# Introduction to Mobile Robotics and Robot Operating System (ROS)

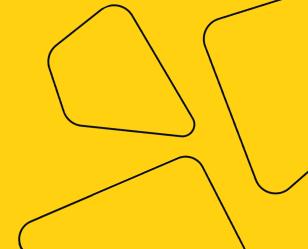
Lecture 3. Kinematics models of wheeled robots.

Probabilistic motion models

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### Outline



- Kinematic models of wheeled robots
  - a. Differential drive
  - b. Tricycle
  - c. Ackermann principle
  - d. Omni- and mecanum-wheels
- 2. Probabilistic motion models
  - a. Odometry-based model
  - b. Speed control based model

### RECURSIVE BAYESIAN POSE ESTIMATION

$$p(\mathbf{x_t}|map, \mathbf{z_t}, \mathbf{u_t}) = C \cdot p(\mathbf{z_t}|\mathbf{x_t}, map) \int_{S} p(\mathbf{x_t}|\mathbf{u_t}, \mathbf{x_{t-1}}) p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}}) d\mathbf{x_{t-1}}$$

$$S$$
 — the probabilistic space of robot poses

$$p(\mathbf{z_t}|\mathbf{x_t}, map)$$
 — observation (measurement) model

$$p(\mathbf{x_t}|\mathbf{u_t},\mathbf{x_{t-1}})$$
 — motion model

$$p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}})$$
 — previous system state (robot pose)



### **KALMAN FILTER**

Prediction:

$$\hat{\mathbf{x}}_t = \mathbf{F}_t \hat{\mathbf{x}}_{t-1} + \mathbf{B}_k \vec{\mathbf{u}}_t$$

$$\hat{\mathbf{\Sigma}}_t = \mathbf{F}_t \mathbf{\Sigma}_{t-1} \mathbf{F}_t^T + \mathbf{Q}_t$$

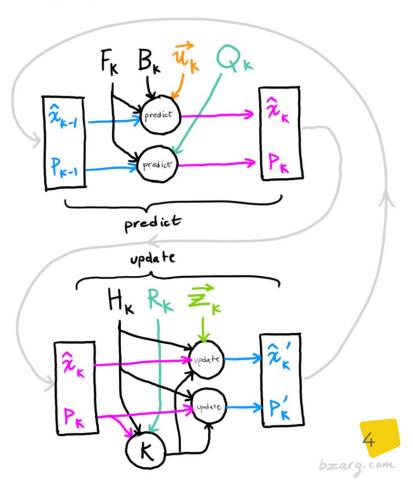
Correction:

$$\mathbf{K}' = \hat{\mathbf{\Sigma}}_t \mathbf{H}_t^T (\mathbf{H}_t \hat{\mathbf{\Sigma}}_t \mathbf{H}_t^T + \mathbf{R}_t)^{-1}$$

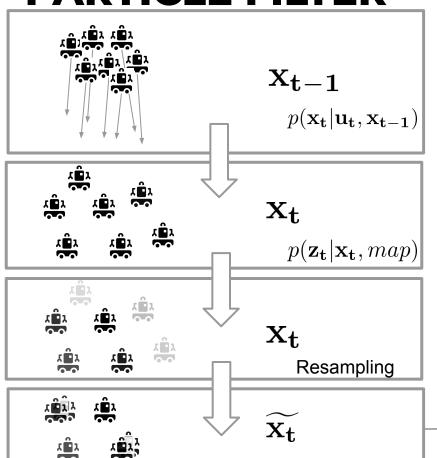
$$\mathbf{x'}_t = \mathbf{H}_t \hat{\mathbf{x}}_t + \mathbf{K'} (\mathbf{z}_t - \mathbf{H}_t \hat{\mathbf{x}}_t)$$

$$\mathbf{\Sigma'}_t = \hat{\mathbf{\Sigma}}_t - \mathbf{K'}\mathbf{H}_t\hat{\mathbf{\Sigma}}_t$$

### Kalman Filter Information Flow



### **PARTICLE FILTER**



#### Algorithm 1 Generic Monte-Carlo localization algorithm

1: procedure  $MCL(\mathbf{x_{t-1}}, m, \mathbf{u_t}, \mathbf{z_t})$ 

2: 
$$\{\mathbf{x_t^n}\} = \{\mathbf{x_t^n}\} = \emptyset$$

3: for n = 1 to N do

4: sample  $x_t^n \sim p(\mathbf{x_t}|\mathbf{u_t}, \mathbf{x_{t-1}^n})$  Motion model

5: 
$$w_t^n = p(\mathbf{z_t}|\mathbf{x_t^n}, map)$$

6: 
$$\{\mathbf{x_t^n}\} = \{\mathbf{x_t^n}\} + \langle x_t^n, w_t^n \rangle$$

Observation model

7: end for

8: for 
$$n = 1$$
 to  $N$  do

9: draw i with probability  $\propto w_t^i$ 

10: 
$$\{\mathbf{x_t^n}\} = \{\mathbf{x_t^n}\} + \langle x_t^i, w_t^i \rangle$$

11: end for

12: return  $\{\mathbf{x_t^n}\}$ 

13: end procedure

Resampling

# RECURSIVE BAYESIAN POSE ESTIMATION

$$p(\mathbf{x_t}|map, \mathbf{z_t}, \mathbf{u_t}) = C \cdot \frac{p(\mathbf{z_t}|\mathbf{x_t}, map)}{p(\mathbf{x_t}|\mathbf{u_t}, \mathbf{x_{t-1}})} p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}}) d\mathbf{x_{t-1}}$$

$$S$$
 — the probabilistic space of robot poses

$$p(\mathbf{z_t}|\mathbf{x_t}, map)$$
 — observation (measurement) model

$$p(\mathbf{x_t}|\mathbf{u_t},\mathbf{x_{t-1}})$$
 — motion model

$$p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}})$$
 — previous system state (robot pose)



# RECURSIVE BAYESIAN POSE ESTIMATION

$$p(\mathbf{x_t}|map, \mathbf{z_t}, \mathbf{u_t}) = C \cdot p(\mathbf{z_t}|\mathbf{x_t}, map) \int_S p(\mathbf{x_t}|\mathbf{u_t}, \mathbf{x_{t-1}}) p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}}) d\mathbf{x_{t-1}}$$

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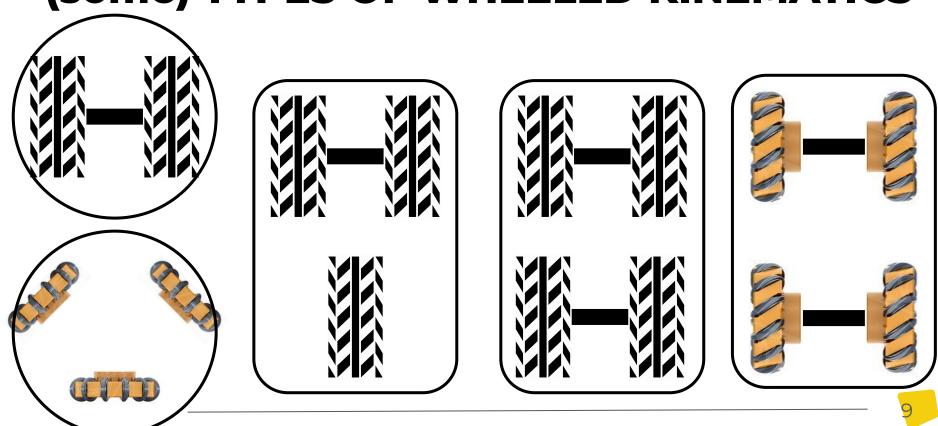


# Kinematic models of wheeled robots

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### (some) TYPES OF WHEELED KINEMATICS

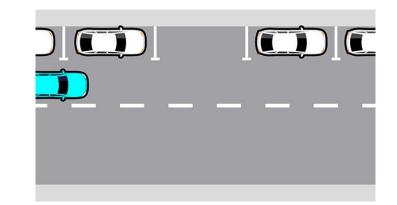


### **HOLONOMIC SYSTEMS**

A robot is called **holonomic** if the number of **controlled** degrees of freedom = the **total** number of degrees of freedom.



- A **nonholonomic system** is a mechanical system on which, in addition to geometric ones, kinematic constraints are also superimposed.
- ☐ Mathematically, nonholonomic constraints are expressed by non-integrable equations.



### **HOLONOMIC SYSTEMS**

- ☐ Holonomic constraints limit the allowed state space (geometry).
- For instance, if there is a truck and a trailer, not all angles between them are possible. This is a holonomic constraint.



- Nonholonomic constraints
  limit the control space relative
  to the current state.
- For instance, a car can not move sideway.



### DIRECT AND INVERSE KINEMATICS PROBLEMS

- ☐ The direct kinematics

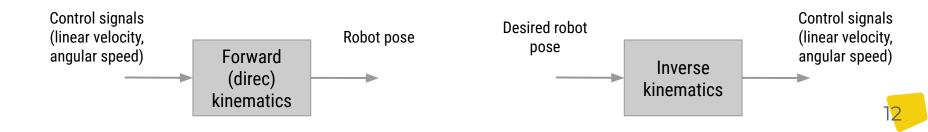
  problem having control

  parameters (for example, wheel

  speeds) and motion time, find

  the position into which the

  robot has moved.
- problem is to find the control parameters that move the robot into a given position in a given time.









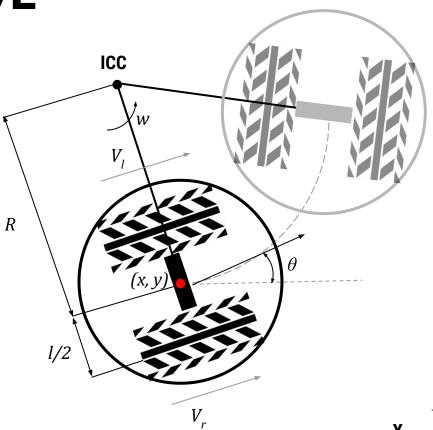
ICC – Instantaneous Center of Curvature

 $(x, y, \theta)$  – wheel axle center coordinates

 $V_r$ 

the speed of the right and left wheels.
 Controlled parameters.





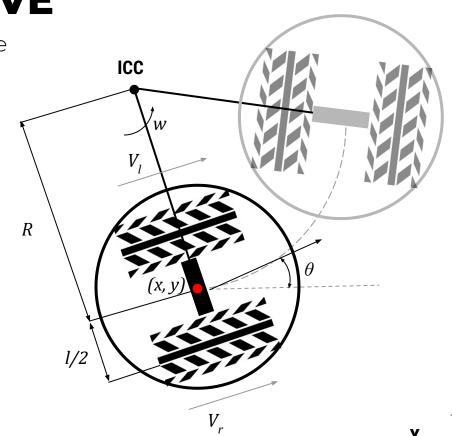


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**ICC** – Instantaneous Center of Curvature  $(x, y, \theta)$  – wheel axle center coordinates

$$w(R + \frac{l}{2}) = V_r$$
$$w(R - \frac{l}{2}) = V_l$$

$$w = \frac{V_r - V_l}{l} \quad V = \frac{V_l + V_r}{2}$$
$$R = \frac{l}{2} \frac{V_r + V_l}{V_r - V_l}$$



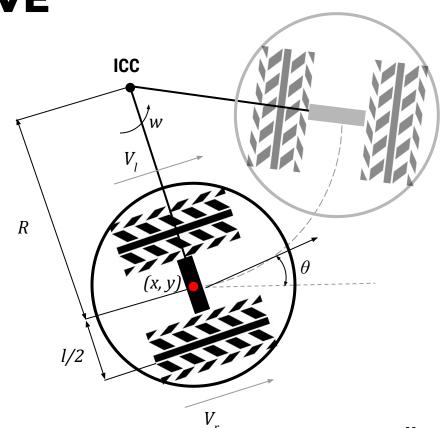
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#### 3 types of motion:

 $V_l = V_r$  — linear motion. The radius of rotation is **infinity**. The angular velocity is **zero**.

 $V_l = -V_r$  — rotation around the center. The radius of rotation is zero.

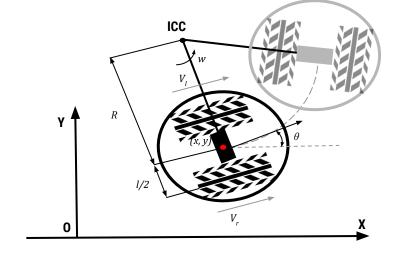
 $V_l = 0 \ (V_r = 0)$  — rotation around the left (right) wheel. The radius of rotation is l/2.



### **DIFFERENTIAL DRIVE FORWARD**

### **KINEMATICS**

$$ICC = [x - R\sin(\theta), y + R\cos(\theta)]$$



At the time moment  $t+\delta t$  the robot pose is defined as:

$$\begin{bmatrix} x' \\ y' \\ \theta' \end{bmatrix} = \begin{bmatrix} \cos(\omega\delta t) & -\sin(\omega\delta t) & 0 \\ \sin(\omega\delta t) & \cos(\omega\delta t) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x - ICC_x \\ y - ICC_y \\ \theta \end{bmatrix} + \begin{bmatrix} ICC_x \\ ICC_y \\ \omega\delta t \end{bmatrix}$$



### **DIFFERENTIAL DRIVE FORWARD**

### **KINEMATICS**

$$x(t) = \int_0^t V(t)cos[\theta(t)]dt$$

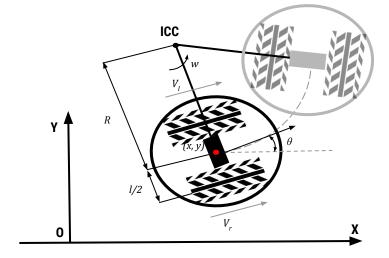
$$y(t) = \int_0^t V(t)sin[\theta(t)]dt$$

$$\Theta(t) = \int_0^t \omega(t)dt$$

$$x(t) = \frac{1}{2} \int_0^t [v_r(t) + v_l(t)] \cos[\theta(t)] dt$$

$$y(t) = \frac{1}{2} \int_0^t [v_r(t) + v_l(t)] \sin[\theta(t)] dt$$

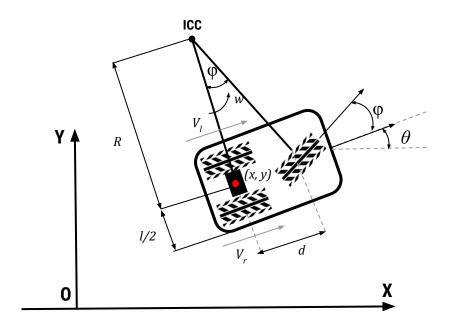
$$\Theta(t) = \frac{1}{l} \int_0^t [v_r(t) - v_l(t)] dt$$



### **TRICYCLE**

$$ICC = [x - R\sin(\theta), y + R\cos(\theta)]$$

$$R = \frac{d}{\tan \varphi}$$



At the time moment  $\mathbf{t}+\delta\mathbf{t}$  the robot pose is

$$\begin{bmatrix} defined as: \\ y' \\ \theta' \end{bmatrix} = \begin{bmatrix} cos(\omega\delta t) & -sin(\omega\delta t) & 0 \\ sin(\omega\delta t) & cos(\omega\delta t) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x - ICC_x \\ y - ICC_y \\ \theta \end{bmatrix} + \begin{bmatrix} ICC_x \\ ICC_y \\ \omega\delta t \end{bmatrix}$$

$$\begin{bmatrix} x - ICC_x \\ y - ICC_y \\ \theta \end{bmatrix} + \begin{bmatrix} ICC_x \\ ICC_y \\ \omega \delta t \end{bmatrix}$$

### **TRICYCLE**

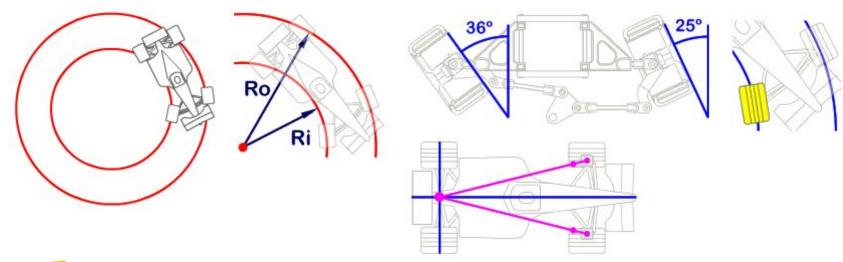
Features:

- Can not rotate in place
- When using 4 wheels, a differential for the rear wheels and an Ackermann steering geometry for the steering wheels are required



### **ACKERMANN STEERING PRINCIPLE**

Steering geometry principle designed to allow steering wheels to go around circles of different radii and to avoid wheel slip.



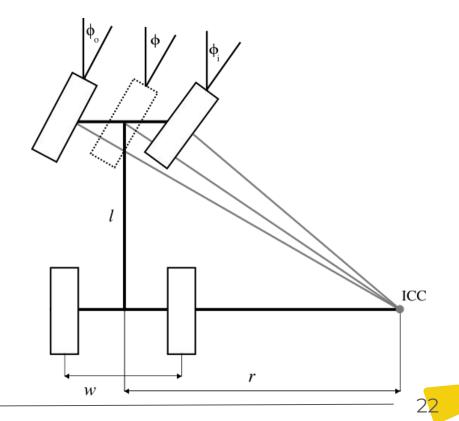


### **ACKERMANN STEERING PRINCIPLE**

$$tan(\phi) = \frac{l}{r}$$

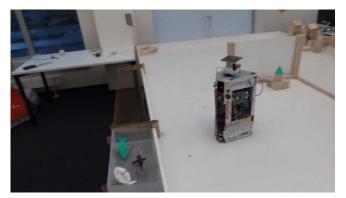
$$tan(\phi_i) = \frac{\iota}{r - \frac{w}{2}}$$

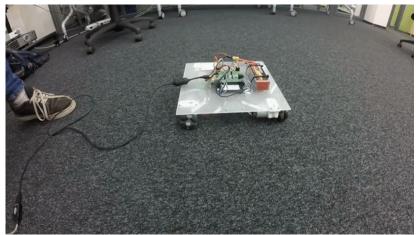
$$tan(\phi_o) = \frac{l}{r + \frac{w}{2}}$$





### **OMNIDIRECTIONAL WHEELS**







# MECANUM WHEELS (ILON WHEEL, SWEDISH WHEEL)



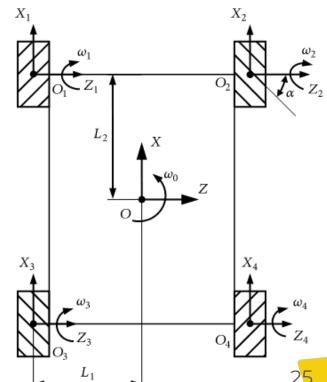




# MECANUM WHEELS (ILON WHEEL, SWEDISH WHEEL)

$$\begin{bmatrix} v_x \\ v_z \\ \omega_0 \end{bmatrix} = \frac{r}{4} \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & -1 & -1 & 1 \\ -\frac{1}{L_1 + L_2} & \frac{1}{L_1 + L_2} & -\frac{1}{L_1 + L_2} & \frac{1}{L_1 + L_2} \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \\ \omega_4 \end{bmatrix}$$

Motion type	$\omega_{1}$	$\omega_2$	$\omega_3$	$\omega_4$
Straight	ω	ω	ω	ω
Perpendicular	ω	-ω	-ω	ω
45° motion	0	ω	ω	0
In place rotation	ω	-ω	ω	-ω





### Probabilistic motion models

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# RECURSIVE BAYESIAN POSE ESTIMATION

$$p(\mathbf{x_t}|map, \mathbf{z_t}, \mathbf{u_t}) = C \cdot p(\mathbf{z_t}|\mathbf{x_t}, map) \int_S p(\mathbf{x_t}|\mathbf{u_t}, \mathbf{x_{t-1}}) p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}}) d\mathbf{x_{t-1}}$$

$$C$$
 — normalization coefficient

$$S$$
 — the probabilistic space of robot poses

$$p(\mathbf{z_t}|\mathbf{x_t}, map)$$
 — observation (measurement) model

$$p(\mathbf{x_t}|\mathbf{u_t},\mathbf{x_{t-1}})$$
 — motion model

$$p(\mathbf{x_{t-1}}|map, \mathbf{z_{t-1}}, \mathbf{u_{t-1}})$$
 — previous system state (robot pose)



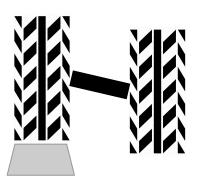
# WHY DO WE NEED PROBABILISTIC MOTION MODELS?

- Actuators, like sensors, are not absolutely accurate.
- External factors also affect the precision of motion.

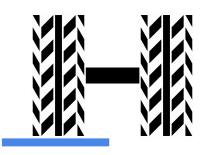
Difference in wheel diameters



Obstacles



Slippage on various surfaces



### PROBABILISTIC MOTION MODELS

In practice, there are 2 types of motion models:

- Odometry-based
- □ Speed control based (dead reckoning)-

Historically was used in ships navigation

- Odometry-based models are used when the robot is equipped with wheels encoders.
- Speed-based models are used when there are no encoders.

  They are based on calculating the traveled distance given the speed and travel time.



### **ODOMETRY-BASED MODEL**

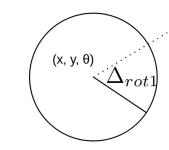
- The robot is moving from  $(x, y, \theta)$  to  $(x', y', \theta')$
- $\Box$  Encoders provide the following information:  $u_t = (\Delta_{trans}, \Delta_{rot1}, \Delta_{rot2})$

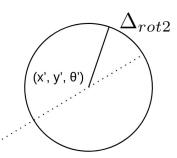
$$\Delta_{trans} = \sqrt{(x - x')^2 + (y - y')^2}$$

$$\Delta_{rot1} = atan2(y'-y, x'-x) - \theta$$

$$\Delta_{rot2} = \theta' - \theta - \Delta_{rot1}$$







### **NOISE MODEL**

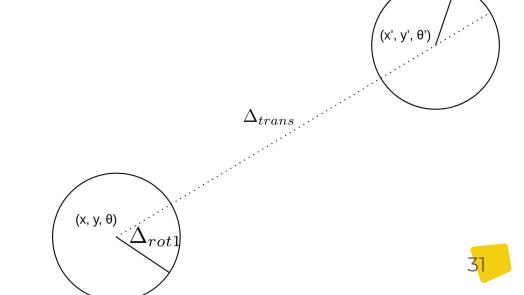
Real motion is prone to error (noise):

$$\hat{\Delta}_{trans} = \Delta_{trans} + \eta_1$$

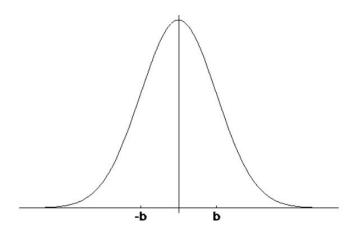
$$\hat{\Delta}_{rot1} = \Delta_{rot1} + \eta_2$$

$$\hat{\Delta}_{rot2} = \Delta_{rot2} + \eta_3$$

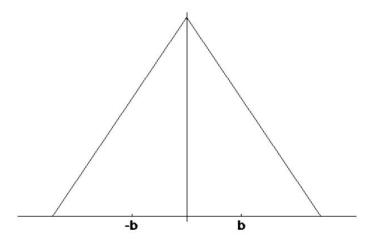




### **NOISE MODEL**



$$\varepsilon_{\sigma^2}(x) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{1}{2}\frac{x^2}{\sigma^2}}$$



$$\varepsilon_{\sigma^2}(x) = \begin{cases} 0 \text{ if } |x| > \sqrt{6\sigma^2} \\ \frac{\sqrt{6\sigma^2 - |x|}}{6\sigma^2} \end{cases}$$



### **NOISE MODELING**

- 1. Algorithm **prob\_normal\_distribution**(*a*,*b*):
- 2. return  $\frac{1}{\sqrt{2\pi b^2}} \exp\left\{-\frac{1}{2}\frac{a^2}{b^2}\right\}$

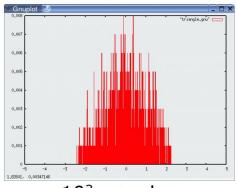
- 1. Algorithm **prob\_triangular\_distribution**(*a*,*b*):
- 2. return  $\max \left\{ 0, \frac{1}{\sqrt{6} \ b} \frac{|a|}{6 \ b^2} \right\}$

### SAMPLING FROM NOISE MODEL

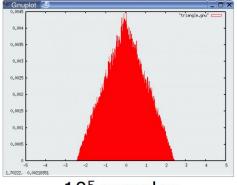
- Algorithm sample\_normal\_distribution(b):
- 2. return  $\frac{1}{2}\sum_{i=1}^{12} rand(-b,b)$

- 1. Algorithm **sample\_triangular\_distribution**(*b*):
- 2. return  $\frac{\sqrt{6}}{2} \left[ \operatorname{rand}(-b, b) + \operatorname{rand}(-b, b) \right]$

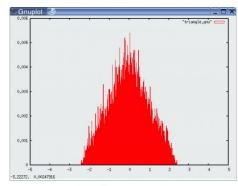
### **SAMPLING FROM NOISE MODEL**



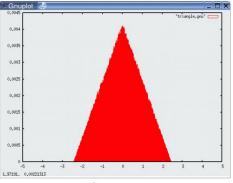
10<sup>3</sup> samples



10<sup>5</sup> samples



10<sup>4</sup> samples



10<sup>6</sup> samples



### POSE POSTERIOR DISTRIBUTION ESTIMATION

hypotheses odometry

- 1. Algorithm motion\_model\_odometry (x, x')  $[\bar{x}, \bar{x}']$
- 2.  $\delta_{trans} = \sqrt{(\overline{x}' \overline{x})^2 + (\overline{y}' \overline{y})^2}$
- 3.  $\delta_{rot1} = atan2(\bar{y}' \bar{y}, \bar{x}' \bar{x}) \bar{\theta}$  odometry params (**u**)
- 4.  $\delta_{rot2} = \overline{\theta}' \overline{\theta} \delta_{rot1}$
- 5.  $\hat{\delta}_{trans} = \sqrt{(x'-x)^2 + (y'-y)^2}$
- 6.  $\hat{\delta}_{rot1} = atan2(y'-y, x'-x) \theta$  values of interest (**x**,**x**')
- 7.  $\hat{\delta}_{rot2} = \theta' \theta \hat{\delta}_{rot1}$
- 8.  $p_1 = \operatorname{prob}(\delta_{\text{rot1}} \hat{\delta}_{\text{rot1}}, \alpha_1 \mid \delta_{\text{rot1}} \mid +\alpha_2 \delta_{\text{trans}})$
- 9.  $p_2 = \text{prob}(\delta_{\text{trans}} \hat{\delta}_{\text{trans}}, \alpha_3 \delta_{\text{trans}} + \alpha_4 (|\delta_{\text{rot1}}| + |\delta_{\text{rot2}}|))$



- girafe 10.  $p_3 = \text{prob}(\delta_{\text{rot}2} \hat{\delta}_{\text{rot}2}, \alpha_1 | \delta_{\text{rot}2} | + \alpha_2 \delta_{\text{trans}})$ 
  - 11. return  $p_1 \cdot p_2 \cdot p_3$

### SAMPLING FROM MOTION MODEL

Algorithm sample\_motion\_model(u, x):

$$u = \langle \delta_{rot1}, \delta_{rot2}, \delta_{trans} \rangle, x = \langle x, y, \theta \rangle$$

- 1.  $\hat{\delta}_{rot1} = \delta_{rot1} + \text{sample}(\alpha_1 | \delta_{rot1} | + \alpha_2 \delta_{trans})$
- 2.  $\hat{\delta}_{trans} = \delta_{trans} + \text{sample}(\alpha_3 \delta_{trans} + \alpha_4 (|\delta_{rot1}| + |\delta_{rot2}|))$
- 3.  $\hat{\delta}_{rot2} = \delta_{rot2} + \text{sample}(\alpha_1 | \delta_{rot2} | + \alpha_2 | \delta_{trans})$
- 4.  $x' = x + \hat{\delta}_{trans} \cos(\theta + \hat{\delta}_{rot1})$
- 5.  $y' = y + \hat{\delta}_{trans} \sin(\theta + \hat{\delta}_{rot1})$

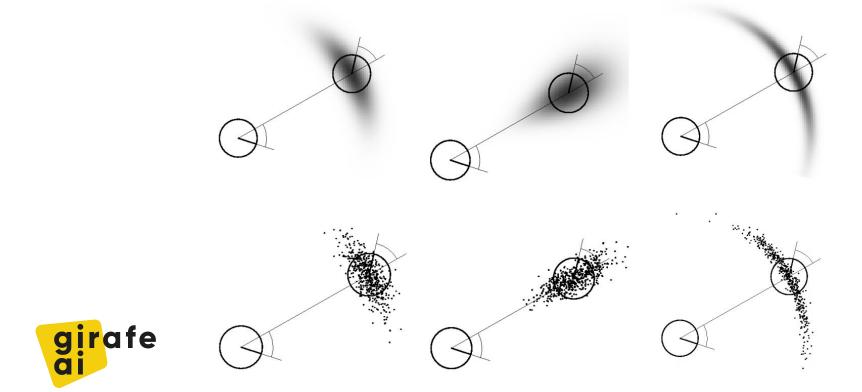
sample\_normal\_distribution

$$\mathbf{6.} \quad \theta' = \theta + \hat{\delta}_{rot1} + \hat{\delta}_{rot2}$$



7. Return  $\langle x', y', \theta' \rangle$ 

# **EXAMPLE OF ODOMETRY-BASED MOTION MODEL**



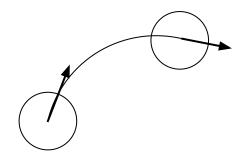


### **SPEED-BASED MOTION MODEL**

- Such a model assumes that we control the parameters of the robot's motion linear and angular velocity
- ☐ The robot moves along a circular arc
- Control signals (speeds) are subject to noise

$$\hat{v} = v + \mathcal{E}_{\alpha_1 |v| + \alpha_2 |\omega|}$$

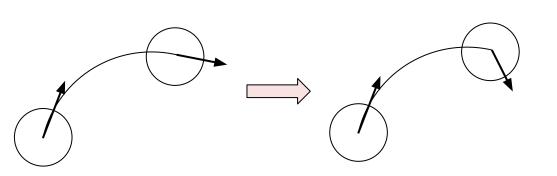
$$\hat{\omega} = \omega + \varepsilon_{\alpha_3|\nu| + \alpha_4|\omega|}$$





### **SPEED-BASED MOTION MODEL**

☐ To allow the final turn, a third motion parameter is introduced



$$\hat{v} = v + \mathcal{E}_{\alpha_1 |v| + \alpha_2 |\omega|}$$

$$\hat{\omega} = \omega + \varepsilon_{\alpha_3|\nu| + \alpha_4|\omega|}$$

$$\hat{\gamma} = \mathcal{E}_{\alpha_{5}|v| + \alpha_{6}|\omega|}$$



### **SPEED-BASED MOTION MODEL**

$$x' = x - \frac{\hat{v}}{\hat{\omega}}\sin\theta + \frac{\hat{v}}{\hat{\omega}}\sin(\theta + \hat{\omega}\Delta t)$$

$$y' = y + \frac{\hat{v}}{\hat{\omega}}\cos\theta - \frac{\hat{v}}{\hat{\omega}}\cos(\theta + \hat{\omega}\Delta t)$$

$$\theta' = \theta + \hat{\omega}\Delta t + \hat{\gamma}\Delta t$$



### SAMPLING FROM SPEED-BASED MOTION MODEL

1: Algorithm sample\_motion\_model\_velocity( $u_t, x_{t-1}$ ):

2: 
$$\hat{v} = v + \mathbf{sample}(\alpha_1 v^2 + \alpha_2 \omega^2)$$

3: 
$$\hat{\omega} = \omega + \mathbf{sample}(\alpha_3 v^2 + \alpha_4 \omega^2)$$

4: 
$$\hat{\gamma} = \mathbf{sample}(\alpha_5 v^2 + \alpha_6 \omega^2)$$

5: 
$$x' = x - \frac{\hat{v}}{\hat{\omega}}\sin\theta + \frac{\hat{v}}{\hat{\omega}}\sin(\theta + \hat{\omega}\Delta t)$$

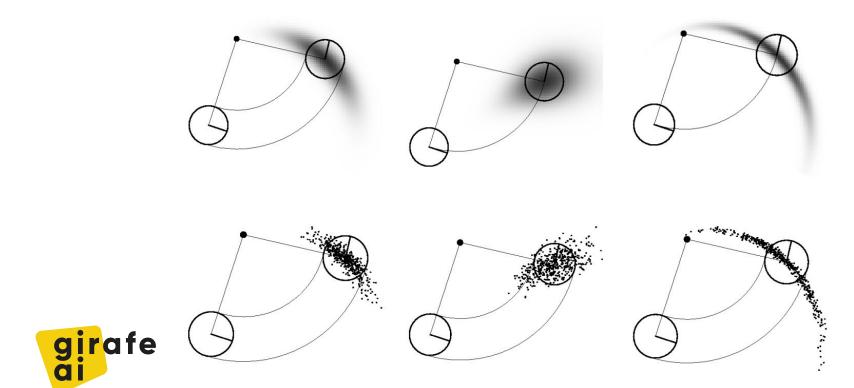
6: 
$$y' = y + \frac{\hat{v}}{\hat{\omega}} \cos \theta - \frac{\hat{v}}{\hat{\omega}} \cos(\theta + \hat{\omega}\Delta t)$$

7: 
$$\theta' = \theta + \hat{\omega}\Delta t + \hat{\gamma}\Delta t$$

8: return 
$$x_t = (x', y', \theta')^T$$



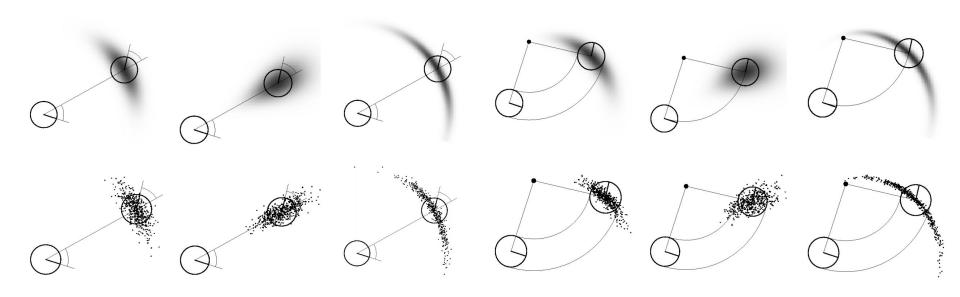
# **EXAMPLE OF SPEED-BASED MOTION MODEL**





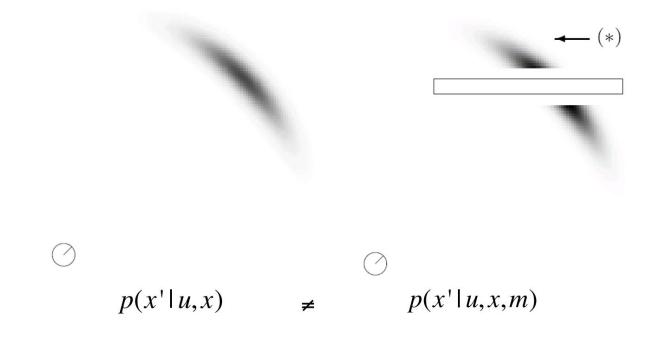
#### **ODOMETRY-BASED MODEL**

#### **SPEED-BASED MODEL**





# MOTION MODELS ACCOUNTING FOR ENVIRONMENT





Approximation:  $p(x'|u,x,m) = \eta \ p(x'|m) \ p(x'|u,x)$ 



# ADDITIONAL RESOURCES

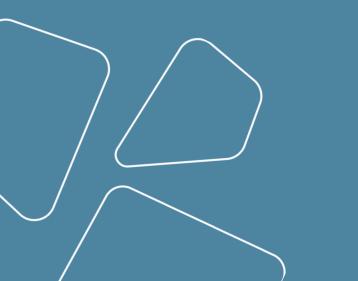


- Probabilistic Robotics (in Notion). Chapter 5.
- 3. Mobility: wheels and wheas









### Thanks for attention!

Questions? Additions? Welcome!

# girafe

