# artemide ver.3.00

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User manual for artemide package, which evaluated TMDs and related cross-sections.

## Manual is updating.

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If you use the artemidev.1.??, please, quote [?]. If you use the artemidev.2.??, please, quote [?]. If you use the artemidev.2.06, please, quote [?].

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Stable Repository: https://github.com/VladimirovAlexey/artemide-public Dev Repository: https://github.com/VladimirovAlexey/artemide-development

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# Glossary

TMD = Transverse Momentum Dependent

PDF = Parton Distribution Function

FF = Fragmentation Function

NP = Non-perturbative

DY = Drell-Yan process

SIDIS = Semi-Inclusive Deep-Inelastic Scattering

**LO = Leading order** (in QCD perturbation theory)

NLO = Next-to-Leading order, (in QCD perturbation theory)

 $N^2LO = Next-to-Next-to-Leading order (etc), (in QCD perturbation theory)$ 

**LP** = **Leading power** (in power expansion of TMD factorization)

NLP = Next-to-Leading power (etc), (in power expansion of TMD factorization)

**KPC** = Kinematic power corrections

## I. GENERAL STRUCTURE AND USER INPUT OF ARTEMIDE

### A. General concept

The artemide is a package of Fortran modules for calculation in TMD factorization framework. It is has a modular structure, where each module is responsible for evaluation of some theory construct. For instance: a TMD distribution, a TMD evolution factor, cross-section. Each module produces a single function, which is a composite of integrals/products of lower-level functions. Thus, each level of operation can be used as is, in other programs. The highest-level task is the evaluation of cross-section within the TMD factorization theorem, including all needed integrations, and factors, i.e., such that it can be directly compared to the data. It also includes several tools for analysis of the obtained values, such as variation of scales, search for limiting parameters, etc. The theory structure of artemide is discussed in the next section. The dependency structure of modules is presented in fig.1.

Initially the artemide project was created for pure theoretical games. Since the beginning artemide appears to be successful also in the phenomenology, (and nowadays it is mostly used for it). Nonetheless, conceptually artemide is build as the theory playground, and will continue to be developed in this direction. That is why it architecture is not very optimal from the pure numerical point of view. In fact, there are several ways to optimize the code, melting together some modules and structures, but in this case artemide will lose it theoretical cleanness. Also artemide contains a lot of "unpractical" and rare options, and possibility to control each parameter. The positive side is the possibility to easily implement the new theory founding and check them, which is regularly done.

Wide spectrum of application of artemide code makes it difficult to create a convenient interface. Moreover, at the current stage of development, I prioritize the quality of computation, to the user interface. So, the interface is changing from version to version and often is not compatible with earlier versions. It slowly converges to the (almost) perfect shape – convenient for a wider community. If you have a particular task and not sure how to operate with artemide in this case, better write an e-mail.

The main rule (implemented in ver.2.00) each part encapsulates its theory parameters. It does not affect/change/interact with other modules, except requests for functions. A change of a parameter in a module can require a change in another module for consistency (however, I attempt to avoid such cases). Then each parameter must be changed individually in each module. However, the module aTMDe\_control does it automatically. So, I suggest to use aTMDe\_control to avoid possible inconsistencies.

**Historical note:** In versions before ver.2.00 this rule was not implemented. I tried to make connections between modules such that they automatically control consistency. However, at some moment (after inclusion of many hadrons and different types of cross-sections, and different orders) it became practically tough to keep such a system. So, I rearrange some modules (e.g. variation of  $c_4$  scale was in TMDs, while it related to definition of TMD it-self), removed connections between modules (no link for change of NP parameters, etc.), and introduce aTMDe\_control.

#### B. Organization of TMD factorized cross-section and its implementation in artemide

The ultimate goal of the artemide is to evaluate the observables in the TMD factorization framework, such as cross-section, asymmetries, etc. The general structure of the TMD factorized fully differential cross-section is

$$\frac{d\sigma}{dX} = d\sigma(q_T) = prefactor \times F, \tag{1.1}$$

where prefactor a process-dependent and experiment-dependent prefactor, and F is the reduced structure function. Example, for the photon induced Drell-Yan process one has for  $d\sigma/dq_T$ 

$$\begin{split} prefactor &= \frac{4\pi}{9sQ^2} |C_V(Q,\mu_H)|^2 \mathcal{P}(\text{cuts}), \\ F &= \int \frac{bdb}{2} J_0(bq_T) \sum_f |e_f|^2 F_f(x_A,b;\mu_H,\zeta_A) F_{\bar{f}}(x_B,b;\mu_H,\zeta_B), \end{split}$$

where  $\mathcal{P}(\text{cuts})$  is the weighting factor for fiducial cuts. For specific expression we refer in corresponding sections of this text. The structure function F is generally defined as

$$F(q_T, x_1, x_2; \mu, \zeta_1, \zeta_2) = \int \frac{bdb}{2} b^n J_n(bq_T) \sum_{ff'} z_{ff'} F_1^f(x_1, b; \mu, \zeta_1) F_2^{f'}(x_2, b; \mu, \zeta_2), \tag{1.2}$$



FIG. 1: Modules of artemide: purpose and dependencies

where  $F_{1,2}$  are TMD distributions (of any origin and polarization),  $z_{ff'}$  is the process dependent flavor mixing factor. The number n is also process dependent, e.g. for unpolarized observables it is n=0, while for SSA's it is n=1. Evaluation structure functions F is performed in the module TMDF. The evaluation of cross-sections is performed in the modules TMDX. The TMD distributions are evaluated by the module TMDs and related submodules.

In this way, the computation of TMD-factorized cross-section can be naturally split into ordered parts. Each part is evaluated in corresponding module of artemide. See example, of evaluation scheme in fig.2.

#### C. User defined functions and options

The artemide package has been created such that it allows to control each aspect of TMD factorization theorem. The TMD factorization has a large number of free, and "almost-free" parameters. It is a generally difficult task to provide a convenient interface for all these inputs. I do my best to make the interface convenient; however, some parts (e.g., setup of  $f_{NP}$ ) could not be simpler (at least within FORTRAN). Also, take care that artemide is evolving, and I try to keep back compatibility, but it is not the main option.

Starting from ver.2.0, artemide uses the text initialization file, which contains all required information on static parameters for a given setup. Throughout the text I call this file constants-file.

The user has to provide (or **use the default values**) the set of parameters, that control various aspects of evaluation. It includes PDF sets,  $f_{NP}$ , perturbative scales, parameters of numerics, non-QCD inputs, etc. There are three input sources for statical parameters.

General parameters: These are working parameters of artemide, such as amount of output, tolerance of integration routines, number of NP parameters, type of used evolution, griding parameters, triggering of particular contributions, etc. There are many of them, and typically they are unchanged. These are set in constants-file. Changes do not require recompilation.

External physics input: It includes the definition of  $\alpha_s$ , collinear PDFs, and other distributions. Twist-2 distributions are taken from LHAPDF [?], with routines defined in QCDinput module. For non-QCD parameters, e.g.  $\alpha_{QED}$ , SM parameters, there is a module EWinput. These are set in constants-file. Changes do not require recompilation.

**NP** model: The NP model consists in NP profiles of TMD distributions, NP model for large-b evolution, selection of scales  $\mu$ , etc. These parameter and functions enter nearly each low level module. The code for corresponding functions is provided by user, in appropriate files, which are collected in the subdirectory src/Model. The name of files are shown on diagram in colored blobs adjusted to the related module. **Changes require recompilation.** 

#### Comments:

- IMPORTANT: Each module is initialized individually via constants-file. So, each module can be used independently on the full package, given proper section of constants-file and submodules (see diagram). However, unless you understand what is going on, it is recommended to use aTMDe\_setup module for creation of constant-file, and aTMDe\_control module for proper control, initialization and operations of sub-modules.
- constants-file can be saved and used in future to reproduce setup. I try to keep compatibility between these files.
- constants-file is created and modified within aTMDe\_setup module. It could be also modified manually.
- NP functions are typically defined with a number of numeric parameters. The value of these parameters could be changed without restart (or recompilation) of the artemide by appropriate command. E.g. (call TMDs\_SetNPParameters(lambda)) on the level of TMDs module. See sections of corresponding modules.
- The number of parameters in the model for each module is set in constants-file.

- The directory /Model together with constants-file are convenient to keep as they are. They contain full information about particular evaluation, and thus results can be always reproduced (at least within the same version of artemide). I provide results of our extraction as such directories.
- Before ver.2.0, the interface was different and chaotic.

#### D. Installation

Download and unpack artemide. The actual code is in the /src. Check the makefile. You must provide options FC and FOPT, which are defined in the top of it. FC is the FORTRAN compiler, FOPT is additional options for compiler (e.g. linking to LHAPDF library).

There is no actual installation procedure, there is just compilation. If model, inputs, etc, are set correctly (typical problem is linking to LHAPDF, be sure that it is installed correctly), then make compiles the library. The result are object files (\*.o) (which are collected in /obj) and module files (\*.mod) (which are collected in /mod).

The test of current compilation could be performed by make test. It compiles program test.f90 from /Prog and run it (default test uses NPDF31\_nnlo\_as\_0118 set from LHAPDF, check that it is present in your LHAPDF installation). Program test runs some elementary code with minimum input. Output is shown later

Next, do your code, include appropriate modules of artemide, and compile it together with object-files (do not forget to add proper references to module files -I/mod). It should work! Linking could be done automatically if you call for make program TARGET=..., where ... is the name of the file with the code.

```
artemide.control: initialization done.
uTMDPDF: Grid is built ( 250 x 750) calc.time= 0.53s.
Calculating some values for cross-section one-by-one (DY around Z-boson peak, ATLAS 8TeV kinematics)
ptMax
                                 xSec
                                 3.0000000000000000
                                                             48.499041273610260
  3.0000000000000000
                                 5.0000000000000000
                                                             57.189916866533792
  5.0000000000000000
                                 7.0000000000000000
                                                             49.321931214709110
Now the same by list
It must be faster since you use OPENMP
          48.499041273610260
                                      57.189916866533792
                                                                   49.321931214709110
The programm evaluation took
                                 8.8279999999999994
                                                           sec. (CPU time)
                                 6.1287177319172770
   programm evaluation took
                                                                (wallclock time)
                                                           sec.
  you do not like so many terminal messages check the parameter outputlevel in constants file.
   forget to cite artemide [1706.01473]
```

## E. Python interface: harpy

For simplicity of data analysis the artemide has a python interface, called harpy (linking is made by f2py library). It is not possible to interfacing the artemide directly to python since artemide is made on fortran95. Artemide uses some features of Fortran95, such as interfaces, and indirect list declarations, which are alien to python. Also I have not found any convenient way to include several dependent Fortran modules in f2py (if you have suggestion just tell me). Therefore, I made a wrap module harpy.f90 that call some useful functions from artemide with simple declarations. It contains limited set of functions useful for phenomenology, and definitely cannot replace the FORTRAN interface for deep studies.

The compilation of harpy is slightly more complicated.

- 1. In the makefile check the variable Fpath (in the top part of the file). Put-in the full path for fortran compiler. It is needed by f2py.
- 2. (optional, does not work on Mac (?)) Run make harpy-signature. This will create an interface file (artemide.pyf for all functions in the harpy.f90. This file is already provided in the distribution, so if you did not change harpy.f90, you better skip this step. For some reason, it does not work on Mac.
- 3. Run make harpy. It compiles harpy.f90 with interface artemide.pyf linking to artemide. The result is artemide.so.

All files are in /harpy. Link it to python and work. There is also extra python harpy.py which has several most important function.

# F. Constants file and version compatibility

Constants files contains the list of work-flow parameters, such as physical constants, LHA grid names, numerical setup, etc. Each constants file has version number (does not coincide with the version of artemide).

On the module initialization the constants file is read, parameter are setup. Thus, the version of constants file should be adjusted to version of artemide if you run modules separately.

The workflow is deferent of the initialization of artemide is made by the artemide\_control. In this case, the artemide creates a copy of the initial constants-file (aTMDe\_temporary), and (in the case the versions do not match) fill the absent options by default parameter. After it the lower-level modules are initialized by aTMDe\_temporary. Naturally, in this case the versions should match (if not something is wrong with installation).

You can update the constants-file to an actual version by make update TARGET=...

where ... is the path to constants-file to be updated. The updated version will have all content of the original file, + new options setup by default setting.



 ${\ensuremath{\mbox{\scriptsize FIG.}}}\xspace\, 2:$  Evaluation of DY cross-section by  $\ensuremath{\mbox{\scriptsize artemide}}\xspace$ 

#### II. THEORY

#### This section is under construction.

In this section, the details of theoretical input coded in artemide is given. This section does not pretend to be a comprehensive review of TMD factorization. Only superficial details and references to particular realizations are given. For detailed and accurate description of the theory see specialized literature.

#### A. Definition of TMD distributions

TO BE WRITTEN. In this section, there will be operator definition of TMD distributions, and details on way the perturbative matching and NP-medeling is realized in artemide.

$$F_f(x,b) = \int_x^1 \frac{dz}{z} C_{f \leftarrow f'}(z, b^*, c_4 \mu_{\text{OPE}}) f_{f'}(\frac{z}{x}, c_4 \mu_{\text{OPE}}) f_{NP}^f(x, z, b, \{\lambda\}), \tag{2.1}$$

where  $f_f(x,\mu)$  is PDF of flavor f, C is the coefficient function in  $\zeta$ -prescription,  $f_{NP}$  is the non-perturbative function. The variable  $c_4$  is used to test the scale variation sensitivity of the TMD PDF. The NNLO coefficient functions used in the module were evaluated in [?] (please, cite it if use).

# PLAN TO ADD

- Definition of TMD distributions, operators, Lorenz structures, coordinate and momentum space.
- Perturbative matching, and  $\zeta$ -prescription
- NP-modeling

#### B. Evolution of TMD distributions

The detailed theory is given in the article [?]. The NLO rapidity anomalous dimension has been evaluated in [?]. The NNLO rapidity anomalous dimension has been evaluated in [?]?

The evolution of TMD distribution of any kind is given by the following pair of equations

$$\mu^2 \frac{d}{d\mu^2} F_{f \leftarrow h}(x, b; \mu, \zeta) = \frac{\gamma_F^f(\mu, \zeta)}{2} F_{f \leftarrow h}(x, b; \mu, \zeta), \tag{2.2}$$

$$\zeta \frac{d}{d\zeta} F_{f \leftarrow h}(x, b; \mu, \zeta) = -\mathcal{D}^f(\mu, b) F_{f \leftarrow h}(x, b; \mu, \zeta), \tag{2.3}$$

where  $F_{f\leftarrow h}$  is the TMD distribution (TMDPDF or TMDFF) of the parton f in hadron h. The function  $\gamma_F(\mu,\zeta)$  is called the TMD anomalous dimension and contains both single and double logarithms. The function  $\mathcal{D}(\mu,b)$  is called the rapidity anomalous dimension. TMD and rapidity anomalous dimensions have not unified notation in the literature, for comparison of notation see table I in ref.[?]. The only important quantum number for TMDs is the color representation the initiating parton, which is tied to the parton flavor, namely, quark (fundamental representation) or gluon (adjoint representation). However, as the TMD evolution does not mix the flavors and for simplicity of notation, we omit the flavor index f in this section, unless it is important.

The uniqueness of solution for the coupled system (2.2)-(2.3) is guaranteed by the integrability condition

$$\zeta \frac{d}{d\zeta} \gamma_F(\mu, \zeta) = -\mu \frac{d}{d\mu} \mathcal{D}(\mu, b), \tag{2.4}$$

The mutual dependence can be worked out explicitly due to the fact that the ultraviolet divergences of the TMD operator partially overlap with the rapidity divergences, (see e.g. [??]),

$$\zeta \frac{d}{d\zeta} \gamma_F(\mu, \zeta) = -\Gamma(\mu), \tag{2.5}$$

$$\mu \frac{d}{d\mu} \mathcal{D}(\mu, b) = \Gamma(\mu), \tag{2.6}$$

where  $\Gamma$  is the (light-like) cusp anomalous dimension. The equation (2.5) entirely fixes the logarithm dependence of the TMD anomalous dimension, which reads

$$\gamma_F(\mu,\zeta) = \Gamma(\mu) \ln\left(\frac{\mu^2}{\zeta}\right) - \gamma_V(\mu). \tag{2.7}$$

The anomalous dimension  $\gamma_V$  refers to the finite part of the renormalization of the vector form factor. In contrast, the equation (2.6) cannot fix the logarithmic part of  $\mathcal{D}$  entirely, but only order by order in perturbation theory, because the parameter  $\mu$  is also responsible for the running of the coupling constant.

The solution of eq. (2.2)-(2.3) can be written as

$$F(x,b;\mu_f,\zeta_f) = R[b;(\mu_f,\zeta_f) \to (\mu_i,\zeta_i)]F(x,b;\mu_i,\zeta_i), \tag{2.8}$$

where R is the TMD evolution factor. The general form of the evolution factor is

$$R[b; (\mu_f, \zeta_f) \to (\mu_i, \zeta_i)] = \exp\left[\int_P \left(\gamma_F(\mu, \zeta) \frac{d\mu}{\mu} - \mathcal{D}(\mu, b) \frac{d\zeta}{\zeta}\right)\right],\tag{2.9}$$

where  $(\mu_f, \zeta_f)$  and  $(\mu_i, \zeta_i)$  refer respectively to a final and initial set of scales. Here, the  $\int_P$  denotes the line integral along the path P in the  $(\mu, \zeta)$ -plane from the point  $(\mu_f, \zeta_f)$  to the point  $(\mu_i, \zeta_i)$ . The integration can be done on an arbitrary path P, and the solution is independent on it, thanks to the integrability condition eq. (2.4).

The TMD evolution factor R obeys the transitivity relation

$$R[b; (\mu_1, \zeta_1) \to (\mu_2, \zeta_2)] = R[b; (\mu_1, \zeta_1) \to (\mu_3, \zeta_3)] R[b; (\mu_3, \zeta_3) \to (\mu_2, \zeta_2)], \tag{2.10}$$

where  $(\mu_3, \zeta_3)$  is arbitrary point in  $(\mu, \zeta)$ -plane and the point inversion property

$$R[b; (\mu_1, \zeta_1) \to (\mu_2, \zeta_2)] = R^{-1}[b; (\mu_2, \zeta_2) \to (\mu_1, \zeta_1)].$$
 (2.11)

These equations are the cornerstones of the evolution mechanism, since they allow an universal definition of the non-perturbative distributions and the comparison of different experiments.

Different realizations of TMD evolution (if they are compatible with the factorization theorem) can be casted into selected of different paths of integration ADD PICTURE. All choices are equivalent, up to next-to-given order perturbative corrections, treatment of NP parts, and implementation of matching for TMD distributions. In artemide sevaral paths are presented, however, the matching of TMD distribution to collinear distributions is done in  $\zeta$ -prescription.

## 1. Equipotential lines & $\zeta$ -prescription

The  $\zeta$ -prescription is based on consideration of equipotential lines for evolution equations (2.2)-(2.3) (or lines of null-evolution, for description of evolution potential and its properties see [?]). An equipotential line  $\ell(b) = (\mu, \zeta)$  is determined by values of anomalous dimensions  $\gamma_F$  and  $\mathcal{D}$  at given b. The equation for line  $\ell(b)$  can be written in the form  $\zeta = \zeta(\mu, b)$ . In this parameterization the for function  $\zeta(\mu, b)$  is

$$-\Gamma(\mu)\ln\left(\frac{\zeta(\mu,b)}{\mu^2}\right) - \gamma_V(\mu) = 2\mathcal{D}(\mu,b)\frac{d\ln\zeta(\mu,b)}{d\ln\mu^2}.$$
 (2.12)

Among set of equipotential lines there is a single special equipotential line, which passes thorough the saddle point of the evolution field. The saddle point ( $\mu_{\text{saddle}}$ ,  $\zeta_{\text{saddle}}$ ) is defined by the equations

$$\mathcal{D}(\mu_{\text{saddle}}, b) = 0, \qquad \gamma_V(\mu_{\text{saddle}}, \zeta_{\text{saddle}}) = 0.$$
 (2.13)

Note, that the value of  $\mu_{\text{saddle}}$  depends on value of b, and on NP model for  $\mathcal{D}$ . In general it could be found only numerically. In typical models  $\mu_{\text{saddle}}$  is decreasing monotonous function of b. At certain large values of b it passes though the Landau pole, and its value could not be determined. This line we denote as

special equipotential line = 
$$\zeta_{\mu}(b)$$
,  $(\mu_{\text{saddle}}, \zeta_{\text{saddle}}) \in \zeta_{\mu}(b)$ . (2.14)

By definition a TMD distribution is the same for all points of equipotential line. In particular it means that there is no dependence on variable  $\mu$ , since a variation of  $\mu$  is compensated by appropriate variation in  $\zeta(\mu)$ .

Important note: The presence of NP part in  $\mathcal{D}$  makes determination of special line involved. We distinguish three "realizations" of the special line. The exact which is determined by equation (2.12) and boundary conditions (2.14) (its values can be calculated by function zetaSL). The perturbative realization where NP part is dropped (its values can be calculated by functions zetaMUperp and zetaMUresum). And user-defined which is given by user in TMDR\_model.f90 file.

#### 2. Exact solution for evolution to special line

There is a possibility to define the evolution to the optimal equipotential line in perturbation theory for any NP input, at any b. Instead of problematic variable b one uses the function  $\mathcal{D}(\mu, b)$  as a variable. With the ansatz  $\zeta_{\mu} = \mu^2 \exp(-g(\mu, b))$  we rewrite equation (2.12) as

$$2\mathcal{D}(\mu, b) \left( 1 - \frac{dg(\mu, b)}{d \ln \mu^2} \right) - \Gamma(\mu)g(\mu, b) + \gamma_V(\mu) = 0.$$
 (2.15)

or

$$2\mathcal{D}\left(1 - \frac{\partial g(\mu, \mathcal{D})}{\partial \ln \mu^2} - \frac{\Gamma(\mu)}{2}g'(\mu, \mathcal{D})\right) - \Gamma(\mu)g(\mu, \mathcal{D}) + \gamma_V(\mu) = 0, \tag{2.16}$$

where  $g' = dg/d\mathcal{D}$ . The boundary condition (2.13) is transformed to the condition that g is regular at  $\mathcal{D} \to 0$ . Note, that this condition does not depends on b and thus determines the function unambiguously at any b, even if saddle point is behind the Landau-pole values.

The equation (2.16) is simplified further with introduction of new function  $\tilde{g}(a_s, \mathcal{D}) = \mathcal{D}g(\mu, \mathcal{D})$ :

$$2\mathcal{D} + 2\beta(a_s)\frac{\partial \tilde{g}(a_s, \mathcal{D})}{\partial a_s} - \Gamma(a_s)\tilde{g}'(a_s, \mathcal{D}) + \gamma_V(a_s) = 0, \tag{2.17}$$

with boundary condition  $\tilde{g}(a_s,0)=0$ . The general solution reads

$$\tilde{g}(a_s, \mathcal{D}) = -\frac{\mathcal{D}}{2} \int^{a_s} \frac{da}{\beta(a)} - \int^{a_s} da \frac{\gamma_V(a)}{2\beta(a)} - \int^{a_s} da \frac{\Gamma(a)}{2\beta(a)} \int^a \frac{da'}{\beta(a')} + \Phi\left(\mathcal{D} + \int^{a_s} da \frac{\Gamma(a)}{2\beta(a)}\right), \tag{2.18}$$

where  $\Phi$  is a solution of the following transcendental equation

$$\Phi\left(\int^{a_s} da \frac{\Gamma(a)}{2\beta(a)}\right) = \int^{a_s} da \frac{\gamma_V(a)}{2\beta(a)} + \int^{a_s} da \frac{\Gamma(a)}{2\beta(a)} \int^a \frac{da'}{\beta(a')}.$$
 (2.19)

Unfortunately, this equation is practically impossible to solve for higher then NNLL anomalous dimensions. It is straightforward to show that at large- $\mathcal{D}$  the solution is

$$\tilde{g}(a_s, \mathcal{D} \to \infty) = \mathcal{D} \int^{a_s} \frac{-1}{\beta(a)} da + \dots$$
 (2.20)

Note that asymptotic is defined up to a constant.

The function g is convenient to derive as perturbative expansion

$$g(\mu, \mathcal{D}) = \frac{1}{a_s(\mu)} \sum_{n=0}^{\infty} a_s^n(\mu) g_n(\mathcal{D}).$$
(2.21)

We have found

$$g_0 = \frac{e^{-p} + p - 1}{\beta_0 p}, \tag{2.22}$$

$$g_1 = g_0 \left( \frac{\beta_1}{\beta_0} - \frac{\Gamma_1}{\Gamma_0} \right) + \frac{\gamma_1}{\gamma_0} - \frac{\beta_1}{2\beta_0^2} p, \tag{2.23}$$

$$g_2 = g_0 \frac{\beta_2 \Gamma_0 - \beta_1 \Gamma_1}{\beta_0 \Gamma_0} + \frac{\cosh p - 1}{p} \frac{\beta_0 \Gamma_1^2 - \beta_0 \Gamma_0 \Gamma_2 + \beta_1 \Gamma_0 \Gamma_1 - \beta_2 \Gamma_0}{\beta_0^2 \Gamma_0^2} + \frac{e^p - 1}{p} \frac{\Gamma_0 \gamma_2 - \Gamma_1 \gamma_1}{\Gamma_0^2}, \tag{2.24}$$

where  $p = 2\beta_0 \mathcal{D}/\Gamma_0$ .

There is an additional problem that appears at NNNLO, namely, the coefficient  $g_3$  is negative. It results to a singular solution for  $\zeta_{\mu}$  at large- $\mathcal{D}$ . It indicates that the series has bad convergence properties. This problems occur for very large  $\mathcal{D} > 0.9 - 1.1$ . Currently to by-pass this problem the 4-loop exact  $\zeta$ -line is not used (3-loop expression is used instead). For small- $\mathcal{D}$  the difference is negligible.

The solution for the evolution from  $(\mu, \zeta) \to (\mu, \zeta_{\mu})$  is

$$R[b;(\mu,\zeta)\to(\mu,\zeta_{\mu})] = \exp\left(-\mathcal{D}(\mu)\ln\left(\frac{\zeta}{\mu^2}\right) - \mathcal{D}(\mu,b)g(\mu,\mathcal{D})\right). \tag{2.25}$$

## C. Expressions for evolution functions in artemide

Here are the expression for various evolution functions how they are written in artemide in TMDR-module.

1. Fixed order RAD:

 $\begin{array}{ll} \texttt{Dpert(mu,bT,f):} & \text{returns } \mathcal{D}^f(b,\mu) \text{ [real(dp)]} \\ \texttt{mu, bT [real(dp)] scales in GeV, f[integer] flavour.} \\ & \text{Order is controlled by orderD } (=n_{\max}). \text{ At orderD=0, Dpert=0.} \end{array}$ 

Solving (2.6) we get

$$\mathcal{D}(b,\mu) = \sum_{n=1}^{\infty} a_s^n \sum_{k=0}^n \mathbf{L}_{\mu}^k d^{(n,k)},$$
 (2.26)

where  $d^{(n,0)}$  are obtained by calculation. The coefficients  $d^{(n,k)}$  are

$$\begin{split} d^{(1,1)} &= \frac{\Gamma_0}{2}, \\ d^{(2,2)} &= \frac{\Gamma_0 \beta_0}{4}, \\ d^{(2,1)} &= \frac{\Gamma_1}{2}, \\ d^{(3,3)} &= \frac{\Gamma_0 \beta_0^2}{6}, \\ d^{(3,2)} &= \frac{\Gamma_0 \beta_1 + 2\Gamma_1 \beta_0}{4}, \\ d^{(3,1)} &= \frac{\Gamma_2 + 4\beta_0 d^{(2,0)}}{2}, \end{split}$$

where flavor on both sides is the same.

2. Resummed RAD:

 $\begin{array}{ll} \mathtt{Dresum}(\mathtt{mu},\mathtt{bT,f})\colon & \mathtt{returns}\ \mathcal{D}^f_{\mathtt{resum}}(b,\mu)\ [\mathtt{real}(\mathtt{dp})] \\ \mathtt{mu},\ \mathtt{bT}\ [\mathtt{real}(\mathtt{dp})]\ \mathtt{scales}\ \mathtt{in}\ \mathtt{GeV},\ \mathtt{f}[\mathtt{integer}]\ \mathtt{flavour}. \\ \\ \mathtt{Order}\ \mathtt{is}\ \mathtt{controlled}\ \mathtt{by}\ \mathtt{orderDresum}\ (=n_{\max}).\ \mathtt{At}\ \mathtt{orderDresum}=0,\ \mathtt{Dresum}=-\frac{\Gamma_0}{2\beta_0}\ln(1-X). \end{array}$ 

One can resumm the logarithms in this expression and write it as

$$\mathcal{D}_{\text{resum}} = -\frac{\Gamma_0}{2\beta_0} \Big[ \ln(1-X) + \sum_{n=1}^{\infty} \frac{a_s^n}{(1-X)^n} \sum_{k,l=0}^n X^k \ln^l(1-X) d_r^{(n,k,l)} \Big], \qquad X = \beta_0 a_s \mathbf{L}_{\mu}, \tag{2.27}$$

the coefficients  $d_r$  are

$$\begin{split} d_r^{(1,0,1)} &= B_1, & d_r^{(1,1,0)} = B_1 - G_1, & d_r^{(1,0,0)} = 0, \\ d_r^{(2,0,2)} &= -\frac{B_1^2}{2}, & d_r^{(2,0,1)} = B_1 G_1, \\ d_r^{(2,2,0)} &= \frac{1}{2} \left( G_2 - B_1 G_1 - B_2 + B_1^2 \right) & d_r^{(2,1,0)} = B_1 G_1 - G_2, \\ d_r^{(2,0,0)} &= -2 \frac{d^{(2,0)} \beta_0}{\Gamma_0}, & d_r^{(2,2,2)} = d_r^{(2,1,1)} = 0, \end{split}$$

$$\begin{split} d_r^{(3,0,3)} &= \frac{B_1^3}{3}, \qquad d_r^{(3,0,2)} = -\frac{B_1^3}{2} - B_1^2 G_1, \qquad d_r^{(3,0,1)} = B_1 G_2 + 4 \frac{d^{(2,0)} \beta_1}{\Gamma_0}, \\ d_r^{(3,1,1)} &= B_1 B_2 - B_1^3, \qquad \text{other } d_r^{(3,k>0,l>0)} = 0, \\ d_r^{(3,3,0)} &= \frac{1}{3} \left( B_1^3 - 2 B_1 B_2 + B_3 - B_1^2 G_1 + B_2 G_1 + B_1 G_2 - G_3 \right), \\ d_r^{(3,2,0)} &= -\frac{1}{2} B_1^3 + B_1 B_2 - \frac{B_3}{2} + B_1^2 G_1 - B_2 G_1 - B_1 G_2 + G_3, \\ d_r^{(3,1,0)} &= B_1 G_2 - G_3, \qquad d_r^{(3,0,0)} = -2 \frac{d^{(3,0)} \beta_0}{\Gamma_0} \end{split}$$

Here,

$$G_i = \frac{\Gamma_i}{\Gamma_0}, \qquad B_i = \frac{\beta_i}{\beta_0}$$

3. Fixed order  $\zeta$ -line:

 $\begin{array}{ll} \mathtt{zetaMUpert(mu,bT,f):} & \mathtt{returns} \ \zeta^f(b,\mu) \ [\mathtt{real(dp)}] \\ \mathtt{mu, bT} \ [\mathtt{real(dp)}] \ \mathtt{scales} \ \mathtt{in} \ \mathtt{GeV, f[integer]} \ \mathtt{flavour.} \\ \mathtt{Order} \ \mathtt{is} \ \mathtt{controlled} \ \mathtt{by} \ \mathtt{orderZETA} \ (=n_{\max}). \ \mathtt{At} \ \mathtt{orderZETAi0, zetaMUpert=1.} \\ \end{array}$ 

The solution of (2.12) in PT can be written as

$$\zeta^f(b,\mu) = \frac{C_0 \mu}{b} e^{-v}, \qquad v = \sum_{n=0}^{\infty} a_s^n \sum_{k=0}^{n+1} \mathbf{L}_{\mu} v^{(n,k)}. \tag{2.28}$$

The perturbative boundary condition is that v is regular at  $L \to 0$ . The first coefficients are

$$\begin{split} v^{(0,0)} &= g_1, & v^{(0,1)} &= 0, \\ v^{(1,2)} &= \frac{\beta_0}{12}, & v^{(1,1)} &= 0, & v^{(1,0)} &= \mathbf{d}^{(2,0)} - g_1 G_1 + g_2, \\ v^{(2,3)} &= \frac{\beta_0^2}{24}, & v^{(2,2)} &= \frac{\beta_0}{12} \left( B_1 + G_1 \right), & v^{(2,1)} &= \frac{\beta_0}{2} \left( \frac{8}{3} \mathbf{d}^{(2,0)} - g_1 G_1 + g_2 \right), \\ v^{(2,0)} &= \mathbf{d}^{(3,0)} - \mathbf{d}^{(2,0)} G_1 + g_1 G_1^2 - g_2 G_1 - g_1 G_2 + g_3, \end{split}$$

here

$$\mathbf{d}^{(n,k)} = \frac{d^{(n,k)}}{\Gamma_0}, \qquad g_i = \frac{\gamma_V^{(i)}}{\Gamma_0}, \qquad G_i = \frac{\Gamma_i}{\Gamma_0}, \qquad B_i = \frac{\beta_i}{\beta_0}.$$

4. Resummed  $\zeta$ -line:

 $\begin{array}{ll} \texttt{zetaMUresum(mu,bT,f):} & \texttt{returns} \ \zeta^f_{\text{resum}}(b,\mu) \ [\texttt{real(dp)}] \\ \texttt{mu, bT} \ [\texttt{real(dp)}] \ \texttt{scales} \ \texttt{in GeV, f[integer]} \ \texttt{flavour.} \\ \textbf{Order is controlled by orderZETA.} \\ \end{array}$ 

REMOVED in v.2.03. TO BE REINTRODUCED LATER.

5. Exact  $\zeta$ -line:

zetaSL(mu,bT,f): returns  $\zeta_{\rm exact}^f(b,\mu)$  [real(dp)] mu, bT [real(dp)] scales in GeV, f[integer] flavour. Order is controlled by orderZETA. At orderZETAjO, zetaMUpert=1. Currently at the order =3, the result is NNLO. Due to instability of N³LO at very large  $\mathcal{D}$ .

The solution for  $\zeta$  can be written as

$$\zeta(b,\mu) = \mu^2 \exp\left(-g(a_s, \mathcal{D})\right). \tag{2.29}$$

The function g is convinient to present as

$$g(a_s, \mathcal{D}) = \frac{\Omega(a_s, p)}{a_s \beta_0}, \qquad p = \frac{2\beta_0 \mathcal{D}}{\Gamma_0},$$
 (2.30)

where  $\Omega$  is convenient to present in the following form

$$\Omega(a_s, p) = \sum_{n=0}^{\infty} a_s^n \Omega_n(p), \qquad (2.31)$$

with

$$\begin{split} &\Omega_0 = z_1, \qquad \Omega_1 = (B_1 - G_1)z_1 + g_1 - \frac{B_1}{2}p, \\ &\Omega_2 = \frac{B_2 - B_1G_1 + G_1^2 - G_2}{2}z_1 + \frac{-B_2 + B_1G_1 + G_1^2 - G_2 - 2G_1g_1 + 2g_2}{2}z_{-1} + g_2 - g_1G_1 \\ &\Omega_3 = \frac{2B_3 + B_1^2G_1 - B_2G_1 - G_1^3 + 3G_1G_2 - B_1B_2 - B_1G_2 - 2G_3}{6}z_1 \\ &+ \frac{G_1 - B_1}{2} \left( -B_2 + B_1G_1 + G_1^2 - G_2 - 2G_1g_1 + 2g_2 \right) z_{-1} \\ &\left[ \frac{-B_3 + B_1^2G_1 + 2B_2G_1 - 4G_1^3 + 6G_1G_2 - B_1B_2 + B_1G_2 - 2G_3}{12} + (2G_1 - B_1) \frac{G_1g_1 - g_2}{2} - \frac{G_2g_1 - g_3}{2} \right] z_{-2} \\ &+ G_1^2g_1 - G_2g_1 - G_1g_2 + g_3. \end{split}$$

Here

$$B_i = \frac{\beta_i}{\beta_0}, \qquad G_i = \frac{\Gamma_i}{\Gamma_0}, \qquad g_i = \gamma^{(i)} \frac{\beta_0}{\Gamma_0}, \qquad z_n = \frac{e^{-np} - 1 + np}{p}.$$
 (2.32)

Note that  $\lim_{p\to 0} z_n \sim n^2 p/2$ .

# III. ATMDE\_SETUP MODULE

The module aTMDe\_setup creates and modifies the constants-file. It is a stand-alone module, which does not require the rest modules (however, it is called by aTMDe\_control).

List of commands optional parameters are shown in blue.

Command	Sec.	Short description
artemide_Setup_Default(order)	III A	The main command which initializes variables by default values corresponded to a particular order.
<pre>artemide_Setup_fromFile(file,prefix,order)</pre>	III A	The main command which initialize variables by pre-saved values in file. prefix is path to the file. order is the order of default version of parameters (used if versions of files are incompatible).
<pre>CreateConstantsFile(file,prefix)</pre>	-	Write a new constants-file according to current modification.
CheckConstantsFile(file,prefix)	-	Function (logical). Compare the version of constants-file. Returns .true. if version of file $\xi$ = version of artemide, .false. otherwise.
artemide_include(arg1,arg2,,arg10)	-	Include the modules into the initialization procedure. arg is (string) with the module name.
Set_outputLevel(level,numMessages)	-	Set the level of artemide-messages to (int)level. 0= only critical, 1=+warnings, 2=+module evaluation information, 3=+ details. Default=2. (integer)numMessages set number of non-critical Warnings of the same type to show (prevent spaming by same messages).
Set_uPDF(hadron,setName,replica)	VA	Assign the hadron for uPDF with number hadron(int) a PDF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0).
Set_uFF(hadron,setName,replica)	VA	Assign the hadron for uFF with number hadron(int) a FF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0).
Set_lpPDF(hadron,setName,replica)	VA	Assign the hadron for (unpolarized)PDF that is used by lpTMDPDF with number hadron(int) a PDF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0).
Set_quarkMasses(mC,mB,mT)	-	Set values for pole quark masses, charm, bottom and top (real), which determine $N_f$ -thresholds. Default mC=1.4, mB=4.75, mT=173.
Set_EWparameters( alphaInv,massZ,massW,widthZ,widthW, massH,widthH,vevHIGGS, sin2ThetaW,UD,US,UB,CD,CS,CB)	-	Set parameters of electro-weak theory. alphaInv=inverse $\alpha_{QED}(M_Z)$ . UD,US,UB,CD,CS,CB are elements of CKM matrix. Masses and widths are in GeV.
Set_TMDR_order(order)	??	Set the perturbative order of anomalous dimensions used for evolution. order=string(8)
Set_TMDR_evolutionType(num)	??	Set the type of evolution solution used to (int)num.
Set_TMDR_lengthNParray(num)	??	Set the length of $\lambda_{NP}$ for $\mathcal{D}_{NP}$ to num(int).
Set_uTMDPDF(hadron,setName,replica)	V A ??	Assign the hadron for uTMDPDF with number hadron(int) a PDF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0). Automatically calls for Set_uPDF.
Set_uTMDPDF_order(order)	??	Set the perturbative order of convolution. order=string(8)
Set_uTMDPDF_gridEvaluation (prepareGrid,includeGluon)	??	Set the trigger to prepare the grid, and to include the gluons in the grid (default=.false.). Both logical.
Set_uTMDPDF_lengthNParray(num)	??	Set the length of $\lambda_{NP}$ for uTMDPDF NP model to num(int).
Set_uTMDFF(hadron,setName,replica)	V A ??	Assign the hadron for uTMDFF with number hadron(int) a FF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0). Automatically calls for Set_uFF.

Set_uTMDFF_order(order)	??	Set the perturbative order of convolution. order=string(8)
Set_uTMDFF_gridEvaluation (prepareGrid,includeGluon)	??	Set the trigger to prepare the grid, and to include the gluons in the grid (default=.false.). Both logical.
Set_uTMDFF_lengthNParray(num)	??	Set the length of $\lambda_{NP}$ for uTMDFF NP model to num(int).
Set_lpTMDPDF(hadron,setName,replica)	V A ??	Assign the hadron for lpTMDPDF with number hadron(int) a PDF set setName(string) in LHAPDF library. It will be initialized in with replica replica(int)(default =0). Automatically calls for Set_lpPDF.
Set_lpTMDPDF_order(order)	??	Set the perturbative order of convolution. order=string(8)
Set_lpTMDPDF_gridEvaluation (prepareGrid,includeGluon)	??	Set the trigger to prepare the grid, and to include the gluons in the grid (default=.true.). Both logical.
Set_lpTMDPDF_lengthNParray(num)	??	Set the length of $\lambda_{NP}$ for lpTMDPDF NP model to num(int).

# A. aTMDe\_Setup

# TO BE WRITTEN



 $FIG.\ 3:\ Scheme\ of\ creation\ and\ modification\ of\ {\tt constants-file}\ by\ {\tt aTMDe\_setup}.$ 

## IV. ATMDE\_CONTROL MODULE

The module aTMDe\_setup is used to coordinate the operation of other modules. It does not bring any new features, just operates other modules in proper order. It is only for convenience.

List of commands optional parameters are shown in blue.

Command	Sec.	Short description
artemide_Initialize(file,prefix,order)	III A	The command which initialize modules according to constants-file created by artemide_Setup_fromFile(file,prefix,order) .
artemide_ShowStatistics()		Shows some information.
artemide_SetNPparameters(lambdaNP)	IV A	Receive a (real*8)list of NP parameters, split it according to current setup and passes NP parameters to appropriate modules. Reset modules counters.
artemide_SetNPparameters_TMDR(lambdaNP)	IV A	Reset NP parameters of TMDR-module by (real*8) list lambdaNP. Reset modules counters.
artemide_SetNPparameters_uTMDPDF(lambdaNP)	IV A	Reset NP parameters of uTMDPDF-module by (real*8) list lambdaNP. Reset modules counters.
artemide_SetNPparameters_uTMDFF(lambdaNP)	IV A	Reset NP parameters of uTMDFF-module by (real*8) list lambdaNP. Reset modules counters.
artemide_SetNPparameters_lpTMDFF(lambdaNP)	IV A	Reset NP parameters of lpTMDFF-module by (real*8) list lambdaNP. Reset modules counters.
artemide_SetReplica_TMDR(num)	IV A	Reset NP parameters of TMDR-module by values corresponding to replica (int)num. Reset modules counters.
artemide_SetReplica_uTMDPDF(num)	IV A	Reset NP parameters of uTMDPDF-module by values corresponding to replica (int)num. Reset modules counters.
artemide_SetReplica_uTMDFF(num)	IV A	Reset NP parameters of uTMDFF-module by values corresponding to replica (int)num. Reset modules counters.
artemide_SetReplica_lpTMDPDF(num)	IV A	Reset NP parameters of lpTMDPDF-module by values corresponding to replica (int)num. Reset modules counters.
artemide_SetScaleVariations(c1,c2,c3,c4)	-	Change the value of scale-variation constants $c_1 - c_4$ .
artemide_GetReplicaFromFile(file,rep,array)	_	Read the .rep file (path is file), and search for the replica (int)rep. Return the (real*8,allocatable)array of NP parameters. This command can work without initialization of artemide-control, in this case, no check of consistency is performed and warning raised.
artemide_NumOfReplicasInFile(file)	-	Read the .rep file (path is file), and return the number of replicas saved in it.

# A. Passing non-perturbative parameters

The important part of the initialization is the number of NP parameters for each TMD distributions under consideration. Each TMD-evaluating module (say, uTMDPDF, uTMDFF, etc.) requires  $n_i$  number of parameters. The numbers are specified in constants-file. The number must be greater then zero  $n_i > 0$  for any used module, i.e.  $f_{NP}$  is at least 1-parametric (if it is not so, just do not use the parameter in the definition of  $f_{NP}$ , but keep  $n_i > 0$ ). These numbers are read during the initialization procedure, and allocate the memory.

The set of particular values of these parameters can be done by several ways.

**Option I:** Set all values in a single call call artemide\_SetNPParameters(lambda) where

 $\{\lambda_i\}$  real\*8(1: $\sum_i n_i$ ) The set of parameters which define the non-perturbative functions  $f_{NP}$  within modules. It is split into parts and send to corresponding modules. I.e. lambda(1: $n_0$ )  $\rightarrow$ uTMDR, lambda( $n_0 + 1:n_0 + n_1$ )  $\rightarrow$ uTMDPDF, lambda( $n_0 + n_1 + 1:n_0 + n_1 + n_2$ )  $\rightarrow$ uTMDFF (fixed order).

Option II: Set value for particular function. For it call artemide\_SetNPparameters\_???(lambdaNP), where ??? is module name, e.g.

artemide\_SetNPparameters\_uTMDPDF(lambdaNP) will set parameters for unpolarized TMDPDF.

Option III: You can use presaved values of  $\lambda_{NP}$  for a given function. They are provided by model file (if provided). To set NP-input given by integer num, call artemide\_SetReplica\_???(num), where ??? is module name, e.g. artemide\_SetReplica\_uTMDPDF(num)

will set parameters for unpolarized TMDPDF.

# V. QCDINPUT MODULE

The module QCDinput gives an interface to external function provided by the user, such as PDF, FF, values of alpha-strong. It is completely user defined. In particular, in the default version it is linked to LHAPDF library [?].

List of available commands optional parameters are shown in blue.

Command	Description
QCDinput_Initialize(file,prefix)	Subroutine to initialize anything what is needed. (string) file is the name of constants-file, which contains initialization information. (string)prefix is appended to file if provided.
As(Q)	Returns the (real*8) value of $\alpha_s(Q)/(4\pi)$ . $Q$ is (real*8).
xPDF(x,Q,hadron)	Returns the (real*8(-5:5)) value of $xf(x,Q)$ for given hadron. x, Q are (real*8), hadron is (integer).
xFF(x,Q,hadron)	Returns the (real*8(-5:5)) value of $xd(x,Q)$ for given hadron. x, Q are (real*8), hadron is (integer).
x_hPDF(x,Q,hadron)	Returns the (real*8(-5:5)) value of $xg_1(x,Q)$ for given hadron ( $g_1$ =helicity distribution). x, Q are (real*8), hadron is (integer).
mCHARM	(real*8)Constant for mass of charm quark.
mBOTTOM	(real*8)Constant for mass of bottom quark.
QCDinput_SetPDFreplica(num,h)	Changes the unpolarized PDF replica number for hadron <b>h</b> to <b>rep</b> .
QCDinput_SetFFreplica(num,h)	Changes the unpolarized FF replica number for hadron h to rep.
QCDinput_SetlpPDFreplica(num,h)	Changes the replica of PDF associated with linearly polarized gluon PDF number for hadron h to rep.
QCDinput_SethPDFreplica(num,h)	Changes the replica of helicity PDF number for hadron h to rep.

# A. Initialization

TOBE WRITTEN

## VI. EWINPUT MODULE

EWinput module contains definitions of various physical parameters of elector-weak interactions, such as masses of Z and W bosons, CKM matrix, code for evolution of  $\alpha_{QED}$  etc.

TOBE WRITTEN

#### A. $\alpha_{QED}$

This implementation has been added in ver.2.03. In earlier versions the code for  $\alpha_{QED}$  had a bug that generated slightly lower values (independently on the values of  $\mu$ ).

The QED coupling constant is set by the one-loop QED evolution with LO matching at thresholds. In order to tune it finer, the value of  $\beta_0$  is modified by  $\beta_0 \to \beta_0 + \delta\beta$ , where  $\delta\beta$  is found by exact implementation of two boundary values,  $\alpha_{\text{QED}}(m_{\tau})$  and  $\alpha_{\text{QED}}(m_{Z})$ .

The LO evolution is

$$\alpha(\mu) = \frac{1}{\alpha_0^{-1} + 2\beta_0 \ln(\mu/\mu_0)},\tag{6.1}$$

where  $\beta_0 = -(3\pi)^{-1} N_{eff}$  with

$$N_{eff} = \sum_{\substack{\text{active} \\ \text{leptons}}} 1 + N_c \sum_{\substack{\text{active} \\ \text{quarks}}} e_q^2.$$
 (6.2)

In artemide I account the following threasholds

$$\frac{\mu}{N_{eff}} \begin{vmatrix} \mu < m_e (\sim m_u, m_d) & \mu < m_\mu (\sim m_s) & \mu < m_c & \mu < m_\tau & \mu < m_b & \mu < m_t & \mu > m_t \\ \hline 0 & \frac{8}{3} & 4 & \frac{16}{3} & \frac{19}{3} & \frac{20}{3} & 8 \\ \end{vmatrix}$$

So the actual formula for  $\alpha_{QED}$  is

$$\alpha_{\text{QED}}(\mu) = \frac{1}{\alpha_Z^{-1} + 2\bar{\beta} \left[ N_{eff}(\mu) \ln \left( \frac{\mu}{m_{th}} \right) + \sum_{m_i \in m_{th}} N_{eff} \ln \left( \frac{m_i}{m_{i+1}} \right) \right]},$$
(6.3)

where  $m_{th}$  are all threasholds from  $\mu$  till  $M_Z$ . The constant  $\bar{\beta}$  is defined by exact matching at  $M_Z$  and  $m_{\tau}$ . For default values  $\bar{\beta}/\beta_0 \sim 1.002\%$ , so it accounts for really tiny effects.

#### VII. TMD EVOLUTION MODULES

The TMD evolution has several implementation. The artemide v3 (and higher) is hard-coded to use the fixed- $\mu$  evolution (see ref.[?]). This choice is made after many test performed in earlier versions or artemide (where the type of evolution was selected by user), and the demonstration that they are equivalent within perturbative uncertainty.

The fixed- $\mu$  scale corresponds to evolution along  $\zeta$  is with fixed- $\mu$  solution to the special equi-potential line, and evolution along  $\mu$  along equi-potential line (this part is unity by definition). The evolution factor reads

$$R[b, (\mu_1, \zeta_1) \to (\mu_2, \zeta_2)] = \frac{R[b, (\mu_1, \zeta_1) \to (\mu_1, \zeta_{\mu_1})]}{R[b, (\mu_2, \zeta_2) \to (\mu_2, \zeta_{\mu_2})]}, \tag{7.1}$$

$$R[b, (\mu, \zeta) \to (\mu, \zeta_{\mu})] = \exp\left(-\mathcal{D}(\mu, b) \ln\left(\frac{\zeta}{\zeta_{\mu}(b)}\right)\right),$$
 (7.2)

where  $\mathcal{D}$  is the Collins-Soper kernel, and  $\zeta_{\mu}(b)$  is the special  $\zeta$ -line.

The Collins-Soper kernel is defined as

$$\mathcal{D}^f(\mu, b) = \mathcal{D}^f_{\text{pert}}(\mu_{\text{OPE}}, b) + \int_{\mu_{\text{OPE}}}^{\mu} \frac{d\mu'}{\mu'} \Gamma^f(\mu') + \mathcal{D}^f_{\text{NP}}(b), \tag{7.3}$$

where  $\mathcal{D}_{pert}^f$  is the high-scale perturbative part, and  $\mathcal{D}_{NP}$  is the non-perturbative model (e.g.  $g_K b^2$ ) The module for evolution includes three modules

- TMD\_AD this module contains collection of all anomalous dimensions and related quantities. Logically it is equivalent to \_OPE modules.
- TMDR\_model this module contains the user-defined non-perturbative input.
- TMDR this module interface TMD\_AD and TMDR\_model into the evolution factor, and perform the general control.

The initialization is happened thorough the TMDR-module.

At small values of parameter  $Q=Q_0$  the point  $(Q,Q^2)$  crosses the  $\zeta$ -lines. The value of  $Q_0$  depends on b. The dangerous situation is then hard scale of the process Q is smaller then  $Q_0$  at large  $b=b_{\infty}$ . In this case the evolution kernel  $R[b_{\infty},(Q,Q^2)\to\zeta_{\mu}]>1$ , which is generally implies that it grows to infinity. However, it happens only at small values of Q. E.g. at NNLO the typical value of  $Q_0$  is  $\sim 1.5 \, \text{GeV}$ . That should be taken into account during consideration of low-energy experiment and especially their error-band, since the point  $(c_2Q,Q^2)$  could cross the point at larger values of Q.

The function LowestQ() returns the values (real\*8(1:3))  $\{Q_{-1}, Q_0, Q_{+1}\}$ , which are solution of equation  $Q^2 = \zeta_{cQ}(b)$ , for (fixed bu) large values of b.  $Q_{-1}$  corresponds to c = 0.5,  $Q_0$  corresponds to c = 1 and  $Q_{+1}$  corresponds to c = 2.

1. INI-parameters

Parameters for TMD-evolution modules (section \*3).

Entry	Type	Description	
A.p1	str	Order of the evolution <i>standardized</i> . Could be LO, NLO, (see table below for details)	
A.p2	T/F	The flag to override the <i>standard</i> evolution definition. If T, than instead of A.p1 the orders defined in A.p3 – A.p6 are used.	
A.p3	str	Order of $\Gamma_{\text{cusp}}$ . LO= $a_s\Gamma_0$ , NLO= $a_s\Gamma_0+a_s^2\Gamma_1$ , etc.	
A.p4	str	Order of $\gamma_V$ . LO=0, NLO= $a_s\gamma_1$ , etc.	
A.p5	str	Order of $\mathcal{D}_{pert}$ . LO=0, NLO= $a_s \mathbf{L} + d^{(1,0)}$ , etc.	
A.p6	str	Order of $\zeta_{\mu}$ (exact solution). LO= $a_s^{0*}$ (exact solution), etc.	
B.p1	int	Number of NP parameters.	
C.p1	real	real Tolerance general (used for check of variable modifications, etc. Does not affect integration precision). (default $=10^{-6}$ )	
C.p2	real	Small-b value at which the evolution is frozen (default $=10^{-6}$ )	
C.p3	real	Parameter for smoothing the small-b value of exact $\zeta$ -line (see below) (default =0.01).	

The table of correspondence between standard definition and particular definitions

order	$\Gamma_{ m cusp}$	$\gamma_V$	D *	$\mathcal{D}_{ ext{resum}}$	$\zeta_{\mu}$ **
LO	$a_s^1$	$a_s^0$	$a_s^0$	$a_s^0$	$a_s^0$
NLO	$a_s^2$	$a_s^1$	$a_s^1$	$a_s^1$	$a_s^2$
NNLO=N2LO	$a_s^3$	$a_s^2$	$a_s^2$	$a_s^2$	$a_s^3$
NNNLO=N3LO	$a_s^4$	$a_s^3$	$a_s^3$	$a_s^2$	$a_s^4$
N4LO	$a_s^5$	$a_s^4$	$a_s^4$	$a_s^3$	$a_s^{5***}$

<sup>\*</sup>  $\mathcal{D}_{\text{resum}}$  starts from  $a_s^0$ , it already contains  $\Gamma_0$ .

# Notes:

- ullet For very small-values of b the value of b is fixed.
- For very large positive values of  $\mathcal{D}$  (i.e. for  $b > 25 \text{GeV}^{-1}$  or so), the exact solution for  $\zeta$ -line diverges exponentially at 3- and 4- loops. It is because the coefficient infront of rising terms is negative. To prevent the divergence, the corresponding terms are expanded in  $a_s$  up to needed power  $(\alpha_s^6)$ .

# 2. Functions

XX=name of module (e.g. uTMDPDF, uTMDFF, etc.)

<sup>\*\*</sup> Definition of  $\zeta_{\mu}$  is correct only in the natural ordering, i.e. LO,NLO,NNLO. Proper definition in + orders would make the function too heavy. The resumed version has the same counting.

<sup>\*\*\*</sup> The finite part =0, since  $d^{(5,0)}$  is unknown.

Entry	Type	Description
TMDR_Initialize(file,prefix)	subroutine	Initialize the module from INI-file.
TMDR_SetScaleVariation(c1)	subroutine	Sets globally a new value for constant $c_1$ .
TMDR_SetNPparameters(lambda)	subroutine	Set a new vector of NP parameters $\lambda_{\rm NP}$ . The new vector must be same size as declared at the setup.
TMDR_CurrentNPparameters()	real(:)	Returns the current vector for $\lambda_{\mathrm{NP}}$ .
CS_kernel(mu,b,f)	real	Returns the value Collins-Soper kernel at scale $\mu$ , point $b$ for flavor $f$ .
zetaNP(mu,b,f)	real	Returns the value $\zeta_{\mu}$ for give CS kernel at scale $\mu$ , point $b$ for flavor $f$ .
TMDR_Rzeta(b,muf,zetaf,f)	real	Return the factor $R$ for evolution from the point $(\mu, \zeta)$ down to the special evolution line.
TMDR_R(b, muf, zetaf, mui, zetai, f)	real	Return the factor $R$ for evolution from the point $(\mu_f, \zeta_f)$ to $(\mu_i, \zeta_i)$ .
LowestQ()	real	Attempts to compute the lowest available scale $Q$ , for which the evolution converges.

#### A. TMD\_AD module

The module TMD\_AD give access to various perturbative anomalous dimensions needed for TMD evolution. This module is essential part of TMDR module, and thus initialized by it.

List of available commands

Command	Sec.	Short description
TMD_AD_Initialize(oC,oV,oD,oDr,oZ)	??	Initialization of module. The (integer) parameters (oC,oV,oD,oDr,oZ) are orders of definition for anomalous dimensions ( $\Gamma_{\text{cusp}}$ , $\gamma_V$ , $\mathcal{D}_{\text{pert}}$ , $\mathcal{D}_{\text{resum}}$ , $\zeta_{\text{pert}}$ ).
GammaCusp(mu,f)		$=\Gamma_{ m cusp}^f(\mu)$
gammaV(mu,f)		$=\gamma_V^f(\mu)$
Dpert(mu,bT,f)		$=\mathcal{D}^f_{\mathrm{pert}}(b,\mu)$
Dresum(mu,bT,f)		$=\mathcal{D}_{ ext{resum}}^f(b,\mu)$
zetaMUpert(mu,bT,f)		$=\zeta_{ m pert}^f(b,\mu)$
zetaSL(mu,rad,f)		$=\zeta_{\mathrm{exact}}^f(\mathcal{D},\mu)$ (Note, the argument.)
RADEvolution(mu0,mu1,f)		$=\int_{\mu_0}^{\mu_1} \frac{d\mu^2}{\mu^2} \frac{\Gamma(\mu)}{2}$ The evolution constant for $\mathcal{D}$

#### Notes:

- The integral over  $\mu$  is done using exact analytical formula by decomposition of  $\beta$ -function over roots.
- The exact expression for  $\zeta$ -line is numerically unstable at very small-b. It is due to its double-exponential nature which requires exponentiation and cancellation of large-numbers. However, it could be computed analytically in this regime as expansion. Thus, to stabilize the computation of expression the following formula is used

$$\zeta_{\mu} = e^{-b^2/S} \zeta_{\text{pert}} + (1 - e^{-b^2/S}) \zeta_{\text{exact}}.$$
(7.4)

Here, S is the smoothing parameter. It should be small enough to guaranty non-impact of approximation (approx. S < 0.05).

#### B. TMDR\_model

This module gives the expression for  $\mathcal{D}$ . It could be modified by user, and one of modules that form a TMD model (together with models for TMD-distributions).

Making this module follow the interface

public:: ModelInitialization(NPlength)

public:: ModelUpdate(NParray)
real(dp),public:: DNP(b,f)
real(dp),public:: bSTAR(b)
real(dp),public:: muOPE(b,c1)

ModelInitialization(NPlength): this subroutine is called during the initialization of TMDR. The integer,intent(in)::NParray(:) is the length of array of NP-parameters. Use this subroutine to make preparation of the model.

ModelUpdate(NParray): this subroutine is called during the TMDR\_setNPparameters(NParray). The real(dp),intent(in)::NParray(:) is the array of NP-parameters passed to TMDR\_setNPparameters. Use this subroutine to recompute model parameters (if needed), save NP-parameters (if needed), etc.

DNP(b,f): the function returns the value,  $\mathcal{D}_{NP}^f(b)$ . It contains only NP part.

bSTAR(b): the function returns the value,  $b^*(b)$  used instead of b within  $\mathcal{D}_{pert}$ 

muOPE(b,c1): the function returns the value,  $\mu_{OPE}$  used as reference scale of  $\mathcal{D}_{pert}$ . The parameter  $c_1$  is the prescription used during the scale variation.

Important: the module TMDR\_model is compiled before TMDR, and thus can use only lower-level modules: TMD\_AD, QCDinput, etc.

## VIII. MODULES COMPUTING OPTIMAL TMD DISTRIBUTIONS

There are many TMD distributions each computed in a separate module. All TMD distributions are split in the following classes:

- Pure Twist-2 OPE These are uTMDPDF, uTMDFF, 1pTMDPDF. These TMD distributions are defined by twist-2 collinear distribution at small-b
- Pure Twist-3 OPE These are SiversTMDPDF. These TMD distributions are defined by twist-3 collinear distribution at small-b
- Twist-2 & Twist-3 OPE These are wgtTMDPDF. These TMD distributions are defined by twist-2 (WW-term) and twist-3 collinear distribution at small-b

These lists are to be extended in the future.

Each module consists of several sub-modules, which have names as TMDname\_X. The X corresponds to

- OPE this module computes the convolution of the twist-2 (or twist-3) coefficient function with corresponding PDF
- model this module contains all information about NP-part and other free-parameters (such as  $\mu_{\text{OPE}}$  of the given TMD distribution. These modules could be edited by user, to implement/update/fit TMDs.

The most part of modules are identical. There are a few differences in the implementation. So, first the general structure is presented, and then particularities.

Different OPE's are known up to different orders. Consequently, the modules implement them at different orders. The orders are denoted as

$$\begin{array}{ccc} \text{NA} & : \rightarrow & \text{no OPE} \\ \text{LO} & : \rightarrow & C = \mathcal{O}(a_s^0) \\ \text{NLO} & : \rightarrow & C = \mathcal{O}(a_s^1) \\ \text{NNLO} & = \text{N2LO} & : \rightarrow & C = \mathcal{O}(a_s^2) \\ \text{NNNLO} & = \text{N3LO} & : \rightarrow & C = \mathcal{O}(a_s^3). \end{array}$$

- The NA option is used to remove any relation to collinear distributions. In this case  $TMD(x,b) = f_{NP}(x,b)$
- If the coefficient function at LO/NLO/.. is zero, the convolution is also zero. E.g. linearly polarized gluons start at  $\sim a_s$ , the convolution is zero at LO.

List of available orders for different distributions

The functions are computed by the following rule

$$uTMDPDF = [C \times f]_{tw2}(x,b)F_{NP}(x,b), \tag{8.1}$$

$$uTMDFF = [C \times d]_{tw2}(x, b)F_{NP}(x, b), \tag{8.2}$$

$$1pTMDPDF = [C \times f]_{tw2}(x, b)F_{NP}(x, b), \tag{8.3}$$

$$\text{wgtTMDPDF} = [C \times h]_{\text{tw2}}(x, b) F_{\text{NP}}(x, b) + [C \times T]_{\text{tw3}}(x, b) F_{\text{NP}}^{\text{tw3}}(x, b), \tag{8.4}$$

$$\texttt{SiversTMDPDF} = [C \times T]_{\text{tw3}}(x, b) F_{\text{NP}}^{\text{tw3}}(x, b), \tag{8.5}$$

where f, d, h are collinear distributions of twist-2, and  $[C \times h]_{\text{tw2}}$  is corresponding convolution; T are collinear distributions of twist-3, and  $[C \times T]_{\text{tw3}}$  is corresponding convolution;  $F_{\text{NP}}(x,b)$  and  $F_{\text{NP}}^{\text{tw3}}(x,b)$  are non-perturbative functions to be fit. NP functions are defined in the XX model modules, and share the same  $\lambda_{\text{NP}}$  (array of parameters). This structure correctly reproduces the small-b properties of TMD-distributions. The convolutions are computed in separate modules see sec.VIII B, VIII C.

# $1. \quad INI-parameters$

# Parameters universal for all such modules which include only tw2 or tw3 OPE (mixed case see below).

Entry	Type	Description
A.p1	str	Order of the coefficient function. Could be N/A, LO, NLO, (see table below for details)
A.p2	T/F	Trigger to prepare the grid (T=prepare). Preparation is done on the initialization stage.
A.p3	T/F	Trigger to include the gluon TMD into the grid (T=include). Doubles the computation time. If not included, gluon contribution is 0.
A.p4	int>0	Number of hadrons/grid to prepare. This must coincide with 1.??.p1 (corresponding PDF number in QCDinput). The type of TMD is dictated by the collinear PDF and $f_{\rm NP}$ .
A.p5	T/F	Trigger the test of the grid (T=run the test). Take the same time as computation of the grid (by a single processor). Requires A.p2=T. Example Result is shown in sec.VIIIB4.
B.p1	int	Number of NP parameters.
B.p2	real	$B_{\text{MAX-ABS}}$ , a large number such that $b > B_{\text{MAX-ABS}}$ the TMD is returned 0. (default 100).
C.p1	real	Tolerance for integration (default $=10^{-6}$ )
C.p2	real	Tolerance general (used for check of variable modifications, etc. Does not affect integration precision). (default $\pm 10^{-6}$ )
C.p3	int	Maximum number of iteration for adaptive integration. (default $=10^4$ )
D.p1	real	$x_{\min}$ for the grid (see (8.11))
D.p2	real	$p_x$ for the grid (see (8.11))
D.p3	real	$b_{\min}$ for the grid (see (8.12)). [It is not related to parameter $b_{\min}$ of $b^*$ -prescription!]
D.p4	real	$b_{\text{max}}$ for the grid (see (8.12)) [It is not related to parameter $b_{\text{max}}$ of $b^*$ -prescription!]
D.p5	integer	Number of nodes in the x-grid
D.p6	integer	Number of nodes in the b-grid

- wgtTMDPDF has extra section E, which has the same fields as the section A, but responsible for twist-3 convolution.
- For SiversTMDPDF the convolution is twist-3. The section C, is absence since it is not yet implemented.

 $\it 2. \quad Functions$ 

XX=name of module (e.g. uTMDPDF, uTMDFF, etc.)

Entry	Type	Description					
XX_Initialize(file,prefix)	subroutine	Initialize the module from INI-file.					
<pre>XX_SetPDFreplica(rep,h)</pre>	subroutine	Passes to XX_OPE_SetPDFreplica					
XX_SetScaleVariation(c4)	subroutine	Passes to XX_OPE_SetScaleVariation					
XX_SetLambdaNP(lambda)	subroutine	Set a new vector of NP parameters $\lambda_{\rm NP}$ . The new vector must be same size as declared at the setup.					
<pre>XX_CurrentLambdaNP()</pre>	real(:)	Returns the current vector for $\lambda_{\mathrm{NP}}$ .					
XX_lowScale5(x,bT,h)	real(-5:5)	Returns the value of TMD distributions for given (x,b) (reals) and hadron h. The value is the vector over flavors.					

#### A. \_model modules

same for uTMDFF\_model and lpTMDPDF\_model.

This module gives the expression for  $f_{NP}$ ,  $\mu_{OPE}$  and  $b^*$ . It could be written by user, and one of modules that form a TMD model (together with models for TMD-evolution).

Making this module follow the interface

public:: ModelInitialization

public:: ModelUpdate

real(dp),public,dimension(-5:5):: FNP

real(dp),public:: bSTAR
real(dp),public:: muOPE

If there is a twist-3 part of small-b matching, there are extra functions

real(dp),public,dimension(-5:5):: FNP\_tw3

real(dp),public:: bSTAR\_tw3
real(dp),public:: mu0PE\_tw3
which contribute to the twist-3 term.

ModelInitialization(NParray): this subroutine is called during the initialization of XX module. The integer,intent(in)::NPlength(:) is the size of the array of NP-parameters. Use this subroutine to make preparation of the model.

ModelUpdate(NParray): this subroutine is called during the XX\_setNPparameters(NParray). The real(dp),intent(in)::NParray(:) is the array of NP-parameters passed to TMDR\_setNPparameters. Use this subroutine to recompute model parameters (if needed), save NP-parameters (if needed), etc.

FNP(x,b,hadron,lambdaNP): the function returns  $f_{NP}^{f,h}(x,b,\lambda)$ .

bSTAR(b,x,y): the function returns  $b^*(b)$  function.

mu\_OPE(b,x,y,c4): the function returns  $\mu_{OPE}(z,b)$  function.

Important: the module XX\_model is compiled before XX, and thus can use only lower-level modules: TMD\_AD, QCDinput, etc.

# B. \_OPE modules (tw2)

OPE modules compute the following convolution

$$[C \times f](x) = \int_{x}^{1} \frac{dy}{y} C(y, \mathbf{L}) f\left(\frac{x}{y}, \mu_{\text{OPE}}\right)$$
(8.6)

$$= \frac{1}{x} \int_{x}^{1} dy C(y, \mathbf{L}) F\left(\frac{x}{y}, \mu_{\text{OPE}}\right), \tag{8.7}$$

where F(x) = xf(x) and

$$\mathbf{L} = \ln\left(\frac{\mu_{\text{OPE}}^2 b^2}{4e^{-2\gamma_E}}\right). \tag{8.8}$$

OPE modules are initialized automatically from the corresponding TMD module.

## Extra notes:

• The convolution is convergent, but the convolution kernel has singularity at  $y \to 1$ . To stabilize the integral, it is computed as

$$\int_{x}^{1} dy(...) = \int_{x}^{y_{C}} dy(...) + \int_{y_{C}}^{1} dy(...).$$
(8.9)

The first term is computed by the adaptive algorithm. The second term is computed by the approximate formulas

$$\int_{y_C}^1 dy \frac{f(x/y) - f(x)}{1 - y} = f(x/y_C) - f(x),$$

$$\int_{y_C}^1 dy \frac{f(x/y) - f(x)}{1 - y} \ln(1 - y) = (f(x/y_C) - f(x))(\ln(1 - y_C) - 1),$$

$$\int_{y_C}^1 dy \frac{f(x/y) - f(x)}{1 - y} \ln^2(1 - y) = (f(x/y_C) - f(x))(2 - \ln(1 - y_C) + 2\ln^2(1 - y_C)),$$

$$\int_{y_C}^1 dy f(x/y)g(y) = f(x) \int_{y_C}^1 dy g(y),$$

where g(y) is integrable, and the last integral is taken explicitly.

- The parameter  $y_C = 1 10^{-4}$  (for a moment) is fixed. It provides the accuracy of the last integral (6-7 digits), which is far better than.
- For  $x \sim y_C$  the accuracy drops. In this case, the values of  $y_C$  is recomputed by formula  $y_C = (100 + x)/101$  (i.e. it is 2-digits closer to 1 than x).
- The definition of TMDFF does not perfectly match the definition of collinear FF. There is a relative factor  $1/z^2$ . So the convolution reads

$$D(z,b) = \int_{z}^{1} \frac{dy}{y} \mathbb{C}\left(\frac{z}{y}, \mathbf{L}_{\mu}\right) \frac{d(y,\mu)}{y^{2}} = \frac{1}{z^{3}} \int_{z}^{1} dy [y^{2}C](y, \mathbf{L}_{\mu}) D(\frac{z}{y}, \mu), \tag{8.10}$$

where D(z) = zd(z).

#### 1. Functions

# XX=name of module (e.g. uTMDPDF, uTMDFF, etc.)

(3,									
Entry	Type	Description							
XX_OPE_Initialize(file,prefix)	subroutine	Initialize the module from INI-file.							
XX_resetGrid()	subroutine	Force recomputation of the grid. Only if griding is ON.							
XX_OPE_testGrid()	subroutine	Run the test of grid (see sec. VIII B 4). Only if griding is ON.							
XX_OPE_SetPDFreplica(rep,h)	subroutine	Switch the PDF replica to rep(int) for hadron h (int). Recompute the grid (if griding is ON). If the new replica is as before nothing is done.							
XX_OPE_SetScaleVariation(c4)	subroutine	Change the scale variation parameter $c_4$ (it enters the definition of $\mu_{\rm OPE}$ ). Recompute the grid (if griding is ON). The parameter (real)c4 is restricted to $0.1 < c_4 < 10$ .							
XX_OPE_convolution(x,b,h,G)	dp_real(-5:5)	Returns (8.6) for $(x,b)=((real)x, (real)b)$ , and hadron number (int)h. In the case of NA returns 1. If grid is computed restore from the grid. The flag $(T/F)G$ is optional. It indicates the inclusion of gluon into the result. Note, that if gluons were not included into the grid they are zero.							

## 2. Model parameters.

The OPE is fully deterministic formula, but it contains the free scale, and often one implement  $b^*$ -modification. These parameters are written in model-module. Namely:

- bSTAR(bT,x,y) = is the function used instead of b in L in eqn. (8.6).
- muOPE(bt,x,y,c4) = is the function used for  $\mu_{OPE}$ .

In both cases, the variables x and y are defined as in eqn. (8.6). The parameter  $c_4$  is the scale variation parameter.

3. Scale variation.

TO BE WRITTEN

4. Grid

For fitting procedure one often needs to evaluate TMDs multiple times. For example, for fit performed in [?] the evaluation of singe  $\chi^2$  entry requires  $\sim 16 \times 10^6$  calls of uTMDPDF\_... So, every call of uTMDPDF\_... at NNLO order, requires  $\sim 200$  calls of pdfs, depending on x, b and  $\lambda$ 's, in order to evaluate the integral over y. In such situations, it is much faster to make a grid of TMD distributions for a given set of non-pertrubative parameters (i.e. the grid is in x and b), and then use this grid for the interpolation of TMD values. The calculation of a grid is not a very fast procedure, nonetheless, for large computation (number of TMD calls  $> 10^4 - 10^5$ ) is more efficient.

The grid used in the artemide 3.0 is:

Arcosh grid with control parameter

$$i = 0, ..., N_x,$$
  $x_i = \frac{1}{\cosh^p(\Delta_x(i - N_x))},$   $\Delta_x = \frac{\operatorname{arccosh}(1/x_{\min}^{1/p})}{N_x},$   $\operatorname{inv}[x] = N_x - \frac{\operatorname{arccosh}(1/x^{1/p})}{\Delta_x}.$  (8.11)

This grid is alike logarithmic at small-x, but has extra points at  $x \to 1$ . Therefore, one does not need extra griding at large-x. The parameter p gives extra flexibility. At  $p_x > 1$  the density of points at  $x \to 1$  grows.

Exponential grid with  $b_{\min}$ 

$$b_i = B_{\min} e^{-i\Delta_b}, \qquad \Delta_b = \frac{1}{N_b} \ln \left( \frac{b_{\min}}{B_{\max}} \right), \qquad \text{inv}[b] = \frac{1}{\Delta_b} \ln \left( \frac{b_{\min}}{b} \right).$$
 (8.12)

This grid has a lot of points at small-b. and for  $b < b_{\min}$  one could freeze the value.

The interpolation is cubic. The grid is build for the finite domain of  $x \in (x_{\min}, 1)$  and  $b \in (0, b_M)$ .

- For  $x < x_{\min}$  the program will be terminated (with an error).
- For  $b < b_{\min}$  the code returns the value at  $b_{\min}$  (default  $b_{\min} = 10^{-6}$ ).
- For  $b > b_{\text{max}}$ , the extrapolation is used:

$$f(b) = \frac{a_1}{b} + \frac{a_2}{\ln b} \tag{8.13}$$

The values  $a_{1,2}$  are found from the last two points of the grid  $\{b_1, f_1\}$  and  $\{b_2, f_2\}$ .

All these parameters can be changed in constants file. However, we recommend to use default values, since they were checked. The check could be performed by the call TestGrid() subroutine of corresponding module. It computes values for central points of grids-cells from grid and from direct computation, and returns the average of  $(f_{\text{exract}}/f_{\text{computed}}-1)$ . This check can be also called by option in the constants file.

I have found that for uTMDPDF the grid with  $(N_x = 400, p_x = 2, x_{\min} = 10^{-5})$  and  $(N_b = 200, b_{\min} = 10^{-6}, b_{\max} = 25)$  produce the interpolation quality as shown (test made at NNLO nnpdf31\_nnlo)

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5. <b<< td=""><td>BMAX</td><td>  0.48372E-04  </td><td>  0.53025E-04  </td><td>0.43636E-04</td><td>  0.00000E+00</td><td>  0.43465E-04</td><td>  0.52785E-04</td><td>0.48412E-04</td></b<<>	BMAX	0.48372E-04	0.53025E-04	0.43636E-04	0.00000E+00	0.43465E-04	0.52785E-04	0.48412E-04
10^-4 <x<< td=""><td>0.01</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.01							
0 <b<< td=""><td></td><td>  0.44373E-06  </td><td>0.40601E-06  </td><td>0.41975E-06</td><td>  0.00000E+00</td><td>  0.37784E-06</td><td>  0.34930E-06</td><td>0.44395E-06</td></b<<>		0.44373E-06	0.40601E-06	0.41975E-06	0.00000E+00	0.37784E-06	0.34930E-06	0.44395E-06
0.1 <b<< td=""><td>1.</td><td>0.93679E-05</td><td>0.66184E-05  </td><td>0.57894E-05</td><td>  0.00000E+00</td><td>  0.35293E-05</td><td>0.44275E-05</td><td>0.92845E-05</td></b<<>	1.	0.93679E-05	0.66184E-05	0.57894E-05	0.00000E+00	0.35293E-05	0.44275E-05	0.92845E-05
1. <b<   5.<b<< td=""><td>5. BMAX</td><td>  0.12521E-04     0.16492E-03  </td><td>  0.29436E-05     0.36479E-04  </td><td>0.26138E-05 0.22847E-04</td><td>  0.00000E+00   0.00000E+00</td><td>  0.33127E-05   0.48635E-04</td><td>  0.33215E-05   0.39458E-04</td><td>0.11045E-04 0.67263E-03</td></b<<></b< 	5. BMAX	0.12521E-04     0.16492E-03	0.29436E-05     0.36479E-04	0.26138E-05 0.22847E-04	0.00000E+00   0.00000E+00	0.33127E-05   0.48635E-04	0.33215E-05   0.39458E-04	0.11045E-04 0.67263E-03
i								
0.01 <x<< td=""><td>0.1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.1							
0 <b<< td=""><td>0.1</td><td>  0.36916E-05  </td><td>0.16644E-05  </td><td>0.11713E-05</td><td>  0.00000E+00</td><td>  0.72487E-06</td><td>  0.67086E-06</td><td>0.34891E-05</td></b<<>	0.1	0.36916E-05	0.16644E-05	0.11713E-05	0.00000E+00	0.72487E-06	0.67086E-06	0.34891E-05
0.1 <b<< td=""><td>1.</td><td>  0.35591E-04  </td><td>0.22837E-04  </td><td>0.17531E-04</td><td>0.00000E+00</td><td>  0.60829E-05</td><td>0.12328E-04</td><td>0.33161E-04</td></b<<>	1.	0.35591E-04	0.22837E-04	0.17531E-04	0.00000E+00	0.60829E-05	0.12328E-04	0.33161E-04
1. <b<< td=""><td>5.</td><td>  0.51807E-03  </td><td>0.12126E-04  </td><td>0.93863E-05</td><td>  0.00000E+00</td><td>  0.70368E-05</td><td>  0.34347E-05</td><td>0.41678E-03</td></b<<>	5.	0.51807E-03	0.12126E-04	0.93863E-05	0.00000E+00	0.70368E-05	0.34347E-05	0.41678E-03
5. <b<< td=""><td>BMAX</td><td>  0.19295E-03  </td><td>  0.23647E-01  </td><td>0.20959E-03</td><td>  0.00000E+00</td><td>  0.11907E-02</td><td>  0.10972E-03</td><td>0.32283E-03</td></b<<>	BMAX	0.19295E-03	0.23647E-01	0.20959E-03	0.00000E+00	0.11907E-02	0.10972E-03	0.32283E-03
0.1 <x<< td=""><td>0.8</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.8							
0 <b<< td=""><td>0.1</td><td>  0.26653E-02  </td><td>0.12698E-02  </td><td>0.29909E-03</td><td>  0.00000E+00</td><td>  0.21281E-03</td><td>0.26701E-04</td><td>0.93337E-03</td></b<<>	0.1	0.26653E-02	0.12698E-02	0.29909E-03	0.00000E+00	0.21281E-03	0.26701E-04	0.93337E-03
0.1 <b<< td=""><td>1.</td><td>  0.28405E-02  </td><td>0.42081E-02  </td><td>0.29125E-02</td><td>  0.00000E+00</td><td>0.62434E-03</td><td>0.12346E-03</td><td>0.84058E-02</td></b<<>	1.	0.28405E-02	0.42081E-02	0.29125E-02	0.00000E+00	0.62434E-03	0.12346E-03	0.84058E-02
1. <b<< td=""><td>5.</td><td>  0.17468E-01  </td><td>0.34065E-01  </td><td>0.61586E-01</td><td>0.00000E+00</td><td>0.12291E-02</td><td>0.22105E-03</td><td>0.70745E-02</td></b<<>	5.	0.17468E-01	0.34065E-01	0.61586E-01	0.00000E+00	0.12291E-02	0.22105E-03	0.70745E-02
5. <b<< td=""><td>BMAX</td><td>  0.14342E-01  </td><td>0.14207E+00  </td><td>0.21854E+00</td><td>  0.0000E+00</td><td>  0.18476E-02</td><td>  0.37234E-03</td><td>0.22346E-01</td></b<<>	BMAX	0.14342E-01	0.14207E+00	0.21854E+00	0.0000E+00	0.18476E-02	0.37234E-03	0.22346E-01
0.8 <x<< td=""><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	1							
0 <b<< td=""><td>0.1</td><td>  0.89323E-03  </td><td>0.91579E-03  </td><td>0.24787E-02</td><td>  0.00000E+00</td><td>  0.17615E-02</td><td>0.88343E-03</td><td>0.90570E-03</td></b<<>	0.1	0.89323E-03	0.91579E-03	0.24787E-02	0.00000E+00	0.17615E-02	0.88343E-03	0.90570E-03
0.1 <b<< td=""><td>1.</td><td>  0.11133E-02  </td><td>0.12141E-02  </td><td>0.14404E-02</td><td>0.00000E+00</td><td>  0.92049E-02</td><td>0.11007E-02</td><td>0.11588E-02</td></b<<>	1.	0.11133E-02	0.12141E-02	0.14404E-02	0.00000E+00	0.92049E-02	0.11007E-02	0.11588E-02
1. <b<< td=""><td>5.</td><td>  0.71137E-03  </td><td>0.12381E-02  </td><td>0.11313E-02</td><td>0.00000E+00</td><td>  0.97426E-02</td><td>  0.64774E-03</td><td>0.10339E-02</td></b<<>	5.	0.71137E-03	0.12381E-02	0.11313E-02	0.00000E+00	0.97426E-02	0.64774E-03	0.10339E-02
5. <b<< td=""><td>BMAX</td><td>  0.79151E-03  </td><td>0.19174E-02  </td><td>0.12531E-02</td><td>  0.00000E+00</td><td>  0.75118E-02</td><td>  0.66856E-03</td><td>0.17425E-02</td></b<<>	BMAX	0.79151E-03	0.19174E-02	0.12531E-02	0.00000E+00	0.75118E-02	0.66856E-03	0.17425E-02
		<del></del>	<del></del>	<del></del>				

and another (test made at NNLO MSHT20nnlo)

	`	sBar		uBar		dBar		gluon		d	1	u		S
ı İ								6						
   0 <x<1< th=""><th>0^-1</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></x<1<>	0^-1													
0 <b<< td=""><td>0.1  </td><td>0.11650E-05</td><td>0.1</td><td>1346E-05</td><td>1 0</td><td>.11423E-05</td><td>0</td><td>.00000E+00</td><td>1</td><td>0.11424E-05</td><td>ı</td><td>0.11396E-05</td><td>ı</td><td>0.11652E-05</td></b<<>	0.1	0.11650E-05	0.1	1346E-05	1 0	.11423E-05	0	.00000E+00	1	0.11424E-05	ı	0.11396E-05	ı	0.11652E-05
0.1 <b<< td=""><td>1.  </td><td>0.11753E-03</td><td></td><td>0244E-03</td><td></td><td>.10565E-03</td><td></td><td>.00000E+00</td><td>1</td><td>0.10384E-03</td><td></td><td>0.10092E-03</td><td></td><td>0.11776E-03</td></b<<>	1.	0.11753E-03		0244E-03		.10565E-03		.00000E+00	1	0.10384E-03		0.10092E-03		0.11776E-03
1. <b<   5.<b<< td=""><td>5.  </td><td>0.37190E-05 0.33373E-05</td><td></td><td>5364E-05 1269E-05</td><td></td><td>.35956E-05 .40635E-05</td><td></td><td>.00000E+00</td><td>!</td><td>0.33541E-05 0.37846E-05</td><td></td><td>0.31261E-05 0.35646E-05</td><td></td><td>0.37422E-05 0.33547E-05</td></b<<></b< 	5.	0.37190E-05 0.33373E-05		5364E-05 1269E-05		.35956E-05 .40635E-05		.00000E+00	!	0.33541E-05 0.37846E-05		0.31261E-05 0.35646E-05		0.37422E-05 0.33547E-05
5. <b< td=""><td>BMAX  </td><td>0.333/3E-05</td><td></td><td>1269E-05</td><td></td><td>.40635E-05</td><td></td><td>.00000E+00</td><td>Ц</td><td>0.3/846E-05</td><td><u> </u></td><td>0.35646E-05</td><td><u> </u></td><td>0.33547E-05</td></b<>	BMAX	0.333/3E-05		1269E-05		.40635E-05		.00000E+00	Ц	0.3/846E-05	<u> </u>	0.35646E-05	<u> </u>	0.33547E-05
10^-4 <x<< td=""><td>0.01</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.01													
0 <b<< td=""><td>0.1  </td><td>0.20660E-05</td><td>0.2</td><td>2980E-05</td><td>1 0</td><td>.23392E-05</td><td>1 0</td><td>.00000E+00</td><td>ī</td><td>0.22987E-05</td><td>ı</td><td>0.22387E-05</td><td>ı</td><td>0.20747E-05</td></b<<>	0.1	0.20660E-05	0.2	2980E-05	1 0	.23392E-05	1 0	.00000E+00	ī	0.22987E-05	ı	0.22387E-05	ı	0.20747E-05
0.1 <b<< td=""><td>1.  </td><td>0.48562E-04</td><td></td><td>8204E-04</td><td></td><td>.48411E-04</td><td></td><td>.00000E+00</td><td>1</td><td>0.41674E-04</td><td></td><td>0.36914E-04</td><td></td><td>0.48751E-04</td></b<<>	1.	0.48562E-04		8204E-04		.48411E-04		.00000E+00	1	0.41674E-04		0.36914E-04		0.48751E-04
1. <b<< td=""><td>5.  </td><td>0.71871E-05</td><td></td><td>4337E-05</td><td></td><td>.10047E-04</td><td></td><td>.00000E+00</td><td>!</td><td>0.80426E-05</td><td></td><td>0.71569E-05</td><td></td><td>0.73251E-05</td></b<<>	5.	0.71871E-05		4337E-05		.10047E-04		.00000E+00	!	0.80426E-05		0.71569E-05		0.73251E-05
5. <b<< td=""><td>BMAX  </td><td>0.27158E-04</td><td>  0.1</td><td>4867E-02</td><td>1 0</td><td>.17802E-03</td><td>I 0</td><td>.00000E+00</td><td><u> </u></td><td>0.19150E-03</td><td><u> </u></td><td>0.11361E-03</td><td><u> </u></td><td>0.29411E-04</td></b<<>	BMAX	0.27158E-04	0.1	4867E-02	1 0	.17802E-03	I 0	.00000E+00	<u> </u>	0.19150E-03	<u> </u>	0.11361E-03	<u> </u>	0.29411E-04
0.01 <x<< td=""><td>0.1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.1													
0 <b<< td=""><td>0.1  </td><td>0.25235E-05</td><td>0.1</td><td>4207E-05</td><td>1 0</td><td>.12489E-05</td><td>1 0</td><td>.00000E+00</td><td>ı</td><td>0.71199E-06</td><td>L</td><td>0.77710E-06</td><td>1</td><td>0.24029E-05</td></b<<>	0.1	0.25235E-05	0.1	4207E-05	1 0	.12489E-05	1 0	.00000E+00	ı	0.71199E-06	L	0.77710E-06	1	0.24029E-05
0.1 <b<< td=""><td>1.  </td><td>0.43022E-04</td><td></td><td>1937E-04</td><td></td><td>.25031E-04</td><td></td><td>.00000E+00</td><td>1</td><td>0.65584E-05</td><td></td><td>0.14865E-04</td><td></td><td>0.38493E-04</td></b<<>	1.	0.43022E-04		1937E-04		.25031E-04		.00000E+00	1	0.65584E-05		0.14865E-04		0.38493E-04
1. <b<< td=""><td>5.  </td><td>0.10195E-04</td><td></td><td>0127E-05</td><td></td><td>.59895E-05</td><td></td><td>.00000E+00</td><td>!</td><td>0.39661E-05</td><td></td><td>0.45043E-05</td><td></td><td>0.94613E-05</td></b<<>	5.	0.10195E-04		0127E-05		.59895E-05		.00000E+00	!	0.39661E-05		0.45043E-05		0.94613E-05
5. <b<< td=""><td>BMAX  </td><td>0.14108E-02</td><td>0.1</td><td>5608E-03</td><td>1 0</td><td>.16798E-03</td><td>I 0</td><td>.00000E+00</td><td>Ц</td><td>0.23174E-03</td><td><u> </u></td><td>0.99539E-04</td><td>Ц</td><td>0.34846E-03</td></b<<>	BMAX	0.14108E-02	0.1	5608E-03	1 0	.16798E-03	I 0	.00000E+00	Ц	0.23174E-03	<u> </u>	0.99539E-04	Ц	0.34846E-03
0.1 <x<< td=""><td>0.8</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	0.8													
0 <b<< td=""><td>0.1  </td><td>0.23264E-02</td><td>0.2</td><td>3508E-03</td><td>1 0</td><td>.23301E-03</td><td>1 0</td><td>.00000E+00</td><td>ı</td><td>0.94527E-04</td><td>L</td><td>0.37975E-04</td><td>1</td><td>0.19354E-03</td></b<<>	0.1	0.23264E-02	0.2	3508E-03	1 0	.23301E-03	1 0	.00000E+00	ı	0.94527E-04	L	0.37975E-04	1	0.19354E-03
0.1 <b<< td=""><td>1.  </td><td>0.31564E-02</td><td>0.5</td><td>2721E-03</td><td>1 0</td><td>.58486E-03</td><td>0</td><td>.00000E+00</td><td>1</td><td>0.16827E-03</td><td>ı</td><td>0.10961E-03</td><td>1</td><td>0.46416E-03</td></b<<>	1.	0.31564E-02	0.5	2721E-03	1 0	.58486E-03	0	.00000E+00	1	0.16827E-03	ı	0.10961E-03	1	0.46416E-03
1. <b<< td=""><td>5.  </td><td>0.46704E-03</td><td></td><td>1070E-02</td><td></td><td>.18598E-02</td><td></td><td>.00000E+00</td><td>1</td><td>0.11239E-03</td><td></td><td>0.37525E-04</td><td></td><td>0.13732E-02</td></b<<>	5.	0.46704E-03		1070E-02		.18598E-02		.00000E+00	1	0.11239E-03		0.37525E-04		0.13732E-02
5. <b<< td=""><td>BMAX  </td><td>0.14440E-02</td><td>  0.8</td><td>0850E-03</td><td>1 0</td><td>.76572E-02</td><td>  0 </td><td>.00000E+00</td><td></td><td>0.15361E-03</td><td>   </td><td>0.57673E-04</td><td><u> </u></td><td>0.18912E-02</td></b<<>	BMAX	0.14440E-02	0.8	0850E-03	1 0	.76572E-02	0 	.00000E+00		0.15361E-03	 	0.57673E-04	<u> </u>	0.18912E-02
0.8 <x<< td=""><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></x<<>	1													
0 <b<< td=""><td>0.1</td><td>0.21035E-02</td><td>0.4</td><td>6467E-02</td><td>1 0</td><td>.38157E-02</td><td>1 0</td><td>.00000E+00</td><td>ı</td><td>0.21238E-02</td><td>ı</td><td>0.19796E-02</td><td>ī</td><td>0.65294E-02</td></b<<>	0.1	0.21035E-02	0.4	6467E-02	1 0	.38157E-02	1 0	.00000E+00	ı	0.21238E-02	ı	0.19796E-02	ī	0.65294E-02
0.1 <b<< td=""><td>1.</td><td>0.15020E-02</td><td>0.1</td><td>5593E-02</td><td>1 0</td><td>.15573E-02</td><td></td><td>.00000E+00</td><td>I</td><td>0.15401E-02</td><td></td><td>0.15054E-02</td><td></td><td>0.17746E-02</td></b<<>	1.	0.15020E-02	0.1	5593E-02	1 0	.15573E-02		.00000E+00	I	0.15401E-02		0.15054E-02		0.17746E-02
1. <b<< td=""><td>5. l</td><td>0.12826E-02</td><td></td><td>2936E-02</td><td></td><td>.12934E-02</td><td></td><td>.00000E+00</td><td></td><td>0.14148E-02</td><td></td><td>0.13307E-02</td><td></td><td>0.13065E-02</td></b<<>	5. l	0.12826E-02		2936E-02		.12934E-02		.00000E+00		0.14148E-02		0.13307E-02		0.13065E-02
5. <b<< td=""><td>BMAX  </td><td>0.13151E-02</td><td>0.1</td><td>3234E-02</td><td>1 0</td><td>.13232E-02</td><td>0</td><td>.00000E+00</td><td></td><td>0.14735E-02</td><td>I</td><td>0.13732E-02</td><td></td><td>0.13325E-02</td></b<<>	BMAX	0.13151E-02	0.1	3234E-02	1 0	.13232E-02	0	.00000E+00		0.14735E-02	I	0.13732E-02		0.13325E-02

I.e. the average accuracy for very large x is  $\sim 0.1\%$  (3 digits), for large x is  $\sim 0.01\%$  (4 digits) and better (5-6 digits) for the rest. The further improvement is slow, and seems to be limited by the precision of the integration routine. The examples are shown in fig.4.

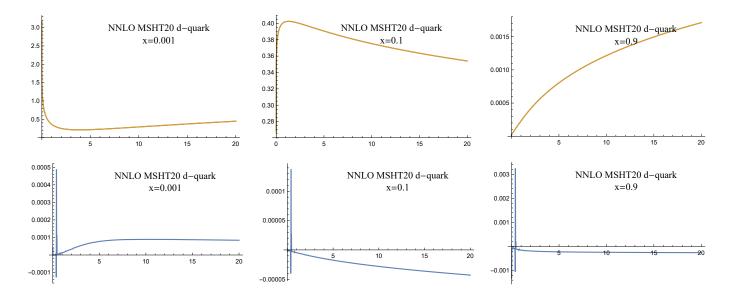


FIG. 4: Example of convolution (vs.b). Upper row is the convolution. Lower row is the ratio of extraction vs. computation. The peak in vicinity  $b \sim 0.4$  is the quark threshold.

## Extra Notes:

• Grid is computed by parallel do (if OMP is enabled).

5. Technical notes

## Convolution

The convolution integral reads

$$I(x) = \int_{x}^{1} \frac{dz}{z} C(z) f\left(\frac{x}{z}\right) f_{NP}(x, z), \tag{8.14}$$

where the function C(z) has a general form

$$C(z) = C_0 \delta(1-z) + (C_1(z))_{\perp} + C_2(z). \tag{8.15}$$

Here the plus-distribution is undestood in the usual way

$$(C_1(z))_+ = C_1(z) - \delta(1-z) \int_0^1 dy C_1(y) dy.$$
(8.16)

In NNLO coefficient function there are only possible two (..)<sub>+</sub> terms, 1/(1-z) and  $\ln(1-z)/(1-z)$ . In order to simplify the integration we rewrite

$$I(x) = \frac{1}{x} \int_{x}^{1} dz C(z) \tilde{f}\left(\frac{x}{z}\right) f_{NP}(x, z), \qquad \tilde{f}(z) = z f(z).$$
(8.17)

Then the integral is split as

$$I(x) = \frac{1}{x} \Big\{ I_2(x) + C_0 \tilde{f}(x) f_{NP}(x, 1) + \tilde{f}(x) f_{NP}(x, 1) \int_0^x dz C_1(z) \Big\},$$
(8.18)

where

$$I_{2}(x) = \int_{x}^{1} dz \left[ C_{1}(z) \left( \tilde{f} \left( \frac{x}{z} \right) f_{NP}(x, z) - \tilde{f}(x) f_{NP}(x, 1) \right) + C_{1}(z) \tilde{f} \left( \frac{x}{z} \right) f_{NP}(x, z) \right]$$
(8.19)

Presumably, the term  $\sim C_0$  give the dominant contribution w, since it is  $\sim 1$  whereas the other terms  $\sim a_s$ . Therefore, it serves as the estimation of the integral value, with respect to which the integration convergence is calculated. The convolution integral is evaluated by the G7K15 rule adaptively with given tolerance with respect to w.

The integral I is calculated in the procedure Common\_lowScale50 and Common\_lowScale5, which is common for all twist-2 terms. The integral  $I_2$  is calculated in the iterative procedures MellinConvolutionVectorPart50 and MellinConvolutionVectorPart5, which is common for all twist-2 terms.

In the case of TMDFF we have the coefficient function with the structure  $C(z)/z^2$  (plus-distribution,  $\delta$ , etc, are multiplied by  $1/z^2$ ), and collinear function  $f(z)/z^2$ . In this case it is convenient to rewrite

$$I(x) = \int_{x}^{1} \frac{dz}{z} \frac{C(z)}{z^{2}} \frac{f\left(\frac{x}{z}\right)}{(x/z)^{2}} f_{NP}(x, z) = \frac{1}{x^{3}} \int_{x}^{1} dz C(z) \hat{f}\left(\frac{x}{z}\right) f_{NP}(x, z), \qquad \hat{f}(z) = z f(z).$$
 (8.20)

Since the common-code calculates the integral PDF-like convolution, I divide by factor  $1/x^2$  all output of the common-code.

#### Coefficient functions

The coefficient function is spit to 6 terms.

$$C_{q \leftarrow q}, \quad C_{q \leftarrow g}, \quad C_{g \leftarrow q}, \quad C_{g \leftarrow \bar{q}}, \quad C_{q \leftarrow \bar{q}}, \quad C_{q \leftarrow \bar{q}}, \quad C_{q \leftarrow q'},$$

$$(8.21)$$

where  $C_{q\leftarrow q}$  and  $C_{q\leftarrow \bar{q}}$  contain non-singlet part only. The singlet contribution is given in  $C_{q\leftarrow q'}$ . So, the convolution for a quark (e.g. q=u) reads

$$F_u = C_{q \leftarrow q} \otimes q_u + C_{q \leftarrow g} \otimes q_g + C_{q \leftarrow \bar{q}} \otimes q_{\bar{u}} + C_{q \leftarrow q'} \otimes \sum_{f \in q, \bar{q}} q_f.$$

$$(8.22)$$

For gluon

$$F_g = C_{g \leftarrow g} \otimes q_g + C_{g \leftarrow q} \otimes \sum_{f \in q, \bar{q}} q_f. \tag{8.23}$$

The kernels are split into regular, singular and  $\delta$ -parts, where singular contains  $(\ln(1-x)/(1-x))_+^n$  terms,  $\delta$  contains only  $\delta(1-x)$  terms, and regular is the rest. Singular and  $\delta$ -terms are present only for  $C_{q\leftarrow q}$  and  $C_{g\leftarrow g}$ .

The regular part is decomposed further, into singular (but integrable) terms at  $x \to 0$  and  $x \to 1$ , and the finite part. The singular terms are computed exactly, while the finite part is fitted to linear combination of several functions. The basis of fit is such that the expressions are exact for coefficients which do not contain PolyLog functions. These are NLO, leading log [at all orders], large-Nf [at all orders], and some others. The full basis for the regular part is

$$\left\{ \underbrace{\ln \bar{x}, \ln^2 \bar{x}, \ln^3 \bar{x}, \ln^4 \bar{x}, \ln^5 \bar{x}, \frac{1}{x}, \frac{\ln x}{x}, \frac{\ln^2 x}{x}, \ln x, \ln^2 x, \ln^3 x, \ln^4 x, \ln^5 x,}_{\text{singular-integrable}} \right.$$
(8.24)

$$\underbrace{1, x}_{\text{cutt}}, x \bar{x}, x \left(\frac{\ln x}{1-x} + 1\right), \frac{x \ln^2 x}{1-x}, \frac{x \ln^3 x}{1-x}, x \ln x, x \ln^2 x, x \ln^3 x, x \ln^4 x, x \bar{x} \ln x, x \bar{x} \ln^2 x, x \bar{x} \ln^3 x, x \ln^2 $

$$\bar{x} \ln \bar{x}, \bar{x} \ln^2 \bar{x}, \bar{x} \ln^3 \bar{x}, x \bar{x} \ln \bar{x}, x \bar{x} \ln^2 \bar{x}, x \bar{x} \ln^3 \bar{x}, \ln x \ln \bar{x}, x \ln x \ln \bar{x}, x \bar{x} \ln x \ln \bar{x}, \frac{\ln \bar{x} (1 - x^2 + 2 \ln x)}{1 - x}, \frac{\bar{x} (\ln x + x)}{x} \Big\}.$$

Decomposed in this basis the coefficient functions are very presice. The typical relative precision is  $10^{-8} - 10^{-10}$  for the finite part (other terms are exact). The worst presicion happen at small  $x \sim 10^{-5}$  for  $g \leftarrow g$  channel where relative precision is  $\sim 10^{-5} - 10^{-6}$ .

Similar ansatz is used for uTMDFF, with some term removed (which are sensitive to small-x region). Precision in the case of TMDFF is slightly worse  $10^{-6}-10^{-8}$ . The worst precision is for N<sup>3</sup>LO  $q \rightarrow q'$  channel, where it is  $\sim 10^{-4}-10^{-6}$ . However, it is very good precision which guaranties about 10-12 preside digits for the physical convolution.

# C. \_OPE modules (tw3)

OPE modules compute the following convolution

$$[C \times T](x) = \int [dy] C_{\text{tw3}}(y_{1,2,3}), \mathbf{L}) T(y_{1,2,3}, \mu_{\text{OPE}}), \qquad (8.25)$$

where T is a twist-three function (qgq-correlator) and

$$\mathbf{L} = \ln\left(\frac{\mu_{\text{OPE}}^2 b^2}{4e^{-2\gamma_E}}\right). \tag{8.26}$$

OPE modules are initialized automatically from the corresponding TMD module.

Twist-3 convolution is not implemented yet. All function are placeholders. The only working order is NA.

## 1. Functions

# XX=name of module (e.g. uTMDPDF, uTMDFF, etc.)

Entry	Туре	Description					
XX_OPE_Initialize(file,prefix)	subroutine	Initialize the module from INI-file. (common with tw2-part)					
XX_tw3_resetGrid()	subroutine	Force recomputation of the grid. Only if griding is ON.					
XX_OPE_tw3_testGrid()	subroutine	Run the test of grid (see sec.VIIIB4). Only if griding is ON.					
<pre>XX_OPE_tw3_SetPDFreplica(rep,h)</pre>	subroutine	Switch the PDF replica to rep(int) for hadron h (int). Recompute the grid (if griding is ON). If the new replica is as before nothing is done.					
XX_OPE_tw3_SetScaleVariation(c4	subroutine	Change the scale variation parameter $c_4$ (it enters the definition of $\mu_{\rm OPE}$ ). Recompute the grid (if griding is ON). The parameter (real)c4 is restricted to $0.1 < c_4 < 10$ .					
XX_OPE_tw3_convolution(x,b,h,G)	dp_real(-5:5)	Returns (8.25) for $(x,b)=((real)x, (real)b)$ , and hadron number (int)h. In the case of NA returns 1. If grid is computed restore from the grid. The flag $(T/F)G$ is optional. It indicates the inclusion of gluon into the result. Note, that if gluons were not included into the grid they are zero.					

## 2. Model parameters.

The OPE is fully deterministic formula, but it contains the free scale, and often one implement  $b^*$ -modification. These parameters are written in model-module. Namely:

- bSTAR(bT,x,y) = is the function used instead of b in L in eqn.(8.6).
- muOPE(bt,x,y,c4) = is the function used for  $\mu_{OPE}$ .

In both cases, the variables x and y are defined as in eqn. (8.6). The parameter  $c_4$  is the scale variation parameter.

3. Scale variation.

Not implemented yet

4. Grid

Not implemented yet

# IX. TMDS MODULE

The module TMDs joins the lower modules and performs the evaluation of various TMD distributions in the  $\zeta$ -prescription. Generally a TMD distribution is given by the expression

$$F_f(x,b;\mu,\zeta) = R_f[b,(\mu,\zeta) \to (\mu_i,\zeta_{\mu_i})]\tilde{F}_f(x,b), \tag{9.1}$$

where R is the TMD evolution kernel,  $\tilde{F}$  is a TMD distribution at low scale. The scale  $\mu_i$  is dependent on the evolution type, and could be out of use. Note, that TMDs initializes the lower modules automatically. Therefore, no special initializations should be done.

List of available commands

Command	Type	Sec.	Short description
TMDs_Initialize(file,prefix)	subrout.	-	Initialization of module. (string) file is the name of constants-file, which contains initialization information. (string)prefix is appended to file if provided.
TMDs_SetScaleVariations(c1,c3)	subrout.	IXD	Set new values for the scale-variation constants.
uTMDPDF_5(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD PDF (gluon term undefined)
uTMDPDF_50(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD PDF (gluon term defined)
uTMDFF_5(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF (gluon term undefined)
uTMDFF_50(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF (gluon term defined)
lpTMDPDF_50(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Linearly polarized gluon TMD PDF (quarks are zero)
SiversTMDPDF_5(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Sivers TMD PDF (gluon term undefined)
SiversTMDPDF_50(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	Sivers TMD PDF (gluon term defined)
wgtTMDPDF_5(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	worm-gear T TMD PDF (gluon term undefined)
wgtTMDPDF_50(x,b,mu,zeta,h)	(real*8(-5:5))	IXB	worm-gear T TMD PDF (gluon term defined)
uTMDPDF_5(x,b,h)	(real*8(-5:5))	IXB	Unpolarized TMD PDF at optimal line (gluon term undefined)
uTMDPDF_50(x,b,,h)	(real*8(-5:5))	IXB	Unpolarized TMD PDF at optimal line (gluon term defined)
uTMDFF_5(x,b,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF at optimal line(gluon term undefined)
uTMDFF_50(x,b,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF at optimal line (gluon term defined)
lpTMDPDF_50(x,b,,h)	(real*8(-5:5))	IXB	Linearly polarized gluon TMD PDF at optimal line (quarks are zero)
SiversTMDPDF_5(x,b,h)	(real*8(-5:5))	IXB	Sivers TMD PDF at optimal line (gluon term undefined)
SiversTMDPDF_50(x,b,,h)	(real*8(-5:5))	IXB	Sivers TMD PDF at optimal line (gluon term defined)
wgtTMDPDF_5(x,b,h)	(real*8(-5:5))	IXB	Worm gear T TMD PDF at optimal line (gluon term undefined)
wgtTMDPDF_50(x,b,,h)	(real*8(-5:5))	IXB	Worm gear T TMD PDF at optimal line (gluon term defined)
uPDF_uPDF(x1,x2,b,mu,zeta,h1,h2)	(real*8(-5:5))	IXC	Product of Unpolarized TMD PDF $f_{q \leftarrow h_1}(x_1) f_{\bar{q} \leftarrow h_1}$ at the same scale (gluon term undefined)
uPDF_anti_uPDF(x1,x2,b,mu,zeta,h1,h2)	(real*8(-5:5))	IXC	Product of Unpolarized TMD PDF $f_{q \leftarrow h_1}(x_1) f_{q \leftarrow h_1}$ at the same scale (gluon term undefined)

# List of functions which must be provided by a model code

Input	Short description
mu_LOW(b)	The value of $\mu_i$ used in the evolutions of type 1 and 2 (improved $\mathcal{D}$ and $\gamma$ ). See [?].
muO(b)	The value of $\mu_0$ used in the evolution of type 1 (improved $\mathcal{D}$ ). See [?].

#### A. Definition of low-scales

The low scales  $\mu_i$  and  $\mu_0$  are defined in the functions mu\_LOW(bt) and mu0(bt) which can be found in the end of TMDs.f90 code. Modify it if needed.

# B. Evaluating TMDs

The expression for unpolarized TMD PDF is obtained by the functions  $(real*8(-5:5))uTMDPDF_5(x,b,mu,zeta,h)$  where

- x (real\*8) Bjorken- x (0 < x < 1)
- b (real\*8) Transverse distance (b > 0) in GeV
- mu (real\*8) The scale  $\mu_f$  in GeV. Typically,  $\mu_f = Q$ .
- zeta (real\*8) The scale  $\zeta_f$  in GeV<sup>2</sup>. Typically,  $\zeta_f = Q^2$ .
  - h (integer) The hadron type.

This function return the vector real\*8(-5:5) for  $\bar{b}, \bar{c}, \bar{s}, \bar{u}, \bar{d}, ?, d, u, s, c, b$ .

- Gluon contribution in uTMDPDF\_5 is undefined, but taken into account in the mixing contribution. The point is that evaluation of gluons slow down the procedure approximately by 40%, and often is not needed. To calculate the full flavor vector with the gluon TMD, call uTMDPDF\_50(x,b,mu,zeta,h), where all arguments defined in the same way.
- The other TMDs, such as unpolarized TMDFF, transversity, etc. are obtained by similar function see the table in the beginning of the section.
- Each function has version without parameters mu and zeta. It corresponds to the evaluation of a TMS at optimal line [?]. Practically, it just transfers the outcome of corresponding TMD module, e.g.module uTMDPDF, see sec.??.

# C. Products of TMDs

The the evaluation of majority of cross-sections one needs the product of two TMDs at the same scale. There are set of functions which return these products. They are slightly faster then just evaluation and multiplication, due to the flavor blindness of the TMD evolution. The function have common interface

```
(real*8(-5:5)) uPDF_uPDF(x1,x2,b,mu,zeta,h1,h2) where
```

- x1,x2 (real\*8) Bjorken-x's (0 < x < 1)
  - b (real\*8) Transverse distance (b > 0) in GeV
  - mu (real\*8) The scale  $\mu_f$  in GeV. Typically,  $\mu_f = Q$ .
- zeta (real\*8) The scale  $\zeta_f$  in GeV<sup>2</sup>. Typically,  $\zeta_f = Q^2$ .
- h1,h2 (integer) The hadron's types.

The function return a product of the form  $F_{f_1 \leftarrow h_1}(x_1, b; \mu, \zeta) F_{f_2 \leftarrow h_2}(x_2, b; \mu, \zeta)$ , where  $f_{1,2}$  and the type of TMDs depend on the function.

# D. Theoretical uncertainties

TMDs\_SetScaleVariations(c1,c3,c4) changes the scale multiplicative factors  $c_i$  (see [?], sec.6). The default set of arguments is (1,1,1), i.e. the scales as they given in corresponding functions. This subroutine changes c1 and c3 constants and call corresponding subroutines for variation of c4 in TMD defining packages. Note, that in some types of evolution particular variations absent.

#### X. TMDF MODULE

This module evaluates the structure functions, that are universally defined as

$$F(Q^2, q_T, x_1, x_2, \mu, \zeta_1, \zeta_2) = \int_0^\infty \frac{bdb}{2} b^n J_n(bq_T) \sum_{ff'} z_{ff'}(Q^2) F_1^f(x_1, b; \mu, \zeta_1) F_2^{f'}(x_2, b; \mu, \zeta_2), \tag{10.1}$$

where

- $Q^2$  is hard scale.
- $q_T$  is transverse momentum in the factorization frame. It coincides with measured  $q_T$  in center-mass frame for DY, but  $q_T \sim p_T/z$  for SIDIS.
- $x_1$  and  $x_2$  are parts of collinear parton momenta. I.e. for DY  $x_{1,2} \simeq Qe^{\pm y}/\sqrt{s}$ , while for SIDIS  $x_2 \sim z$ . It can also obtain power correction, ala Nachmann variables.
- $\mu$  is the hard factorization scale  $\mu \sim Q$
- $\zeta_{1,2}$  are rapidity factorization scales. In the standard factorization scheme  $\zeta_1\zeta_2=Q^4$ . It can also be modified by power corrections.
- f, f' are parton flavors.
- $z_{ff'}$  is the process related function. E.g. for photon DY on  $p + \bar{p}$ ,  $z_{ff'} = \delta_{ff'} |e_f|^2$ .
- n The order of Bessel transformation is defined by structure function. E.g. for unpolarized DY n=1. For SSA's n=1. In general for angular modulation  $\sim \cos(n\theta)$ .
- $F_{1,2}^f$  TMD distribution (PDF or FF) of necessary polarization and flavor.

Some structure functions are multiplied by a constant with mass dimension (e.g. Sivers asymmetry). This constant (called global mass scale = M) is defined globally in the constants file.

<u>List of available commands</u> Command Type Sec. Short description TMDF\_Initialize(file, prefix) ХА Initialization of module. (string) file is the name subrout. of constants-file, which contains initialization information. (string)prefix is appended to file if provided. TMDF\_ShowStatistic()) Print current statistic on the number of calls.  $\operatorname{subrout}.$ TMDF\_ResetCounters() subrout. Reset intrinsic counters. E.g. release convergence ISlost state. TMDF\_F(Q2,qT,x1,x2,mu,zeta1,zeta2,N) (real\*8)ΧВ Evaluates the structure function

#### A. Initialization

Prior the usage module is to be initialized (once per run) by call TMDF\_Initialize(file)

It reads constants-file and initialize it-self accordingly.

# B. Evaluating Structure functions

The value of the structure function is obtained by (real\*8)TMDF\_F(Q2,qT,x1,x2,mu,zeta1,zeta2,N) where

 $Q2 \text{ (real*8) hard scale in GeV}^2$ .

qT (real\*8) modulus of transverse momentum in the factorization frame in GeV,  $q_T > 0$ 

x1 (real\*8) x passed to the first TMD distribution (0 < x1 < 1)

x2 (real\*8) x passed to the first TMD distribution (0 < x2 < 1)

mu (real\*8) The hard scale  $\mu$  in GeV. Typically,  $\mu = Q$ .

zeta1 (real\*8) The scale  $\zeta_f$  in GeV<sup>2</sup> for the first TMD distribution. Typically,  $\zeta_f = Q^2$ .

zeta2 (real\*8) The scale  $\zeta_f$  in GeV<sup>2</sup> for the second TMD distribution. Typically,  $\zeta_f = Q^2$ .

N (integer) The number of process.

The function returns the value of

$$F^{N}(Q^{2}, q_{T}, x_{1}, x_{2}, \mu, \zeta_{1}, \zeta_{2}) = \int_{0}^{\infty} \frac{bdb}{2} b^{n} J_{n}(bq_{T}) \sum_{ff'} z_{ff'}^{N}(Q^{2}) F_{1}^{f}(x_{1}, b; \mu, \zeta_{1}) F_{2}^{f'}(x_{2}, b; \mu, \zeta_{2}).$$
(10.2)

The parameter n depends on the argument N and uniformly defined as

$$\begin{array}{ll} n=0 & \text{ for } \mathbb{N} < 10000 \\ n=1 & \text{ for } \mathbb{N} \in [10000, 20000] \\ n=2 & \text{ for } \mathbb{N} \in [20000, 30000] \\ n=3 & \text{ for } \mathbb{N} > 30000 \end{array}$$

The particular values of  $z_{ff'}$  and  $F_{1,2}$  are given in the following table. User function can be implemented by code modification.

#### Notes on the integral evaluation:

- The integral is uniformly set to 0 for  $q_T < 10^{-7}$ .
- The integrand is uniformly set to 0 for  $b > 10^3$ .
- If for any element of evaluation (including TMD evolution factors and convolution integrals, and the integral of the structure function it-self) obtained divergent value. The trigger is set to ON. In this case, the integral returns uniformly large value 10<sup>100</sup> for all integrals without evaluation. The trigger is reset by new values of NP parameters. It is done in order to cut the improper values of NP parameters in the fastest possible way, which speed up fitting procedures.
- The Fourier is made by Ogata quadrature, which is double exponential quadrature. I.e.

$$\int_0^\infty \frac{bdb}{2} b^n I(b) J_n(q_T b) \simeq \frac{1}{q_T^{n+2}} \sum_{k=1}^\infty \tilde{\omega}_{nk} b_{nk}^{n+1} I\left(\frac{b_{nk}}{q_T}\right), \tag{10.3}$$

where

$$b_{nk} = \frac{\psi(\tilde{h}\tilde{\xi}_{nk})}{\tilde{h}} = \tilde{\xi}_{nk} \tanh(\frac{\pi}{2}\sinh(\tilde{h}\tilde{\xi}_{nk}))$$

$$\tilde{\omega}_{nk} = \frac{J_n(\tilde{b}_{nk})}{\tilde{\xi}_{nk}J_{n+1}^2(\tilde{\xi}_{nk})} \psi'(\tilde{h}\tilde{\xi}_{nk})$$

Here,  $\tilde{\xi}_{nk}$  is k'th zero of  $J_n(x)$  function. Note, that  $\tilde{h} = h/\pi$  in the original Ogata's notation.

- The convergence properties of the quadrature essentially depends on h. I have found that  $h \sim q_T$ . For accurate evolution of integrals at different values of  $q_T$  I set  $h = h_0 s$ , where s is defined for intervals of  $q_T$ .
- The sum over k is restricted by  $N_{\text{max}}$  where  $N_{\text{max}}$  is hard coded number,  $N_{\text{max}} = 200$ .

• The sum over k is evaluated until the sum of absolute values of last four terms is less than tolerance. If  $M > N_{\text{max}}$  the integral declared divergent, and the trigger is set to ON.

# WARNING!

The error for Ogata quadrature is defined by parameters h and M(number of terms in the sum over k). In the parameter M quadrature is double-exponential, i.e. converges fast as M approaches  $N_{\rm max}$ . And the convergence of the sum can be simply checked. In the parameter h the quadrature is quadratic (the convergence is rather poor). The convergence to the true value of integral is very expensive especially at large  $q_T$  (it requires the complete reevaluation of integral at all nodes). Unfortunately,  $N_{\rm max} \sim h^{-1}$ , and has to find the balance value for h. In principle, TMD functions decays rather fast, and suggested default value h=0.005 is trustful. Nonetheless, we suggest to test other values (\*/2) of h to validate the obtained values in your model.

The adaptive check of convergence will implemented in the future versions.

#### C. Enumeration of structure functions

List of enumeration of structures functions N < 10000

N	$z_{ff'}$	$F_1$	$F_2$	Short description	Gluon req.
0					
9999	_	_	_	Test cases (see X D)	no
9998					
1	$\delta_{ar{f}f'} e_f ^2$	$f_1$	$f_1$	$(\mathrm{unpol.})p + p \to \gamma$	no
2	$\delta_{ff'} e_f ^2$	$f_1$	$f_1$	$(\mathrm{unpol.})p + \bar{p} \to \gamma$	no
3	$\delta_{\bar{f}f'} \frac{(1-2 ef s_w^2)^2 - 4e_f^2 s_w^4}{8s_w^2 c_w^2}$	$f_1$	$f_1$	$(\mathrm{unpol.})p + p \to Z$	no
4	$\delta_{ff'} \frac{(1-2 ef s_w^2)^2 - 4e_f^2 s_w^4}{8s_w^2 c_w^2}$	$f_1$	$f_1$	$(\mathrm{unpol.})p + \bar{p} \to Z$	no
5	$\delta_{\bar{f}f'} \frac{z_{ll'}z_{ff'}}{\alpha_{\rm em}^2}$ given in (2.8) of [?]	$f_1$	$f_1$	$(\text{unpol.})p + p \to Z + \gamma$	no
6	$\delta_{ff'} \frac{z_{ll'} z_{ff'}}{\alpha_{\rm em}^2}$ given in (2.8) of [?]	$f_1$	$f_1$	$(\text{unpol.})p + \bar{p} \to Z + \gamma$	no
7	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + p \to W^+$	no
8	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + p \to W^-$	no
9	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + p \to W^{\pm}$	no
10	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + \bar{p} \to W^+$	no
11	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + \bar{p} \to W^-$	no

					n
12	$\frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$f_1$	$f_1$	$(\text{unpol.})p + \bar{p} \to W^{\pm}$	no
13	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	$(\text{unpol.})p + p \to W^+$ (for narrow-width approx.)	no
14	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	(unpol.) $p + p \rightarrow W^-$ (for narrow-width approx.)	no
15	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	(unpol.) $p + p \to W^{\pm}$ (for narrow-width approx.)	no
16	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	(unpol.) $p + \bar{p} \to W^+$ (for narrow-width approx.)	no
17	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	(unpol.) $p + \bar{p} \to W^-$ (for narrow-width approx.)	no
18	$\frac{ V_{ff'} ^2}{4s_w^2}$	$f_1$	$f_1$	(unpol.) $p + \bar{p} \to W^{\pm}$ (for narrow-width approx.)	no
20	$f_g(x_1)f_g(x_2) + h_1^{\perp}(x_1)h_1^{\perp}(x_2)$	-	-	$(\text{unpol.})h + h \to H$ Elementary Higgs production	yes
21	$f_g(x_1)f_g(x_2)$	$f_1$	$f_1$		yes
22	$h_{1g}^{\perp}(x_1)h_{1g}^{\perp}(x_2)$	$h_1^\perp$	$h_1^\perp$		yes
101	$\delta_{ar{f}f'} e_f ^2$	$f_1^h$	$f_1$	(unpol.) $h + p \rightarrow \gamma$ (with $h = 2$ )	no
102	$\delta_{ff'} e_f ^2$	$f_1^h$	$f_1$	$(\text{unpol.})h + \bar{p} \to \gamma(\text{with } h = 2)$	no
103	$\delta_{ff'} e_f ^2$	$f_1^h$	$f_1$	(unpol.) $\bar{h} + p \rightarrow \gamma$ (with $h = 2$ ). Note, that it is equal 102	no
104	$\delta_{ar{f}f'} e_f ^2$	$f_1^h$	$f_1$	(unpol.) $\bar{h} + \bar{p} \rightarrow \gamma$ (with $h = 2$ ). Note, that it is equal 101	no
1001	$R_{\bar{f}f'}^{Cu}e_fe_{f'}$ see (3.1) of [?]	$f_1$	$f_1^{Cu}$	$\begin{array}{c} (\text{unpol.})p + Cu \to \gamma \text{ (roughly simulates isostructure of Cu, used to describe E288 experiment in } \\ [?\ ]) \end{array}$	no
1002	$R_{\bar{f}f'}^{2H}e_fe_{f'}$ see (3.1) of [?] with $Z=1$ and $A=2$	$f_1$	$f_1^{^2H}$	(unpol.) $p +^2 H \to \gamma$ (roughly simulates isostructure of $^2H$ , used to describe E772 experiment)	no
1003	$R_{ff'}^W e_f e_{f'}$ see (3.1) of [?] with $Z=74$ and $A=183$	$f_1$	$f_1^W$	$\begin{array}{c} (\text{unpol.})\bar{p}+W\to\gamma \text{ (roughly simulates isostructure of }W(\text{tungsten}), \text{ used to describe E537}\\ \text{experiment)} \end{array}$	no
1004	$R_{\bar{f}f'}^W e_f e_{f'}$ see (3.1) of [?] with $Z=74$ and $A=183$	$f_1$	$f_1^W$	(unpol.) $h+W\to\gamma$ , where $h$ is hadron 2 (roughly simulates isostructure of $\pi^-+W(\text{tungsten})$ , used to describe E537 experiment)	no
2001	$\delta_{ff'} e_f ^2$	$f_1^p$	$d_1^{h_1}$	$(\mathrm{unpol})p + \gamma \to h_1$	no
200N	$\delta_{ff'} e_f ^2$	$f_1^p$	$d_1^{h_N}$	(unpol) $p + \gamma \rightarrow h_N$ , for $N = \{1,, 9\}$ (including case 2001)	no

2011	$\delta_{ff'} e_f ^2$	$f_1^d$	$d_1^{h_1}$	$(\text{unpol})d + \gamma \rightarrow h_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
201N	$\delta_{ff'} e_f ^2$	$f_1^d$	$d_1^{h_N}$	(unpol) $d + \gamma \to h_N$ , for $N = \{1,, 9\}$ (including case 2011). Here, d is isoscalar target $(p+n)/2$ .	no
2021	$\delta_{far{f}'} e_f ^2$	$f_1^p$	$d_1^{\bar{h}_1}$	$(\mathrm{unpol})p + \gamma  o ar{h}_1$	no
202N	$\delta_{far{f}'} e_f ^2$	$f_1^p$	$d_1^{ar{h}_N}$	(unpol) $p + \gamma \rightarrow \bar{h}_N$ , for $N = \{1,, 9\}$ (including case 2021)	no
2031	$\delta_{far{f}'} e_f ^2$	$f_1^d$	$d_1^{\bar{h}_1}$	$(\text{unpol})d + \gamma \rightarrow \bar{h}_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
203N	$\delta_{f\bar{f}'} e_f ^2$	$f_1^d$	$d_1^{ar{h}_N}$	(unpol) $d + \gamma \to \bar{h}_N$ , for $N = \{1,, 9\}$ (including case 2031). Here, d is isoscalar target $(p+n)/2$ .	no
204N	$\delta_{ff'} e_f ^2$	$f_1^n$	$d_1^{h_N}$	(unpol) $n + \gamma \to h_N$ , for $N = \{1,, 9\}$ . n is neutron target $n = p(u \leftrightarrow d)$	no
205N	$\delta_{ff'} e_f ^2$	$f_1^n$	$d_1^{h_N}$	$(\text{unpol})n + \gamma \to \bar{h}_N, \text{ for } N = \{1,, 9\}. \text{ n is neutron target } n = p(u \leftrightarrow d).$	no
2101	$\delta_{ff'} e_f ^2$	$f_1^p$	$d_1^{h_{1+2}}$	(unpol) $p + \gamma \to h_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
2102	$\delta_{ff'} e_f ^2$	$f_1^p$	$d_1^{h_{1+2+3}}$	(unpol) $p+\gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3}=h_1+h_2+h_3$	no
2103	$\delta_{ff'} e_f ^2$	$f_1^d$	$d_1^{h_{1+2}}$	(unpol) $d + \gamma \to h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
2104	$\delta_{ff'} e_f ^2$	$f_1^d$	$d_1^{h_{1+2+3}}$	(unpol) $d+\gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no
2105	$\delta_{ff'} e_f ^2$	$f_1^n$	$d_1^{h_{1+2}}$	(unpol) $n + \gamma \to h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
2106	$\delta_{ff'} e_f ^2$	$f_1^n$	$d_1^{h_{1+2+3}}$	(unpol) $n+\gamma \to h_{1+2+3}$ , where $h_{1+2+3}=h_1+h_2+h_3$ and n is neutron target $n=p(u \leftrightarrow d)$ .	no
2111	$\delta_{far{f}'} e_f ^2$	$f_1^p$	$d_1^{h_{1+2}}$	(unpol) $p + \gamma \to \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
2112	$\delta_{far{f}'} e_f ^2$	$f_1^p$	$d_1^{h_{1+2+3}}$	(unpol) $p+\gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3}=h_1+h_2+h_3$	no
2113	$\delta_{f\bar{f}'} e_f ^2$	$f_1^d$	$d_1^{h_{1+2}}$	(unpol) $d + \gamma \to \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
2114	$\delta_{far{f}'} e_f ^2$	$f_1^d$	$d_1^{h_{1+2+3}}$	(unpol) $d+\gamma \to \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no

2115	$\delta_{far{f}'} e_f ^2$	$f_1^n$		(unpol) $n + \gamma \to \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
2116	$\delta_{far{f}'} e_f ^2$	$f_1^n$	$d_1^{h_{1+2+3}}$	$ \begin{array}{l} (\text{unpol})n+\gamma \to \bar{h}_{1+2+3}, \text{ where } h_{1+2+3} = h_1 + h_2 + \\ h_3 \text{ and n is neutron target } n = p(u \leftrightarrow d). \end{array} $	no

# $10000{\leqslant}{\tt N}{<}20000$

N	$z_{ff'}$	$F_1$	$F_2$	Short description	Gluon req.
10000 19999 19998	_	_	_	Test cases (see X D)	no
10001	$-M\delta_{\bar{f}f'} e_f ^2$	$-(f_{1T}^{\perp})^p$	$f_1$	$(\text{Sivers})p^{\uparrow} + p \to \gamma$	no
10005	$-M\delta_{\bar{f}f'}\frac{z_{ll'}z_{ff'}}{\alpha_{\rm em}^2}$ given in (2.8) of [?]	$-(f_{1T}^{\perp})^p$	$f_1$	$(Sivers)p^{\uparrow} + p \to Z + \gamma$	no
10007	$-M\frac{1}{4s_w^2}\frac{ V_{ff'} ^2}{4s_w^2}\frac{Q^4}{(Q^2-M_W^2)^2+\Gamma_W^2M_W^2}$	$-(f_{1T}^{\perp})^p$	$f_1$	$(\text{Sivers})p^{\uparrow} + p \to W^{+}$	no
10008	$-M\frac{1}{4s_w^2}\frac{ V_{ff'} ^2}{4s_w^2}\frac{Q^4}{(Q^2-M_W^2)^2+\Gamma_W^2M_W^2}$	$-(f_{1T}^{\perp})^p$	$f_1$	$(\text{Sivers})p^{\uparrow} + p \to W^{-}$	no
10101	$+M\delta_{ar{f}f'} e_f ^2$	$f_1^h$	$-(f_{1T}^{\perp})^p$	(Sivers) $h + p^{\uparrow} \to \gamma$ (with $h = 2$ )	no
10102	$+M\delta_{ff'} e_f ^2$	$f_1^h$	$-(f_{1T}^{\perp})^{\bar{p}}$	$(\text{Sivers})h + \bar{p}^{\uparrow} \to \gamma(\text{with } h = 2)$	no
10103	$+M\delta_{ff'} e_f ^2$	$f_1^h$	$-(f_{1T}^{\perp})^p$	(Sivers) $\bar{h} + p^{\uparrow} \rightarrow \gamma$ (with $h = 2$ ). Note, that it is equal 10102	no
10104	$+M\delta_{ar{f}f'} e_f ^2$	$f_1^h$	$-(f_{1T}^\perp)^{\bar p}$	(Sivers) $\bar{h} + \bar{p}^{\uparrow} \rightarrow \gamma$ (with $h = 2$ ). Note, that it is equal 10101	no
12001	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_1}$	$(\text{Sivers})p^{\uparrow} + \gamma \to h_1$	no
1200N	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_N}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow h_N$ , for $N = \{1,, 9\}$ (including case 12001)	no
12011	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_1}$	(Sivers) $d^{\uparrow} + \gamma \to h_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
1201N	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_N}$	(Sivers) $d^{\uparrow} + \gamma \to h_N$ , for $N = \{1,, 9\}$ (including case 12011). Here, d is isoscalar target $(p+n)/2$ .	no
12021	$-M\delta_{far{f'}} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{ar{h}_1}$	$(\mathrm{Sivers})p^{\uparrow} + \gamma \to \bar{h}_1$	no
1202N	$-M\delta_{far{f}'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{ar{h}_N}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow \bar{h}_N$ , for $N = \{1,, 9\}$ (including case 12021)	no

			1		
12031	$-M\delta_{far{f'}} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{\bar{h}_1}$	(Sivers) $d^{\uparrow} + \gamma \rightarrow \bar{h}_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
1203N	$-M\delta_{far{f'}} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{ar{h}_N}$	(Sivers) $d^{\uparrow} + \gamma \to \bar{h}_N$ , for $N = \{1,, 9\}$ (including case 12031). Here, d is isoscalar target $(p+n)/2$ .	no
1204N	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_N}$	(Sivers) $n^{\uparrow} + \gamma \to h_N$ , for $N = \{1,, 9\}$ , n is neutron target $n = p(u \leftrightarrow d)$ .	no
1205N	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{ar{h}_N}$	(Sivers) $n^{\uparrow} + \gamma \to \bar{h}_N$ , for $N = \{1,, 9\}$ , n is neutron target $n = p(u \leftrightarrow d)$ .	no
12101	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_{1+2}}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow h_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
12102	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_{1+2+3}}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$	no
12103	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_{1+2}}$	(Sivers) $d^{\uparrow} + \gamma \to h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
12104	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_{1+2+3}}$	(Sivers) $d^{\uparrow} + \gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no
12105	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^n$	$d_1^{h_{1+2}}$	(Sivers) $n^{\uparrow} + \gamma \rightarrow h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
12106	$-M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^n$	$d_1^{h_{1+2+3}}$	(Sivers) $n^{\uparrow} + \gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
12111	$-M\delta_{f\bar{f'}} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_{1+2}}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
12112	$-M\delta_{far{f}'} e_f ^2$	$(f_{1T}^{\perp})^p$	$d_1^{h_{1+2+3}}$	(Sivers) $p^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$	no
12113	$-M\delta_{far{f}'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_{1+2}}$	(Sivers) $d^{\uparrow} + \gamma \to \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
12114	$-M\delta_{far{f}'} e_f ^2$	$(f_{1T}^{\perp})^d$	$d_1^{h_{1+2+3}}$	(Sivers)) $d^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no
12115	$-M\delta_{f\bar{f'}} e_f ^2$	$(f_{1T}^{\perp})^n$	$d_1^{h_{1+2}}$	(Sivers) $n^{\uparrow} + \gamma \to \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
12116	$-M\delta_{far{f}'} e_f ^2$	$(f_{1T}^{\perp})^n$	$d_1^{h_{1+2+3}}$	(Sivers) $n^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
	$\downarrow\downarrow\downarrow\downarrow$ Enumeration for $I$	$F_{LT}$ in SI	DIS is sa	me as for $F_{UT}$ with $(12 \rightarrow 13) \downarrow \downarrow \downarrow$	
13001	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^\perp)^p$	$d_1^{h_1}$	$(\mathrm{wgt})p^{\uparrow} + \gamma \to h_1$	no
1300N	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{h_N}$	$(\text{wgt})p^{\uparrow} + \gamma \rightarrow h_N$ , for $N = \{1,, 9\}$ (including case 12001)	no

13011	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_1}$	$(\text{wgt})d^{\uparrow} + \gamma \rightarrow h_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
1301N	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_N}$	(wgt) $d^{\uparrow} + \gamma \rightarrow h_N$ , for $N = \{1,, 9\}$ (including case 12011). Here, d is isoscalar target $(p+n)/2$ .	no
13021	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{\bar{h}_1}$	$(\text{wgt})p^{\uparrow} + \gamma \to \bar{h}_1$	no
1302N	$+M\delta_{far{f'}} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{ar{h}_N}$	$\begin{array}{ c c c c c c }\hline (\text{wgt})p^{\uparrow} + \gamma \to \bar{h}_N, \text{ for } N = \{1,,9\} \text{ (including case 12021)} \end{array}$	no
13031	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{\bar{h}_1}$	$(\text{wgt})d^{\uparrow} + \gamma \rightarrow \bar{h}_1$ . Here, d is isoscalar target $(p+n)/2$ .	no
1303N	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{ar{h}_N}$	(wgt) $d^{\uparrow} + \gamma \rightarrow \bar{h}_N$ , for $N = \{1,, 9\}$ (including case 12031). Here, d is isoscalar target $(p+n)/2$ .	no
1304N	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_N}$	$(\text{wgt})n^{\uparrow} + \gamma \to h_N$ , for $N = \{1,, 9\}$ , n is neutron target $n = p(u \leftrightarrow d)$ .	no
1305N	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{ar{h}_N}$	$(\text{wgt})n^{\uparrow} + \gamma \to \bar{h}_N$ , for $N = \{1,, 9\}$ , n is neutron target $n = p(u \leftrightarrow d)$ .	no
13101	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{h_{1+2}}$	$(\text{wgt})p^{\uparrow} + \gamma \rightarrow h_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
13102	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{h_{1+2+3}}$	$(\text{wgt})p^{\uparrow} + \gamma \to h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$	no
13103	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_{1+2}}$	$(\text{wgt})d^{\uparrow} + \gamma \rightarrow h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
13104	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_{1+2+3}}$	(wgt) $d^{\uparrow} + \gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no
13105	$+M\delta_{ff'} e_f ^2$	$(g_{1T}^{\perp})^n$	$d_1^{h_{1+2}}$	$(\text{wgt})n^{\uparrow} + \gamma \to h_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
13106	$+M\delta_{ff'} e_f ^2$	$(f_{1T}^{\perp})^n$	$d_1^{h_{1+2+3}}$	(wgt) $n^{\uparrow} + \gamma \rightarrow h_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
13111	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{h_{1+2}}$	$(\text{wgt})p^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$	no
13112	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^p$	$d_1^{h_{1+2+3}}$	(wgt) $p^{\uparrow} + \gamma \to \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$	no
13113	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_{1+2}}$	$(\text{wgt})d^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and d is isoscalar target $(p+n)/2$ .	no
13114	$+M\delta_{f\bar{f'}} e_f ^2$	$(g_{1T}^{\perp})^d$	$d_1^{h_{1+2+3}}$	$(\text{wgt})d^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and d is isoscalar target $(p+n)/2$ .	no

13115	$+M\delta_{far{f}'} e_f ^2$	$(g_{1T}^{\perp})^n$	$d_1^{h_{1+2}}$	(wgt) $n^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2}$ , where $h_{1+2} = h_1 + h_2$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
13116	$+M\delta_{far{f'}} e_f ^2$	$(g_{1T}^{\perp})^n$	$d_1^{h_{1+2+3}}$	(wgt) $n^{\uparrow} + \gamma \rightarrow \bar{h}_{1+2+3}$ , where $h_{1+2+3} = h_1 + h_2 + h_3$ and n is neutron target $n = p(u \leftrightarrow d)$ .	no
13200	$+M\delta_{\bar{f}f'}\frac{\bar{z}_{ll'}z_{ff'}}{\alpha_{\rm em}^2}$ given in (2.8) of [?]	$(g_{1T}^{\perp})^p$	$(-1)^f f_1$	$G^1_{TU}$ cross-section in $p^{\uparrow} + p \rightarrow Z + \gamma$	no
13201	$+M\frac{1}{4s_w^2}\frac{ V_{ff'} ^2}{4s_w^2}\frac{Q^4}{(Q^2-M_W^2)^2+\Gamma_W^2M_W^2}$	$(g_{1T}^{\perp})^p$	$(-1)^f f_1$	$G_{TU}^1$ cross-section in $p^{\uparrow} + p \to W^+$	no
П	$+ M \frac{1}{4s_w^2} \frac{ V_{ff'} ^2}{4s_w^2} \frac{Q^4}{(Q^2 - M_W^2)^2 + \Gamma_W^2 M_W^2}$	$(g_{1T}^{\perp})^p$	$(-1)^f f_1$	$G^1_{TU}$ cross-section in $p^{\uparrow} + p \to W^-$	no

# $20000 \le N < 30000$

N	$z_{ff'}$	$F_1$	$F_2$	Short description	Gluon req.
20000					
29999	_	_	_	Test cases (see X D)	no
29998					

# 30000≤N

N	$z_{ff'}$	$F_1$	$F_2$	Short description	Gluon req.
30000					
39999	_	_	_	Test cases (see X D)	no
39998					

Notes on parameters and notation:  $s_w^2,\,M_Z,\,\Gamma_Z,\,{\rm etc.}$  are defined in constants  $f_1$ -unpolarized TMDPDF

 $d_1$ -unpolarized TMDFF

 $f_{1T}^{\perp}$ -Sivers function

 $g_{1T}^{\perp}$ -wgt-function (-1)<sup>f</sup> is (+1) for f=quark, and (-1) for f=anti-quark.

Everywhere proton is expected to be hadron number 1.

# D. Tests

The test options are called by process number N + 0, N + 9999 and N + 9998. In these case, the integrand set by a fixed function. In the case N+0

$$N + 0: \sum zFF \to e^{-0.2b}.$$
 (10.4)

The cases N + 9999 and N + 9998 are dependent on parameters of the function:

$$N + 9999: \sum zFF \to e^{-\mu b} (1 + x_1 b^2 + x_2 b^4),$$
 (10.5)

$$N + 9998: \sum zFF \to e^{-\mu b^2} (1 + x_1 b^2 + x_2 b^4).$$
 (10.6)

In all cases the Hankel integral could be evaluated. They read

9999: 
$$F = \frac{1}{2\mu^2 (1+X)^{3/2}} \left( 1 + \frac{x_1}{\mu^2} \frac{6-9X}{(1+X)^2} + \frac{15x_2}{\mu^4} \frac{8-40X+15X^2}{(1+X)^4} \right), \tag{10.7}$$

1999: 
$$F = \frac{3\sqrt{X}}{2\mu^3 (1+X)^{5/2}} \left( 1 + \frac{5x_1}{\mu^2} \frac{4-3X}{(1+X)^2} + \frac{105x_2}{\mu^4} \frac{8-20X+5X^2}{(1+X)^4} \right), \tag{10.8}$$

$$29999: F = \frac{15X}{2\mu^4(1+X)^{7/2}} \left( 1 + \frac{21x_1}{\mu^2} \frac{2-X}{(1+X)^2} + \frac{63x_2}{\mu^4} \frac{48 - 80X + 15X^2}{(1+X)^4} \right), (10.9)$$

$$39999: F = \frac{105X^{3/2}}{2\mu^5(1+X)^{9/2}} \left( 1 + \frac{9x_1}{\mu^2} \frac{8-3X}{(1+X)^2} + \frac{495x_2}{\mu^4} \frac{16-20X+3X^2}{(1+X)^4} \right), (10.10)$$

where  $X = q_T^2/\mu^2$ .

9998: 
$$F = \frac{e^{-Y}}{4\mu} \left( 1 + \frac{x_1}{\mu} (1 - Y) + \frac{x_2}{\mu^2} (2 - 4Y + Y^2) \right), \tag{10.11}$$

19998: 
$$F = \frac{e^{-Y}\sqrt{Y}}{4\mu^{3/2}} \left( 1 + \frac{x_1}{\mu} (2 - Y) + \frac{x_2}{\mu^2} (6 - 6Y + Y^2) \right), \tag{10.12}$$

29998: 
$$F = \frac{e^{-Y}Y}{4\mu^2} \left( 1 + \frac{x_1}{\mu} (3 - Y) + \frac{x_2}{\mu^2} (12 - 8Y + Y^2) \right), \tag{10.13}$$

39998: 
$$F = \frac{e^{-Y}Y^{3/2}}{4\mu^{5/2}} \left( 1 + \frac{x_1}{\mu} (4 - Y) + \frac{x_2}{\mu^2} (20 - 10Y + Y^2) \right), \tag{10.14}$$

where  $Y = q_T^2/(4\mu)$ .

# XI. TMDX\_DY MODULE

This module evaluates cross-sections with the Drell-Yan-like kinematics. I.e. it expects the following kinematic input, (s, Q, y) which defines the variables x's, etc.

The general structure of the cross-section is

$$\Delta\sigma(q_T) = \int_{bin} dX \ prefactor 2 \times F, \tag{11.1}$$

where

$$dX = dQ^2 dy dq_T^2$$
.

So, for a small bin

$$\Delta\sigma(q_T) \approx \Delta X \frac{d\sigma}{dX}, \qquad \Delta X = (Q_{\text{max}}^2 - Q_{\text{min}}^2)(y_{\text{max}} - y_{\text{min}})(q_{T_{\text{max}}}^2 - q_{T_{\text{min}}}^2). \tag{11.2}$$

Prefactor2 accumulates the definition of the phase-space, process and cross-section. Generally, the prefactor2  $\times F$  is

where F is defined in (10.1) or (14.1). There are following feature of current implementation

• In the current version the scaling variables are set as

$$\mu^2 = \zeta_1 = \zeta_2 = Q^2. \tag{11.4}$$

Currently, it is hard coded and could not be easily modified. However, there is a possibility to vary the value of  $\mu$  as  $\mu = c_2 Q$ , where  $c_2$  is variation parameter (see sec.XIE).

- For the definition of (cuts for lepton pair)-function see [?]. It is evaluated within module LeptonCutsDY.f90. The presence of cuts, and their parameters are set by the SetCuts subroutine.
- The expression for the hard factor H is taken from [?]. It is the function of  $\ln(Q/\mu_H)$  and  $a_s(\mu_H)$ ). Since in the current realization  $\mu_H = Q$ , the logarithm is replaced by  $\ln(c_2)$ , where  $c_2$  is the variation constant.

The cross-section can be computed by two different means. Using LP factorization or using KPC-resummed factorization. The selection is done by the parameter A.p.2. One behavior totally exclude another.

This section is to be updated by definition of kinematics

List of available commands

Command	Type	Sec.	Short description
TMDX_DY_Initialize(order)	subrout.	XI A	Initialization of module.
TMDX_DY_ShowStatistic()	subrout.	_	Print current statistic on the number of calls.
TMDX_DY_ResetCounters()	subrout.	_	Reset intrinsic counters of the module.
TMDX_DY_SetScaleVariation(c2)	subrout.	_	Set new value for the scale-variation constant $c_1$
xSec_DY(X,proc,s,qT,Q,y,iC,CutP,Num)	subrout.	XIC	Evaluates cross-section completely integrated the bin.
xSec_DY_List(X,proc,s,qT,Q,y,iC,CutP,Num)	subrout.	XIC	Evaluates cross-section completely integrated the bin over the list.
xSec_DY_List(X,proc,s,qT,Q,y,iC,CutP,Num)	subrout.	XIC	Evaluates cross-section completely integrated the bin over the list.
xSec_DY_List_BINLESS(X,proc,s,qT,Q,y,iC,CutP,Num)	subrout.	XIC	Evaluates cross-section at the point over the lis

#### A. Initialization

Prior the usage module is to be initialized (once per run) by call TMDX\_DY\_Initialize(file)

The order of used coefficient function is set in constant-file by 'LO'( $a_s^0$ ), 'NLO'( $a_s^1$ ), 'NNLO' or 'N2LO'( $a_s^2$ ), 'N3LO'( $a_s^4$ ), 'N4LO'( $a_s^4$ ). The value in brackets shows the maximum included perturbative order in the hard coefficient function.

# B. The parameters of cross-section

Process: The process is encoded by 4 integer numbers (/p1,p2,p3,p4/) where

- p1 (integer) Defines the prefactor2 that contains the phase space elements and the universal part of factorization formula.
- p2 (integer) Defines the structure function F. See sec.X C.
- p3 (integer) Defines the type of hadron 1.
- p4 (integer) Defines the type of hadron 2.

**Note:** In artemide v.2.07 and earlier the process was encoded by 3 numbers, and did not contained the types of hadrons.

**Kinematics:** Each bin is defined by s (Mandelstam variable,  $GeV^2$ ), Q (virtuality, GeV, [min,max]), y (rapidity, [min,max]) and  $q_T$  (transverse momentum, GeV, [min,max]). If the order of limits is inverted the result is 0.

Lepton cuts: The fiducial cuts on the lepton pair are defined by two variables: logical iC (If inc=.true. the evaluation of cuts will be done, otherwise it will be ignored.). And the array of four reals (p1,p2,eta1,eta2), such that the cuts are defined as

$$|l_T| < \mathtt{p1}, \qquad |l_T'| < \mathtt{p2}, \qquad \mathtt{eta1} < \eta, \eta', \mathtt{eta2}, \tag{11.5}$$

where l and l' are the momenta of produced leptons, with  $l_T$ 's being their transverse components and  $\eta$ 's being their rapidities. For accurate definition of the cut-function see sec.2.6 of [?] (particularly equations (2.40)-(2.42)).

#### C. Cross-section evaluation

The main subroutine is called xSec\_DY and it have the following interface:

xSec\_DY(X,process,s,qT,Q,y,includeCuts,CutParameters,Num)

where

- X is (real\*8) value of cross-section.
- process is integer p, or (integer) array (p1,p2,p3,p4).
- $\bullet$ s is Mandelshtam variable s
- qT is (real\*8)array (qtmin,qtmax)
- Q is (real\*8)array (Qmin,Qmax)
- y is (real\*8)array (ymin,ymax)
- includeCuts is logical
- CutParameters is (real\*8) array (k1,k2,eta1,eta2) OPTIONAL
- Num is even integer that determine number of section in  $q_T$  integral **OPTIONAL**

Note, that optional variables could be omit during the call.

IMPORTANT: Practically, the call of this function coincides with X evaluated by the following set of commands call TMDX\_DY\_SetProcess(process)

- call TMDX\_DY\_XSetup(s,any,any)
- call SetCuts(includeCuts,k1,k2,eta1,eta2)
- call CalcXsec\_DY\_PTint\_Qint\_Yint (X,qtmin,qtmax,Qmin,Qmax,yMin,yMax,Num)

There is also an analogous subroutine that evaluate cross-section by list. It is called xSec\_DY\_List and it have the following interface:

```
xSec_DY_List(X,process,s,qT,Q,y,includeCuts,CutParameters,Num)
```

All variables are analogues to those of xSec\_DY, but should come in lists, i.e. X is (1:n), process is (1:n,1:4), s is (1:n), qT,Q,y are (1:n,1:2), includeCuts is (1:n), CutParameters is (1:n,1:4), and Num is (1:n). Only the Num argument is OPTIONAL arguments. The argument CutParameters must be presented. This command compiled by OPENMP, so runs in parallel on multi-core computers.

Finally, there is an also analogous subroutine that evaluate cross-section by list without bin-integration. It is called xSec\_DY\_List\_BINLESS and it have the following interface:

```
xSec_DY_List(X,process,s,qT,Q,y,includeCuts,CutParameters,Num)
```

All variables are analogues to those of xSec\_DY\_List, but should come in lists of central values, i.e. X is (1:n), process is (1:n,1:4), s is (1:n), qT,Q,y are (1:n), includeCuts is (1:n), CutParameters is (1:n,1:4), and Num is (1:n). Only the Num argument is OPTIONAL arguments. The argument CutParameters must be presented. This command compiled by OPENMP, so runs in parallel on multi-core computers.

# Extra notes:

• The integrations over Q and y are adaptive Simpsons. We have found that it is the fastest (adaptive) method for typical cross-sections with tolerance  $10^{-3} - 10^{-4}$ . Naturally, it is not suitable for higher precision, which however is not typically required.

- The integration over  $p_T$  is not adaptive, since typically  $p_T$ -bins are rather smooth and integral is already accurate if approximated by 4-8 points (default minimal value is set in INI-file, and is automatically increased for larger bins). For unexceptionally large  $q_T$ -bins, or very rapid behavior we suggest to use overloaded versions with manual set of N (number of integral sections).
- For very small value of  $q_T$  the cross-section is frozen at  $q_{T(abs\ min)}$ , which is defined in INI-file (10<sup>-4</sup> by default). It is done to avoid badly converging integrals.
- The evaluation can be done in parallel. The list commands are parallel by default. Basically, in this case, individual values for the list of cross-sections are evaluated in parallel. Unfortunately the parallel scaling-rate is not very high, on 8 processors it is about 400%-500% only. The parallelization is made with OPENMP library. To make the parallel computation possible, add -fopenmp option in the compilation instructions. The maximum number of allowed threads is set constants-file.

#### D. LeptonCutsDY

The calculation of cut prefactor is made in LeptonCutsDY.f90. It has two public procedures: SetCutParameters, and CutFactor.

- The subroutine SetCutParameters(kT,eta1,eta2) set a default version of cut parameters:  $p_{1,2} < k_T$  and  $\eta_1 < \eta < \eta_2$ .
- The overloaded version of the subroutine SetCutParameters (k1,k2,eta1,eta2) set a default version of asymmetric cut parameters.  $p_1 < k_1, p_2 < k_2$  and  $\eta_1 < \eta < \eta_2$ .
- Function  $CutFactor(qT,Q_in,y_in, CutParameters)$  calculates the cut prefactor at the point  $q_T$ , Q, y. The argument CutParameters is **optional**. If it is not present, cut parameters are taken from default values (which are set by SetCutParameters). CutParameters is array (/ k1,k2,eta1,eta2/). The usage of global definition for CutParameters is not recommended, since it can result into running condition during parallel computation. This is interface is left fro compatibility with earlier version of artemide.

#### E. Variation of scale

TO BE WRITTEN

# F. Options for evaluation of DY-like cross-section

1.  $\pi^2$ -resummation

The coefficient function of DY-like cross-section  $|C_V|^2$  is evaluated at  $(-q^2)$  (space-like momentum). Thus, it has contributions  $\sim \pi^2$ , which could be large, especially in the case of Higgs-boson production, see discussion in refs.Ahrens:2009cxz, Ahrens:2008qu. These corrections could be resummed by RG technique [?]. So,

$$|C_V(-q^2)|^2 \to U_\pi |C_V(q^2)|^2,$$
 (11.6)

where  $U_{\pi}$  is the resummation exponent for  $\pi a_s$ -correction. At LO it reads [?]

$$U_{\pi} = \exp\left(\frac{\Gamma_0}{2a_s\beta_0^2}[2a\arctan a - \ln(1+a^2)]\right), \qquad a = \pi a_s.$$
 (11.7)

To use the  $\pi$ -resummed coefficient function switch the corresponded option in constants-file (Option 9.A.p3).

# 2. Power corrections

There are many sources of power corrections. For a moment there is no systematic studies of power corrections for TMD factorization. Nonetheless I include some options in artemide, and plan to make more systematic treatment in the future.

**Exact values of**  $x_{1,2}$  for DY: The TMD distributions enter the cross-section with  $x_1$  and  $x_2$  equal to

$$x_{1} = \frac{q^{+}}{p_{1}^{+}} = \frac{Q}{\sqrt{s}} e^{y} \sqrt{1 + \frac{q_{T}^{2}}{Q^{2}}} \simeq \frac{Q}{\sqrt{s}} e^{y},$$

$$x_{1} = \frac{q^{+}}{p_{1}^{+}} = \frac{Q}{\sqrt{s}} e^{-y} \sqrt{1 + \frac{q_{T}^{2}}{Q^{2}}} \simeq \frac{Q}{\sqrt{s}} e^{-y}.$$
(11.8)

Traditionally, the corrections  $\sim q_T/Q$  are dropped, since they are power corrections. Nonetheless, they could be included since they have different sources in comparison to power corrections to the factorized cross-section. Usage of one or another version of  $x_{1,2}$  is switched in constants-file (Option 9.A.p2).

Exact values for hard scale for DY: The TMD hard coefficient function contains  $\ln(|2q^+q^-|/\mu^2)$  which is usually approximated by  $\ln(Q^2)$ . Similarly, the zeta-scales are normalized as  $\zeta\bar{\zeta} = (2q^+q^-)^2$ , which is usually approximated by  $Q^4$ . So, the exact values of scales are

$$\mu = \sqrt{Q^2 + \mathbf{q}_T^2}, \qquad \zeta_1 = \zeta_2 = Q^2 + \mathbf{q}_T^2.$$
 (11.9)

Traditionally, the corrections  $\sim q_T/Q$  are dropped, since they are power corrections. Nonetheless, they could be included since they have different sources in comparison to power corrections to the factorized cross-section. Usage of one or another version of scales is switched in constants-file (Option 9.A.p4).

#### G. Enumeration of processes (LP case)

# List of enumeration for p2

_	List of enumeration for p2			
p2	prefactor 2	Short description		
1	$\frac{4\pi}{9} \frac{\alpha_{\text{em}}^2(Q)}{sQ^2}  C_V^{DY}(c_2Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). Corresponds to DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . The result is in pb/GeV <sup>2</sup>		
2	$\frac{2\sqrt{Q^2 + q_T^2}}{\sqrt{s}} \cosh y  \frac{4\pi}{9} \frac{\alpha_{\text{em}}^2(Q)}{sQ^2}  C_V^{DY}(c_2 Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). The result is in pb/GeV <sup>2</sup> . <b>Attention!:</b> this process corresponds to computation with the $dX = dx_F dQ^2 dq_T^2$ where $x_F = \frac{2\sqrt{Q^2 + q_T^2}}{\sqrt{s}} \sinh y$ is Feynman $x$ . In this case the integration $y$ is preplaced by the integration over $x_F$ (i.e. limits of integration are treated as for $x_F$ ).		
3	$\frac{4\pi^2}{3} \frac{\alpha_{\text{em}}(Q)}{s} Br_Z  C_V^{DY}(c_2 Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ for the Z-boson production in the narrow width approximation. $Br_Z=0.03645$ is Z-boson branching ration to leptons. $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). The result is in pb/GeV <sup>2</sup>		
4	$\frac{4\pi^2}{3} \frac{\alpha_{\text{em}}(Q)}{s} Br_W  C_V^{DY}(c_2 Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ for the W-boson production in the narrow width approximation. $Br_W=0.1086$ is W-boson branching ration to leptons. $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). Use together with p3=13,,18. In this case, $Q$ is be $M_Z$ . The result is in pb/GeV <sup>2</sup>		
5	$\frac{2}{\pi} \frac{\pi m_H^2 a_s^2(Q)}{36sv^2} C_t^2(m_t, Q)  C_g(Q) ^2  A(x_t) ^2$	Cross-section $\frac{d\sigma}{dyd(q_T^2)}$ for the exclusive Higgs-boson production. The result is in pb/GeV <sup>2</sup> . For definition of functions see [?].		

Here  $R = 0.3893379 \cdot 10^9$  the transformation factor from GeV to pb.

# H. Enumeration of processes (KPC case)

List of enumeration for p2

p2	prefactor 2	Short description
1	$\frac{2\pi^2}{9} \frac{\alpha_{\text{em}}^2(Q)}{s}  C_V^{DY}(c_2Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). Corresponds to DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . The result is in pb/GeV <sup>2</sup>
2	$\frac{2\sqrt{Q^2 + q_T^2}}{\sqrt{s}} \cosh y  \frac{2\pi^2}{9} \frac{\alpha_{\text{em}}^2(Q)}{s}  C_V^{DY}(c_2 Q) ^2 R \times \text{cut}(q_T)$	DY-cross-section $\frac{d\sigma}{dQ^2dyd(q_T^2)}$ . $\operatorname{cut}(q_T)$ is the weight for the lepton tensor with fiducial cuts (see sec.2.6 in [?]). The result is in pb/GeV². <b>Attention!:</b> this process corresponds to computation with the $dX = dx_F dQ^2 dq_T^2$ where $x_F = \frac{2\sqrt{Q^2 + q_T^2}}{\sqrt{s}} \sinh y$ is Feynman $x$ . In this case the integration $y$ is preplaced by the integration over $x_F$ (i.e. limits of integration are treated as for $x_F$ ).
3	_	Absent
4	_	Absent
5	$\frac{\pi m_H^2 a_s^2(Q)}{36sv^2} Q^2 C_t^2(m_t, Q)  C_g(Q) ^2  A(x_t) ^2$	Cross-section $\frac{d\sigma}{dyd(q_T^2)}$ for the exclusive Higgs-boson production. The result is in pb/GeV <sup>2</sup> . For definition of functions see [?]. The correct formula is to be defined, this is LP formula multiplied by large-Q translation factor.

Here  $R = 0.3893379 \cdot 10^9$  the transformation factor from GeV to pb.

# XII. TMDX\_SIDIS MODULE

This module evaluates cross-sections with the SIDIS-like kinematics. I.e. it expects the following kinematic input, (Q, x, z) or (Q, y, z) or (x, y, z), that are equivalent.

The general structure of the cross-section is

$$\frac{d\sigma}{dX} = d\sigma(q_T) = prefactor1 \int [bin] \ prefactor2 \times F, \tag{12.1}$$

where  $dX \sim dl'$ , with l' momentum of scattered lepton. For better definition of parameters see sec.XII G.

List of available commands

List of available commands				
Command	Type	Sec.	Short description	
TMDX_SIDIS_Initialize(file,prefix)	subrout.	XI A	* Initialization of module.	
TMDX_SIDIS_ResetCounters()	subrout.	_	* Reset intrinsic counters of module.	
TMDX_SIDIS_ShowStatistic()	subrout.	_	* Print current statistic on the number of calls.	
TMDX_SIDIS_SetProcess(p)	subrout.	XII A	Set the process	
TMDX_SIDIS_XSetup(s,z,x,Q,mTARGET,mPRODUCT)	subrout.	XII A	Set the kinematic variables (mTARGET and mPRODUCT are optional variables)	
TMDX_SIDIS_SetCuts(inc,yMin,yMax,W2)	subrout.	XIIC	Set global values of cuts	
TMDX_SIDIS_SetScaleVariation(c2)	subrout.	_	* Set new values for the scale-variation constants.	
CalcXsec_SIDIS	subrout.	XIIB	Evaluates cross-section. Many overloaded versions see sec.XIIB.	
xSec_SIDIS(X,process,s,pT,z,x,Q)	subrout.	XIIB	Evaluates cross-section completely integrated over the bin. Can be called without preliminarySet's.	
<pre>xSec_SIDIS_List(X,process,s,pT,z,x,Q)</pre>	subrout.	XIIB	Evaluates cross-section completely integrated over the bin over the list. Can be called without preliminarySet's.	

<sup>\*)</sup> The structure of the module repeats the structure of TMDX\_DY module, with the main change in the kinematic definition. Most part of routines has the same input and output with only replacement  $_DY \rightarrow _SIDIS$ . We do not comment such commands. They marked by \* in the following table.

# A. Setting up the parameters of cross-section

Prior to evaluation of cross-section one must declare which process is considered and to set up the kinematics.

The declaration of the process is made by call TMDX\_SIDIS\_SetProcess(p1,p2,p3) call TMDX\_SIDIS\_SetProcess(p0) where p0=(/p1,p2,p3/) and

- p1 (integer) Defines the *prefactor1* that contains the phase space elements, and generally experimental dependent. Could be set outside of bin-integration.
- p2 (integer) Defines the prefactor2 that contains the universal part of factorization formula. Participate in the bin-integration
- p3 (integer) Defines the structure function F. See sec.X C.

Alternatively, process can be declared by shorthand version call TMDX\_SIDIS\_SetProcess(p)

where p(integer) corresponds to particular combinations of p1,p2,p3. See table.

The kinematic of the process is declared by variables (s,Q,x,z)

call TMDX\_SIDIS\_XSetup(s,Q,x,z)

where **s** is Mandelshtam variable s, **Q** is hard virtuality Q, and (x,z) are standard SIDIS variables. Additionally one can declare masses of target and produced hadrons, by using optional variables

call TMDX\_SIDIS\_XSetup(s,Q,x,z,mTARGET,mPRODUCT)

where corresponding masses are given in GeV. Note, that during initialization procedure the target and produced masses are set from constants-file. These values are used or not used according to triggers for 'mass corrections' set in constants-file.

All non-perturbative parameters are defined in the TMDs and lower-level modules. For user convenience there is a subroutine, which passes the values of parameters to TMDs. It is

call TMDX\_SIDIS\_SetNPParameters(lambda/)

where lambda is real\*8(1:number of parameters)/ or n is the number of replica. See also IXB.

#### B. Cross-section evaluation

After the parameters of cross-section are set up, the values of the cross-section at different  $q_T$  can be obtained by call CalcXsec\_DY(X,qt)

where X is real\*8 variable where cross-section will be stored, qt is real\*8 is the list of values of  $q_T$ 's at which the X is to be calculated. There exists an overloaded version with X (real\*8)(1:N) and qT(real\*8)(1:N), which evaluates the array of crossections over array of  $q_T$ .

Typically, one needs to integrate over bin. There is a whole set of subroutines which evaluate various integrals over bin they are

Subroutine	integral	Comment
CalcXsec_SIDIS(X,pt)	single-point cross-section at given $p_T$	
CalcXsec_SIDIS_Zint_Xint_Qint (X,pt,zMin,zMax,xMin,xMax,Qmin,Qmax)	$\int_{z_{\min}}^{z_{\max}} dz \int_{x_{\min}}^{x_{\max}} dx$ $\int_{Q_{\min}}^{Q_{\max}} 2QdQd\sigma(p_T)$	$ \begin{vmatrix} 0 < z_{\min} < z_{\max} < 1 \\ 0 < x_{\min} < x_{\max} < 1 \\ 0 < Q_{\min} < Q_{\max} \end{vmatrix} $
CalcXsec_SIDIS_PTint_Zint_Xint_Qint (X,ptMin,ptMax,zMin,zMax,xMin,xMax,Qmin,Qmax)	$\int_{z_{\min}}^{z_{\max}} dz \int_{x_{\min}}^{x_{\max}} dx$ $\int_{Q_{\min}}^{Q_{\max}} 2QdQ \int_{pT_{\min}}^{pT_{\max}} 2p_T dp_T d\sigma(p_T)$	$ \begin{vmatrix} 0 < z_{\min} < z_{\max} < 1 \\ 0 < x_{\min} < x_{\max} < 1 \\ 0 < Q_{\min} < Q_{\max} \end{vmatrix} $
More to be added		

**Note 1:** The point  $p_T = 0$  is somewhat problematic, since it leads to flat Hankel integral. Thus for  $p_T < 1$ MeV it is set to 1MeV.

**Note 2:** Each command has overloaded version with arrays for X and qt.

Note 3: Cross-section integrated over  $p_T$  bins have overloaded versions with X, qtmin and qtmax being arrays. Then the integral is done for X(i) from ptmin(i) to ptmax(i).

**Note 4:** There exist special overloaded case for integrated over  $p_T$ -bins, with successive bins. I.e. for bins that adjust to each other. In this case only one argument ptlist is required (instead of qtmin,qtmax). The integration for X(i) is done from ptlist(i) till ptlist(i+1).

Take care that every next function is heavier to evaluate then the previous one. The integrations over Q and y are adaptive Simpsons. We have found that it is the fastest (adaptive) method for typical cross-sections with tolerance  $10^{-3} - 10^{-4}$ . Naturally, it is not suitable for higher precision, which however is not typically required. The integration over pt is not adaptive, since typically  $p_T$ -bins are rather smooth and integral is already accurate if approximated by 5-7 points (default value is set in constants). For larger  $p_T$ -bins we suggest to use overloaded versions with manual set of N (number of integral sections).

There is a subroutine that evaluate cross-section without preliminary call of SetCuts, TMDX\_SIDIS\_SetProcess, TMDX\_SIDIS\_XSetup. It is called xSec\_SIDIS and it have the following interface:

xSec\_SIDIS(X,process,s,pT,z,x,Q,incC,cuts,masses)

where

- X is (real\*8) value of cross-section.
- process is (integer)array (p1,p2,p3).
- s is (real\*8)Mandelshtam variable s
- pT is (real\*8)array (qtmin,qtmax)
- z is (real\*8)array (zmin,zmax)
- x is (real\*8)array (xmin,xmax)
- Q is (real\*8)array (Qmin,Qmax)
- incC is (logical) flag to include cuts.
- cuts is (real\*8) array (ymin, ymax, W2min, W2max) that parameterizes kinematic cuts.
- masses is (real\*8) array (mt,mp) which is  $(M_{target}, m_{produced})$  in GeV OPTIONAL.

IMPORTANT: Practically, the call of this function coincides with X evaluated by the following set of commands call TMDX\_SIDIS\_SetProcess(process)

call TMDX\_SIDIS\_XSetup(s,any,any,any)

call TMDX\_SIDIS\_SetCuts(incC,ymin,ymax,W2min,W2max)

call CalcXsec\_SIDIS\_PTint\_Zint\_Xint\_Qint (X,ptMin,ptMax,zMin,zMax,xMin,xMax,Qmin,Qmax)

However, there is an important difference: the values of s, process which are set by routines ..Set.., are global. For that reason such approach could not be used in a parallel computation. Contrary, in the function xSec\_SIDIS these variables are set locally and thus this function can be used in parallel computations.

There is also analogous subroutine that evaluate cross-section by list. It is called xSec\_SIDIS\_List and it have the following interface:

All variables are analogues to those of xSec\_SIDIS, but should come in lists, i.e. X is (1:n), process is (1:n,1:3), s is (1:n), pT,x,Q,z are (1:n,1:2). This command compiled by OPENMP, so runs in parallel on multi-core computers.

# C. Kinematic cuts

Some experiments put extra constraints on the measurement. Typically, such constraint has the form

$$y_{\min} < y < y_{\max}, \qquad W_{\min}^2 < W^2 < W_{\max}^2.$$
 (12.2)

In this case the integration over x and  $Q^2$  has additional restrictions. Say, if one integrates over a bin:  $x_{\min} < x < x_{\max}$  and  $Q_{\min} < Q < Q_{\max}$  the boundaries of the bin should be modified as (here integration over x is before the integration over Q)

$$\hat{x}_{\min}(Q) < x < \hat{x}_{\max}(Q), \qquad \hat{Q}_{\min}^2 < Q^2 < \hat{Q}_{\max}^2.$$
 (12.3)

where

$$\begin{split} \hat{x}_{\min}(Q) \; &= \; \max\{x_{\min}, \frac{Q^2}{y_{\max}(s-M^2)}, \frac{Q^2}{Q^2 + W_{\max}^2 - M^2}\}, \\ \hat{x}_{\max}(Q) \; &= \; \min\{x_{\max}, \frac{Q^2}{y_{\min}(s-M^2)}, \frac{Q^2}{Q^2 + W_{\min}^2 - M^2}\}, \\ \hat{Q}_{\min}^2 \; &= \; \max\{Q_{\min}^2, x_{\min}y_{\min}(s-M^2), \frac{x_{\min}}{1 - x_{\min}}(W_{\min}^2 - M^2)\}, \\ \hat{Q}_{\max}^2 \; &= \; \min\{Q_{\max}^2, x_{\max}y_{\max}(s-M^2), \frac{x_{\max}}{1 - x_{\max}}(W_{\max}^2 - M^2)\}. \end{split}$$

If some cut is not required, then set corresponding parameter to limiting value, such as  $y_{\min} = 0$ ,  $y_{\max} = 1$ ,  $W_{\min}^2 = 0$ ,  $W_{\max}^2 \gg Q^2$ .

# D. Power corrections

There are many sources of power corrections. For a moment there is no systematic studies of of effect of power corrections for TMD factorization. Nonetheless we include some options in artemide, and plan to make systematic treatment in the future.

Kinematic corrections to the variables/phase space. There are three sources of kinematic corrections to the variables

$$\frac{p_{\perp}}{Q}, \qquad \frac{M}{Q}, \qquad \frac{m}{Q},$$

where M is the target mass, m is the mass of the fragmented hadron. These terms appear in many places of the SIDIS expression (see sec.XII G, for some minimal details), even without accounting for power-suppressed terms in the factorization formula. The nice feature of these correction is that they could be accounted exactly. The majority of these terms appears during of the Lorentz transformation of factorization frame (where the factorization is performed) to the laboratory frame (where the measurement is made).

Exact values for hard scale for SIDIS: The TMD hard coefficient function contains  $\ln(|2q^+q^-|/\mu^2)$  which is usually approximated by  $\ln(Q^2)$ . Similarly, the zeta-scales are normalized as  $\zeta\bar{\zeta} = (2q^+q^-)^2$ , which is usually approximated by  $Q^4$ . So, the exact values of scales are

$$\mu = \sqrt{Q^2 - \mathbf{q}_T^2}, \qquad \zeta_1 = \zeta_2 = Q^2 - \mathbf{q}_T^2.$$
 (12.4)

Traditionally, the corrections  $\sim q_T/Q$  are dropped, since they are power corrections. Nonetheless, they could be included since they have different sources in comparison to power corrections to the factorized cross-section. Usage of one or another version of *scales* is switched in constants-file (Option 10.A.p6).

The accounting of these corrections is switched on/off in constants.

# E. Bin-integration routines

The inclusion of bin-integration is essential for comparison with experiment. The integration over a bin is automatically included in the calculation of cross-section (although routines for unintegrated calculation are also presented). Typically, one does not need an extreme precision from such integration i.e. 4-5 digit precision is typically more then enough to overshoot experimental precision. Also the cross-section is relatively slow-function (exception is Z-boson peak). Therefore, as a based method for bin-integration I have selected the Simpson integration rule. By default, the adaptive Simpson rule is used for integration over z, x,  $Q^2$ , and fixed-number-of-points Simpson method for  $p_T$ -integration.

If the sizes of bins are small and the cross-section is smooth in this region, then it is worth to consider faster (but less accurate) methods for integration. They are set in constants-file in the section.10:B. The methods are

- SA Default. Simpson-adaptive algorithm. Runs with relative tolerance specified in constants-file. Initial estimation of the integral is done with 5-points. Minimal number of points for integration is 9.
- S5 Simpson-fixed-number-of-points algorithm. Estimation of the integral is done with 5-points. No checks for convergence.
- 10 No-integration. Evaluates the central point of the bin and multiply by the bin size (not recommended).

**Note,** the selection of method for integration is available only for some integration (so far integration over x and z). Other methods and integration will be added in future.

## F. Enumeration of processes

List of enumeration for prefactor1

p1

p1	prefactor1	Short description
1	1	No comments.
2	$\frac{Q^2}{y}$	The cross-section $\frac{d\sigma}{dxdydzd(p_{\perp}^2)}$ , in this case integration over $Q^2$ is replaced by integration over $y$ .
3	$\frac{x}{y}$	The cross-section $\frac{d\sigma}{dydQ^2dzd(p_{\perp}^2)}$ , in this case integration over $x$ is replaced by integration over $y$ .

List of enumeration for prefactor2

**p**2

_	<u>P</u> 2				
F	2 prefactor2	Short description			
1	$\frac{2\pi\alpha_{\text{em}}^{2}(Q)}{Q^{4}} \frac{y^{2}}{1-\varepsilon}  C_{V}^{SIDIS}(c_{2}Q) ^{2} c_{0}^{(un)} R$	(unpol.) SIDIS-cross-section $\frac{d\sigma}{dxdQ^2dzd(p_{\perp}^2)}$ . [pb/GeV <sup>2</sup> ].			
2	$\frac{\frac{x}{\pi} \frac{c_0^{(un)}}{\left(1 + \frac{\gamma^2}{2x}\right)}  C_V^{SIDIS}(c_2 Q) ^2$	Prefactor for $F_{UU,T}$ according to the tabulated definition (2.7) of [?].			

Here  $R = 0.3893379 \times 10^9$  the transformation factor from GeV to pb.

$$c_0^{(un)} = \frac{1 + \left(\varepsilon - \frac{\gamma^2}{2}\right) \frac{\rho_\perp^2 - \rho^2}{1 - \gamma^2 \rho^2}}{\sqrt{1 - \gamma^2 \rho_\perp^2}}.$$

# G. SIDIS theory

In many aspects the theory for SIDIS is more complicated then for Drell-Yan. Here I collect the main definition which were used in the artemide. For a more detailed description see ref.[?]. Note, that some parts of definition were derived by me, since I have not found them in the literature.

1. Kinematics

The process is

$$H(P) + l(l) \to l(l') + h(p_h) + X,$$
 (12.5)

with

$$P^2 = M^2, l^2 = l'^2 = m_l^2 \simeq 0, p_h^2 = m^2.$$
 (12.6)

The standard variables used for the description of SIDIS are

$$q = l - l'$$
  $\Rightarrow$   $Q^2 = -q^2, \quad x = \frac{Q^2}{2(Pq)}, \quad y = \frac{(Pq)}{(Pl)}, \quad z = \frac{(Pp_h)}{(Pq)}.$  (12.7)

There are is also a set of power variables used to define power-corrections

$$\gamma = \frac{2Mx}{Q}, \qquad \rho = \frac{m}{zQ}, \qquad \rho_{\perp}^2 = \frac{m^2 + p_{\perp}^2}{z^2 Q^2}.$$
(12.8)

The variables x, y and  $Q^2$  are dependent:  $xy(s-M^2)=Q^2$ . The phase-volume  $dxdQ^2$  can be expressed via dxdy or  $dydQ^2$ :

$$dxdQ^2 = \frac{Q^2}{y}dxdy = \frac{x}{y}dydQ^2.$$
 (12.9)

A phase space point is totally characterized by the following numbers:

$$\{s, x, Q^2, z, \mathbf{p}_T^2\}.$$
 (12.10)

Alternatively, one can replace x or  $Q^2$  by y.

2. Cross-section

The cross-section for SIDIS has the general form

$$\frac{d\sigma}{dx dQ^2 dz d\psi d\phi_h d\mathbf{p}_{h\perp}^2} = \frac{\alpha_{\rm em}^2(Q)}{Q^6} \frac{y^2}{8z} \frac{L_{\mu\nu} W^{\mu\nu}}{\sqrt{1 + \boldsymbol{\rho}_{\perp}^2 \gamma^2}},$$
(12.11)

where  $L_{\mu\nu}$  is the lepton tensor, and  $W_{\mu\nu}$  is the hadron tensor. The hadron tensor contains many term accompanied by polarization angles.

The TMD factorization is performed in the factorization frame with respect to  $q_T^2 \ll Q^2$ . In the factorization frame, the unpolarized part of the hadron tensor

$$W^{\mu\nu} = \frac{-zg_T^{\mu\nu}}{\pi} \int |\mathbf{b}|d|\mathbf{b}|J_0(|\mathbf{b}||\mathbf{q}_T|) \sum_f e_f^2 |C_V(-Q^2, \mu^2)|^2 F_1^f(x_1, \mathbf{b}) D_1^f(z_1, \mathbf{b}) + \dots, \qquad (12.12)$$

where dots denote, polarized terms, and power corrections. The variables  $x_1$  and  $z_1$  are

$$x_1 = -\frac{2x}{\gamma^2} \left( 1 - \sqrt{1 + \gamma^2 \left( 1 - \frac{q_T^2}{Q^2} \right)} \right), \tag{12.13}$$

$$z_{1} = -z \frac{1 - \sqrt{1 + \left(1 - \frac{q_{T}^{2}}{Q^{2}}\right)\gamma^{2}}}{\gamma^{2}} \frac{1 + \sqrt{1 - \rho^{2}\gamma^{2}}}{1 - \frac{q_{T}^{2}}{Q^{2}}}.$$
 (12.14)

The factorization variable  $|q_T|$  is related to the measured variable  $p_{h\perp}$  as

$$|\mathbf{q}_T| = \frac{|\mathbf{p}_{h\perp}|}{z} \sqrt{\frac{1+\gamma^2}{1-\gamma^2 \rho^2}}, \qquad \Leftrightarrow \qquad |\mathbf{p}_{h\perp}| = z|\mathbf{q}_T| \sqrt{\frac{1-\gamma^2 \rho^2}{1+\gamma^2}}. \tag{12.15}$$

Making the convolution with unpolarized leptonic tensor, we get the following expression for the cross-section

$$\frac{d\sigma}{dx dQ^{2} dz d\boldsymbol{p}_{h\perp}^{2}} = 2\pi \frac{\alpha_{\text{em}}^{2}}{Q^{4}} \frac{1}{\sqrt{1 + \boldsymbol{\rho}_{\perp}^{2} \gamma^{2}}} \frac{y^{2}}{2(1 - \varepsilon)} \left\{ 1 + \left( \varepsilon - \frac{\gamma^{2}}{2} \right) \frac{\boldsymbol{\rho}_{\perp}^{2} - \rho^{2}}{1 - \gamma^{2} \rho^{2}} \right\} 
\int |\boldsymbol{b}| d|\boldsymbol{b}| J_{0} \left( \frac{|\boldsymbol{b}||\boldsymbol{p}_{h\perp}|}{z} \sqrt{\frac{1 + \gamma^{2}}{1 - \gamma^{2} \rho^{2}}} \right) \sum_{f} e_{f}^{2} |C_{V}(-Q^{2}, \mu^{2})|^{2} F_{1}^{f}(x_{1}, \boldsymbol{b}) D_{1}^{f}(z_{1}, \boldsymbol{b}), \tag{12.16}$$

where

$$\varepsilon = \frac{1 - y - \frac{\gamma^2 y^2}{4}}{1 - y + \frac{y^2}{2} + \frac{y^2 \gamma^2}{4}}.$$
 (12.17)

#### TMDS\_INKT MODULE

The module TMDs\_inKT is derivative of the module TMDs that provides the TMD in the transverse momentum space. We define

$$F(x, \mathbf{k}_T; \mu, \zeta) = \int \frac{d^2 \mathbf{b}}{(2\pi)^2} F(x, \mathbf{b}; \mu, \zeta) e^{-i(\mathbf{k}_T \mathbf{b})}.$$
 (13.1)

Since all evaluated TMDs depends only on the modulus of b, within the module we evaluate Hankel transformations. These transformations depends on the kind of TMD. Generally the integrals are

$$F(x, |\mathbf{k}_T|; \mu, \zeta) = \int \frac{d|\mathbf{b}|}{2\pi} |\mathbf{b}|^{n+1} J_n(|\mathbf{b}||\mathbf{k}_T|) F(x, |\mathbf{b}|; \mu, \zeta).$$
(13.2)

On top of it there is could be extra prefactors specified in the table. For simplicity these cases indecated by numbers

$$n = 0, F(x, |\mathbf{k}_T|; \mu, \zeta) = \int \frac{d|\mathbf{b}|}{2\pi} |\mathbf{b}| J_0(|\mathbf{b}||\mathbf{k}_T|) F(x, |\mathbf{b}|; \mu, \zeta), (13.3)$$

$$n = 1, F(x, |\mathbf{k}_T|; \mu, \zeta) = \int \frac{d|\mathbf{b}|}{2\pi} |\mathbf{b}|^2 J_1(|\mathbf{b}||\mathbf{k}_T|) F(x, |\mathbf{b}|; \mu, \zeta), (13.4)$$

$$n = 2, F(x, |\mathbf{k}_T|; \mu, \zeta) = -\int \frac{d|\mathbf{b}|}{2\pi} |\mathbf{b}|^3 J_2(|\mathbf{b}||\mathbf{k}_T|) F(x, |\mathbf{b}|; \mu, \zeta). (13.5)$$

$$n = 2, F(x, |\mathbf{k}_T|; \mu, \zeta) = -\int \frac{d|\mathbf{b}|}{2\pi} |\mathbf{b}|^3 J_2(|\mathbf{b}||\mathbf{k}_T|) F(x, |\mathbf{b}|; \mu, \zeta). (13.5)$$

The module TMDs\_inKT uses all functions from the module TMDs. In fact, all technical commands (like Initialize) just transfer the request to TMDs. Thus, the information on these commands can be found in the section IX. For the evaluation of Hankel integral we use the Ogata quadrature see XB (the parameters for it are set in corresponding section of constants.

List of available commands

Command	Type	Sec.	Short description
TMDs_inKT_Initialize(order)	subrout.	IX	Initialization of module.
TMDs_inKT_ResetCounters()	subrout.	-	Reset intrinsic counters of modules
TMDs_inKT_ShowStatistic	subrout.	-	Print current statistic on the number of calls.
testTMDPDF_kT(x,kT)	(real*8(-5:5))	-	Evaluates the Fourier of the text function (see below). $n=0$
uTMDPDF_kT_5(x,kT,h)	(real*8(-5:5))	IX B	Unpolarized TMD PDF at the optimal line (gluon term undefined). $n=0$
uTMDPDF_kT_50(x,kT,h)	(real*8(-5:5))	IX B	Unpolarized TMD PDF at the optimal line (gluon term defined). $n=0$
uTMDPDF_kT_5(x,kT,mu,zeta,h)	(real*8(-5:5))	IX B	Unpolarized TMD PDF (gluon term undefined). $n = 0$
uTMDPDF_kT_50(x,kT,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD PDF (gluon term defined). $n = 0$
uTMDFF_kT_5(x,kT,h)	(real*8(-5:5))	IX B	Unpolarized TMD FF at the optimal line (gluon term undefined). $n=0$
uTMDFF_kT_50(x,kT,h)	(real*8(-5:5))	IX B	Unpolarized TMD FF at the optimal line (gluon term defined). $n=0$
uTMDFF_kT_5(x,kT,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF (gluon term undefined). $n=0$
uTMDFF_kT_50(x,kT,mu,zeta,h)	(real*8(-5:5))	IXB	Unpolarized TMD FF (gluon term defined). $n = 0$
lpTMDPDF_kT_50(x,kT,h)	(real*8(-5:5))	IX B	Linearly polarized gluon TMD PDF at the optimal line (quark terms undefined). $n=2$
lpTMDPDF_kT_50(x,kT,mu,zeta,h)	(real*8(-5:5))	IX B	Linearly polarized gluon TMD PDF (quark terms undefined). $n=2$
SiversTMDPDF_kT_5(x,kT,h)	(real*8(-5:5))	IX B	Sivers TMD PDF at the optimal line (gluon term undefined). $n=1$
SiversTMDPDF_kT_50(x,kT,h)	(real*8(-5:5))	IX B	Sivers TMD PDF at the optimal line (gluon term defined). $n=1$
SiversTMDPDF_kT_5(x,kT,mu,zeta,h)	(real*8(-5:5))	IXB	Sivers TMD PDF (gluon term undefined). $n=1$
SiversTMDPDF_kT_50(x,kT,mu,zeta,h)	(real*8(-5:5))	IXB	Sivers TMD PDF (gluon term defined). $n = 1$

# **Comments:**

- The value of  $k_T$  is expected bigger 1MeV for smaller values the function evaluates at 1MeV.
- For gluonless TMDs (\_5) the gluon term is identically 0.
- The convergence of the integral is checked by convergence of each flavor (until all flavors are convergent).

The function testTMDPDF\_kT(x,kT) returns the Fourier of the following test functions (x is the free parameter

$$\{b^3e^{-xb}, b^2e^{-xb}, be^{-xb}, e^{-xb}, \frac{1}{(b^2+x^2)^4}, \frac{1}{(b^2+x^2)^2}, \frac{1}{b^2+x^2}, b^2e^{-xb^2}, e^{-xb^2}, \frac{J_0(x/b)}{b}, \frac{1}{b}\}.$$

$$(13.6)$$

The result of evaluation should be

$$\left\{ \frac{3}{2\pi} \frac{3k_T^4 - 24k_T^2 x^2 + 8x^4}{(k_T^2 + x^2)^{9/2}}, \frac{3x}{2\pi} \frac{2x^2 - 3k_T^2}{(k_T^2 + x^2)^{7/2}}, \frac{1}{2\pi} \frac{2x^2 - k_T^2}{(k_T^2 + x^2)^{5/2}}, \frac{1}{2\pi} \frac{x}{(k_T^2 + x^2)^{3/2}}, \frac{k_T^2}{(k_T^2 + x^2)^{3/2}}, \frac{k_T^2}{4\pi x} K_1(k_T x), \frac{K_0(k_T x)}{2\pi}, \frac{4x - k_T^2}{16\pi x^3} e^{-k_T^2/(4x)}, \frac{e^{-k_T^2/(4x)}}{4\pi x}, \frac{J_0(2\sqrt{xk_T})}{2\pi k_T}, \frac{1}{2\pi k_T} \right\}.$$
(13.7)

The expressions for functions are selected such that the integral gives reasonable values for 0.05 < x < 1.

# KPC IN TMD FACTORIZATION

The TMD factorization with KPCs is computed using different route. The primary problem is that one must compute these correction in the momentum space. It essentially complicates the computation, since the evolution is done in the position space.

The module TMDFint\_KPC\_DY realizes the computation of the following integral

$$C_{KPC}[K, FF] = 4p_1^+ p_2^+ \int d\xi_1 d\xi_2 \int d^4k_1 d^4k_2 \delta^{(4)}(q - k_1 - k_2) \delta(k_1^2) \delta(k_2^2)$$
(14.1)

$$\delta(k_1^+ - \xi_1 p_1^+) \delta(k_2^- - \xi_2 p_2^-) K \times FF, \tag{14.2}$$

where K is a kinematic kernel, that is resulted from the convolution of tensors, and FF is the product of TMD distributions.

This function has the following interface

where Q,qT,x1,x2,mu are usual variables, and proc1 is (int,int,int)-array with first item being the number of FF, the second and third items being number of hadrons; proc2 is the enumeration of factors K.

#### Realization of convolution

The integral for convolution can be presented as

$$C_{KPC}[K, FF] = \int_0^{\pi/2} d\alpha \int_0^{\pi} d\theta \frac{K \times FF}{2}, \qquad (14.3)$$

where

$$\xi_1 = \frac{x_1}{2} \left( 1 + S + \sqrt{\Lambda} \right), \tag{14.4}$$

$$\xi_2 = \frac{x_2}{2} \left( 1 - S + \sqrt{\Lambda} \right), \tag{14.5}$$

$$\xi_2 = \frac{x_2}{2} \left( 1 - S + \sqrt{\Lambda} \right), \tag{14.5}$$

$$\mathbf{k}_1^2 = \frac{\tau^2}{4} \left( 1 - \Lambda + 2S + S^2 \right), \tag{14.6}$$

$$\mathbf{k}_{2}^{2} = \frac{\tau^{2}}{4} \left( 1 - \Lambda - 2S + S^{2} \right), \tag{14.7}$$

with

$$S = \frac{(\boldsymbol{q}_T \boldsymbol{\Delta})}{\tau^2} = \sqrt{\sin \alpha \frac{\boldsymbol{q}_T^2}{\tau^2}} \cos \theta, \qquad \Lambda = \frac{\lambda(\tau^2, \boldsymbol{k}_1^2, \boldsymbol{k}_2^2)}{\tau^4} = \left(1 - \frac{\boldsymbol{q}_T^2}{\tau^2}\right) (1 - \sin \alpha). \tag{14.8}$$

# Enumeration of factors K

N	K	Short description
1	1	Unpolarized DY case
2	$-\frac{\xi_1}{\xi_2} \frac{\boldsymbol{k}_2^2}{Q^2}$	Unpolarized EW case, term proportional to $\mathcal{P}_1$ and $f_1f_1$
3	$-\frac{\xi_2}{\xi_1} \frac{k_1^2}{Q^2}$	Unpolarized EW case, term proportional to $\mathcal{P}_2$ and $f_1f_1$
4	$\frac{2(\boldsymbol{k}_1\boldsymbol{k}_2)}{Q^2}$	Unpolarized EW case, term proportional to $\mathcal{P}_3$ and $f_1f_1$

	Unpolarized EW case, term proportional to $\mathcal{P}_1$ and $h_1^\perp h_1^\perp$
$6 \frac{\xi_2}{\xi_1} \frac{\boldsymbol{k}_1^2}{Q^2} \frac{(\boldsymbol{k}_1 \boldsymbol{k}_2)}{M^2}$	Unpolarized EW case, term proportional to $\mathcal{P}_2$ and $h_1^{\perp}h_1^{\perp}$
$7 \left  \frac{2k_1^2k_2^2}{M^2Q^2} \right $	Unpolarized EW case, term proportional to $\mathcal{P}_3$ and $h_1^\perp h_1^\perp$
$oxed{8} rac{\xi_1}{x_1} - rac{x_2}{\xi_2} rac{m{k}_2^2}{Q^2 + m{q}_T^2}$	Unpolarized EW case, term proportional to $\mathcal{P}_1^A$ and $f_1f_1$
	Unpolarized EW case, term proportional to $\mathcal{P}_2^A$ and $f_1f_1$