\left(\frac{1}{\delta_s^2} - 1\right)}{2 \log\left(\frac{\Omega_s}{\Omega_c}\right)} \text{ or } N \geq \log(d) / \log(k)$ <p>Where $d = \sqrt{(1/Ap^2) - 1} / \sqrt{(1/As^2) - 1}$ and $k = \frac{\Omega_p}{\Omega_s}$</p> <p>Ap and As are absolute values</p> $s_k = \Omega_c e^{j\phi_k}$	<p>N: order of the filter</p> <p>$H(\Omega) ^2$: Squared magnitude response</p> <p>Ω_p: Pass band edge frequency</p> <p>Ω_p: Stop band edge frequency</p>

			Ω_c : 3-dB cut-off frequency															
13	Chebyshev analog low pass filter response	$ H(\Omega) ^2 = \frac{1}{1 + \epsilon^2 T_N^2\left(\frac{\Omega}{\Omega_p}\right)}$ $T_N(x) = \begin{cases} \cos(N\cos^{-1}x), & x \leq 1 \\ \cosh(N\cosh^{-1}x), & x > 1 \end{cases}$ $N = \frac{\log \left[\frac{\sqrt{1 - \delta_2^2} + \sqrt{1 - \delta_2^2(1 + \epsilon^2)}}{\epsilon \delta_2} \right]}{\log \left[\left(\frac{\Omega_s}{\Omega_p} \right) + \sqrt{\left(\frac{\Omega_s}{\Omega_p} \right)^2 - 1} \right]}$ $N \geq \cosh^{-1}(1/d)/\cosh^{-1}(1/k)$ <p>Where $d=\sqrt{(1 - Ap^2) - 1}/\sqrt{(1 - As^2) - 1}$ and $k = \frac{\Omega_p}{\Omega_s}$</p> $s_k = r_2 \cos(\phi_k) + jr_1 \sin(\phi_k)$ $r_1 = \Omega_p \frac{\beta^2+1}{2\beta}; \quad r_2 = \Omega_p \frac{\beta^2-1}{2\beta}; \quad \beta = \left[\frac{\sqrt{1+\epsilon^2}+1}{\epsilon} \right]^{1/N}$	$\frac{1}{1+\epsilon^2}$: Pass band edge value of $ H(\Omega) ^2$ δ_2^2 : Stop band edge value of $ H(\Omega) ^2$ s_k : Poles of H(s) $\phi_k = \text{pole angle}$ $= \frac{\pi}{2} + \frac{(2k + 1)\pi}{2N},$ $k= 0, 1, 2, \dots, N-1$															
14	Frequency Transformation for analog filters	<p>Prototype Low pass filter has band edge frequency Ω_p</p> <table><thead><tr><th>Type of Transformation</th><th>Transformation</th><th>Band edge frequency of new filter</th></tr></thead><tbody><tr><td>Low pass</td><td>$s \longrightarrow \frac{\Omega_p}{\Omega_{pn}} s$</td><td>$\Omega_{pn}$</td></tr><tr><td>High pass</td><td>$s \longrightarrow \frac{\Omega_p \Omega_{pn}}{s}$</td><td>$\Omega_{pn}$</td></tr><tr><td>Band pass</td><td>$s \longrightarrow \Omega_p \frac{s^2 + \Omega_l \Omega_u}{s(\Omega_u - \Omega_l)}$</td><td>$\Omega_l, \Omega_u$</td></tr><tr><td>Band stop</td><td>$s \longrightarrow \Omega_p \frac{s(\Omega_u - \Omega_l)}{s^2 + \Omega_l \Omega_u}$</td><td>$\Omega_l, \Omega_u$</td></tr></tbody></table>	Type of Transformation	Transformation	Band edge frequency of new filter	Low pass	$s \longrightarrow \frac{\Omega_p}{\Omega_{pn}} s$	Ω_{pn}	High pass	$s \longrightarrow \frac{\Omega_p \Omega_{pn}}{s}$	Ω_{pn}	Band pass	$s \longrightarrow \Omega_p \frac{s^2 + \Omega_l \Omega_u}{s(\Omega_u - \Omega_l)}$	Ω_l, Ω_u	Band stop	$s \longrightarrow \Omega_p \frac{s(\Omega_u - \Omega_l)}{s^2 + \Omega_l \Omega_u}$	Ω_l, Ω_u	
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15	Frequency Transformation for digital filters	Prototype Low pass filter has band edge frequency ω_p		
		Type of Transformation	Transformation	Parameters
		Low pass	$z^{-1} \rightarrow \frac{z^{-1} - a}{1 - az^{-1}}$	$\omega_{pn} = \text{band edge frequency of new filter}$ $a = \frac{\sin[(\omega_p - \omega_{pn})/2]}{\sin[(\omega_p + \omega_{pn})/2]}$
		High pass	$z^{-1} \rightarrow \frac{z^{-1} + a}{1 + az^{-1}}$	$\omega_{pn} = \text{band edge frequency of new filter}$ $a = \frac{\cos[(\omega_p - \omega_{pn})/2]}{\cos[(\omega_p + \omega_{pn})/2]}$
		Band pass	$z^{-1} \rightarrow -\frac{z^{-2} - a_1z^{-1} + a_2}{a_2z^{-2} - a_1z^{-1} + 1}$	$\omega_l = \text{lower band edge frequency}$ $\omega_u = \text{upper band edge frequency}$ $a_1 = \frac{-2\alpha K}{(K+1)}$ $a_2 = \frac{(K-1)}{(K+1)}$ $\alpha = \frac{\cos[(\omega_u + \omega_l)/2]}{\cos[(\omega_u - \omega_l)/2]}$ $K = \cot\left(\frac{\omega_u - \omega_l}{2}\right) \tan\left(\frac{\omega_p}{2}\right)$
		Band stop	$z^{-1} \rightarrow \frac{z^{-2} - a_1z^{-1} + a_2}{a_2z^{-2} - a_1z^{-1} + 1}$	$\omega_l = \text{lower band edge frequency}$ $\omega_u = \text{upper band edge frequency}$ $a_1 = \frac{-2\alpha}{(K+1)}$ $a_2 = \frac{(1-K)}{(1+K)}$ $\alpha = \frac{\cos[(\omega_u + \omega_l)/2]}{\cos[(\omega_u - \omega_l)/2]}$ $K = \tan\left(\frac{\omega_u - \omega_l}{2}\right) \tan\left(\frac{\omega_p}{2}\right)$

16	Linear phase FIR filter frequency response	<div>i) Symmetric impulse response, odd length$H(\omega) = e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \cos \left\{ \omega \left(\frac{M-1}{2} - n \right) \right\} \right]$</div> <div>ii) Symmetric impulse response, even length$H(\omega) = e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M}{2}-1} h(n) \cos \left\{ \omega \left(\frac{M-1}{2} - n \right) \right\} \right]$</div> <div>iii) Anti-symmetric impulse response, odd length$H(\omega) = j e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \sin \left\{ \omega \left(\frac{M-1}{2} - n \right) \right\} \right]$</div> <div>iv) Anti-symmetric impulse response, even length$H(\omega) = j e^{-j\omega\left(\frac{M-1}{2}\right)} \left[2 \sum_{n=0}^{\frac{M}{2}-1} h(n) \sin \left\{ \omega \left(\frac{M-1}{2} - n \right) \right\} \right]$</div>	<div>M: length of the filter</div> <div>$H(\omega)$: Frequency response</div>																																			
17	Linear phase FIR filter design using window functions	<div>Window functions for FIR filter design</div> <table><thead><tr><th>Name of the window</th><th>Window function $0 \leq n \leq M-1$</th><th>Main lobe width</th><th>Peak side lobe (dB)</th><th>Normalized transition width#</th><th>Stop band attenuation (dB)</th></tr></thead><tbody><tr><td>Rectangular</td><td>1</td><td>$4\pi/M$</td><td>-13</td><td>$0.9/(M-1)$</td><td>21</td></tr><tr><td>Hanning</td><td>$0.5 - 0.5 \cos \left(\frac{2\pi n}{M-1} \right)$</td><td>$8\pi/M$</td><td>-32</td><td>$3.1/(M-1)$</td><td>44</td></tr><tr><td>Hamming</td><td>$0.54 - 0.46 \cos \left(\frac{2\pi n}{M-1} \right)$</td><td>$8\pi/M$</td><td>-43</td><td>$3.3/(M-1)$</td><td>53</td></tr><tr><td>Blackman</td><td>$0.42 - 0.5 \cos \left(\frac{2\pi n}{M-1} \right) + 0.08 \cos \left(\frac{4\pi n}{M-1} \right)$</td><td>$12\pi/M$</td><td>-58</td><td>$5.5/(M-1)$</td><td>75</td></tr><tr><td>Keiser*</td><td>$\frac{I_0 \left[\beta \sqrt{\left(\frac{M-1}{2} \right)^2 - \left(n - \frac{M-1}{2} \right)^2} \right]}{I_0 \left[\beta \left(\frac{M-1}{2} \right) \right]}$</td><td></td><td></td><td></td><td>> 70</td></tr></tbody></table> <div>*Keiser window parameters can be controlled by β. $I_0[.]$ is modified Bessel function.</div>	Name of the window	Window function $0 \leq n \leq M-1$	Main lobe width	Peak side lobe (dB)	Normalized transition width#	Stop band attenuation (dB)	Rectangular	1	$4\pi/M$	-13	$0.9/(M-1)$	21	Hanning	$0.5 - 0.5 \cos \left(\frac{2\pi n}{M-1} \right)$	$8\pi/M$	-32	$3.1/(M-1)$	44	Hamming	$0.54 - 0.46 \cos \left(\frac{2\pi n}{M-1} \right)$	$8\pi/M$	-43	$3.3/(M-1)$	53	Blackman	$0.42 - 0.5 \cos \left(\frac{2\pi n}{M-1} \right) + 0.08 \cos \left(\frac{4\pi n}{M-1} \right)$	$12\pi/M$	-58	$5.5/(M-1)$	75	Keiser*	$\frac{I_0 \left[\beta \sqrt{\left(\frac{M-1}{2} \right)^2 - \left(n - \frac{M-1}{2} \right)^2} \right]}{I_0 \left[\beta \left(\frac{M-1}{2} \right) \right]}$				> 70
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		#Transition width is normalized to 2π or equivalently to sampling frequency F_s													
18	Frequency sampling design of FIR filter	$h(n) = \frac{1}{M} \left\{ G(0) + 2 \sum_{k=1}^{\frac{(M-1)}{2}} G(k) \cos \frac{2\pi k}{M} \left(n + \frac{1}{2} \right) \right\},$ <p style="text-align: center;"><i>M odd</i></p> $h(n) = \frac{1}{M} \left\{ G(0) + 2 \sum_{k=1}^{\frac{M}{2}-1} G(k) \cos \frac{2\pi k}{M} \left(n + \frac{1}{2} \right) \right\},$ <p style="text-align: center;"><i>M even</i></p> $h(n) = \frac{1}{M} \left[H(0) + 2 \sum_{k=1}^{\frac{M-1}{2}} \operatorname{Re} \left\{ H(k) e^{\frac{j2\pi nk}{M}} \right\} \right] \text{ M odd}$ $h(n) = \frac{1}{M} \left[H(0) + 2 \sum_{k=1}^{\frac{M}{2}-1} \operatorname{Re} \left\{ H(k) e^{\frac{j2\pi nk}{M}} \right\} \right] \text{ M even}$ $H_d(\omega) = H_r(\omega) e^{-j\omega(M-1)/2}$ <p>Where $\omega = \frac{2\pi k}{M}$</p> $H(k) = H_r(k) e^{\frac{-j2\pi k(M-1)}{2}}$	M: length of the filter $H_d(\omega)$: Desired frequency response $G(k) = (-1)^k H_r \left(\frac{2\pi k}{M} \right)$												
19	Non-parametric power spectrum estimators	<table><thead><tr><th>Estimate</th><th>Quality factor</th><th>Computational requirement</th></tr></thead><tbody><tr><td>Bartlett</td><td>Q_B $= 1.1N\Delta f$</td><td>$N \log_2 \frac{0.9}{\Delta f}$</td></tr><tr><td>Welch (50% overlap)</td><td>Q_W $= 1.39N\Delta f$</td><td>$N \log_2 \frac{5.12}{\Delta f}$</td></tr><tr><td>Blackman-Tukey</td><td>Q_{BT} $= 2.34N\Delta f$</td><td>$N \log_2 \frac{1.28}{\Delta f}$</td></tr></tbody></table>	Estimate	Quality factor	Computational requirement	Bartlett	Q_B $= 1.1N\Delta f$	$N \log_2 \frac{0.9}{\Delta f}$	Welch (50% overlap)	Q_W $= 1.39N\Delta f$	$N \log_2 \frac{5.12}{\Delta f}$	Blackman-Tukey	Q_{BT} $= 2.34N\Delta f$	$N \log_2 \frac{1.28}{\Delta f}$	<p><i>Quality factor</i></p> $Q = \frac{\{E[\text{estimate}]\}^2}{\text{var}[\text{estimate}]}$ <p>Δf: Frequency resolution</p> <p>N: Data frame length</p>
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