



Down under

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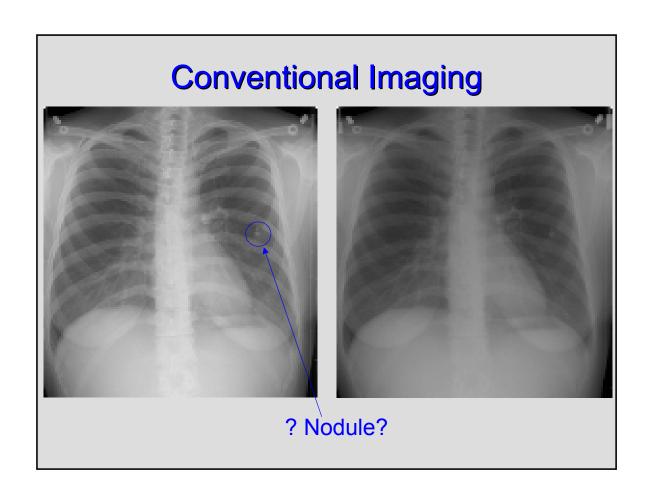
R.E. Alvarez, Ph.D. Aprend Technology, Mountain View, CA

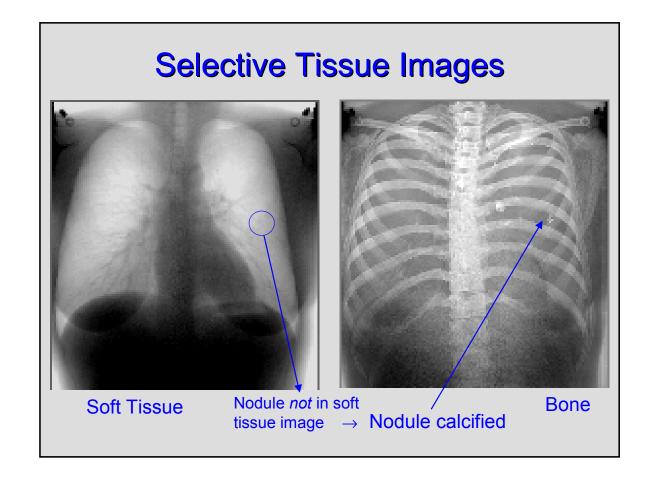
## **Dual-Energy Radiography**

- First proposed by Alvarez and Macovski, 1970's
- Initial clinical implementation by Fuji (early 1990's)
  - "Passive" sandwich PSP detector with Cu filter
- General Electric Medical Systems flat-panel detector with dual energy capability in 1999
- Research detector with switched voltage acquisition
  - "Active" sandwich PSP detector

## Selective tissue imaging

- Bone and soft tissue have energy dependent x-ray attenuation
- Acquisition of two x-ray images of widely different energy allows weighting and subtraction to eliminate one tissue
- Resultant images have higher diagnostic value:
  - Structured noise is removed (e.g., ribs)
  - Tissues are identified as calcified or non-calcified
  - Computer aided detection accuracy is improved





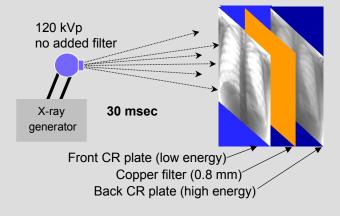
## **Methods**

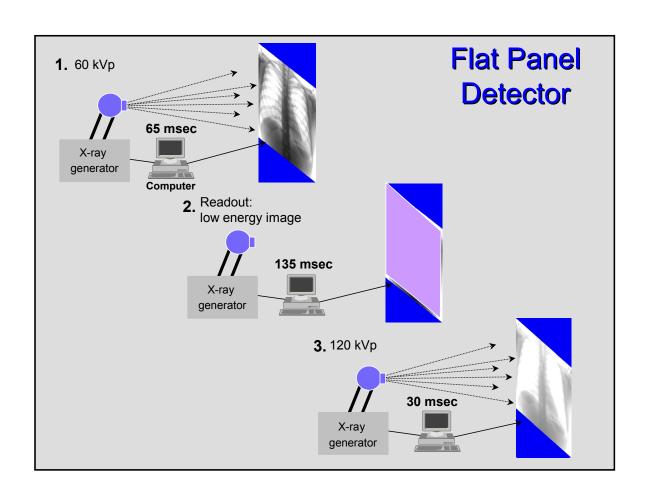
#### Systems comparisons:

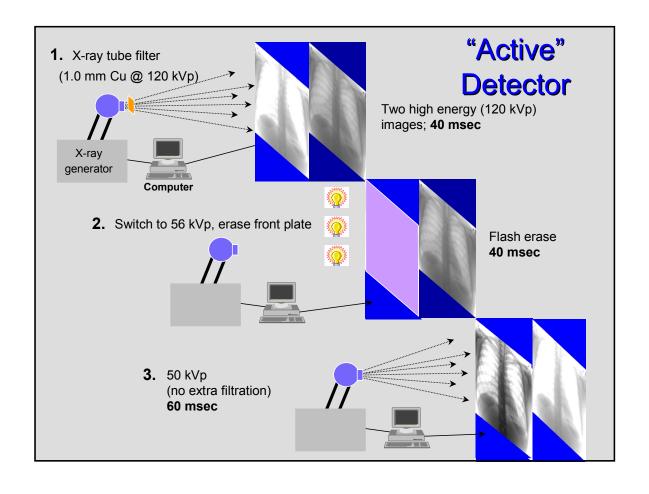
- 1. X-ray spectral quality
- 2. Noise in the cancelled image vs exposure
- 3. Amount of motion artifact.

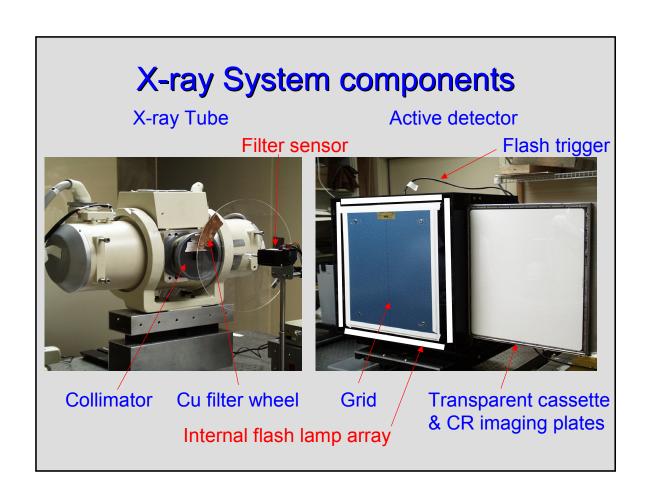
Quantitative measurement of dual energy system performance.

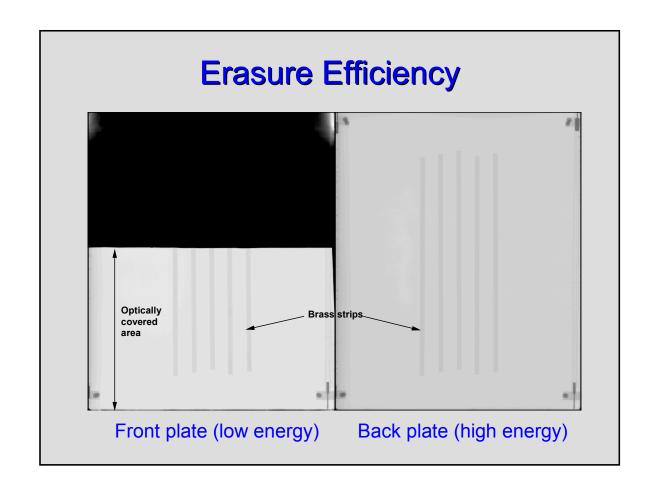
## Sandwich "Passive" Detector

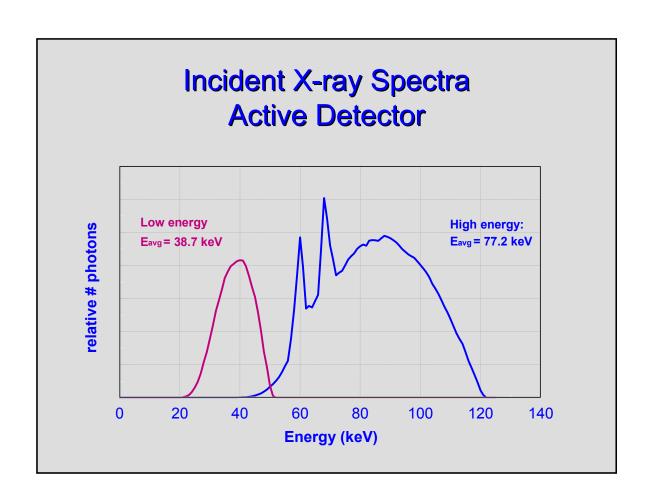


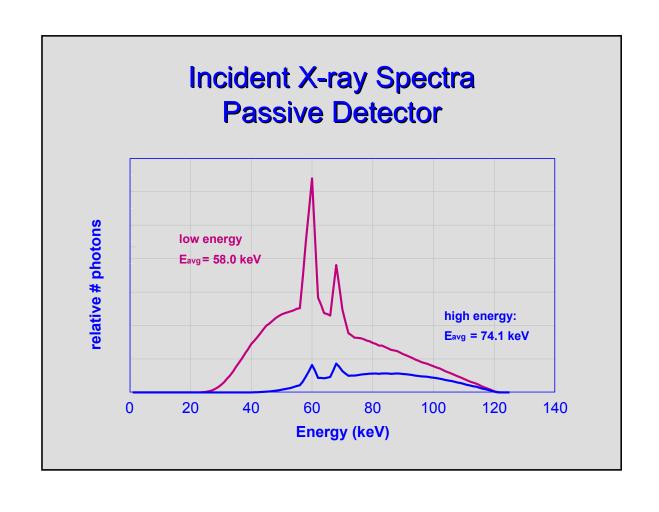


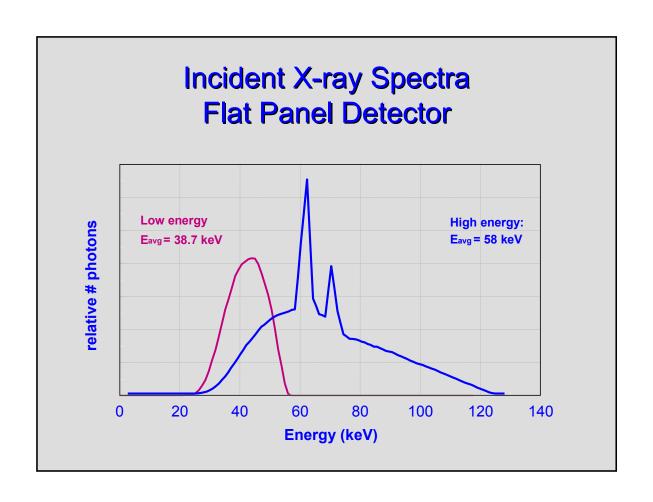


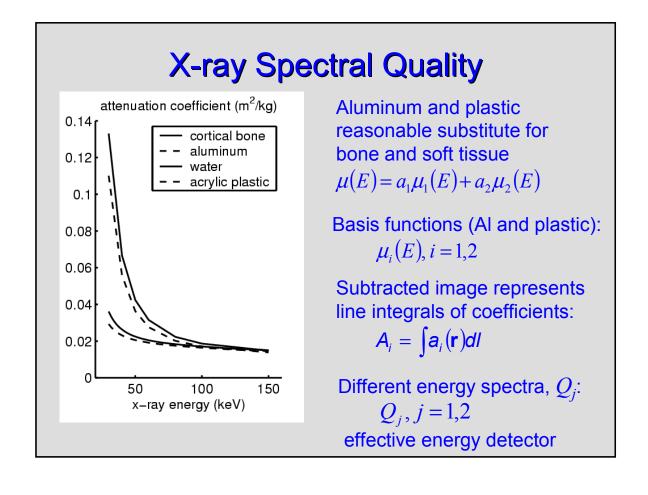












# Subtracted image variance

$$\sigma_{A_{1}}^{2} = \frac{\mu_{22}^{2}}{SNR_{1}^{2}} + \frac{\mu_{12}^{2}}{SNR_{2}^{2}} \qquad \sigma_{A_{2}}^{2} = \frac{\mu_{21}^{2}}{SNR_{1}^{2}} + \frac{\mu_{11}^{2}}{SNR_{2}^{2}} (\mu_{11}\mu_{22} - \mu_{12}\mu_{21})^{2}$$

 $SNR_i$  are computed from images with spectra 1 and 2

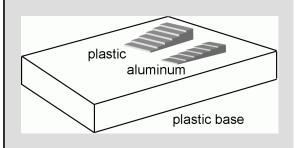
$$\mu_{ij} = -\frac{1}{Q_i} \frac{\partial Q_i}{\partial A_j} = -\frac{\partial \log(Q_i)}{\partial A_j} \quad (i, j = 1, 2)$$

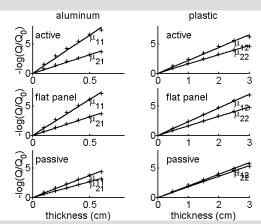
 $u_{i,j}$  are the slopes of the logarithms of image data versus thickness for each energy

$$Q_i = Q_{i0} e^{-A_1 \mu_1(E_i) - A_2 \mu_2(E_i)} \longrightarrow \mu_{ij} = \mu_j(E_i)$$

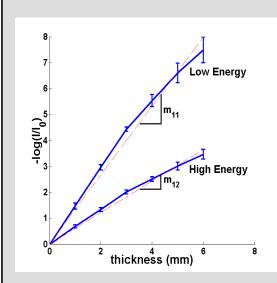
# Spectral quality factor

computed from: 
$$J^2 = (\mu_{11}\mu_{22} - \mu_{12}\mu_{21})^2$$

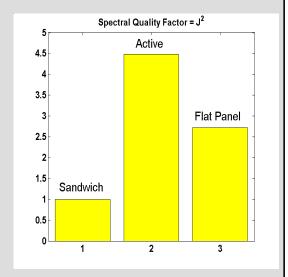




- Plastic wedge: 5-30 mm by 5 mm steps
- Aluminum wedge: 1-8 mm by 8 mm steps



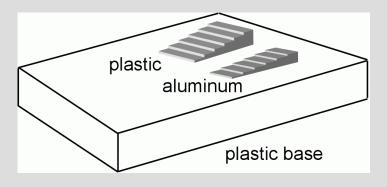
Effective linear attenuation coefficients for the low and high energy beams for bone (active detector)

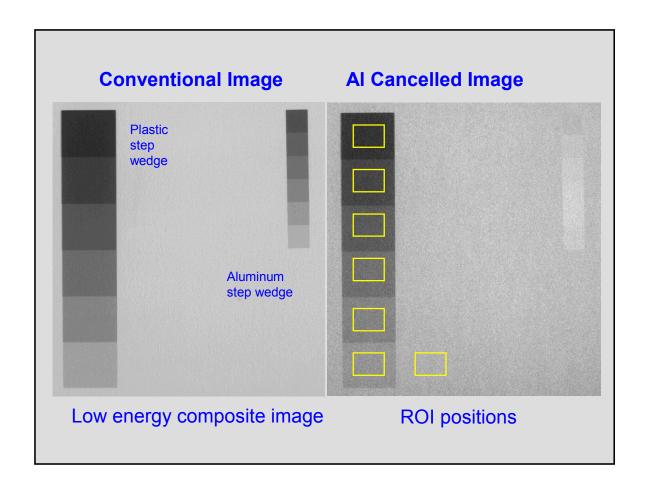


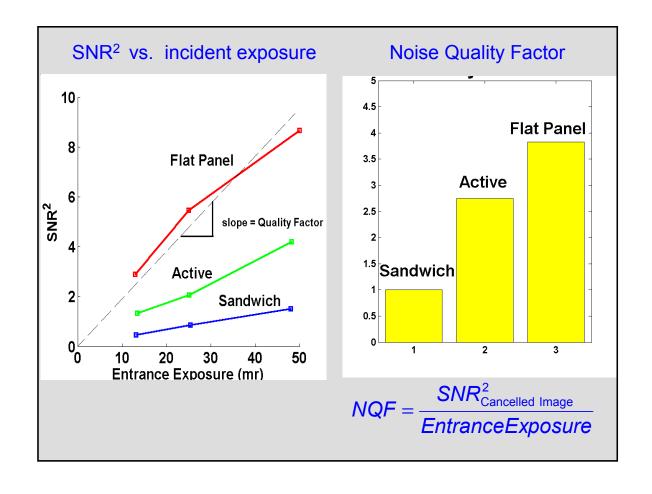
Relative "spectral quality" merit: Normalized to passive detector Larger value indicates lower noise

# Noise vs. Exposure

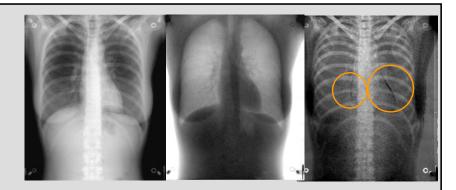
- Plastic wedge: 5-30 mm by 5 mm steps
  - Soft tissue image most important
- SNR: difference of adjacent steps / std dev
- 13, 25 and 50 mR entrance exposure



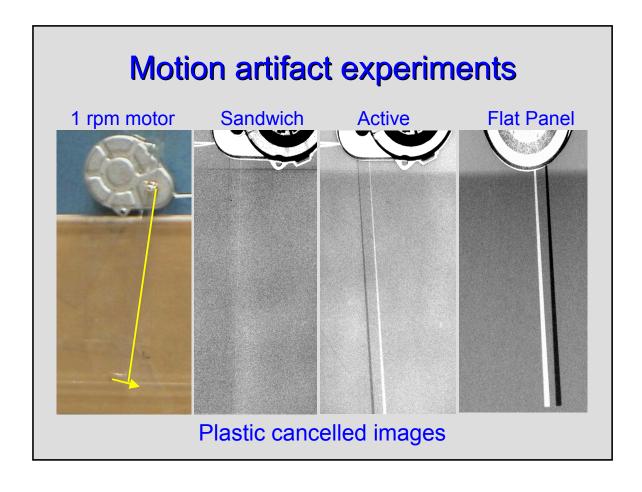


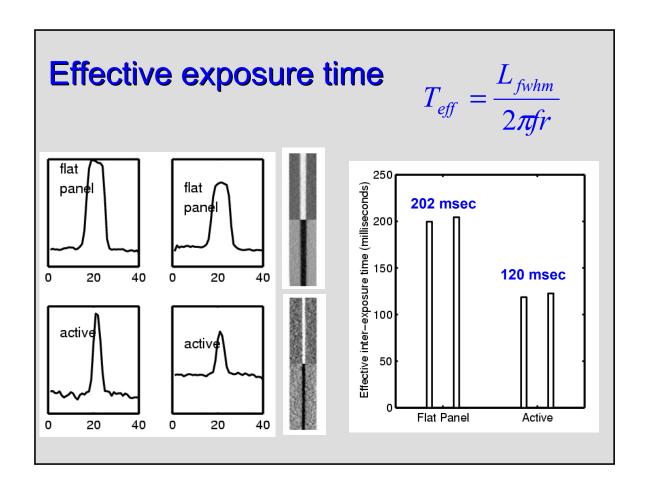


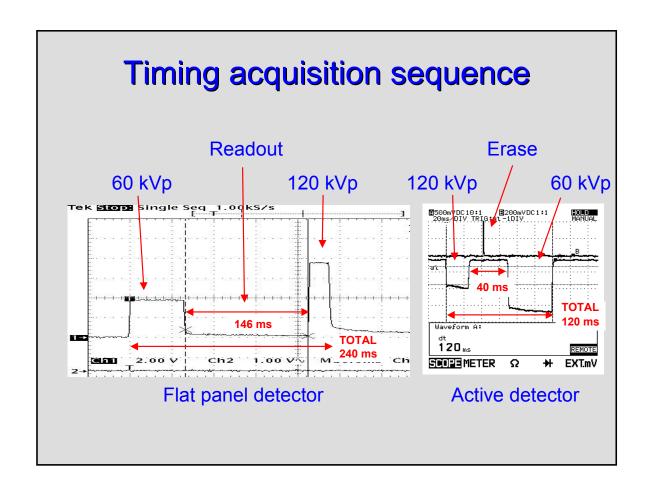
# Motion Artifact



- Involuntary and voluntary motion
- Expressed during energy subtraction
- Evaluation:
  - 1 rpm synchronous motor and plastic bar
  - Acquire typical image sequence
- Use soft-tissue decomposition







#### **Discussion**

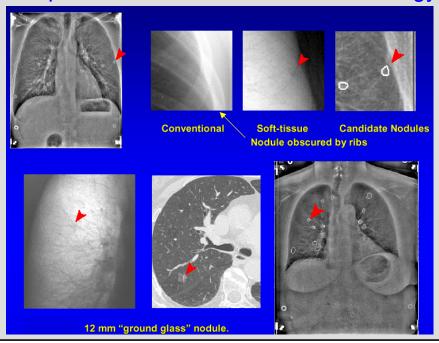
- Several factors must be considered in the design of a dual energy detector
  - Spectral quality issues and dose
  - Effective exposure time
  - Detective Quantum Efficiency of the system

### **Conclusions**

- Flat panel detector provides best noise quality factor (highest DQE)
  - 5.9 (Flat-panel) to 2.7 (Active) to 1 (Passive)
- Passive detector gives best motion immunity (simultaneous image acquisition)
  - 121 msec (Active) to 202 msec (Flat-panel)
- Active detector provides best spectral quality (switched voltage + filtration)
  - 4.5 (Active) to 2.7 (Flat-panel) to 1 (Passive)

#### **Future work**

Computer Aided Detection with dual energy



## **Conclusions**

- Each dual-energy system tested has weaknesses and strengths in terms of spectral quality, motion artifact reduction and image quality factor
- Design of future dual-energy systems should benefit from these investigations