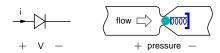
EE101: Diode circuits



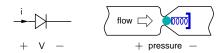
M. B. Patil
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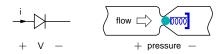




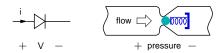
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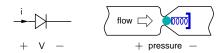
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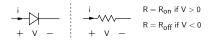
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- * In the forward direction, the diode resistance $R_D = V/i$ would be a function of V. However, it is often a good approximation to treat it as a constant (small) resistance.
- * In the reverse direction, the diode resistance is much larger and may often be treated as infinite (i.e., the diode may be replaced by an open circuit).

Simple models: R_{on}/R_{off} model

Simple models: $R_{\rm on}/R_{\rm off}$ model

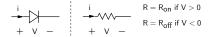


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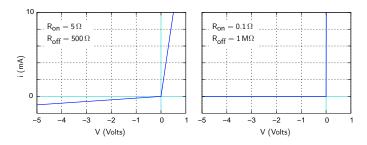
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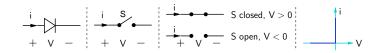
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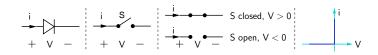
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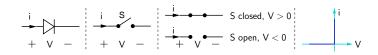
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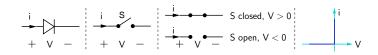




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- * The actual values of V and i for a diode in a circuit get determined by the i-V relationship of the diode and the constraints on V and i imposed by the circuit.

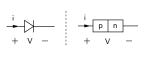




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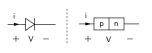
$$\begin{split} k_B &= \text{Boltzmann's constant} = 1.38 \times 10^{-23} \ J/K. \\ q &= \text{electron charge} = 1.602 \times 10^{-19} \ \text{Coul}. \\ T &= \text{temperature in } ^\circ K. \end{split}$$

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- * The "turn-on" voltage (V_{on}) of a diode depends on the value of I_s. V_{on} may be defined as the voltage at which the diode starts carrying a substantial forward current (say, a few mA).

For a silicon diode, $V_{\rm on} \approx 0.7~V$.

For a GaAs diode, $V_{\rm on} \approx 1.1 \ V$.

$$i = I_s \left[\exp \left(\frac{V}{V_T} \right) - 1 \right]$$
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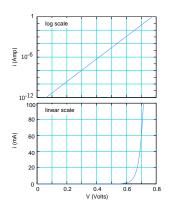
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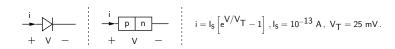
V	$x = V/V_T$	e ^x	i (Amp)
0.1	3.87	0.479×10^{2}	0.469×10^{-11}
0.2	7.74	0.229×10^4	0.229×10^{-9}
0.3	11.6	0.110×10^{6}	0.110×10^{-7}
0.4	15.5	0.525×10^{7}	0.525×10^{-6}
0.5	19.3	0.251×10^9	0.251×10^{-4}
0.6	23.2	0.120×10^{11}	0.120×10^{-2}
0.62	24.0	0.260×10^{11}	0.260×10^{-2}
0.64	24.8	0.565×10^{11}	0.565×10^{-2}
0.66	25.5	0.122×10^{12}	0.122×10^{-1}
0.68	26.3	0.265×10^{12}	0.265×10^{-1}
0.70	27.1	0.575×10^{12}	0.575×10^{-1}
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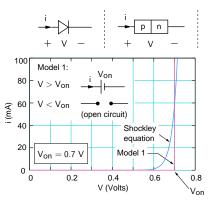
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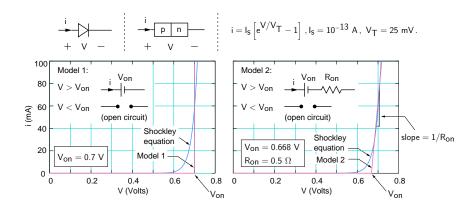
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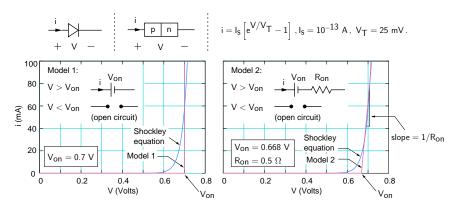




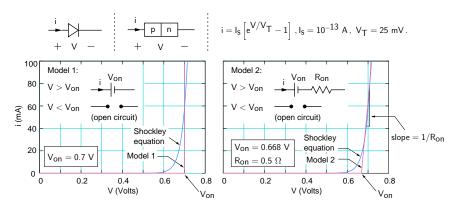


$$\label{eq:interpolation} i = I_{\text{S}} \left[e^{\text{V/V}_{\text{T}}} - 1 \right] \, , I_{\text{S}} = 10^{-13} \, \, \text{A} \, , \, \, \text{V}_{\text{T}} = 25 \, \, \text{mV} \, .$$

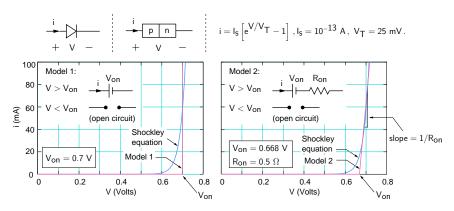




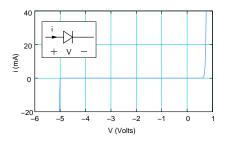
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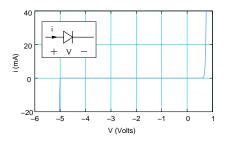


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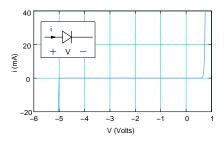


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- * Note that the "battery" shown in the above models is not a "source" of power! It can only absorb power (see the direction of the current), causing heat dissipation.

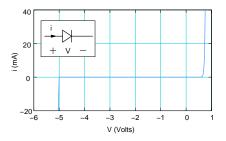




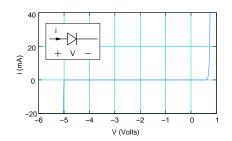
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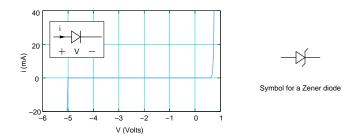


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- * When the reverse bias $V_{\rm R} > V_{\rm BR}$, the diode allows a large amount of current. If the current is not constrained by the external circuit, the diode would get damaged.



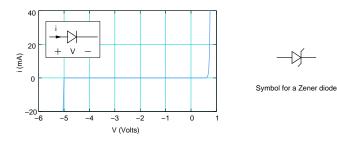


Symbol for a Zener diode



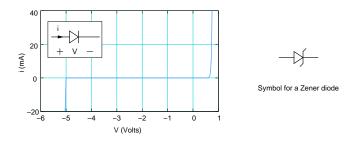
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Reverse breakdown



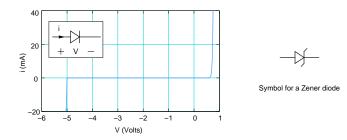
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- * "Zener" diodes typically have $V_{\rm BR}$ of a few Volts, which is denoted by $V_{\rm Z}$. They are often used to limit the voltage swing in electronic circuits.

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Light-emitting diodes (LEDs) emit light when a forward bias is applied.
 Typically, LEDs are made of III-V semiconductors.

An LED emits light of a specific wavelength (e.g., red, green, yellow, blue).

White LEDs combine individual LEDs that emit the three primary colors (red, green, blue) or use a phosphor material to convert monochromatic light from a blue or UV LED to broad-spectrum white light.

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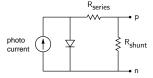


* Solar cells are generally silicon diodes designed to generate current efficiently when solar radiation is incident on the device. A "solar panel" has a large number of individual solar cells connected in series/parallel configuration.

A solar cell can be modelled as a diode in parallel with a current source (representing the photocurrent). In addition, parasitic series and shunt resistances need to be considered.

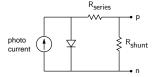
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 Photodiodes are used to detect optical signals (DC or time-varying) and to convert them into electrical signals which can be subsequently processed by electronic circuits. They are used in fibre-optic communication systems, image processing, etc.

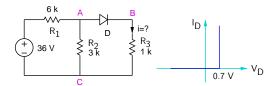
A photodiode works on the same principle as a solar cell, i.e., it converts light into a current. However, its design is optimized for high-sensitivity, low-noise, or high-frequency operation, depending on the application.

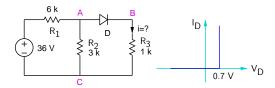
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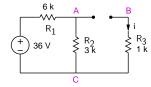
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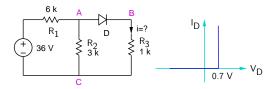
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- * Note that there are diode circuits in which the exponential nature of the diode I-V relationship is made use of. For these circuits, computer simulation would be required to solve the resulting non-linear equations.



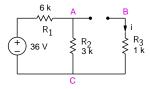


Case 1: D is off.



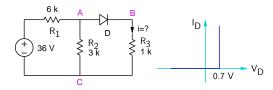


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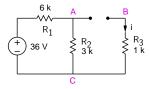


$$V_{\mbox{\footnotesize AB}} = V_{\mbox{\footnotesize AC}} = \frac{3}{9} \times 36 = 12 \mbox{ V} \, , \label{eq:VAB}$$

which is not consistent with our assumption of D being off.



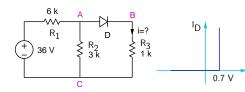
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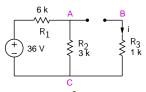
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which is not consistent with our assumption of D being off.

 $\rightarrow\! D$ must be on.

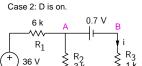


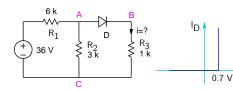
Case 1: D is off.



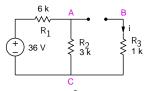
 $V_{AB} = V_{AC} = \frac{3}{9} \times 36 = 12 \text{ V}$, which is not consistent with our assumption of D being off.

 \rightarrow D must be on.





Case 1: D is off.

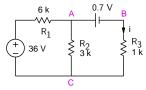


$$V_{AB} = V_{AC} = \frac{3}{9} \times 36 = 12 \text{ V},$$

which is not consistent with our assumption of D being off.

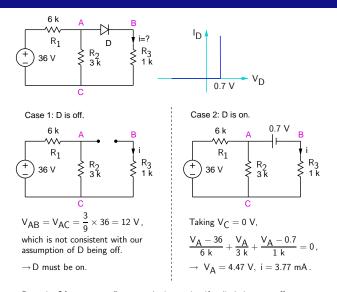
 \rightarrow D must be on.



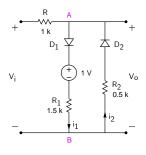


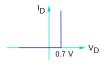
Taking
$$V_C = 0 V$$
,

$$\begin{split} &\frac{V_{\mbox{A}}-36}{6~k} + \frac{V_{\mbox{A}}}{3~k} + \frac{V_{\mbox{A}}-0.7}{1~k} = 0 \,, \\ &\rightarrow &V_{\mbox{A}} = 4.47~V, \; i = 3.77~mA \,. \end{split}$$

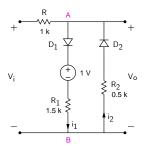


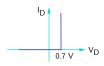
Remark: Often, we can figure out by inspection if a diode is on or off.





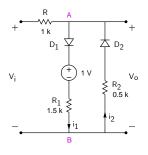
- (a) Plot V_{0} versus $V_{\dot{1}}$ for $-5~V < V_{\dot{1}} < 5~V\,.$
- (b) Plot $V_0(t)$ for a triangular input: -5~V to +5~V, 500 Hz.





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First, let us show that D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off.

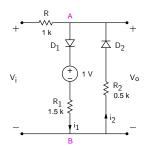


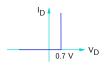


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First, let us show that D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off. Consider D_1 to be on $\rightarrow V_{AB} = 0.7 + 1 + i_1 R_1$.







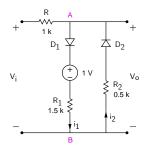
- (a) Plot V_0 versus V_i for $-5~V < V_i < 5~V$.
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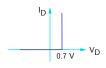
First, let us show that D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off.

Consider D_1 to be on $\rightarrow V_{AB} = 0.7 + 1 + i_1 R_1$.

Note that $i_1 > 0$, since D_1 can only conduct in the forward direction.

 \Rightarrow $V_{AB} > 1.7$ $V \Rightarrow D_2$ cannot conduct.





- (a) Plot V_0 versus V_i for $-5~V < V_i < 5~V$.
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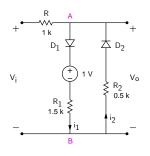
First, let us show that D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off.

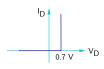
Consider D_1 to be on $\rightarrow V_{AB} = 0.7 + 1 + i_1 R_1$.

Note that $i_1 > 0$, since D_1 can only conduct in the forward direction.

 \Rightarrow $V_{AB} > 1.7$ $V \Rightarrow D_2$ cannot conduct.

Similarly, if D_2 is on, $V_{BA} > 0.7 \ V$, i.e., $V_{AB} < -0.7 \ V \Rightarrow D_1$ cannot conduct.





- (a) Plot V_0 versus V_i for $-5~V < V_i < 5~V$.
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First, let us show that D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off.

Consider D_1 to be on $\rightarrow V_{AB} = 0.7 + 1 + i_1 R_1$.

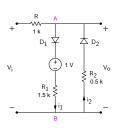
Note that $i_1 > 0$, since D_1 can only conduct in the forward direction.

 \Rightarrow $V_{AB} > 1.7$ $V \Rightarrow D_2$ cannot conduct.

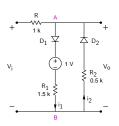
Similarly, if D_2 is on, $V_{BA} > 0.7 \ V$, i.e., $V_{AB} < -0.7 \ V \Rightarrow D_1$ cannot conduct.

Clearly, D_1 on $\Rightarrow D_2$ off, and D_2 on $\Rightarrow D_1$ off.

* For $-0.7~V < V_i < 1.7~V$, both D_1 and D_2 are off. \rightarrow no drop across R, and $V_o = V_i$. (1)



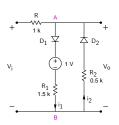
- * For $-0.7~V < V_i < 1.7~V$, both D_1 and D_2 are off. \rightarrow no drop across R, and $V_o = V_i$. (1)
- * For $V_i < -0.7 \ V$, D_2 conducts. $\rightarrow V_o = -0.7 i_2 R_2$. Use KVL to get i_2 : $V_i + i_2 R_2 + 0.7 + R i_2 = 0$.



- * For $-0.7~V < V_i < 1.7~V$, both D_1 and D_2 are off. \rightarrow no drop across R, and $V_o = V_i$. (1)
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* For $V_i > 1.7 \ V$, D_1 conducts. $\rightarrow V_o = 0.7 + 1 + i_1 R_1$. Use KVL to get i_1 : $-V_i + i_1 R + 0.7 + 1 + i_1 R_1 = 0$.

$$ightarrow i_1 = rac{V_i - 1.7}{R + R_1}$$
 , and $V_o = 1.7 + R_1 i_1 = rac{R_1}{R + R_1} \ V_i + 1.7 \ rac{R}{R + R_1}$. (3)

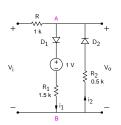


- * For $-0.7~V < V_i < 1.7~V$, both D_1 and D_2 are off. \rightarrow no drop across R, and $V_o = V_i$. (1)
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 , and $V_o = 1.7 + R_1 i_1 = rac{R_1}{R + R_1} \ V_i + 1.7 rac{R}{R + R_1}$. (3)

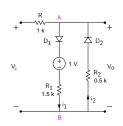
* Using Eqs. (1)-(3), we plot V_o versus V_i . (SEQUEL file: ee101_diode_circuit_1.sqproj)

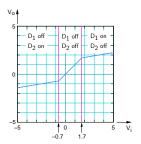


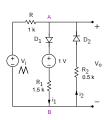
- * For $-0.7~V < V_i < 1.7~V$, both D_1 and D_2 are off. \rightarrow no drop across R, and $V_o = V_i$. (1)
- * For $V_i < -0.7~V$, D_2 conducts. $\to V_o = -0.7 i_2 R_2$. Use KVL to get i_2 : $V_i + i_2 R_2 + 0.7 + R i_2 = 0$.

* For $V_i > 1.7$ V, D_1 conducts. $\rightarrow V_o = 0.7 + 1 + i_1 R_1$. Use KVL to get i_1 : $-V_i + i_1 R + 0.7 + 1 + i_1 R_1 = 0$.

* Using Eqs. (1)-(3), we plot V_o versus V_i. (SEQUEL file: ee101_diode_circuit_1.sqproj)

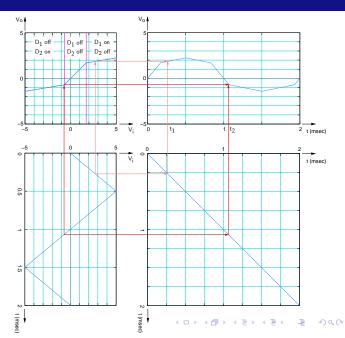


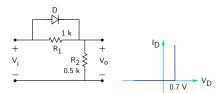




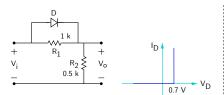
Point-by-point construction of V_{O} versus t:

Two time points, t_1 and t_2 , are shown as examples.

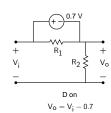


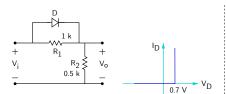


Plot V_0 versus $V_{\dot{1}}$ for $-5~V < V_{\dot{1}} < 5~V\,.$

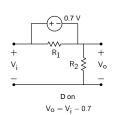


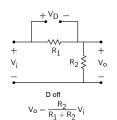
Plot V_0 versus $V_{\dot{1}}$ for $-5~V < V_{\dot{1}} < 5~V$.

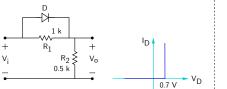


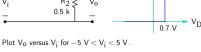


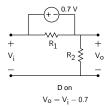
Plot V_{0} versus V_{i} for $-5\ V < V_{i} < 5\ V$.

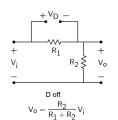




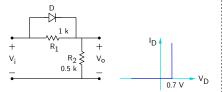


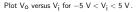


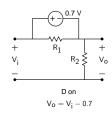


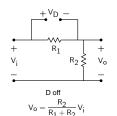


At what value of V_i will the diode turn on?

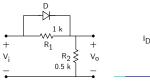






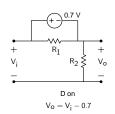


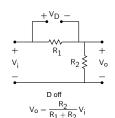
At what value of V_i will the diode turn on? In the off state, $V_D = \frac{R_1}{R_1 + R_2} \; V_i$.





Plot V_{0} versus $V_{\dot{1}}$ for $-5~V < V_{\dot{1}} < 5~V$.



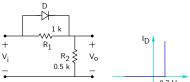


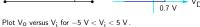
At what value of V_i will the diode turn on?

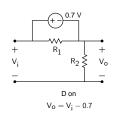
In the off state,
$$V_D=rac{R_1}{R_1+R_2}\;V_i$$
 .

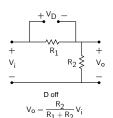
For D to change to the on state, $V_D = 0.7 \ V$.

i.e.,
$$V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05 \ V.$$









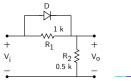
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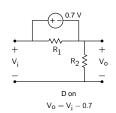
i.e.,
$$V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05 \ V.$$

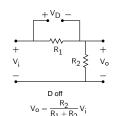
(SEQUEL file: ee101_diode_circuit_2.sqproj)





Plot V_{0} versus $V_{\dot{1}}$ for $-5~V < V_{\dot{1}} < 5~V$.





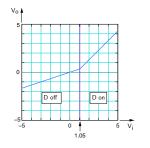
At what value of V_i will the diode turn on?

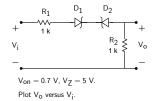
In the off state, $V_D=rac{R_1}{R_1+R_2}\;V_i$.

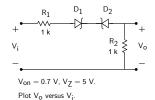
For D to change to the on state, $V_D = 0.7 \ V$.

i.e.,
$$V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05 \ V.$$

(SEQUEL file: ee101_diode_circuit_2.sqproj)





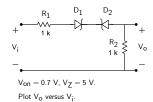


For a current to flow, we have two possibilities:

 D_1 on (forward), D_2 in reverse breakdown

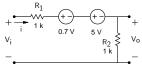
$$V_o = i\,R_2 = \frac{V_i - 5.7}{R_1 + R_2}\,R_2$$

Since i > 0, this can happen only when $V_i > 5.7 \ V.$



For a current to flow, we have two possibilities:

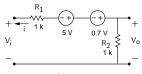
D₁ on (forward), D₂ in reverse breakdown



$$V_0 = i R_2 = \frac{V_i - 5.7}{R_1 + R_2} R_2$$

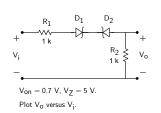
Since i > 0, this can happen only when $V_i > 5.7 \text{ V}$.

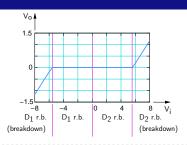
 D_2 on (forward), D_1 in reverse breakdown



$$V_o = -i\,R_2 = \frac{V_i + \,5.7}{R_1 + R_2}\,R_2$$

Since i > 0, this can happen only when $V_{\dot{I}} <$ -5.7 V.





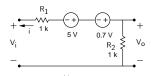
For a current to flow, we have two possibilities:

D₁ on (forward), D₂ in reverse breakdown

$$V_o = i \, R_2 = \frac{V_i - 5.7}{R_1 + R_2} \, R_2$$

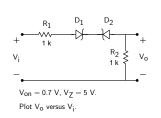
Since i > 0, this can happen only when $V_i > 5.7 \text{ V}$.

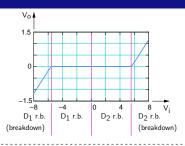
 D_2 on (forward), D_1 in reverse breakdown



$$V_o = -i\,R_2 = \frac{V_i + \ 5.7}{R_1 + R_2}\,R_2$$

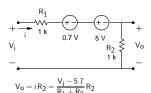
Since i > 0, this can happen only when $V_{\dot{I}} <$ -5.7 V.





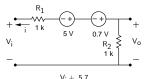
For a current to flow, we have two possibilities:

D₁ on (forward), D₂ in reverse breakdown



Since i > 0, this can happen only when $V_i > 5.7 \text{ V}$.

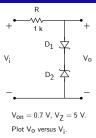
 D_2 on (forward), D_1 in reverse breakdown

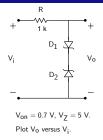


$$V_o = -i \, R_2 = \frac{V_i + 5.7}{R_1 + R_2} \, R_2$$

Since i > 0, this can happen only when $\mbox{V}_{\mbox{\scriptsize i}} <$ -5.7 V.

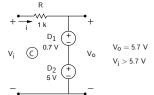
(SEQUEL file: ee101_diode_circuit_3.sqproj)

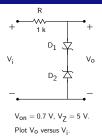




For a current to flow, we have two possibilities:

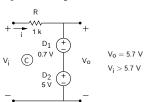
 D_1 on (forward), D_2 in reverse breakdown



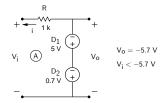


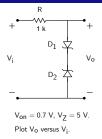
For a current to flow, we have two possibilities:

 D_1 on (forward), D_2 in reverse breakdown



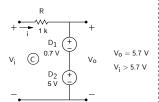
 D_2 on (forward), D_1 in reverse breakdown



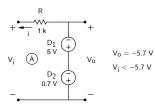


For a current to flow, we have two possibilities:

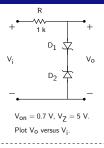
D₁ on (forward), D₂ in reverse breakdown

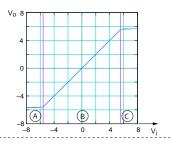


 D_2 on (forward), D_1 in reverse breakdown



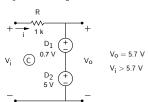
In the range, $-5.7~\text{V} < \text{V}_{\hat{i}} < 5.7~\text{V},$ no current flows, and $\text{V}_{\text{O}} = \text{V}_{\hat{i}}.$



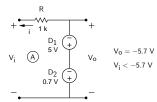


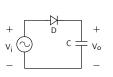
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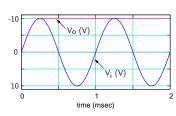
D₁ on (forward), D₂ in reverse breakdown

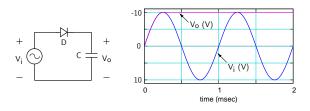


 D_2 on (forward), D_1 in reverse breakdown

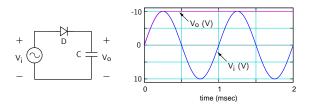




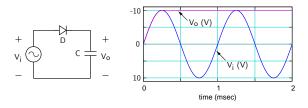




Let $V_o(t)=0$ V at t=0, and assume the diode to be ideal, with $V_{
m on}=0$ V.



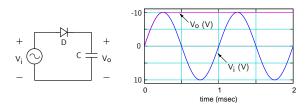
Let $V_o(t) = 0$ V at t = 0, and assume the diode to be ideal, with $V_{on} = 0$ V. For 0 < t < T/4, V_i rises from 0 to V_m . As a result, the capacitor charges.



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Since the on resistance of the diode is small, time constant $\tau \ll T/4$; therefore the charging process is instantaneous $\Rightarrow V_o(t) = V_i(t)$.

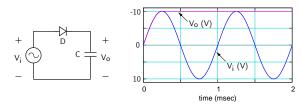


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For t > T/4, V_i starts falling. The capacitor holds the charge it had at t = T/4 since the diode prevents discharging.



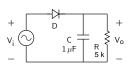
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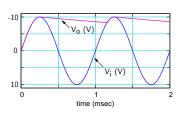
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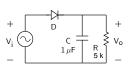
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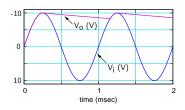
For t > T/4, V_i starts falling. The capacitor holds the charge it had at t = T/4 since the diode prevents discharging.

SEQUEL file: ee101_diode_circuit_5.sqproj

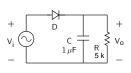


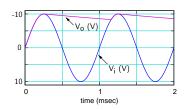






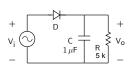
If a resistor is added in parallel, a discharging path is provided for the capacitor, and the capacitor voltage falls after reaching the peak.

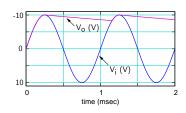




If a resistor is added in parallel, a discharging path is provided for the capacitor, and the capacitor voltage falls after reaching the peak.

When $V_i > V_o$, the capacitor charges again. The time constant for the charging process is $\tau = R_{\text{Th}} C$, where $R_{\text{Th}} = R \parallel R_{\text{on}}$ is the Thevenin resistance seen by the capacitor, R_{on} being the on resistance of the diode.

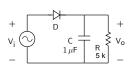


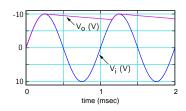


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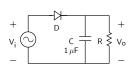


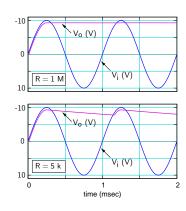
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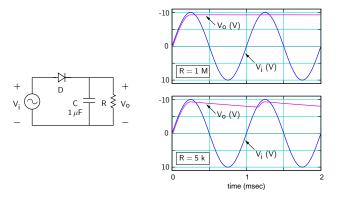
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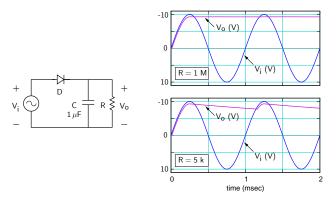
SEQUEL file: ee101_diode_circuit_5a.sqproj



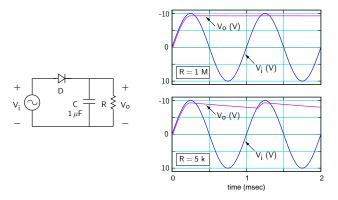




With $V_{\text{on}} = 0.7 \text{ V}$, the capacitor charges up to $(V_m - 0.7 \text{ V})$.



With $V_{\rm on}=0.7~V$, the capacitor charges up to $(V_m-0.7~V)$. Apart from that, the circuit operation is similar.

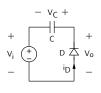


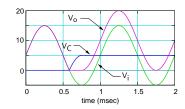
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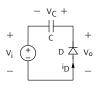
SEQUEL file: ee101_diode_circuit_5a.sqproj

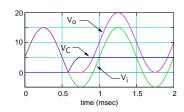




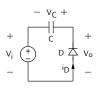


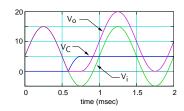
* Assume $V_{\rm on}=0$ V for the diode. When D conducts, $V_D=-V_o=0 \Rightarrow V_C+V_i=0$, i.e., $V_C=-V_i$.



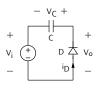


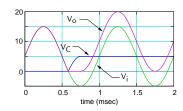
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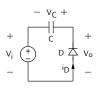
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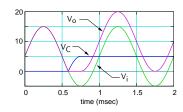




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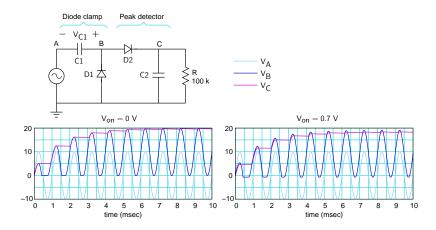


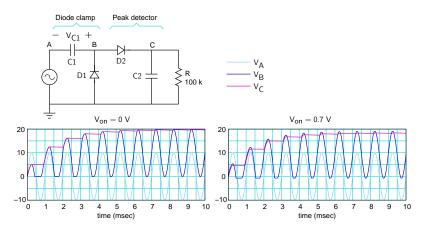


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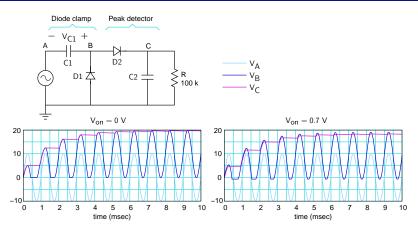
(SEQUEL file: ee101_diode_circuit_6.sqproj)



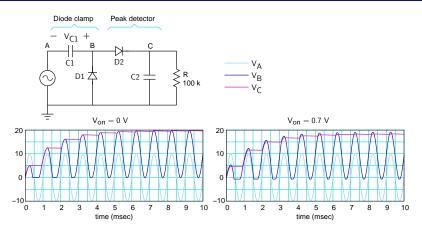




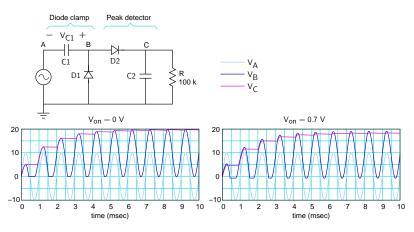
* The diode clamp shifts V_A up by V_m (the amplitude of the AC source), making V_B go from 0 to 2 V_m .



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- * Note that it takes a few cycles to reach steady state. Plot V_{C1} , i_{D1} , i_{D2} versus t and explain the initial behaviour of the circuit.



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(SEQUEL file: ee101_voltage_doubler.sqproj)

