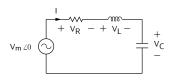
EE101: Resonance in RLC circuits

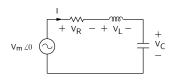


M. B. Patil mbpatil@ee.iitb.ac.in

Department of Electrical Engineering Indian Institute of Technology Bombay

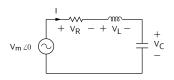


$$\begin{split} \mathbf{I} &= \frac{V_m \angle 0}{R + j\omega L + 1/j\omega C} = \frac{V_m}{R + j(\omega L - 1/\omega C)} \equiv I_m \angle \theta \,, \text{ where} \\ I_m &= \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \,, \quad \theta = -\tan^{-1}\left[\frac{\omega L - 1/\omega C}{R}\right] \,. \end{split}$$



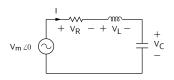
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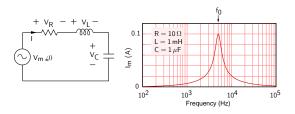
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- * As ω is varied, both I_m and θ change.
- * When $\omega L=1/\omega C$, I_m reaches its maximum value, $I_m^{max}=V_m/R$, and θ becomes 0, i.e., the current I is in phase with the applied voltage.
- * The above condition is called "resonance," and the corresponding frequency is called the "resonance frequency" (ω_0).

$$\omega_0 = 1/\sqrt{LC}$$

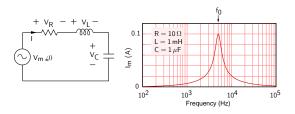


$$I_{m} = \frac{V_{m}}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \,, \ \theta = -\tan^{-1}\left[\frac{\omega L - 1/\omega C}{R}\right] \,. \label{eq:Im}$$



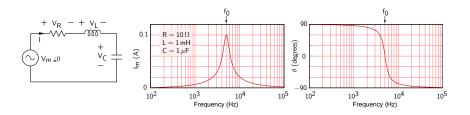
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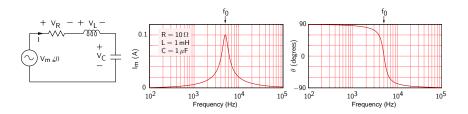
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- * As $\omega \to 0$, the term $1/\omega C$ dominates, and $\theta \to \pi/2$.



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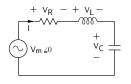
- * As ω deviates from ω_0 , I_m decreases.
- * As $\omega \to 0$, the term $1/\omega C$ dominates, and $\theta \to \pi/2$.
- * As $\omega \to \infty$, the term ωL dominates, and $\theta \to -\pi/2$.

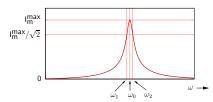


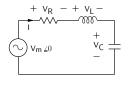
$$I_{\text{m}} = \frac{V_{\text{m}}}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \,, \quad \theta = -\tan^{-1}\left[\frac{\omega L - 1/\omega C}{R}\right] \,. \label{eq:Im}$$

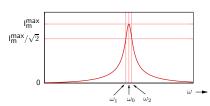
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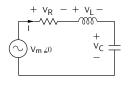


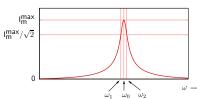




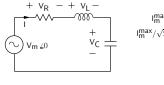


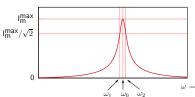
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- * Define ω_1 and ω_2 (see figure) as frequencies at which $I_m = I_m^{max}/\sqrt{2}$, i.e., the power absorbed by R is $P^{max}/2$.

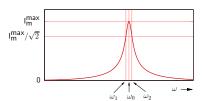




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- * Define ω_1 and ω_2 (see figure) as frequencies at which $I_m = I_m^{max}/\sqrt{2}$, i.e., the power absorbed by R is $P^{max}/2$.
- * The bandwidth of a resonant circuit is defined as $B=\omega_2-\omega_1$, and the quality factor as $Q=\omega_0/B$. Quality is a measure of the sharpness of the I_m versus frequency relationship.



$$I_m = rac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}$$
. For $\omega = \omega_0$, $I_m = I_m^{max} = V_m/R$. For $\omega = \omega_1$ or $\omega = \omega_2$, $I_m = I_m^{max}/\sqrt{2}$.

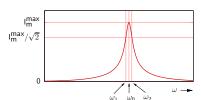


$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}.$$

For
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For
$$\omega=\omega_1$$
 or $\omega=\omega_2$, $\emph{I}_m=\emph{I}_m^{\emph{max}}/\sqrt{2}$.

$$\Rightarrow \frac{1}{\sqrt{2}} \left(\frac{V_m}{R} \right) = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \quad \text{for } \omega = \omega_{1,2} \,.$$



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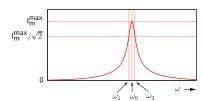
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$$2\,R^2 = R^2 + (\omega L - 1/\omega\,C)^2 \rightarrow R = \pm(\omega L - 1/\omega\,C)\,.$$

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.

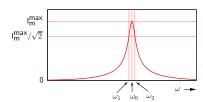
Solving for $\boldsymbol{\omega}$ (and discarding negative solutions), we get

$$\omega_{1,2} = \mp \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}.$$

$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}.$$

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$$\omega = \omega_0$$
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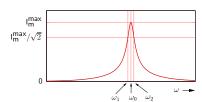
* Bandwidth
$$B = \omega_2 - \omega_1 = R/L$$
.



$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}.$$

For
$$\omega = \omega_0$$
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$$2R^2 = R^2 + (\omega L - 1/\omega C)^2 \to R = \pm (\omega L - 1/\omega C)$$
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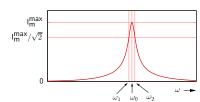
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$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}.$$

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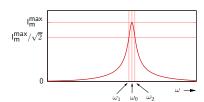
- * Bandwidth $B = \omega_2 \omega_1 = R/L$.
- * Quality $Q = \omega_0/B = \omega_0 L/R$.
- * Show that, at resonance (i.e., $\omega = \omega_0$), $|\mathbf{V}_L| = |\mathbf{V}_C| = Q V_m$.



$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}.$$

For
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$$\Rightarrow \frac{1}{\sqrt{2}} \left(\frac{V_m}{R} \right) = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \quad \text{for } \omega = \omega_{1,2} \,.$$

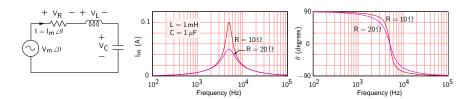
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$$\omega = \omega_{1,2}$$

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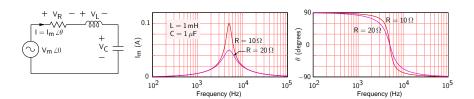
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- * Quality $Q = \omega_0/B = \omega_0 L/R$.
- * Show that, at resonance (i.e., $\omega=\omega_0$), $|\mathbf{V}_L|=|\mathbf{V}_C|=Q\,V_m$.
- * Show that $\omega_0 = \sqrt{\omega_1 \omega_2}$.

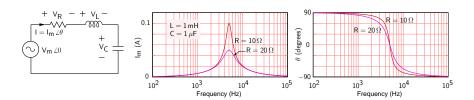


As R is increased,



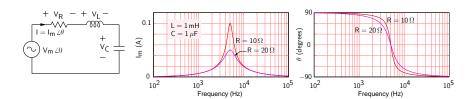
As R is increased,

* The quality factor $Q = \omega_0 L/R$ decreases, i.e., I_m versus ω curve becomes broader.



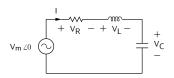
As R is increased,

- * The quality factor $Q = \omega_0 L/R$ decreases, i.e., I_m versus ω curve becomes broader
- * The maximum current (at $\omega = \omega_0$) decreases (since $I_m^{max} = V_m/R$).

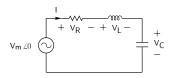


As R is increased,

- * The quality factor $Q = \omega_0 L/R$ decreases, i.e., I_m versus ω curve becomes broader.
- * The maximum current (at $\omega = \omega_0$) decreases (since $I_m^{max} = V_m/R$).
- * The resonance frequency ($\omega_0 = 1/\sqrt{LC}$) is not affected.

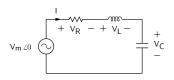


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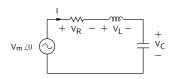
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* For $\omega<\omega_0,\,\omega L<1/\omega C$, the net impedance is capacitive, and the current leads the applied voltage.



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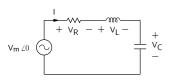
- * For $\omega<\omega_0,\,\omega L<1/\omega C$, the net impedance is capacitive, and the current leads the applied voltage.
- * For $\omega=\omega_0$, $\omega L=1/\omega\,\mathcal{C}$, the net impedance is purely resistive, and the current is in phase with the applied voltage.



$$\begin{split} \mathbf{I} &= \frac{V_m \angle 0}{R + j\omega L + 1/j\omega C} = \frac{V_m}{R + j(\omega L - 1/\omega C)} \equiv I_m \angle \theta \,, \, \text{where} \\ I_m &= \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} \,, \quad \theta = -\tan^{-1}\left[\frac{\omega L - 1/\omega C}{R}\right] \,. \end{split}$$

- * For $\omega<\omega_0,\,\omega L<1/\omega C$, the net impedance is capacitive, and the current leads the applied voltage.
- * For $\omega = \omega_0$, $\omega L = 1/\omega C$, the net impedance is purely resistive, and the current is in phase with the applied voltage.
- * For $\omega > \omega_0$, $\omega L > 1/\omega C$, the net impedance is inductive, and the current lags the applied voltage.

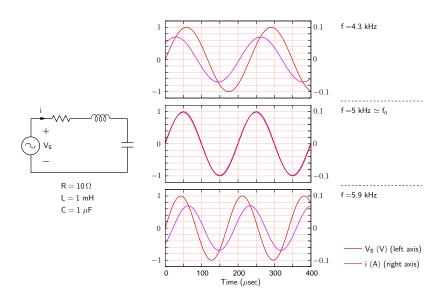




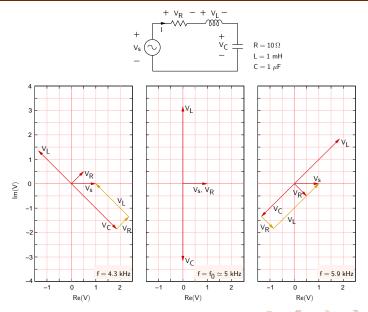
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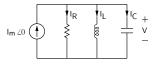
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- * For $\omega > \omega_0$, $\omega L > 1/\omega C$, the net impedance is inductive, and the current lags the applied voltage.
- * Let us look at an example (next slide).



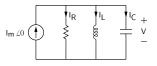


Resonance in series RLC circuits: phasor diagrams



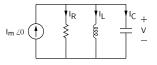


$$I_m \angle 0 = \mathbf{Y} \mathbf{V}$$
, where $\mathbf{Y} = G + j\omega C + 1/j\omega L$ $(G = 1/R)$.
$$\mathbf{V} = \frac{I_m \angle 0}{G + j\omega C + 1/j\omega L} = \frac{I_m}{G + j(\omega C - 1/\omega L)} \equiv V_m \angle \theta$$
, where
$$V_m = \frac{I_m}{\sqrt{G^2 + (\omega C - 1/\omega L)^2}}, \quad \theta = -\tan^{-1}\left[\frac{\omega C - 1/\omega L}{G}\right].$$



$$I_m \angle 0 = \mathbf{Y} \mathbf{V}$$
, where $\mathbf{Y} = G + j\omega C + 1/j\omega L$ $(G = 1/R)$.
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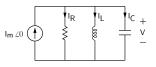
* As ω is varied, both V_m and θ change.



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- * The above condition is called "resonance," and the corresponding frequency is called the "resonance frequency" (ω_0).

$$\omega_0 = 1/\sqrt{LC}$$



Series RLC circuit:
$$I_m = \frac{V_m}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}\,, \quad \theta = -\tan^{-1}\left[\frac{\omega L - 1/\omega C}{R}\right]\,.$$
 Parallel RLC circuit: $V_m = \frac{I_m}{\sqrt{G^2 + (\omega C - 1/\omega L)^2}}\,, \quad \theta = -\tan^{-1}\left[\frac{\omega C - 1/\omega L}{G}\right]\,.$

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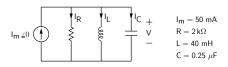


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- * Show that $\omega_0 = \sqrt{\omega_1 \omega_2}$.



Resonance in parallel RLC circuits: home work



- * Calculate ω_0 , f_0 , B, Q.
- * Calculate I_R , I_L , I_C at $\omega = \omega_0$, ω_1 , ω_2 .
- * Verify graphically that $I_R + I_L + I_C = I_s$ in each case.
- * Plot the power absorbed by R as a function of frequency for $f_0/10 < f < 10\,f_0$.