Feedback Linearization for a Nonlinear Quarter-Car Model

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Overview

1. Model

2. Controller Design

3. Simulation

Model

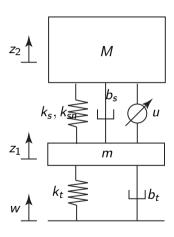


Figure: Quarter-Car Model

$$m\ddot{z}_1 = F_s + F_d - F_t - F_b - u \tag{1}$$

$$M\ddot{z}_2 = -F_s - F_d + u \tag{2}$$

The forces produces by the springs and dampers are the following:

$$F_s = k_s(z_2 - z_1) + k_{sn}(z_2 - z_1)^3$$
 (3)

$$F_d = b_s(\dot{z}_2 - \dot{z}_1) \tag{4}$$

$$F_t = k_t(z_1 - w) \tag{5}$$

$$F_b = b_t(\dot{z}_1 - \dot{w}) \tag{6}$$

State Space

Define state variables

$$x_1 = z_2, \ x_2 = \dot{z}_2, \ x_3 = z_1, \ x_4 = \dot{z}_1$$

$$\dot{x}_{1} = x_{2} \qquad (7) \text{ where}
\dot{x}_{2} = \frac{1}{M} (-F_{s} - F_{d} + u) \qquad (8) \qquad F_{s} = k_{s} (x_{1} - x_{3}) + k_{sn} (x_{1} - x_{3})^{3} \qquad (12)
\dot{x}_{3} = x_{4} \qquad (9) \qquad F_{d} = b_{s} (x_{2} - x_{4}) \qquad (13)
\dot{x}_{4} = \frac{1}{m} (F_{s} + F_{d} - F_{t} - F_{b} - u) \qquad (10) \qquad F_{t} = k_{t} (x_{3} - w) \qquad (14)
y = x_{1} \qquad (11)$$

System

The system is represented in the following form

$$\dot{x} = f(x) + g(x)u
y = h(x)$$
(16)

where $x = \begin{bmatrix} x_1 & x_2 & x_3 & x_4 \end{bmatrix}$ is the state vector, u is the control input, and $y = x_1$ is the output. f(x), g(x), and h(x) are given as follows

$$f(x) = \begin{bmatrix} x_2 \\ \frac{1}{M}(-F_s - F_d) \\ x_4 \\ \frac{1}{m}(F_s + F_d - F_t - F_b) \end{bmatrix}; \ g(x) = \begin{bmatrix} 0 \\ \frac{1}{M} \\ 0 \\ -\frac{1}{m} \end{bmatrix}; \ h(x) = [x_1]$$
 (17)

Lie Derivatives and Coordinate Change

$$y = x_{1} = y_{1}$$

$$\dot{y} = \dot{y}_{1} = \dot{x}_{1} = x_{2} = y_{2}$$

$$\ddot{y} = \dot{y}_{2} = \dot{x}_{2} = \frac{1}{M} (-F_{s} - F_{d}) + \frac{1}{M} u$$

$$(20)$$

$$L_{f}h = \frac{\partial h}{\partial x} \times f(x) = x_{2}$$

$$L_{g}h = \frac{\partial h}{\partial x} \times g(x) = 0$$

$$L_{g}h = \frac{1}{M} (-F_{s} - F_{d})$$

$$L_{g}L_{f}h = \frac{1}{M} (-F_{s} - F_{d})$$

$$L_{g}L_{f}h = \frac{1}{M} (-F_{s} - F_{d})$$

$$(24)$$

the system relative degree is 2. Also, n-r=4-2=2

(24)

Coordinate Change and Zero Dynamics

$$\begin{bmatrix} y_1 \\ y_2 \\ z_1 \\ z_2 \end{bmatrix} = \begin{bmatrix} h(x) \\ L_f(x) \\ \phi_1(x) \\ \phi_2(x) \end{bmatrix} = \begin{bmatrix} x_1 \\ x_2 \\ -x_3 + w \\ Mx_2 + mx_4 - mw \end{bmatrix}$$

 ϕ_1 and ϕ_2 are selected such that $L_g\phi=0$, and T is a diffeomorphism Check for zero dynamics

$$\dot{z} = \begin{bmatrix} \dot{\phi}_1 \\ \dot{\phi}_2 \end{bmatrix} = \begin{bmatrix} -\frac{z_2 - My_2}{m} \\ k_t z_1 - b_t \frac{z_2 - My_2}{m} \end{bmatrix}$$

$$\dot{z} = f_z(z,0,0) = \begin{bmatrix} -\frac{1}{m}z_2 \\ k_tz_1 - \frac{b_t}{m}z_2 \end{bmatrix}$$

is Horowitz or can be proven a.s using a Lyapunov function

(25)

(26)

(27)

Controller and Closed Loop Dynamics

$$u = \frac{1}{L_g L_f h(x)} [v - L_f^2 h(x)] = M[v + k_s (x_1 - x_3) + k_{sn} (x_1 - x_3)^3 + b_s (x_2 - x_4)]$$
 (28)

close loop dynamics:

$$A = egin{bmatrix} 0 & 1 \ -\gamma_1 & -\gamma_2 \end{bmatrix}$$

Choose $-\gamma_1$ and $-\gamma_2$ such that $Real(\lambda_1, \lambda_2) < 0$ for the controller to be stable

Controller

y is required to track a smooth signal y_a

$$u = \frac{1}{L_s L_f h(x)} [v - L_f^2 h(x)] = M[v + k_s (x_1 - x_3) + k_{sn} (x_1 - x_3)^3 + b_s (x_2 - x_4)]$$

where

$$v = \ddot{y_d} - K_1 e - K_2 \dot{e}$$
$$e = y - y_d$$

This will lead to

$$\ddot{y}=\ddot{y_d}-K_1e-K_2\dot{e}$$

$$\ddot{e} + K_2 \dot{e} + K_1 e = 0$$

(31)

(29)

(30)

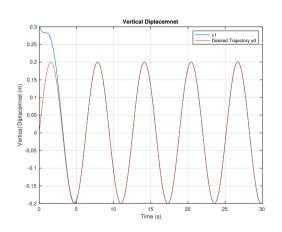
 $\ddot{e} + K_2 \dot{e} + K_1 e = 0$ when $K_1 > 0$ and $K_2 > 0$, the error will decay to zero. This means that the output will follow the desired trajectory.

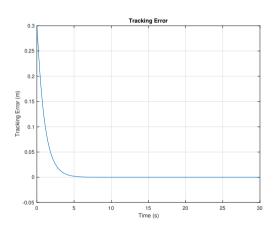
Parameters

Parameters	Values
М	600 kg
m	100 kg
k _s	15000 N/m
b _s	1500 Ns/m
k _t	200000 N/m
b_t	2000 Ns/m
k _{sn}	1000 N/m

Table: System parameters

Results





Results Cont.

