

Vincent De Comarmond Institute of Mine Seismology

Introducing th Idea of Full Waveform Inversion.

Using the costs

Getting useful expressions out of th cost.

Understanding the Adjoint wavefield.

Home cooked

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Full Waveform Inversion

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The Ideas behind full Waveform inversion.

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Introducing Full Waveform Inversion

 The idea of Full Waveform Inversion is quite a simple one.



The Ideas behind full Waveform inversion.

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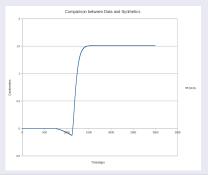
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Introducing Full Waveform Inversion

- The idea of Full Waveform Inversion is quite a simple one.
- Imagine that we record a controlled event .





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What does this model tell us about the mine?

 We spend some time building an accurate computer model of the mine.



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- We spend some time building an accurate computer model of the mine.
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 However we first need to make sure that the model is reasonable.



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- The controlled event gives us the perfect opportunity to test the model of the mine.



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- Let us then check to see how the seismograms computed by our model compare to the seismograms we recorded.



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- Once the model has been built we want to use it.
 However we first need to make sure that the model is reasonable.
- The controlled event gives us the perfect opportunity to test the model of the mine.
- Let us then check to see how the seismograms computed by our model compare to the seismograms we recorded.
- Henceforth the seismograms produced by the model shall be called synthetics, whilst the recorded seismograms will be called data.



Comparing the Model to our data.

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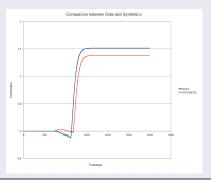
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Comparing the seismograms...

 Consider the following picture showing how the two seismograms overlap or rather don't

Figure: The output of our model vs. what we recorded





Comparing the Model to our data II

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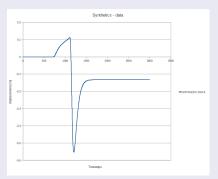
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Comparing the seismograms...

 Something more informative to look at is the difference between the data and the synthetics.

Figure: Model waveform - Recorded waveform





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How do we measure the difference.

• Perhaps we want to give our model a score. To do this all the differences need to be positive. Consider the way we measure the length between two points \vec{p} and $\vec{p_0}$.

$$(\vec{p} - \vec{p_0})^2 = (p_x - p_{0,x})^2 + (p_y - p_{0,y})^2 + (p_z - p_{0,z})^2$$



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• Let us try the same thing with our seismograms.



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- Let us try the same thing with our seismograms.
- But simply subtracting the seismograms from one another is not reasonable, as this will give a time-dependent quantity.



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- Let us try the same thing with our seismograms.
- But simply subtracting the seismograms from one another is not reasonable, as this will give a time-dependent quantity.
- Let us just add the values together for all times i.e integrate over time.



The Cost

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• The above procedure results in the following measure for "cost" where \vec{s} represents the components of the displacement seismogram for the synthetics and \vec{d} represents the components of the displacement seismogram for the data.

$$\chi = \frac{1}{2} \int_0^T \|\vec{s}(t) - \vec{d}(t)\|^2 dt$$

• Here [0,T] is the chosen observation time.



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$$\chi = \frac{1}{2} \int_0^T \|\vec{s}(t) - \vec{d}(t)\|^2 dt$$

- Here [0,T] is the chosen observation time.
- It is quite likely that the same event is recorded at many stations, so we should allow for this possibility.
 Also the cost depends on the model parameters used.
 So the above definition can be extended.



The Cost II

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The cost of our model of the mine.

 This leads to the following definition of cost, which measures how bad the model is.

$$\chi[\vec{m}] = \frac{1}{2} \sum_{r=1}^{N} \int_{0}^{T} \|\vec{s}(\vec{x}_{r}, t, \vec{m}) - \vec{d}(\vec{x}_{r}, t)\|^{2} dt$$

Where: \vec{m} is the model vector, containing all the parameters describing our model.

 $\vec{s}(\vec{x}_r,t,\vec{m})=$ The Synthetic seismograms i.e.: the output of our model

 $\vec{d}(\vec{x}_r, t) =$ The Data i.e.: the seismograms we record.

[0, T] = The observation time



How good/bad is this cost?

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Have we made a good choice for our cost?

 Although the above cost is very intuitive, and it tells us exactly what we want to know it has the following problems:



How good/bad is this cost?

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Final Remark

Have we made a good choice for our cost?

- Although the above cost is very intuitive, and it tells us exactly what we want to know it has the following problems:
- It is not a robust measure outliers can become dominant.
- The numerical value is determined largely by the large-amplitude waveforms, this means that data contained in small amplitude P wave phase changes can easily be lost.
- This measure (the L2 norm) emphasises the non-linearity that is inherent in the seismic wave equation. This is particularly problematic for the inversion procedure used.



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Now that we know the cost of everything how do we proceed?

 So in the story, we've made a model, we know that it is wrong and we know how much it costs.



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- So in the story, we've made a model, we know that it is wrong and we know how much it costs.
- We could build many models of the same mine and see which model has the lowest cost. However this would not be a very efficient way to proceed.



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- We could build many models of the same mine and see which model has the lowest cost. However this would not be a very efficient way to proceed.
- A far better way to proceed is ask how the cost changes when the model changes.



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- So in the story, we've made a model, we know that it is wrong and we know how much it costs.
- We could build many models of the same mine and see which model has the lowest cost. However this would not be a very efficient way to proceed.
- A far better way to proceed is ask how the cost changes when the model changes.
- Thus what we seek is the functional derivative $\frac{\delta \chi[m]}{\delta m}$. It is easy to see that this is given by:

$$\delta \chi = \sum_{r=1}^{N} \int_{0}^{T} [s_i(\vec{x}_r, t, \vec{m}) - d_i(\vec{x}_r, t)] \delta s_i(\vec{x}_r, t, \vec{m})$$



Turning the wheels - the Born Approximation:

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Evaluating $\delta s_i(\vec{x}_r, t, \vec{m})$

• To evaluate $\delta s_i(\vec{x}_r,t,\vec{m})$, one needs to make use of the Born Approximation.



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Evaluating $\delta s_i(\vec{x}_r, t, \vec{m})$

- To evaluate $\delta s_i(\vec{x}_r,t,\vec{m})$, one needs to make use of the Born Approximation.
- Recall the Seismic wave equation in a source-free region:

$$\rho \frac{\partial^2}{\partial t^2} u_i^{(0)} - \frac{\partial}{\partial x_i} c_{ijkl} \epsilon_{kl}^{(0)} = 0$$

This can we written as: $\mathcal{L}^{(0)}u_i^{(0)}=0$



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This can we written as: $\mathcal{L}^{(0)}u_i^{(0)}=0$

• The Born approximation says that a small small perturbation in the medium ($\mathcal{L}^{(0)} \to \mathcal{L}^{(0)} + \delta \mathcal{L}$) will cause a small perturbation in the wavefield ($u_i^{(0)} \to u_i^{(0)} + \delta u_i$).



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Evaluating $\delta s_i(\vec{x}_r, t, \vec{m})$

• Thus the following equation must be satisfied:

$$(\mathcal{L}^{(0)} + \delta \mathcal{L})(u_i^{(0)} + \delta u_i) = 0$$

$$\Rightarrow \mathcal{L}^{(0)} \delta u_i = -\delta \mathcal{L} u_i^{(0)} + \mathcal{O}(\delta^2)$$



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• Thus the following equation must be satisfied:

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• And hence $\delta u_i = -(\mathcal{L}^{(0)})^{-1} \delta \mathcal{L} u_i^{(0)} + \mathcal{O}(\delta^2)$.



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- And hence $\delta u_i = -(\mathcal{L}^{(0)})^{-1} \delta \mathcal{L} u_i^{(0)} + \mathcal{O}(\delta^2)$.
- Further, as we can solve the seismic wave equation (at least numerically), we have:

$$\begin{split} \delta s_i(\vec{x},t) &= -\int\limits_0^t \int\limits_V \left[\delta \rho(\vec{x}') \, G_{ij}(\vec{x},\vec{x}';t-t') \, \frac{\partial^2}{\partial t'^2} s_j(\vec{x}',t') \right. \\ &+ \delta c_{jklm}(\vec{x}') \, \frac{\partial}{\partial x_k'} \, G_{ij}(\vec{x},\vec{x}';t-t') \, \frac{\partial}{\partial x_I'} \, s_m(\vec{x}',t') \right] d^3\vec{x}' \, dt' \end{split}$$



Putting everything together.

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What do we find when putting everything together?

• Putting everything together one finds:

$$\begin{split} \delta \chi &= \sum_{r=1}^{N} \int\limits_{0}^{T} [\mathbf{s}_{i}(\vec{x}_{r},t,\vec{m}) - \mathbf{d}_{i}(\vec{x}_{r},t)] \int\limits_{0}^{t} \int\limits_{V} \left[\delta \rho(\vec{x}') \mathbf{G}_{ij}(\vec{x}_{r},\vec{x}';t-t') \frac{\partial^{2}}{\partial t'^{2}} \mathbf{s}_{j}(\vec{x}',t') \right. \\ &+ \delta \mathbf{c}_{jklm}(\vec{x}') \frac{\partial}{\partial \mathbf{x}'_{k}} \mathbf{G}_{ij}(\vec{x}_{r},\vec{x}';t-t') \frac{\partial}{\partial \mathbf{x}'_{l}} \mathbf{s}_{m}(\vec{x}',t') \right] \mathbf{d}^{3}\vec{x}' \, \mathbf{d}t' \end{split}$$



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 After plenty of algebra one finds that this can be written as :

$$\delta\chi = \int\limits_{\mathcal{U}} \left[\mathcal{K}_{\rho}(\vec{x}) \delta \ln(\rho(\vec{x})) + \mathcal{K}_{\textit{c}_{\textit{ijkl}}}(\vec{x}) \delta \ln(\textit{c}_{\textit{ijkl}}(\vec{x})) \right] \textit{d}^{3}\vec{x}$$



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Following from above ...

• Where the kernels $K_{\rho}(\vec{x})$ and $K_{c_{ijkl}}(\vec{x})$ are defined as follows:

$$K_{\rho}(\vec{x}) = -\int_{0}^{T} \rho(\vec{x}) s_{i}^{\dagger}(\vec{x}, T - t) \frac{\partial^{2}}{\partial t^{2}} s_{i}(\vec{x}, t) dt$$

$$\mathcal{K}_{\mathcal{C}_{ijkl}}(\vec{x}) = -\int\limits_{0}^{T} \epsilon_{jk}^{\dagger}(\vec{x}, T-t) c_{jklm}(\vec{x}) \epsilon_{lm}(\vec{x}, t) dt$$
 [NO \sum]



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• The magic of full waveform inversion really lies in the adjoint wavefield s_i^{\dagger} .



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 [NO \sum]

- The magic of full waveform inversion really lies in the adjoint wavefield s_i^{\dagger} .
- s_i^{\dagger} arises naturally in carrying out the calculation. But what is it and how is it interpreted?



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The Adjoint Wavefield.

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How does one understand the Adjoint Wavefield

• The adjoint wavefield satisfies the following equation:

$$\rho \frac{\partial^2}{\partial t^2} s_i^{\dagger}(\vec{x}, t) - \frac{\partial}{\partial x_i} c_{ijkl} \frac{\partial}{\partial x_k} s_l^{\dagger}(\vec{x}, t) =$$

$$c(\vec{x}, T, t) = c(\vec{x}, T, t) \delta(\vec{x}, \vec{x}) - f(\vec{x}, t) \delta(\vec{x}, \vec{x}) - f(\vec{x}, t) \delta(\vec{x}, t) \delta$$

$$= \sum_{r=1}^{N} \left[s_{i}(\vec{x}_{r}, T-t) - d_{i}(\vec{x}_{r}, T-t) \right] \delta(\vec{x} - \vec{x}_{r}) = f_{i}^{\dagger}(\vec{x}, t)$$



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How does one understand the Adjoint Wavefield

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• But that is just the seismic wave equation with a source term : $f_i^{\dagger}(\vec{x}, t)$



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- But that is just the seismic wave equation with a source term : $f_i^{\dagger}(\vec{x}, t)$
- Where the waveform adjoint source $f_i^{\dagger}(\vec{x}, t)$

$$f_i^{\ \dagger}(\vec{x},t) = \sum_{r=1}^N \bigl[s_i(\vec{x}_r,T-t) - d_i(\vec{x}_r,T-t)\bigr] \delta(\vec{x}-\vec{x}_r)$$



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How can we understand this?

 As the adjoint field satisfies the seismic wave equation, we can just think of it as seismic waves set up by the waveform adjoint source.



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Final Remark

How can we understand this?

- As the adjoint field satisfies the seismic wave equation, we can just think of it as seismic waves set up by the waveform adjoint source.
- But that is just the seismic wave equation with a source term : $f_i^{\dagger}(\vec{x}, t)$
- Note that the waveform adjoint source $f_i^{\ \dagger}(\vec{x},t)$ is just the time-reversed differences between the synthetics and the data, injected at the locations at the sensor locations.

$$f_{i}^{\dagger}(\vec{x},t) = \sum_{r=1}^{N} [s_{i}(\vec{x}_{r},T-t) - d_{i}(\vec{x}_{r},T-t)]\delta(\vec{x}-\vec{x}_{r})$$



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Final Remark

Following from above ...

 Thus the waveform adjoint field can be seen as the seismic wave generated by injecting the mistakes (differences in data and synthetics) we've made back into the model from the sensor where those mistakes were made with reversed time.



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Final Remarks

Following from above ...

- Thus the waveform adjoint field can be seen as the seismic wave generated by injecting the mistakes (differences in data and synthetics) we've made back into the model from the sensor where those mistakes were made with reversed time.
- You may be asking yourself "so what". This is of course a very good question. The answer to the question lies in something I made mention to earlier.



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Final Remark

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- You may be asking yourself "so what". This is of course a very good question. The answer to the question lies in something I made mention to earlier.
- So let us look back at how we use the cost.



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How did the cost change with model perturbations again?

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Recall the expressions:

 Recall that given a model perturbation, the change in cost was :

$$\delta\chi = \int\limits_{V} \left[\textit{K}_{\rho}(\vec{x}) \delta \ln(\rho(\vec{x})) + \textit{K}_{\textit{C}_{\textit{ijkl}}}(\vec{x}) \delta \ln(\textit{c}_{\textit{ijkl}}(\vec{x})) \right] \textit{d}^{3}\vec{x}$$



How did the cost change with model perturbations again?

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Recall the expressions:

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• Where the kernels $K_{\rho}(\vec{x})$ and $K_{c_{ijkl}}(\vec{x})$ were defined as follows:

$$K_{\rho}(\vec{x}) = -\int_{0}^{T} \rho(\vec{x}) s_{i}^{\dagger}(\vec{x}, T-t) \frac{\partial^{2}}{\partial t^{2}} s_{i}(\vec{x}, t) dt$$

$$\mathcal{K}_{\mathcal{C}_{ijkl}}(\vec{x}) = -\int\limits_{0}^{l} \epsilon_{jk}^{\dagger}(\vec{x}, T-t) c_{jklm}(\vec{x}) \epsilon_{lm}(\vec{x}, t) dt$$
 [NO \sum]



So what are these so called Kernels then?

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What are the kernels?

 The kernels as defined above are just the functional derivatives of the cost with respect to the various model parameters.



So what are these so called Kernels then?

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Final Remark

What are the kernels?

- The kernels as defined above are just the functional derivatives of the cost with respect to the various model parameters.
- In other words, at the expense of one extra simulation (for the adjoint wave), the gradients of the model become available to use.



So what are these so called Kernels then?

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Final Remarks

What are the kernels?

- The kernels as defined above are just the functional derivatives of the cost with respect to the various model parameters.
- In other words, at the expense of one extra simulation (for the adjoint wave), the gradients of the model become available to use.
- So for example, If I wanted to know how the model changes with respect to changes in density it would be as simple (or difficult) as computing:

$$\frac{\delta \chi}{\delta \rho(\vec{x})} = K_{\rho}(\vec{x}) = -\int_{0}^{T} \rho(\vec{x}) s_{i}^{\dagger}(\vec{x}, T - t) \frac{\partial^{2}}{\partial t^{2}} s_{i}(\vec{x}, t) dt$$



How the gradients are useful.

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Why is it good to have gradients?

 The gradients are very useful, because they allow the use of efficient techniques to minimise the cost of the model. Consider the definition for the cost once again.

$$\chi[\vec{m}] = \frac{1}{2} \sum_{r=1}^{N} \int_{0}^{T} \|\vec{s}(\vec{x}_{r}, t, \vec{m}) - \vec{d}(\vec{x}_{r}, t)\|^{2} dt$$



How the gradients are useful.

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$$\chi[\vec{m}] = \frac{1}{2} \sum_{r=1}^{N} \int_{0}^{T} \|\vec{s}(\vec{x}_{r}, t, \vec{m}) - \vec{d}(\vec{x}_{r}, t)\|^{2} dt$$

• When the synthetics and the data agree, the cost is zero, a global minimum. If the model is close enough to reality, then the model parameters lie in a well surrounding this global minimum. Further we know that the derivatives should be zero at the minimum, small nearby, and larger further away. Thus the gradients indicate the direction in which the function is increasing.



The Kernels paint a picture for us.

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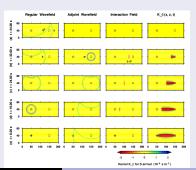
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The Kernels are small where the model is accurate and large where the model is inaccurate.

 Following the above reasoning, and noting that the kernels for the medium are functions of location, one can understand how the kernels can paint a picture of the accuracy of our model.





An example of what it means to be inside a potential well.

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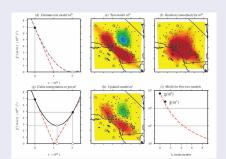
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 If we change the model parameters in the opposite manner the gradients change, then we'll be heading towards the minimum.





An example of what it means to be inside a potential well.

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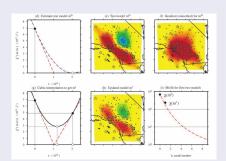
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Final Remarks

 If we change the model parameters in the opposite manner the gradients change, then we'll be heading towards the minimum.



 The minimisation procedure is formalised in the conjugate-gradient algorithm.



The Conjugate-Gradient Algorithm.

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Let us formalise the above

- The above idea can be formalised in the conjugate gradient algorithm.
- The procedure using the Kernals to iteratively improve our model follows:
 - For k=0, $\vec{p}^{(0)}=-\frac{\partial \chi}{\partial \vec{m}}=-g^{(0)}$. If at any stage $\|\vec{p}\|<\varepsilon$, then our model is accurate.
 - ② Find a scalar $\lambda^{(k)}$ that minimises the function $\tilde{\chi}(\lambda) = \chi(m^{(0)} + \lambda \vec{p}^{(k)})$.
 - Update the model as follows: $\vec{m}^{(k+1)} = \vec{m}^{(0)} + \lambda^{(k)} \vec{p}^{(k)}$, calculate $g^{(k+1)} = \frac{\partial}{\partial \vec{m}^{(k+1)}} \chi(\vec{m}^{(k+1)})$.
 - ① Update \vec{p} as follows: $\vec{p}^{(k+1)} = -g^{(k+1)} + \beta_{k+1} \vec{p}^{(k)}$. Where $\beta_{k+1} = \frac{\vec{g}^{(k+1)} \cdot \vec{g}^{(k+1)}}{\vec{g}^{(k)} \cdot \vec{g}^{(k)}}$.
 - If $\|\vec{p}^{(k+1)}\| < \varepsilon$ then the model $\vec{m}^{(k+1)}$ is the one we want. Else we restart from 2.



How is the performance of this procedure.

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Final Remark

Some examples...

 Firstly consider a vector force acting at a certain location in the medium. Further imagine that we know the magnitude and location of the force, but not its orientation. In the same way that the above kernels were derived, one may derive the kernel associated with changes in the force which generates seismic waves.



How is the performance of this procedure.

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Final Remark

Some examples...

- Firstly consider a vector force acting at a certain location in the medium. Further imagine that we know the magnitude and location of the force, but not its orientation. In the same way that the above kernels were derived, one may derive the kernel associated with changes in the force which generates seismic waves.
- The variation of cost with respect to the generating force is given by:

$$\delta \chi = \int_{0}^{T} \int_{V} \delta f_{i}(\vec{x}, t) s_{i}^{\dagger}(\vec{x}, T - t) dV dt$$



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Writing things in terms of angles.

 Thus we can find the derivatives with respect to the polar and azimuthal angles:

$$\frac{\delta \chi}{\delta \theta_j} = \int_0^T \int_V h(t) \mathbf{s}_i^{\dagger}(\vec{x}, T - t) \frac{\partial x_i}{\partial \theta_j} \delta \theta_j dV dt$$



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 The procedure was performed where the initial source orientation was at an angle of 178.2° to the true source orientation. The results follow:



Performance for the inversion of an orientation.

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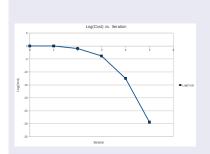
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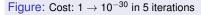
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Performance in terms of re-orienting the source





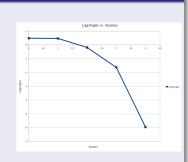


Figure: Angle 178.2° \rightarrow 0° in 5 iterations



What about having the source mis Located?

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Final Remark

Performance in re-Locating a generating force.

 Next consider a generating force, where we know both the orientation of the force, together with its time dependence. The only thing we do not know is the location of the source.



What about having the source mis Located?

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Final Remark

Performance in re-Locating a generating force.

- Next consider a generating force, where we know both the orientation of the force, together with its time dependence. The only thing we do not know is the location of the source.
- In this case the variation of the Cost with respect to the model parameters are given by:

$$\frac{\delta \chi}{\delta x_j} = \delta \vec{x} \cdot \vec{\nabla} \int_0^T h(t) s_j^{\dagger}(\vec{x}, T - t) dt$$



What about having the source mis Located?

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$$\frac{\delta \chi}{\delta x_j} = \delta \vec{x} \cdot \vec{\nabla} \int_0^T h(t) s_j^{\dagger}(\vec{x}, T - t) dt$$

 The iterative procedure was performed where the true location was (0,0,0) and the initial synthetic location is given by (200,100,-50). Thus the initial distance between the source and location is 229m.



Performance for the inversion of an Location

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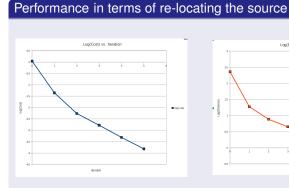


Figure: Cost: $1 \rightarrow 1.5 \times 10^{-4}$ in 5 iterations

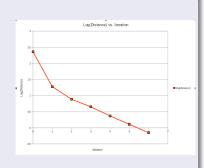


Figure: Mis-location: $229m \rightarrow 0.7m$ in 5 iterations



And sources which are both mis-located and mis-oriented?

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 As before, we assume that we know the details of the force.



And sources which are both mis-located and mis-oriented?

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- As before, we assume that we know the details of the force.
- The variation of the cost with the model parameters are the same as before.



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- As before, we assume that we know the details of the force.
- The variation of the cost with the model parameters are the same as before.
- This time there is however an additional subtlety which makes the problem more complicated. The subtlety lies in the fact that the gradients of the different groups of model parameters do not necessarily reflect the contributions of the various model parameters to the total cost. In the following example the initial angle between the synthetics and data is 15°, and the initial distance between the location for the data and synthetics was 15m



Exposition of what can go wrong.

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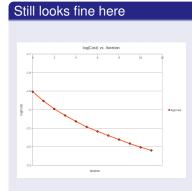
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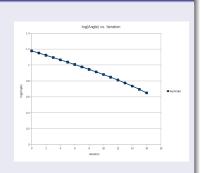


Figure: Alignement Angle: $15^{\circ} \rightarrow 4.5^{\circ}$ in 15 iterations



Exposition of what can go wrong II.

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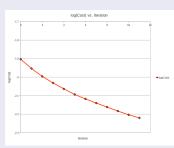
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Look at the very slow convergence





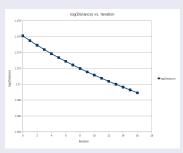


Figure: Mis-location: $15m \rightarrow 14.75m$ in 15 iterations





Another approach?

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Final Remark

Another approach I tried:

 Because of the problems of non-convergence another approach had to be tried. In this approach, in an attempt to escape the dominating effect of the orientation over the location, it was assumed that both groups of model parameters were solely responsible for generating the model cost.



Another approach?

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Final Remar

Another approach I tried:

- Because of the problems of non-convergence another approach had to be tried. In this approach, in an attempt to escape the dominating effect of the orientation over the location, it was assumed that both groups of model parameters were solely responsible for generating the model cost.
- This approach does not do too badly, but has serious problems. In many examples, where the synthetics's initial location and orientation did not lie sufficiently close to the data's location and orientation the model parameters "ran away from" the data parameters.



Still not quite right.

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Final Remark

The other approach works much better:

 Also, as we're always overcompensating for the errors in the model, there is a definite limit on how close the model can come to reality- at which point overcompensation makes the model less accurate rather than more accurate.



Still not quite right.

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Final Remark

The other approach works much better:

- Also, as we're always overcompensating for the errors in the model, there is a definite limit on how close the model can come to reality- at which point overcompensation makes the model less accurate rather than more accurate.
- It is also obvious that the cost is not strictly decreasing, which is a problem for an algorithm which searches for minima. In the following best case scenario, used as an example, the initial distance between the source location and the synthetic location is 60m, and the initial alignment angle between the synthetics and the data is 18°.



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Final Remarks

This approach works much better:

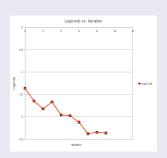


Figure: Cost : $4 \times 10^{-2} \rightarrow 4 \times 10^{-3}$ in 10 iterations

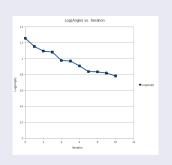


Figure: Alignement angle: $18^{\circ} \rightarrow 6^{\circ}$ in 10 iterations



Hints of problems...

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This works better - but is still not quite right:

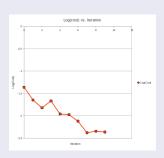


Figure: $4 \times 10^{-2} \rightarrow 4 \times 10^{-3}$ in 10 iterations

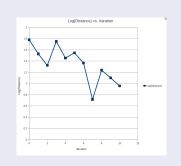


Figure: Mis-loction: $60m \rightarrow 9m$ in 10 iterations



Best results

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The best solution I've come up with yet.

 In an attempt to solve the problems present in the above approach, a modification was made, where only the changes that lead to a lower cost are made.



Best results

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Final Remark

The best solution I've come up with yet.

- In an attempt to solve the problems present in the above approach, a modification was made, where only the changes that lead to a lower cost are made.
- This approach works well, but it does suffer from a drawback in that the computational time is significantly longer. In the following example the initial distance between the source and synthetic locations was 92m and the initial angle between the direction of the synthetics, and the direction of the data was 35°.



Best results so far

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An acceptable result:

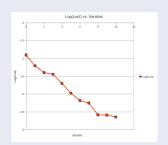


Figure: Cost: $0.12 \rightarrow 0.0022$ in 10 iterations

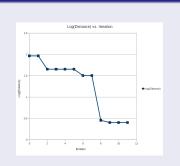


Figure: Mis-location: $92.5m \rightarrow 2.5m$ in 10 iterations



Best results so far

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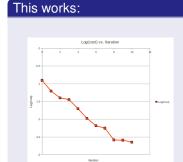
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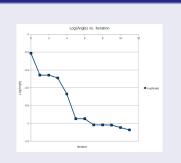


Figure: Alignment Angle: $35^{\circ} \rightarrow 5^{\circ}$ in 10 iterations



What about Moment Sources.

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Final Remark

What about extending this analysis to Moment sources

 Next we consider a moment source, the location of which we know, but the components are unknown to us.



What about Moment Sources.

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Final Remark

What about extending this analysis to Moment sources

- Next we consider a moment source, the location of which we know, but the components are unknown to us.
- The variation of the Cost with respect to the model parameters is given by:

$$\delta \chi = \int_{0}^{T} \int_{\Sigma} \epsilon_{ij}^{\dagger}(\vec{x}, T - t) \delta m_{ij}(\vec{x}, t) dAdt$$

Where
$$\epsilon_{ij}^{\dagger}=rac{1}{2}(rac{\partial}{\partial x_{i}}s_{j}^{\dagger}+rac{\partial}{\partial x_{j}}s_{i}^{\dagger})$$

And Σ is the area of the fault plane.



A Moment source example

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Final Remark

An example with moment sources.

 In the following example, I let the components of the moment tensor change, without letting the magnitude change. It was also assumed that the location and source time function were known. On the following slide, the average difference between the components of the moment tensor is plotted along with the cost function.



A Moment source example

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Final Remark

An example with moment sources.

- In the following example, I let the components of the moment tensor change, without letting the magnitude change. It was also assumed that the location and source time function were known. On the following slide, the average difference between the components of the moment tensor is plotted along with the cost function.
- For the following example the moment tensors considered were:

Data moment tensor

Synthetic moment tensor

$$\begin{pmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{pmatrix}$$

$$\begin{pmatrix}
5 & -6 & 10 \\
-6 & 3 & -7 \\
10 & -7 & 6
\end{pmatrix}$$



Some results

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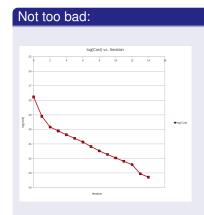
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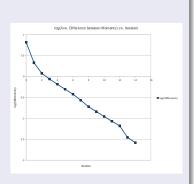


Figure: Average Difference in Moments $:6.56 \rightarrow 0.056$ in 15 iterations



More results

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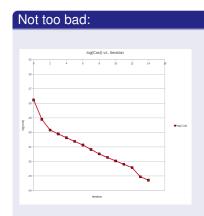
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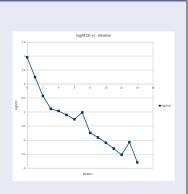


Figure: Differences in $M_{13}:9 \rightarrow 0.0016$ in 15 iterations



Diagonal terms

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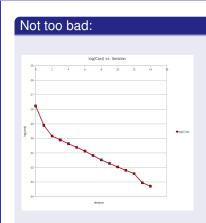
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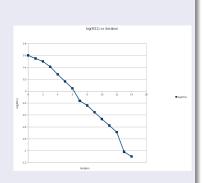


Figure: Differences in $M_{11}:4 \rightarrow 0.08$ in 15 iterations



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Final Remarks

Some final remarks:

 The diagonal and off diagonal terms of the moment tensor appear largely independent. The behaviour of the diagonal and off-diagonal terms are somewhat reminiscent of the relationship between the orientation and location of the force vector for vector force inversion.



Some Notes.

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Final Remarks

Some final remarks:

- The diagonal and off diagonal terms of the moment tensor appear largely independent. The behaviour of the diagonal and off-diagonal terms are somewhat reminiscent of the relationship between the orientation and location of the force vector for vector force inversion.
- The iterative process is not computationally cheap as full waveform modeling in a non homogeneous medium is needed.



Some Notes.

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Final Remarks

Some final remarks:

- The diagonal and off diagonal terms of the moment tensor appear largely independent. The behaviour of the diagonal and off-diagonal terms are somewhat reminiscent of the relationship between the orientation and location of the force vector for vector force inversion.
- The iterative process is not computationally cheap as full waveform modeling in a non homogeneous medium is needed.
- This method of iteratively improving the model is not limited. Nearly every model parameter one can think of can be inverted for using the above procedure. The more model parameters are inverted for, the more difficult and expensive the iterative procedure.



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Final Remarks

Some final remarks:

 The next step to take are to include more model parameters. This will eventually lead to performing inversions for hetrogeneous media.



Where to from here

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Final Remarks

Some final remarks:

- The next step to take are to include more model parameters. This will eventually lead to performing inversions for hetrogeneous media.
- At some stage it is likely that a norm other than the L₂ norm will be needed. Other, more robust norms, which are of greater practical utility have recently become available - however they are less easy to use.



Where to from here

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Final Remarks

Some final remarks:

- The next step to take are to include more model parameters. This will eventually lead to performing inversions for hetrogeneous media.
- At some stage it is likely that a norm other than the L_2 norm will be needed. Other, more robust norms, which are of greater practical utility have recently become available however they are less easy to use.
- Thank you for your time and goodbye.



References.

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