

EMA/ME 601 - Homework 3

A new space vehicle, called the General Purpose Spacecraft (GPSC), is being developed by the Jet Propulsion Lab (JPL) to perform a Lunar-surveying mission. The corresponding FEM is illustrated in Fig. 1. The NASTRAN bulk data deck is listed in Table 1 and a listing of the spacecraft's rigid body mass properties, produced by NASTRAN's Grid Point Weight Generator module, is presented in Table 2. Note that the units are weight. A test article has been developed and a modal survey is being planned. The JPL engineers need some help, but they readily know that your very esteemed and famous professor is very busy and important, and could never be bothered with their trivial problems. So, they come to you for help in selecting target modes and sensor locations. A MATLAB file, called "gpsc.mat" has been placed on Dr. Dan's class webpage. It contains a mass and stiffness matrix, "M" and "K", respectively, for a reduced representation of the GPSC, which is not constrained in any way. During the test, the spacecraft will be pinned at the base of the legs pictured below. Vector "DOF1" contains a listing of the dof and their order for "M" and "K". Thirty fixed interface FEM modes, "PHI", have already been supplied and do not have to be recomputed. Vector "DOF2" contains a listing of the dof and their order for "PHI". Vector "w" contains a listing of the corresponding modes in Hertz. I suggest that you reorder all matrices to give a numerically ascending sort. Make listings, plots, etc., to show details of computations and summarize results. Show listings of all MATLAB functions used in this analysis.

1. Generate a MATLAB function to compute *Effective Mass* and use it to rank the fixed interface modes of the spacecraft. Select a set of target modes based upon each of them having at least 5.0% effective mass in any of the six rigid body directions. Determine the total effective mass for your target mode set in each rigid body direction and comment on the sets dynamic completeness.
2. The target modes identified in task 1 will have to be identified during the modal test and then later correlated with the FEM representation. Generate MATLAB functions to rank candidate sensor locations based on *Modal Kinetic Energy* and *Effective Independence*. Pick a single initial candidate set of sensor locations and use your MATLAB functions to select a final set for the test that will accurately identify your target modes using each of the sensor placement techniques. The final sensor sets should contain $(n_{target} + 5)$ locations.

3. Use the *Modal Assurance Criterion* and any other measure that might be appropriate to determine which of the two sensor sets produces the most independent target mode partitions and the greatest target mode response signal strength.

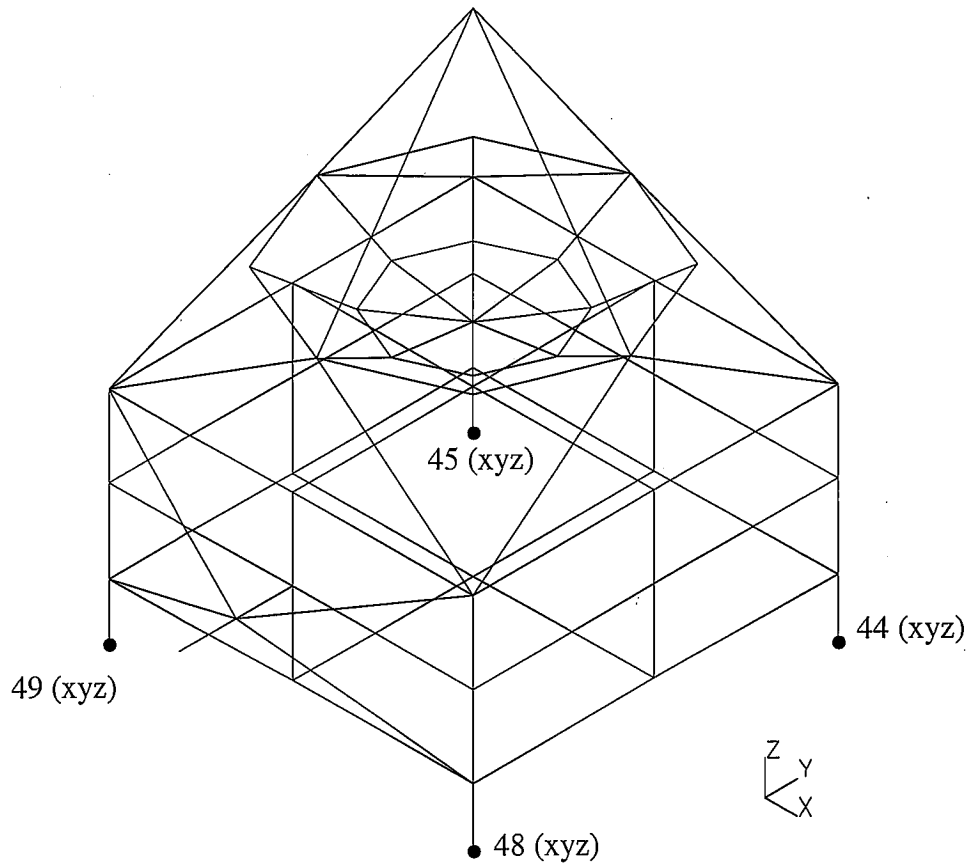


Fig. 1. GPSC finite element model.

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1
1  GENERAL PURPOSE SPACECRAFT (GPSC) - FEM
  FINITE ELEMENT MODEL (FEM)
0  NORMAL MODES ANALYSIS
0
0      A  DISPLACEMENT SET
0      -1-    -2-    -3-    -4-    -5-    -6-    -7-    -8-    -9-    -10-

1=      35-1    35-2    35-3    42-1    42-2    42-3    36-1    36-2    36-3    50-1 = 10
11=     50-2    50-3    43-1    43-2    43-3    46-1    46-2    46-3    47-1    47-2 = 20
21=     47-3    39-1    39-2    39-3    41-1    41-2    41-3    25-1    25-2    25-3 = 30
31=     33-1    33-2    33-3    34-1    34-2    34-3    26-1    26-2    26-3    37-1 = 40
41=     37-2    37-3    28-1    28-2    28-3    31-1    31-2    31-3    38-1    38-2 = 50
51=     38-3    30-1    30-2    30-3    40-1    40-2    40-3    23-1    23-2    23-3 = 60
61=     24-1    24-2    24-3    27-1    27-2    27-3    29-1    29-2    29-3    32-1 = 70
71=     32-2    32-3    19-1    19-2    19-3    20-1    20-2    20-3    21-1    21-2 = 80
81=     21-3    22-1    22-2    22-3    10-1    10-2    10-3    18-1    18-2    18-3 = 90
91=      2-1     2-2     2-3     3-1     3-2     3-3    11-1    11-2    11-3     5-1 = 100
101=     5-2     5-3    13-1    13-2    13-3    14-1    14-2    14-3     6-1     6-2 = 110
111=     6-3     9-1     9-2     9-3    17-1    17-2    17-3     1-1     1-2     1-3 = 120
121=    16-1    16-2    16-3    15-1    15-2    15-3     8-1     8-2     8-3     7-1 = 130
131=     7-2     7-3     4-1     4-2     4-3    12-1    12-2    12-3

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Table 1. NASTRAN Bulk Data Deck

```

$-----
$  GENERAL  PURPOSE  SPACECRAFT  MODEL  (GPSC)
$-----
$  Last modified:  Chris Flanigan  13-May-94
$                   Dan Kammer     17-Oct-96  Transformed to CSA
$-----
$
$
$  Concentrated mass data
$  -----
$
$      2      3      4      5      6      7      8      9
$      EID    G      CID    M
CONM2  1001   18      10     200.
CONM2  1002   42      10     425.
CONM2  1003   40      10     250.
$
$  Local coordinate systems
$  -----
$
$      CID      RID      A1      A2      A3      B1      B2      B3
$
CORD2R  10      0      0.      0.      0.      0.      0.      1.
        1.      0.      0.
CORD2C  20      10      0.      0.      120.    120.    0.      120.
        0.      0.      0.
$
$  Grid point bulk data
$  -----
$
$      ID      CP      X1      X2      X3      CD
$
GRID    1      20      60.000  2.4E-14  0.00000  10
GRID    2      20      60.000  17.500  0.00000  10
GRID    3      20      58.628  12.569  12.758  10
GRID    4      20      58.628  347.43  -12.758  10
GRID    5      20      58.628  12.569  -12.758  10
GRID    6      20      57.223  2.7E-14  18.042  10
GRID    7      20      60.000  342.50  0.00000  10
GRID    8      20      57.223  360.00  -18.042  10
GRID    9      20      58.628  347.43  12.758  10
GRID   10      20      60.000  35.000  0.00000  10
GRID   11      20      54.844  26.341  24.335  10
GRID   12      20      54.844  333.66  -24.335  10
GRID   13      20      54.844  26.341  -24.335  10
GRID   14      20      49.149  3.7E-14  34.415  10
GRID   15      20      60.000  325.00  0.00000  10
GRID   16      20      49.149  360.00  -34.415  10
GRID   17      20      54.844  333.66  24.335  10
GRID   18      20      0.00000  0.00000  0.00000  10
GRID   19      10      39.520  39.520  48.000  10
GRID   20      10     -39.520  39.520  48.000  10
GRID   21      10      39.520  -39.520  48.000  10
GRID   22      10     -39.520  -39.520  48.000  10
GRID   23      10      3.8E-06  39.520  48.000  10

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GRID	24	10	39.520-3.8E-06	48.000	10
GRID	25	10	39.520 39.520	30.000	10
GRID	26	10	-39.520 39.520	30.000	10
GRID	27	10	-39.520 3.8E-06	48.000	10
GRID	28	10	39.520 -39.520	30.000	10
GRID	29	10	-3.8E-06 -39.520	48.000	10
GRID	30	10	-3.8E-06 -51.520	30.000	10
GRID	31	10	-39.520 -39.520	30.000	10
GRID	32	10	0.00000 0.00000	48.000	10
GRID	33	10	3.8E-06 39.520	30.000	10
GRID	34	10	39.520-3.8E-06	30.000	10
GRID	35	10	39.520 39.520	12.000	10
GRID	36	10	-39.520 39.520	12.000	10
GRID	37	10	-39.520 3.8E-06	30.000	10
GRID	38	10	-3.8E-06 -39.520	30.000	10
GRID	39	10	39.520 -39.520	12.000	10
GRID	40	10	-3.8E-06 -63.520	30.000	10
GRID	41	10	-39.520 -39.520	12.000	10
GRID	42	10	3.8E-06 39.520	12.000	10
GRID	43	10	39.520-3.8E-06	12.000	10
GRID	44	10	39.520 39.520	0.00000	10
GRID	45	10	-39.520 39.520	0.00000	10
GRID	46	10	-39.520 3.8E-06	12.000	10
GRID	47	10	-3.8E-06 -39.520	12.000	10
GRID	48	10	39.520 -39.520	0.00000	10
GRID	49	10	-39.520 -39.520	0.00000	10
GRID	50	10	0.00000 0.00000	12.000	10

\$

\$ Centerline grid at the interface plane

\$

\$

	ID	CP	X1	X2	X3	CD
GRID	99	10	0.	0.	0.	0

\$

	EID	REFGRID	REFC	WT1	C1	G1	G2
RBE3	99	99	123456	1.0	123	44	45
	48	49					

\$

\$

\$ Shell elements

\$

\$

	EID	PID	G1	G2	G3
CTRIA3	1	13	3	6	1
CTRIA3	2	13	2	3	1
CTRIA3	3	13	5	2	1
CTRIA3	4	13	8	5	1
CTRIA3	5	13	4	8	1
CTRIA3	6	13	7	4	1
CTRIA3	7	13	9	7	1
CTRIA3	8	13	6	9	1

\$

	EID	PID	G1	G2	G3	G4
CQUAD4	9	13	6	3	11	14
CQUAD4	10	13	3	2	10	11
CQUAD4	11	13	2	5	13	10
CQUAD4	12	13	5	8	16	13

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CQUAD4	13	13	8	4	12	16
CQUAD4	14	13	4	7	15	12
CQUAD4	15	13	7	9	17	15
CQUAD4	16	13	9	6	14	17

\$

\$

\$ Bar elements

\$ -----

\$

\$	EID	PID	GA	GB	X1	X2	X3
CBAR	17	5	41	49	1.000	0.000	0.000
CBAR	18	5	36	45	1.000	0.000	0.000
CBAR	19	5	39	48	1.000	0.000	0.000
CBAR	20	5	35	44	1.000	0.000	0.000
CBAR	21	2	46	41	0.000	0.000	1.000
CBAR	22	2	36	46	0.000	0.000	1.000
CBAR	23	2	41	47	0.000	0.000	1.000
CQUAD4	24	10	50	47	41	46	
CQUAD4	25	10	50	46	36	42	
CBAR	26	2	42	36	0.000	0.000	1.000
CBAR	27	2	47	39	0.000	0.000	1.000
CQUAD4	28	10	50	43	39	47	
CQUAD4	29	10	50	42	35	43	
CBAR	30	2	35	42	0.000	0.000	1.000
CBAR	31	2	39	43	0.000	0.000	1.000
CBAR	32	2	43	35	0.000	0.000	1.000
CBAR	33	5	31	41	1.000	0.000	0.000
CQUAD4	34	11	37	46	41	31	
CQUAD4	35	11	37	26	36	46	
CBAR	36	5	26	36	1.000	0.000	0.000
CBAR	37	4	41	30	0.000	0.000	1.000
CQUAD4	38	11	38	31	41	47	
CQUAD4	39	11	33	42	36	26	
CBAR	40	4	30	39	0.000	0.000	1.000
CQUAD4	41	11	38	47	39	28	
CQUAD4	42	11	33	25	35	42	
CBAR	43	5	28	39	1.000	0.000	0.000
CQUAD4	44	11	34	28	39	43	
CQUAD4	45	11	34	43	35	25	
CBAR	46	5	25	35	1.000	0.000	0.000
CBAR	47	2	30	40	0.000	0.000	1.000
CBAR	48	2	38	30	0.000	0.000	1.000
CBAR	49	5	22	31	1.000	0.000	0.000
CQUAD4	50	11	37	31	22	27	
CQUAD4	51	11	37	27	20	26	
CBAR	52	5	20	26	1.000	0.000	0.000
CBAR	53	4	22	30	0.000	0.000	1.000
CQUAD4	54	11	38	29	22	31	
CQUAD4	55	11	33	26	20	23	
CBAR	56	4	21	30	0.000	0.000	1.000
CQUAD4	57	11	38	28	21	29	
CQUAD4	58	11	33	23	19	25	
CBAR	59	5	21	28	1.000	0.000	0.000
CQUAD4	60	11	34	24	21	28	
CQUAD4	61	11	34	25	19	24	
CBAR	62	5	19	25	1.000	0.000	0.000
CBAR	63	3	27	22	0.000	0.000	1.000

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CBAR	64	3	20	27	0.000	0.000	1.000
CBAR	65	3	22	29	0.000	0.000	1.000
CQUAD4	66	12	32	27	22	29	
CQUAD4	67	12	32	23	20	27	
CBAR	68	3	23	20	0.000	0.000	1.000
CBAR	69	3	29	21	0.000	0.000	1.000
CQUAD4	70	12	32	29	21	24	
CQUAD4	71	12	32	24	19	23	
CBAR	72	3	19	23	0.000	0.000	1.000
CBAR	73	3	21	24	0.000	0.000	1.000
CBAR	74	3	24	19	0.000	0.000	1.000
CBAR	75	4	22	15	0.000	0.000	1.000
CBAR	76	4	15	21	0.000	0.000	1.000
CBAR	77	4	21	14	0.000	0.000	1.000
CBAR	78	4	14	19	0.000	0.000	1.000
CBAR	79	4	19	10	0.000	0.000	1.000
CBAR	80	4	10	20	0.000	0.000	1.000
CBAR	81	4	20	16	0.000	0.000	1.000
CBAR	82	4	16	22	0.000	0.000	1.000
CBAR	83	4	15	18	0.000	0.000	1.000
CBAR	84	4	14	18	0.000	0.000	1.000
CBAR	85	4	10	18	0.000	0.000	1.000
CBAR	86	4	16	18	0.000	0.000	1.000
CBAR	87	2	47	50	0.000	0.000	1.000
CBAR	88	2	43	50	0.000	0.000	1.000
CBAR	89	2	42	50	0.000	0.000	1.000
CBAR	90	2	46	50	0.000	0.000	1.000

\$

\$ CONSTRAIN BASE OF LEGS

\$

\$

	SID	C	G1	G2	G3	G4
SPC1	10	123456	44	45	48	49

\$

\$

\$ GENERAL PURPOSE SPACECRAFT - pretest model

\$

\$

\$ MATERIAL AND PHYSICAL PROPERTY DATA

\$

\$

	PID	MID	A	I1	I2	J
PBAR	2	1	4.	1.33	1.33	2.667
PBAR	3	1	1.	.0833	.0833	.1667
PBAR	4	1	.7654	.04662	.04662	.09324
PBAR	5	1	9.	6.75	6.75	12.5

\$

\$

	PID	MID	T	MID2	12I/T3	MID3	TS/T	NSM
PSHELL	10	1	1.	1		1		.5
PSHELL	11	1	.25	1		1		
PSHELL	12	1	.25	1		1		
PSHELL	13	1	.5	1		1		

\$

	MID	E	G	NU	RHO
MAT1	1	1.E+07		.3	.1

\$

TABLE 2. NASTRAN Grid Point Generator

1 GENERAL PURPOSE SPACECRAFT (GPSC) - FEM OCTOBER 24, 1996 CSA/NASTRAN 2/08/96 PAGE 14
 FINITE ELEMENT MODEL (FEM) MATRIX PROCESSING FOR SUPERELEMENT 0 (RESIDUAL)
 0 NORMAL MODES ANALYSIS

OUTPUT FROM GRID POINT WEIGHT GENERATOR

REFERENCE POINT = 0

MO - RIGID BODY MASS MATRIX IN BASIC COORDINATE SYSTEM

```

***
* 5.712471E+03 .000000E+00 .000000E+00 .000000E+00 1.218244E+05 2.064367E+02 *
* .000000E+00 5.712471E+03 .000000E+00 -1.218244E+05 .000000E+00 6.225555E-04 *
* .000000E+00 .000000E+00 5.712471E+03 -2.064367E+02 -6.225555E-04 .000000E+00 *
* .000000E+00 -1.218244E+05 -2.064367E+02 1.140252E+07 -1.265985E-01 1.039334E-02 *
* 1.218244E+05 .000000E+00 -6.225555E-04 -1.265985E-01 9.685567E+06 3.085192E+05 *
* 2.064367E+02 6.225555E-04 .000000E+00 1.039334E-02 3.085192E+05 9.654570E+06 *
***

```

S - TRANSFORMATION MATRIX FOR SCALAR MASS PARTITION

```

***
* 1.000000E+00 .000000E+00 .000000E+00 *
* .000000E+00 1.000000E+00 .000000E+00 *
* .000000E+00 .000000E+00 1.000000E+00 *
***

```

DIRECTION

MASS AXIS SYSTEM (S)	MASS	X-C.G.	Y-C.G.	Z-C.G.
X	5.712471E+03	.000000E+00	-3.613790E-02	2.132604E+01
Y	5.712471E+03	1.089818E-07	.000000E+00	2.132604E+01
Z	5.712471E+03	1.089818E-07	-3.613790E-02	.000000E+00

I(S) - INERTIAS RELATIVE TO C.G.

```

***
* 8.804481E+06 1.266210E-01 -2.366998E-02 *
* 1.266210E-01 7.087536E+06 -3.041167E+05 *
* -2.366998E-02 -3.041167E+05 9.654562E+06 *
***

```

I(Q) - PRINCIPAL INERTIAS

```

***
* 8.804481E+06 *
* 7.051999E+06 *
* 9.690099E+06 *
***

```

Q - TRANSFORMATION MATRIX

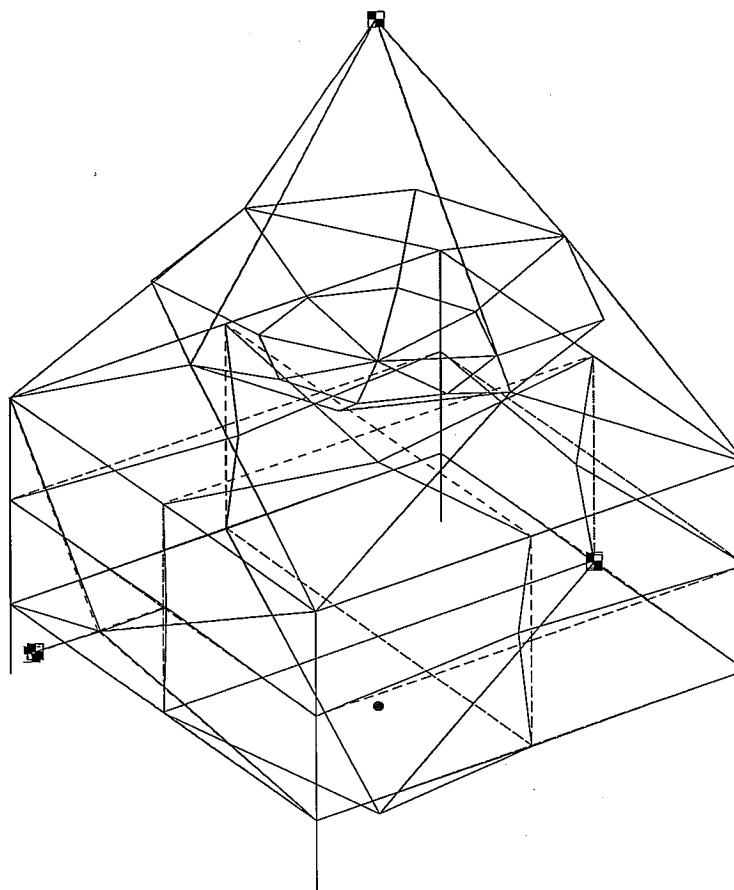
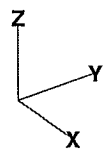
$$I(Q) = QT*IBAR(S)*Q$$

```

***
* 1.000000E+00 .000000E+00 .000000E+00 *
* .000000E+00 9.932418E-01 1.160630E-01 *
* .000000E+00 -1.160630E-01 9.932418E-01 *
***

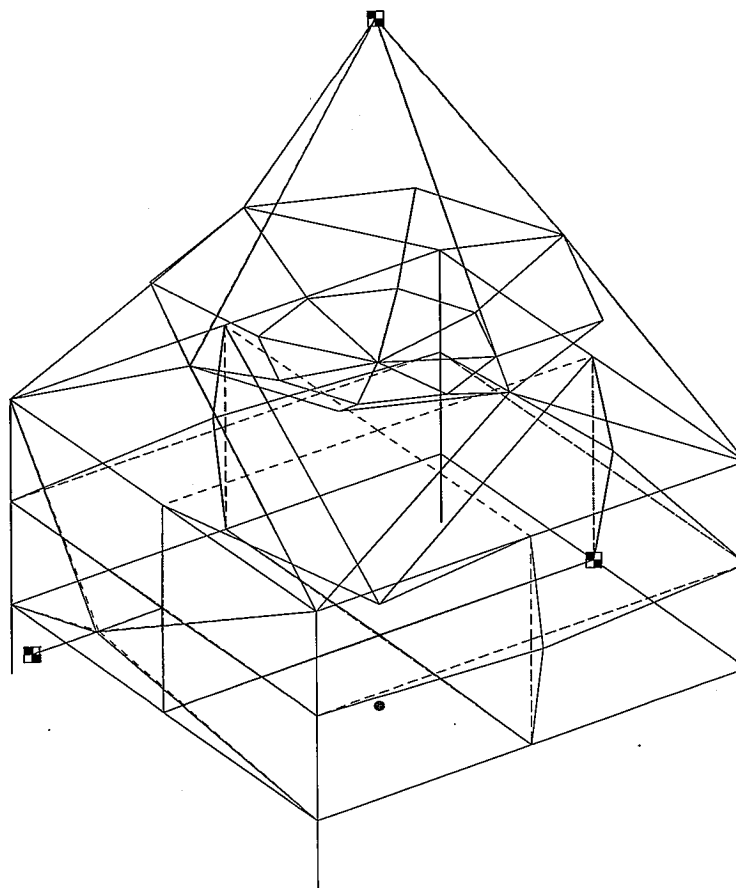
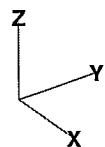
```


V1
C1



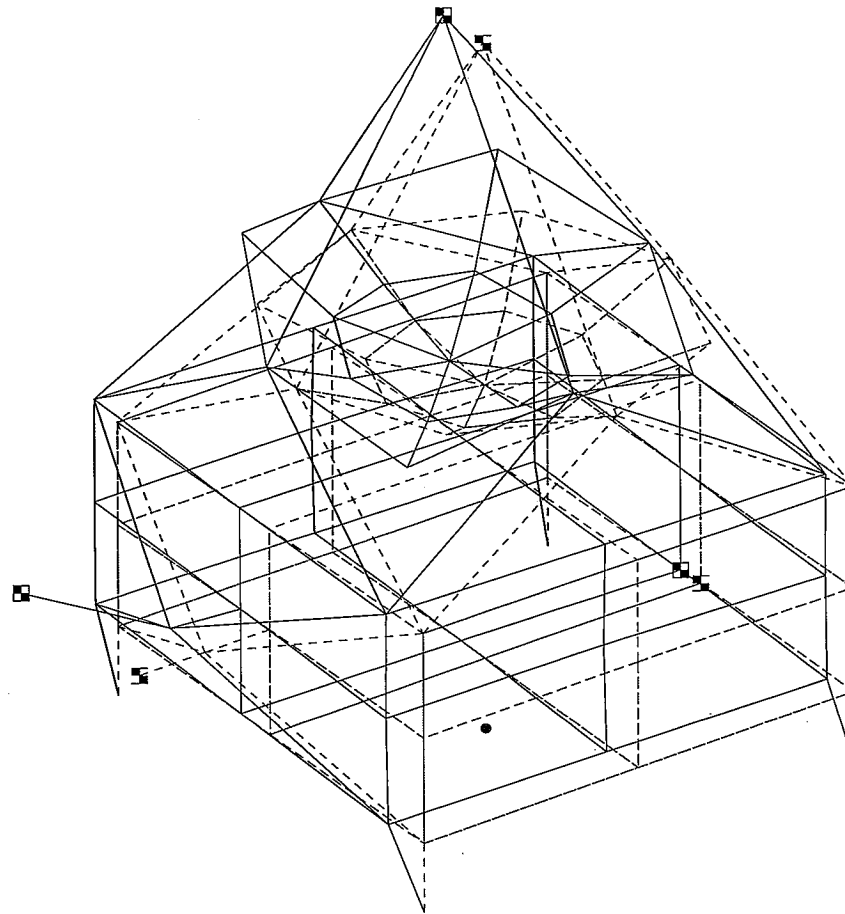
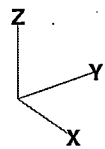
Output Set: Mode 1 13.58455 Hz
Deformed(0.631): Total Translation

V1
C1



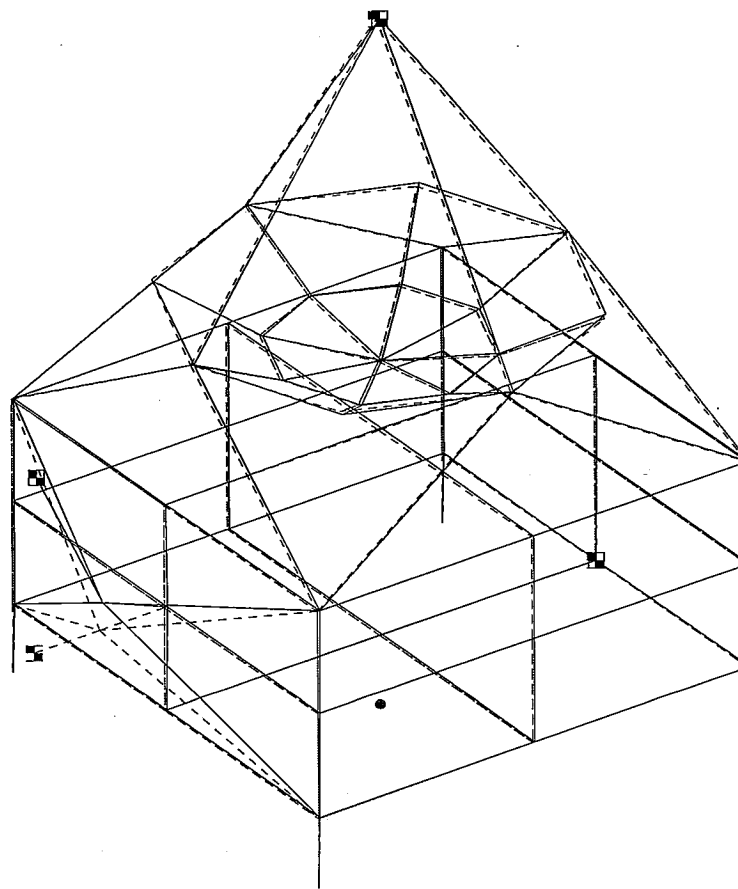
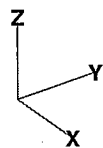
Output Set: Mode 2 16.03862 Hz
Deformed(3.116): Total Translation

V1
C1



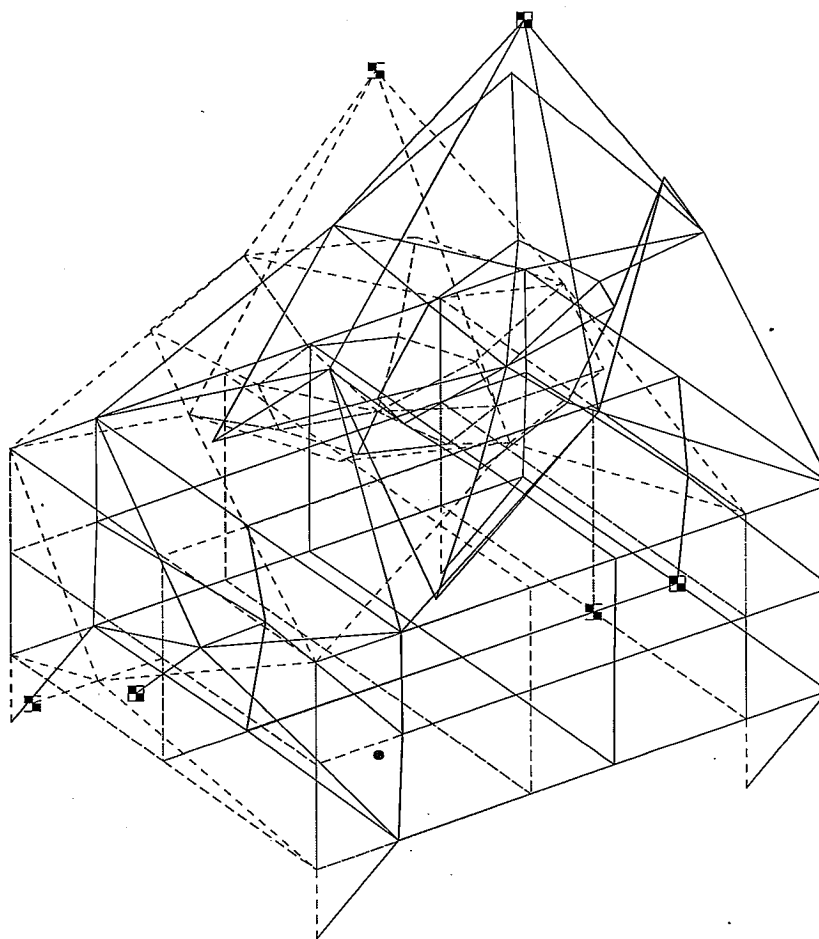
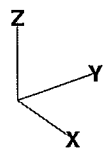
Output Set: Mode 3 17.55071 Hz
Deformed(0.866): Total Translation

V1
C1



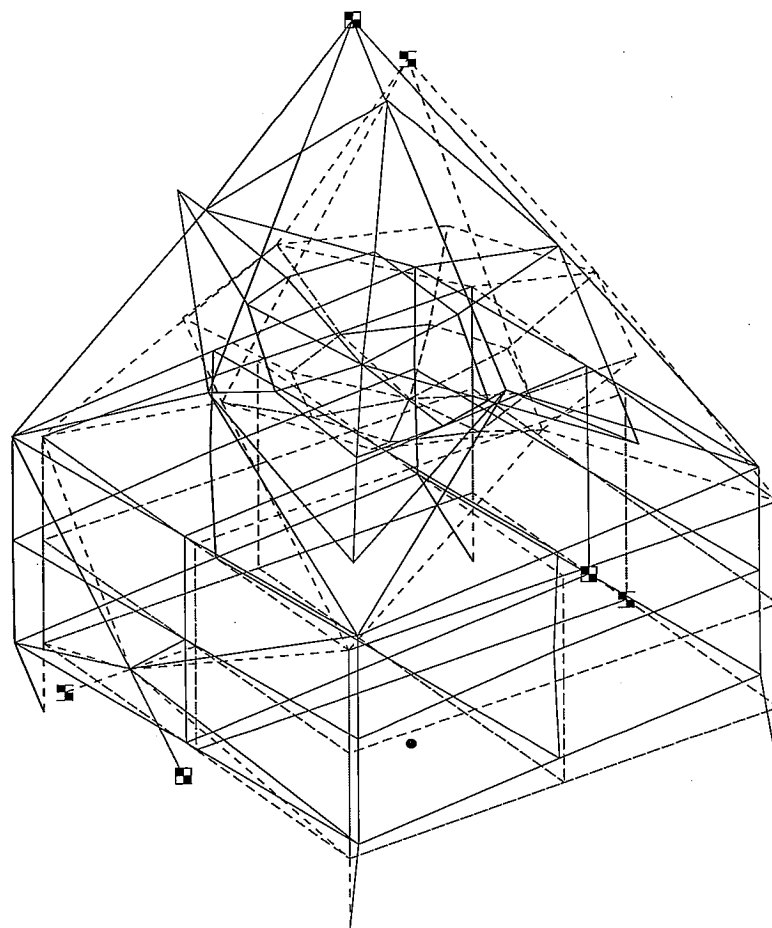
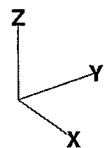
Output Set: Mode 4 17.65018 Hz
Deformed(1.234): Total Translation

V1
C1



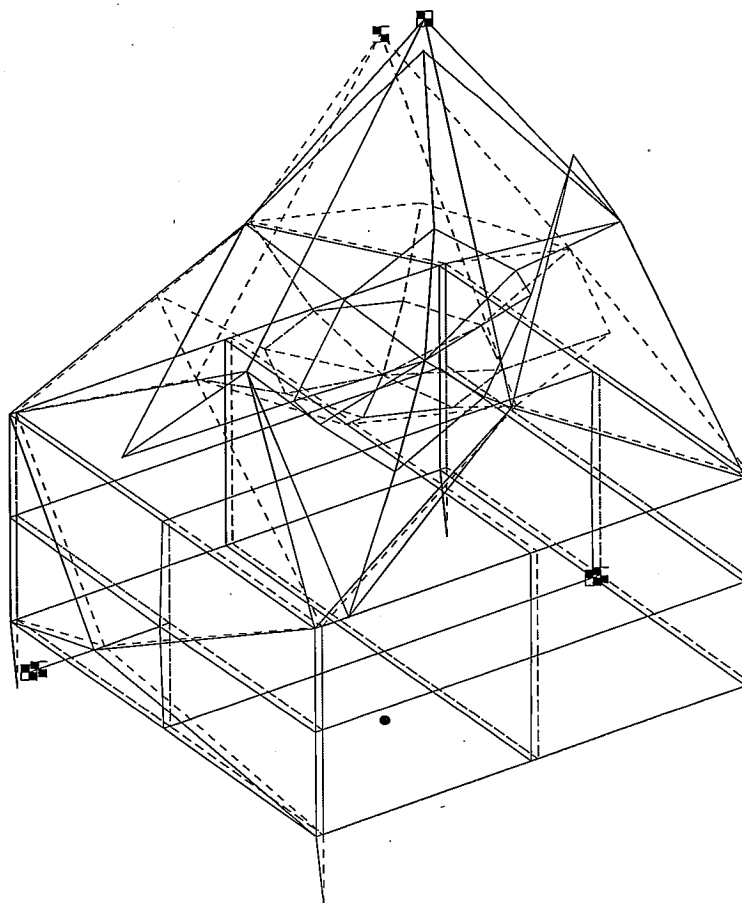
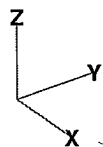
Output Set: Mode 5 18.63145 Hz
Deformed(0.482): Total Translation

V1
C1



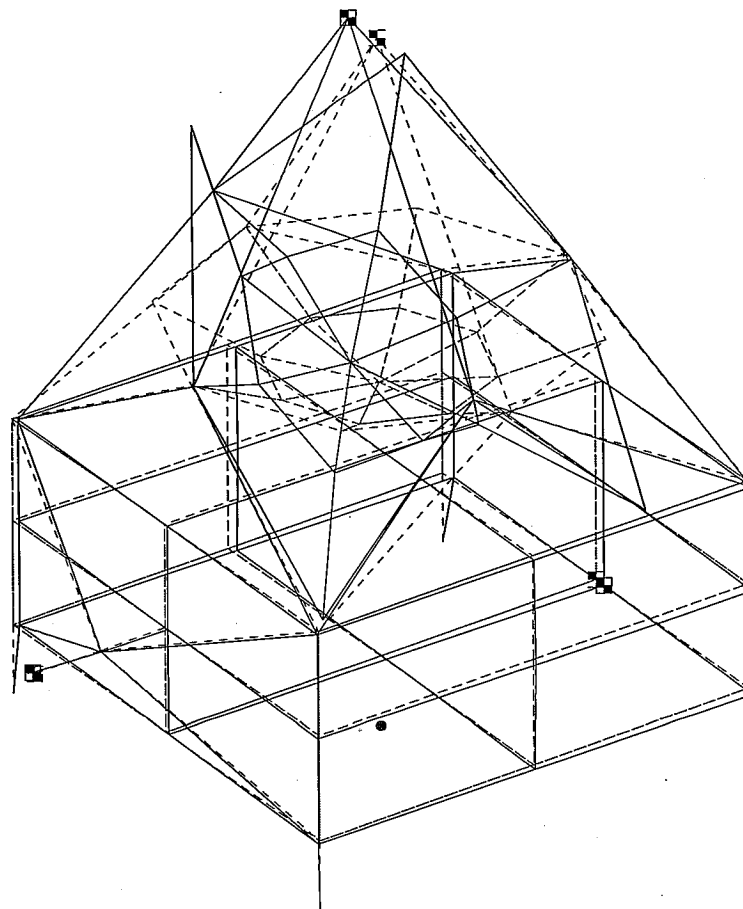
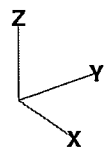
Output Set: Mode 6 20.73723 Hz
Deformed(0.778): Total Translation

V1
C1



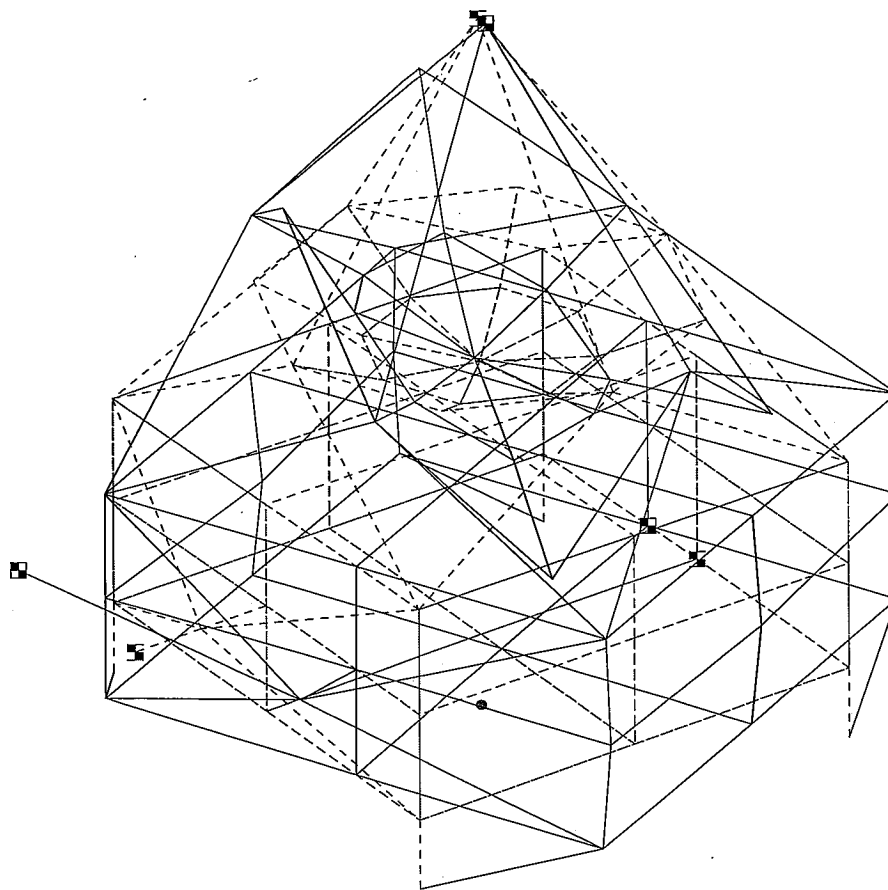
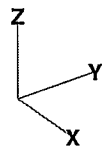
Output Set: Mode 7 24.9424 Hz
Deformed(2.258): Total Translation

V1
C1



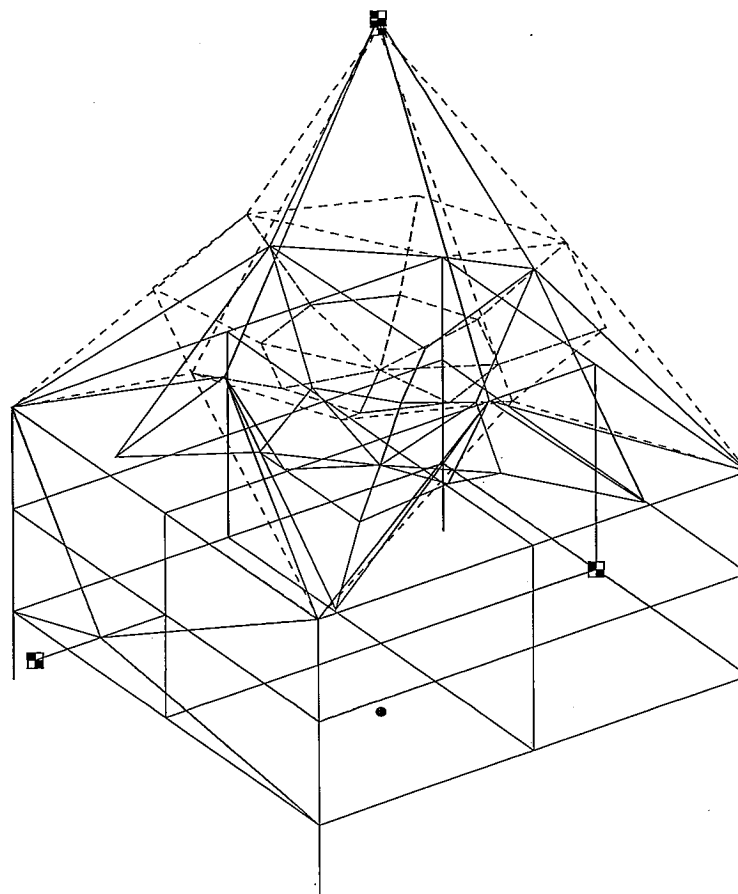
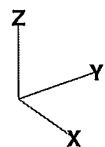
Output Set: Mode 8 25.03358 Hz
Deformed(2.212): Total Translation

V1
C1



Output Set: Mode 9 29.94975 Hz
Deformed(0.419): Total Translation

V1
C1



Output Set: Mode 10 37.09415 Hz
Deformed(2.287): Total Translation