



# Standard Test Method for On-Line Determination of Anions and Carbon Dioxide in High Purity Water by Cation Exchange and Degassed Cation Conductivity<sup>1</sup>

This standard is issued under the fixed designation D 4519; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

<sup>ε1</sup> NOTE—Footnotes were editorially removed in June 1999.

## 1. Scope

1.1 This on-line test method includes hydrogen exchange and degassing by boiling and provides means for determining anions (such as  $\text{Cl}^-$ ,  $\text{SO}_4^{4-}$ ,  $\text{NO}_3^-$ , and  $\text{F}^-$ ) at levels as low as 2 µg/L (2 ppb) and carbon dioxide at the level of 0.01 to 10 mg/L (ppm) at 25°C in high purity water and steam condensate by measuring electrical conductivity.

1.2 The conductivity of all anions (except  $\text{OH}^-$ ) is determined and not the conductivity of an individual anion if more than one is present. If only one anion is present (such as  $\text{Cl}^-$  or  $\text{SO}_4^{4-}$ ), reference to Table 1 and Table 2 or Figs. 1-3 provides the chloride or sulfate and  $\text{CO}_2$  concentration.

1.3 This test method has been improved in accuracy by using a modern microprocessor instrument for conductivity and temperature measurement and appropriate temperature compensation algorithms for compensation to 25°C.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

## 2. Referenced Documents

### 2.1 ASTM Standards:

D1066 Practice for Sampling Steam<sup>2</sup>

D1125 Test Methods for Electrical Conductivity and Resistivity of Water<sup>2</sup>

D1129 Terminology Relating to Water<sup>2</sup>

D1192 Specifications for Equipment for Sampling Water and Steam in Closed Conduits<sup>2</sup>

D1193 Specification for Reagent Water<sup>2</sup>

D2186 Test Methods for Deposit-Forming Impurities in Steam<sup>3</sup>

D2777 Practice for Determination of Precision and Bias of

TABLE 1 Increase in Conductivity of Pure Water Expressed as Chloride Ion or Sulfate Ion

Conductivity due to Chlorides	Concentration Chlorides (PPB)	Conductivity due to Sulfates	Concentration Sulfates (PPB)
0.0548	0.0	0.0548	0.0
0.0595	1	0.0608	1
0.0651	2	0.0669	2
0.0717	3	0.0732	3
0.0791	4	0.0797	4
0.0872	5	0.0862	5
0.0958	6	0.0929	6
0.1049	7	0.0997	7
0.1145	8	0.1066	8
0.1243	9	0.1137	9
0.1344	10	0.1208	10
0.2427	20	0.1969	20
0.3560	30	0.2780	30
0.4709	40	0.3616	40
0.5865	50	0.4455	50
0.7023	60	0.5320	60
0.8183	70	0.6181	70
0.9345	80	0.7044	80
1.0507	90	0.7909	90
1.1669	100	0.8775	100
2.2209	200	1.7470	200
5.8252	500	4.362	500

Applicable Methods of Committee D-19 on Water<sup>2</sup>  
D3370 Practices for Sampling Water from Closed Conduits<sup>2</sup>  
D3864 Guide for Continual On-Line Monitoring Systems for Water Analysis<sup>2</sup>

## 3. Terminology

3.1 *Definitions*—For definitions of terms used in this test method, refer to Test Methods D 1125 and Terminology D 1129.

## 4. Summary of Test Method

4.1 This test method measures the anion concentration (such as  $\text{Cl}^-$  and  $\text{SO}_4^{4-}$ ) by measuring the electrical conductivity of the anions after passing cooled condensate or high purity water through a cation exchanger in the hydrogen form, then through an electric reboiler. Passage through the cation resin replaces cations (including ammonia and amines) in the water with hydrogen ions. This eliminates interference in the measurement of anions. Three conductivity cells located in the instrument provide measurements of the influent conductivity, cation

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee D-19 on Water and is the direct responsibility of Subcommittee D19.03 on Sampling of Water and Water-Formed Deposits, Surveillance of Water, and Flow Measurement of Water.

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<sup>2</sup> *Annual Book of ASTM Standards*, Vol 11.01.

<sup>3</sup> *Annual Book of ASTM Standards*, Vol 11.02.

**TABLE 2 25°C Conductivity of the Sample Immediately After the Cation Column, Relating to the CO<sub>2</sub> Concentration with the Anion Component Subtracted Out (See 11.7)**

Conductivity μs/cm	Carbon Dioxide	
	ppm	ppb
0.0548	0	0
0.09	0.01	10
0.12	0.02	20
0.16	0.03	30
0.19	0.04	40
0.21	0.05	50
0.24	0.06	60
0.26	0.07	70
0.28	0.08	80
0.3	0.09	90
0.32	0.1	100
0.48	0.2	200
0.61	0.3	300
0.71	0.4	400
0.81	0.5	500
0.89	0.6	600
0.97	0.7	700
1.04	0.8	800
1.11	0.9	900
1.17	1.0	...
1.69	2.0	...
2.09	3.0	...
2.42	4.0	...
2.72	5.0	...
2.98	6.0	...
3.23	7.0	...
3.46	8.0	...
3.67	9.0	...
3.88	10	...
5.46	20	...

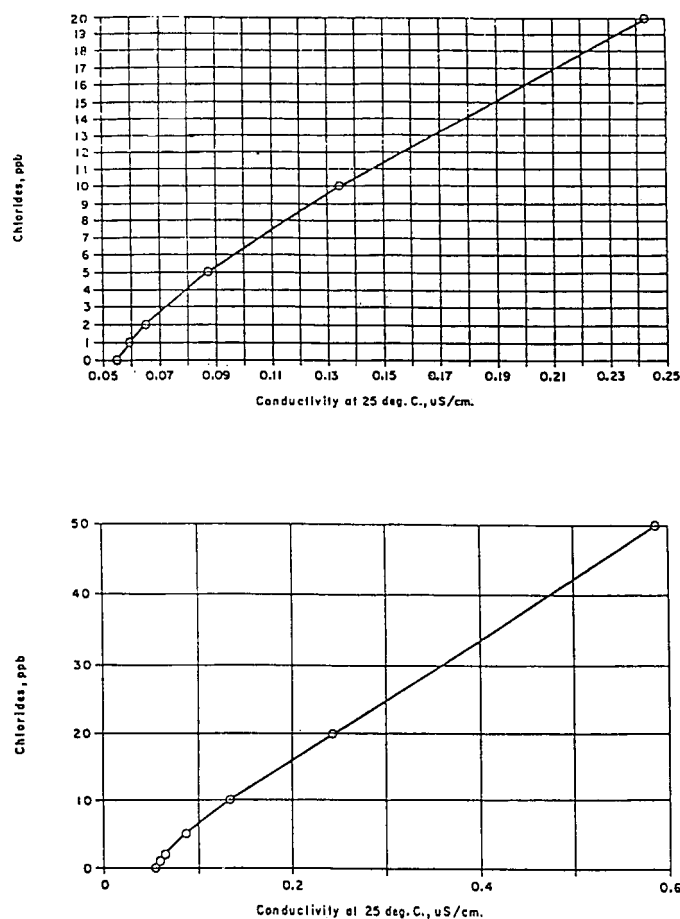
conductivity at the incoming sample temperature, and the effluent conductivity at atmospheric boiling water temperature after acidic (volatile) gas removal. Conductivity values are then corrected to 25°C. While the influent conductivity measurement is not necessary in determining the total anion conductivity, its determination provides a more complete evaluation of the sample, which can also include an estimation of the amine content. Measurement of the cation and reboil effluent conductivities are necessary in determining the composition of the influent (total anions and acidic gas content). Reference to Table 1 and Table 2 or Figs. 1-3, or both, are then necessary to complete the determinations.

## 5. Significance and Use

5.1 This test method can be a useful diagnostic tool in measuring the impurities and detecting their sources in high purity water, the steam condensate of high pressure power plants, and in the process water of certain industries requiring water of the highest purity attainable.

5.2 The measurement of such impurities is most important to these industries since plant outages or product contamination can result from events such as condenser leakage. Also, water quality deviations can occur from condensate polishing and makeup water equipment malfunctions.

5.3 The continuous measurement and trends provided by this test method are of particular interest and can indicate the need for corrections in water treating or operating procedures and equipment. The equipment for this test method can be considered more rugged and adaptable to installation under



**FIG. 1 Chloride Ion vs. Conductivity**

plant operating conditions than the more accurate laboratory methods, such as ion chromatography and atomic absorption.

## 6. Interferences

6.1 It is important to devote particular attention to accurate flow and temperature control as variations can cause inaccuracies. See Annex A1, Annex A2, and Annex A3 for additional information on this subject.

## 7. Apparatus

7.1 *Mechanical Ion Exchanger-Degasser Instrument.*

7.2 *Constant Head Device*, for providing approximately 1.5 m (5 ft) head pressure for water entering the instrument.

7.3 *Constant Temperature Equipment*, for adjusting the influent temperature to 25°C ± 0.5°C.

7.4 *Conductivity Instruments and Sensors*, for measuring the conductivity of the sample to determine the concentration of anions and carbon dioxide. Use of instruments that have a specialized temperature compensation for high purity water (to 25°C) based on an acid such as HCl or H<sub>2</sub>SO<sub>4</sub> is required for this test method.

7.5 *Hydrogen Exchange Cartridge*, 1½ in. inside diameter, 12 in. height, containing 1 lb of 8 % cross-linked styrene-divinylbenzene, strong acid gel cation exchange resin in the H<sup>+</sup> form; U.S. standard mesh 16 by 50 (1190 by 297 μm) may be used. Regenerate with 1500 mL of hydrochloric acid (1 + 6) at a flow rate of 40 to 50 mL/min, followed by rinsing with 300

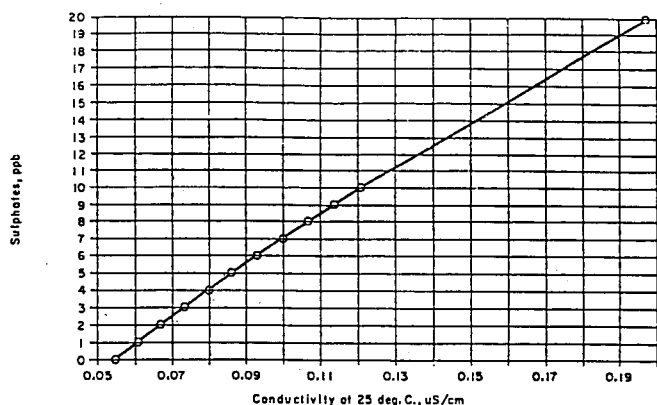


FIG. 2 Sulfate Ion vs. Conductivity

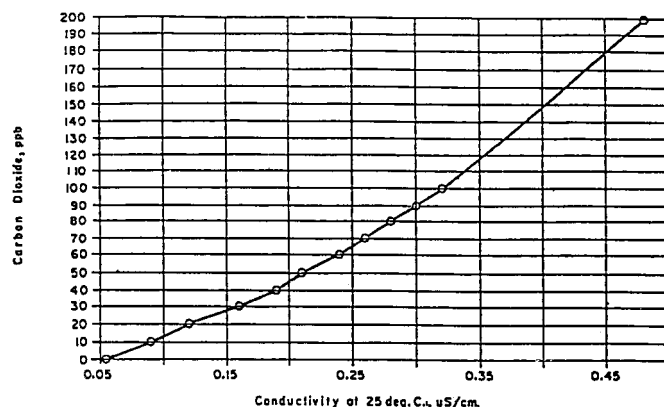


FIG. 3 Carbon Dioxide vs. Conductivity

mL of Type II water at the same flow rate. Then rinse with 3500 mL of Type II water at a flow rate of 100 to 150 mL/min. Rinse down when placing in service.

NOTE 1—The column inside diameter, resin bed height, inlet sample temperature (11.3), and service flowrate (11.4) have been standardized to provide comparable results. They may not be the optimum values. The user should realize that those parameters affect the measurement.

7.6 Software to automate the determination of anions and carbon dioxide is available.

## 8. Reagents

8.1 *Purity of Reagents*—Reagent grade chemicals shall be used in all tests. Unless otherwise indicated, it is intended that all reagents shall conform to the specifications of the American Chemical Society, where such specifications are available.<sup>4</sup> Other grades may be used, provided it is first ascertained that the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination.

8.2 *Purity of Water*—Unless otherwise indicated, references to water shall be understood to mean reagent water conforming

to Specification D 1193, Type II.

8.3 *Chloride Solution, Stock* (1 mL = 0.1 mg  $\text{Cl}^-$ )—Dissolve in water 0.1649 g of sodium chloride ( $\text{NaCl}$ ) dried to constant weight at 105°C, and dilute to 1 L in a thoroughly cleaned polyethylene flask.

8.4 *Chloride Solution, Standard* (1.00 mL = 0.001 mg)—Dilute 10.00 mL of chloride stock solution (8.3) to 1 L with water.

8.4.1 This standard chloride solution is to be used in the calibration of the instrument if desired, or reference can be made to the instruction booklet furnished with the instrument.

8.5 *Hydrochloric Acid* (1 + 6)—Add 100 mL concentrated  $\text{HCl}$  (sp. gr. 1.19) to 600 mL water.

## 9. Sampling

9.1 Collect the sample in accordance with the applicable ASTM standards: Practice D 1066, Specification D 1192, and Practices D 3370.

## 10. Calibration

10.1 The instrument may be calibrated by pumping solutions of known concentrations of  $\text{Cl}^-$  (in  $\text{NaCl}$  form) or  $\text{SO}_4^{--}$  (in  $\text{Na}_2\text{SO}_4$  form) through the instrument and observing the conductivity increases. It may be preferred to use the calibration charts shown in the instruction book accompanying

<sup>4</sup> *Reagent Chemicals, American Chemical Society Specifications*, American Chemical Society, Washington, DC. For suggestions on the testing of reagents not listed by the American Chemical Society, see *Analar Standards for Laboratory Chemicals*, BDH Ltd., Poole, Dorset, U.K., and the *United States Pharmacopeia and National Formulary*, U.S. Pharmaceutical Convention, Inc. (USPC), Rockville, MD.

the instrument or in referenced articles.<sup>5, 6, 7, 8</sup>

10.2 If it is desired to calibrate the instrument using known chloride solutions, the range of 0.001 to 0.010 mg/L (1 to 10 ppb) of chloride may be covered by application of 0.2 to 2.0 mL/min of the standard chloride solution (8.4.1) to the 200 mL/min flow by injecting the flow from a small peristaltic pump to a hypodermic needle inserted in a plastic tubing connection.

## 11. Procedure

### 11.1 Flush out the piping thoroughly by flow of high purity

<sup>5</sup> Lane, R. W., Sollo, F. W., Neff, C. H., "Continuous Monitoring of Anions in Feedwater by Electrical Conductivity," Illinois State Water Survey Reprint 473, Reprinted from "Water and Steam, Their Properties and Current Industrial Applications," Pergamon Press, Oxford and New York, 1980.

<sup>6</sup> Electric Power Research Institute, "Monitoring Cycle Water Chemistry in Fossil Plants," EPRI GS-7556, Vol 1: Monitoring Results.

<sup>7</sup> Continuous Conductivity Monitoring of Anions in High-Purity Water, ASTM STP 742, ASTM, 1981, p. 195.

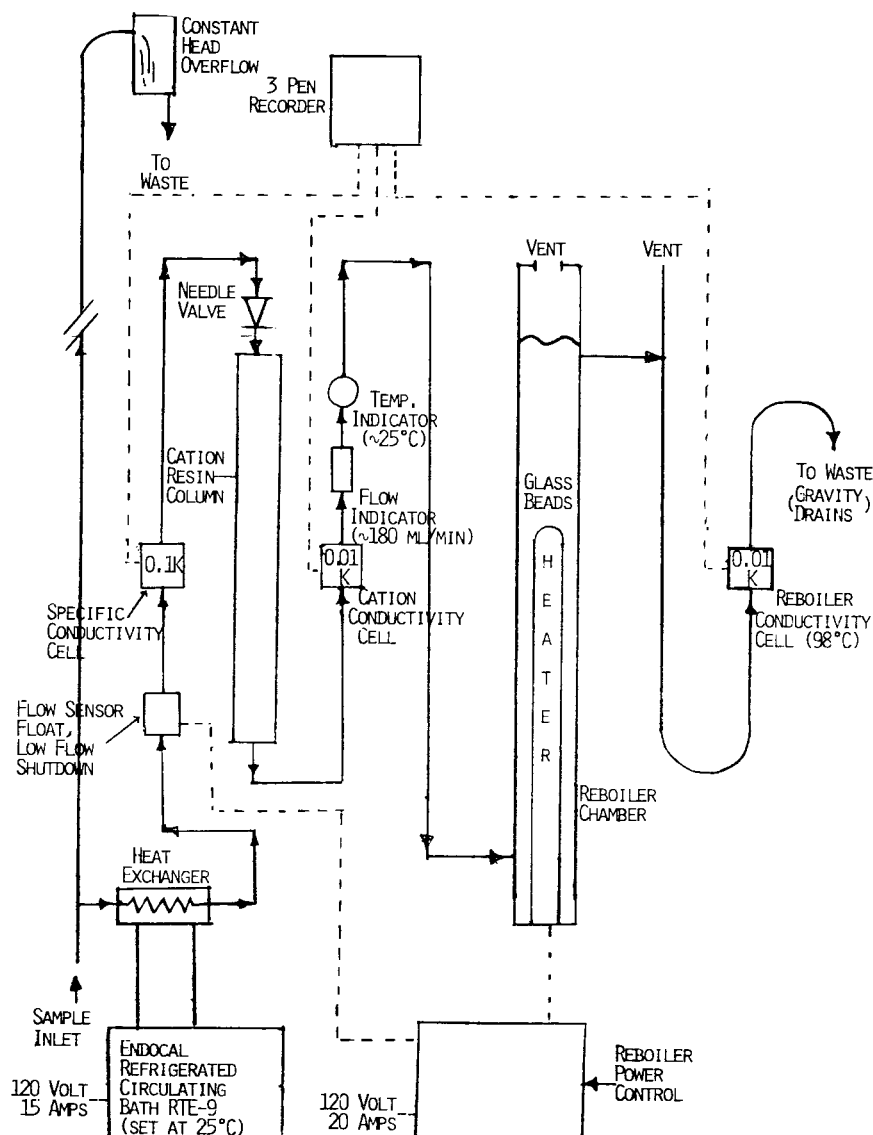
<sup>8</sup> Internal report from Carl C. Scheerer, C.I.P.S., Springfield, IL, April 18, 1989.

water through the instrument before starting the flow of water to be tested.

11.2 Refer to the manufacturer's instruction booklet before starting the instrument. Because of the nature of this measuring technique, it is very important to follow the manufacturer's instructions very carefully in order to achieve accurate results. See Annex A1-Annex A4 for a discussion on the effects caused by variations in operating conditions and interfering substances.

11.3 Connect the high purity water or condensate to be tested to the instrument influent connection. This water should preferably be at a temperature of  $25 \pm 0.5^\circ\text{C}$ . The flow shall first pass through the constant head device, then into the instrument through the hydrogen ion exchanger and electric reboiler and out the reboil chamber effluent (Fig. 4 and Fig. 5).

11.4 Adjust the flow through the instrument to the proper flow rate (200 mL/min), or as specified by the instrument manufacturer. It is important to use a constant head device in order to maintain a stable flow rate, otherwise changes in



**FIG. 4 Flow Diagram for Mechanical-Ion Exchanger-Degasser Instrument**

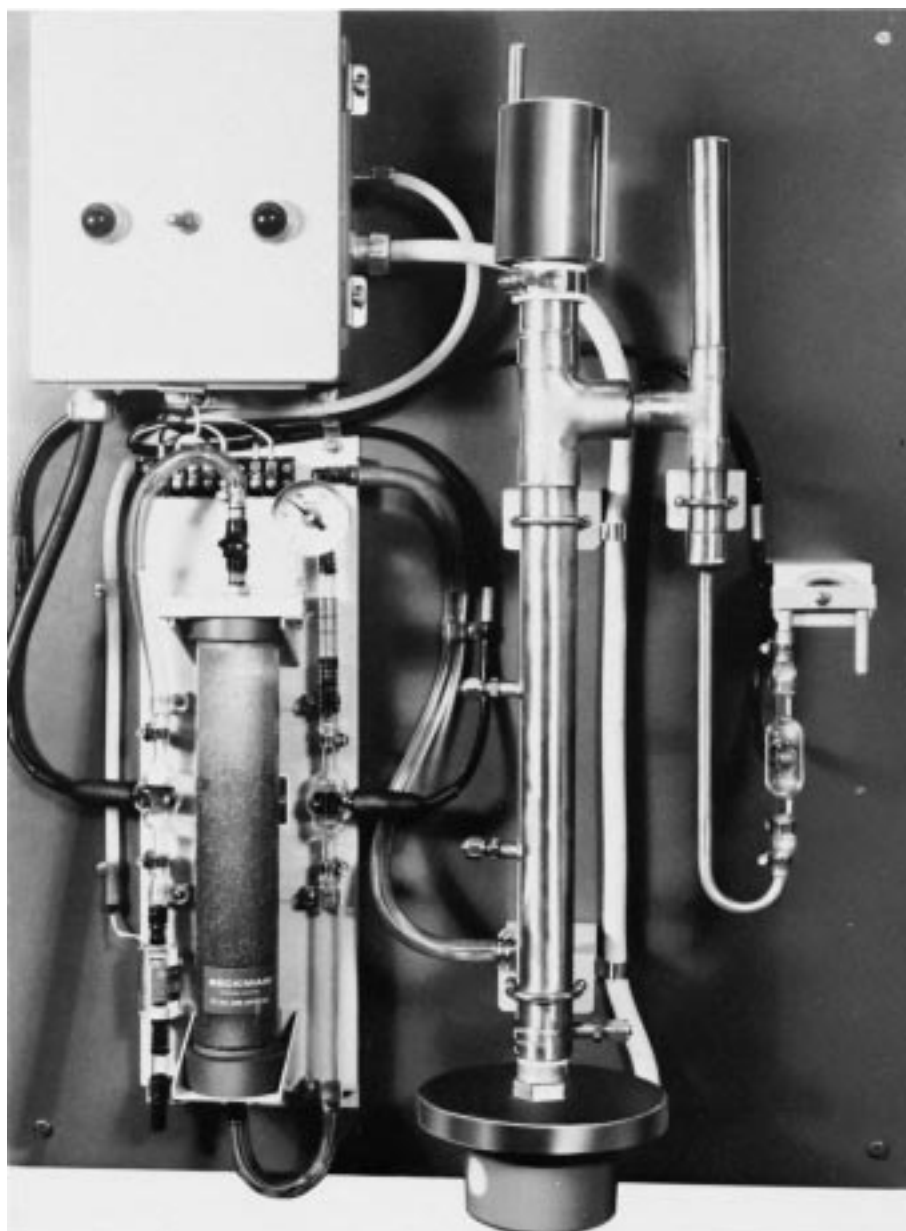


FIG. 5 Mechanical-Ion Exchanger-Degasser Instrument (Larson-Lane Condensate Reboiler)

cation resin exchange efficiency may occur with changes in the flow rate.

11.5 Clean up the system by maintaining the recommended flow rate through the instrument for 24 h or longer to approach a minimum value of  $0.055 \mu\text{S}/\text{cm}$  reading for pure water at the final effluent conductivity. On restart, several hours of operation may be required before this minimum conductivity value is obtained.

11.6 Refer to Table 1, or Fig. 1 and Fig. 2, or both, to determine the equivalent concentration of chloride ion or sulfate ion based on the conductivity reading of the final conductivity cell.

11.7 In order to obtain the volatiles expressed as carbon dioxide in Table 2, subtract the conductivity of pure water ( $0.055 \mu\text{S}/\text{cm}$ ) from the conductivity of the final effluent cell. Then deduct this value from the cation conductivity obtained

from the cell immediately after the cation exchange resin. Use this adjusted conductivity value to look up the concentration of volatiles expressed as a concentration of carbon dioxide in Table 2, or Fig. 3, or both.

11.7.1 Example: Based on a final cell conductivity reading of  $0.087 \mu\text{S}/\text{cm}$  (equivalent to 5 ppb of  $\text{Cl}^-$  in a system predominant in chloride ion),  $0.055 \mu\text{S}/\text{cm}$  is deducted for the conductivity of pure water to obtain a value of  $0.087 - 0.055 = 0.032 \mu\text{S}/\text{cm}$ . Then deduct this number (0.032) from the cation conductivity ( $0.242 - 0.032 = 0.21 \mu\text{S}/\text{cm}$  due to volatiles, which corresponds to 50  $\mu\text{g}/\text{L}$  (ppb) of carbon dioxide, as read from Table 2. This deduction is necessary to account for the anion conductivity (other than carbon dioxide) obtained in the cation conductivity measurement.

11.8 The service life of the cation cartridge may vary from

one month to several months depending on the amine concentration in the influent.

## 12. Report

12.1 Report the results as  $\mu\text{g/L Cl}^-$ , or  $\text{SO}_4^{--}$ , or both, and  $\text{CO}_2$  as obtained from Table 1 and Table 2, or Figs. 1-3, or both.

## 13. Precision and Bias

13.1 Since this test method involves continuous sampling and measurement, Practice D 2777 is not applicable. Footnotes

7 through 10 do show that there is excellent agreement between the theoretical and measured conductivity values of  $\text{Cl}^-$  and  $\text{SO}_4^{--}$  ions in the 0 to 50  $\mu\text{g/L}$  (ppb) range.

## 14. Keywords

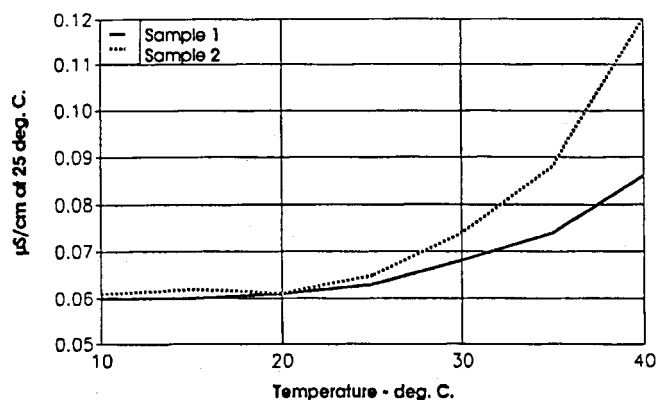
14.1 anion electrical conductivity; carbon dioxide; cation conductivity; degassed cation conductivity; electrical conductivity; high purity water; reboiled conductivity

# ANNEXES

## (Mandatory Information)

### A1. EFFECTS OF THE INFLUENT WATER TEMPERATURE

A1.1 The cation resin loses its ability to maintain its holding power with increases in temperature. Therefore, it is important to maintain a constant temperature so as to avoid any changes in the baseline of the measurement. Fig. A1.1 shows the effects of temperature of the influent water versus the conductivity (at 25°C) of the effluent water of a cation column when supplied with 0.055  $\mu\text{S/cm}$  water.



**FIG. A1.1 Cation Resin Performance, Amount of Ionic Leaching Versus the Flow Rate for IWC Type TCD1 Resin in a 2-in. Diameter Tube**

### A2. EFFECTS OF SAMPLE VELOCITY

A2.1 The cation resin has an optimum dynamic efficiency at a given sample flow rate. Fig. A2.1 depicts the change in conductivity of the effluent of a 2 in. inside diameter column with 1 lb of cation resin versus flow rate. As indicated by this chart, it is important to provide a flow of 200 mL/min through the resin in order to maximize the efficiency of the resin and to minimize resin bleed-off. While this is a larger-sized diameter

cartridge than that described in the present test method (1½ in. (41 mm) inside diameter), the same conclusions and need for accurate flow control are to be expected. Any deviations in the flow rate will cause variations in the baseline of the measurement and therefore should be held to a minimum in order to reduce any errors in measurement. More accurate cation



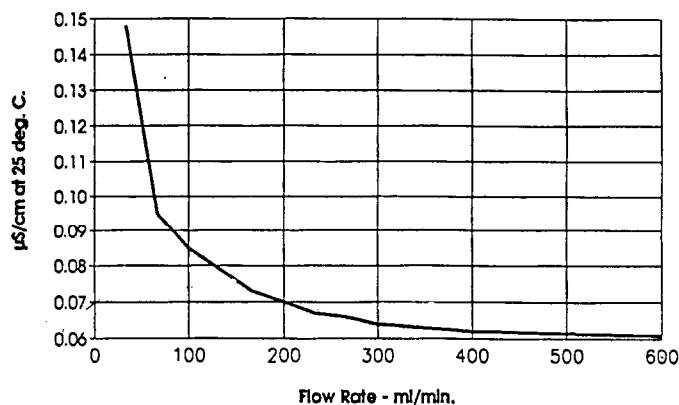


FIG. A2.1 Cation Resin Performance, Amount of Ionic Leaching Versus the Temperature for IWC Type TCD1 Resin in a 2-in. Diameter Tube

conductivity results have been reported with this lesser diameter column.<sup>10</sup>

### A3. TEMPERATURE COMPENSATION OF THE INSTRUMENT

A3.1 In the past, conductivity instruments without temperature compensation were used for this test method. This led to large errors due to fluctuations in temperature at the reboil chamber effluent and difficulty in accounting accurately for conductivity changes resulting from changes in atmospheric boiling water temperature. Due to the steep slope of pure water samples (5 %/°C) and the large temperature variations (often more than 5°C), large errors were introduced and not ac-

counted for. With a modern microprocessor instrument that measures the temperature very accurately and by using appropriate temperature compensation algorithms to correct the conductivity to the equivalent conductivity at 25°C, one can minimize the errors associated with the effluent temperature and the atmospheric pressure over the previous test method described in Test Method D 4519 – 85.

### A4. ORGANIC ACIDS

A4.1 It has been theorized that the final effluent results (degassed cation conductivity) for  $\text{Cl}^-$  and  $\text{SO}_4^{--}$  may be inaccurate if there are appreciable organic acids present (as acetic and formic).<sup>9</sup> However, footnote 9 revealed that the

presence of 100 µg/L TOC (as acetic acid) did not appreciably change the carbon dioxide and the degassed cation conductivity results. There is no other known data available on organic acid removal by this instrumental reboil procedure.

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