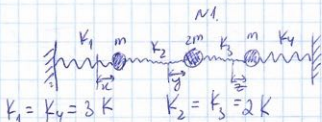


Динамическая работа.



$$\begin{cases} m\ddot{x} = -K_1x - K_2(x-y) = x(-K_1-K_2) + y \cdot K_2 \\ 2m\ddot{y} = K_2(x-y) - K_3(y-z) = x \cdot K_2 + y \cdot (-K_2-K_3) + z \cdot K_3 \\ m\ddot{z} = K_3(y-z) - K_4z = y \cdot K_3 + z \cdot (-K_3-K_4) \end{cases}$$

$$\ddot{X} = -AX$$

$$A = \frac{1}{m} \begin{pmatrix} 5K & -2K & 0 \\ -K & 2K & -K \\ 0 & -2K & 5K \end{pmatrix} = \frac{K}{m} \begin{pmatrix} 5 & -2 & 0 \\ -1 & 2 & -1 \\ 0 & -2 & 5 \end{pmatrix}$$

$$\lambda^3 - 12\lambda^2 + 44\lambda - 30 = 0$$

$$(\lambda - 1)(\lambda - 5)(\lambda - 6) = 0$$

$$\lambda_1 = 1, \lambda_2 = 5, \lambda_3 = 6$$

$$\Rightarrow \text{собств. частоты } A: \frac{K}{m}, \frac{5K}{m}, \frac{6K}{m}; \omega_1^2 = \frac{K}{m}, \omega_2^2 = \frac{5K}{m}, \omega_3^2 = \frac{6K}{m}$$

$$A - \lambda_1 E: \begin{pmatrix} \frac{4K}{m} & -\frac{2K}{m} & 0 \\ -\frac{K}{m} & \frac{K}{m} & -\frac{K}{m} \\ 0 & -\frac{2K}{m} & \frac{4K}{m} \end{pmatrix} = \frac{K}{m} \begin{pmatrix} 4 & -2 & 0 \\ -1 & 1 & -1 \\ 0 & -2 & 4 \end{pmatrix}$$

собств. векторы: $(2, 2, 1)$

$$\begin{vmatrix} 4 & -2 & 0 \\ -1 & 1 & -1 \\ 0 & -2 & 4 \end{vmatrix} = 0$$

2 лев. кол. стр: $\begin{vmatrix} 4 & -2 & 0 \\ -1 & 1 & -1 \end{vmatrix} = 0$

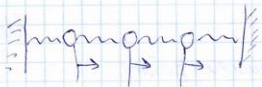
$$A - \lambda_2 E: \frac{K}{m} \begin{pmatrix} 0 & -2 & 0 \\ -1 & -3 & -1 \\ 0 & -2 & 0 \end{pmatrix}$$

$$\begin{pmatrix} 0 & -2 & 0 \\ -1 & -3 & -1 \end{pmatrix} \text{ собств. векторы } (1, 0, -1)$$

$$A - \lambda_3 E: \frac{K}{m} \begin{pmatrix} -1 & -2 & 0 \\ -1 & -4 & -1 \\ 0 & -2 & -1 \end{pmatrix}$$

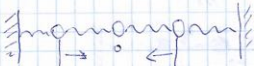
$$\begin{pmatrix} -1 & -2 & 0 \\ -1 & -4 & -1 \end{pmatrix} \text{ собств. векторы: } (2, -1, 2)$$

$$\psi_1 = (1, 2, 1)$$



$$\omega_1 = \sqrt{\frac{k}{m}}$$

$$\psi_2 = (1, 0, -1)$$



$$\omega_2 = \sqrt{\frac{4k}{m}}$$

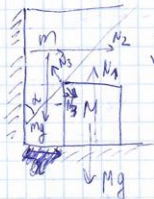
корр.
теорема

$$\psi_3 = (2, -1, 2)$$



$$\omega_3 = \sqrt{\frac{9k}{m}}$$

$\psi_i \cos \omega_i t$, $\psi_i \sin \omega_i t$ $i=1,2,3$ возможные моды



N2.



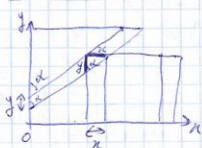
$$\begin{cases} M\ddot{x} = N_3 \cos \alpha \\ M\ddot{y} = N_1 - Mg - N_3 \sin \alpha \\ m\ddot{x} = N_2 - N_3 \cos \alpha \\ m\ddot{y} = N_3 \sin \alpha - mg \end{cases}$$

число степеней свободы: 1

степеней свободы =

= # координат - # связей

= # координат - # связей = 4 - 3 = 1



$$\tan \alpha = \frac{y}{x}$$

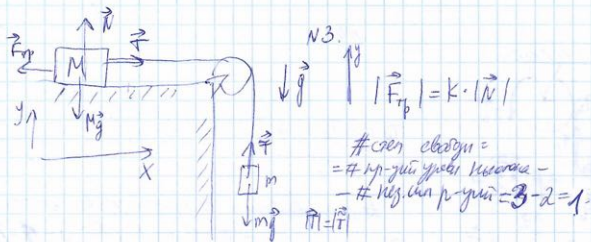
$$\dot{x} = -\dot{y} \cdot \tan \alpha$$

$$\ddot{x} = -\dot{y} \cdot \tan \alpha$$

$$m\ddot{y} = -m\ddot{x} \cdot \tan \alpha = M\ddot{x} \tan \alpha - mg$$

$$\ddot{x} (m \tan \alpha + M \tan \alpha) = +gm$$

$$\Rightarrow \ddot{x} = \frac{mg}{M \tan \alpha + m \tan \alpha}, \quad \ddot{y} = \frac{mg \tan \alpha (1 - 1)}{M \tan \alpha + m \tan \alpha}$$



число степеней свободы: 1

$$(1) M\ddot{x} = T - F_{sp} = T - k \cdot N$$

$$(2) N - Mg = 0 \quad N = Mg$$

$$(3) m\ddot{y} = mg + T$$

или переставляя

$$\begin{aligned} x + y &= c \\ \dot{x} + \dot{y} &= 0 \end{aligned}$$

$$(1) - (3) \quad M(\ddot{x} - \ddot{y}) = -mg - kN$$

$$2M\ddot{x} = -mg - kMg$$

$$\ddot{x} = \ddot{y} = \frac{-g(m + kM)}{2M}$$

$$(1) - (3) \quad M\ddot{x} - m\ddot{y} = -kN + mg$$

$$M\ddot{x} + m\ddot{x} = -kN + mg$$

$$\ddot{x}(M + m) = -kN + mg$$

$$\ddot{x} = \frac{-kN + mg}{M + m} = \frac{-kMg + mg}{M + m}$$

$$\ddot{y} = \frac{kN - mg}{M + m} = \frac{kMg - mg}{M + m}$$

А если куллит не хватает:

$$T = F_{тр}$$

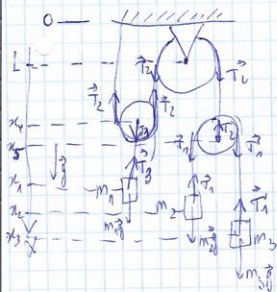
$$F_{тр} \leq \mu N$$

$$T = mg$$

$$mg \leq \mu Mg \Rightarrow m \leq \frac{\mu Mg}{g}$$

при таком условии
Куллит не хватает

N4



$$T_3 = 2T_2 = 4T_1$$

$$T_2 = 2T_1$$

снарядов = # пр-вств у пр-в. системы -
н-в. пр-вств = 3 - 1 = 2

$$|\vec{T}_1| = |\vec{T}_2|$$

$$l_1 = x_3 - x_5 + \pi R_1 + x_2 - x_5 + x_1 - x_4$$

$$l_2 = x_5 - L + \pi R_2 + x_4 - L + \pi R_3 + x_4$$

$$x_1 + x_2 + x_3 + x_4 - x_5 = \text{const}$$

$$\dot{x}_1 + \dot{x}_2 + \dot{x}_3 + \dot{x}_4 + 2\dot{x}_5 = 0$$

$$\ddot{x}_1 + \ddot{x}_2 + \ddot{x}_3 + 3\ddot{x}_4 = 0$$

$$x_1 - x_5 = \text{const} \quad \dot{x}_1 - \dot{x}_5 = 0$$

$$\Rightarrow 4\ddot{x}_1 + \ddot{x}_2 + \ddot{x}_3 = 0$$

$$x_1 + x_2 + x_3 - x_4 - 2x_5 = \text{const}$$

$$2x_4 + x_5 = \text{const}$$

$$2\dot{x}_4 = -\dot{x}_5$$

$$\ddot{x}_4 = -\ddot{x}_5$$

$$\begin{cases} m_3 \ddot{x}_3 = m_3 g - T_2/2 \\ m_2 \ddot{x}_2 = m_2 g - T_2/2 \\ m_1 \ddot{x}_1 = m_1 g - 2T_2 \end{cases}$$

$$\begin{cases} \ddot{x}_3 = g - \frac{T_2}{2m_3} \\ \ddot{x}_2 = g - \frac{T_2}{2m_2} \\ \ddot{x}_1 = g - \frac{2T_2}{m_1} \end{cases}$$

$$\Rightarrow 4(g - \frac{2T_2}{m_1}) + g - \frac{T_2}{2m_2} + g - \frac{T_2}{2m_3} = 0$$

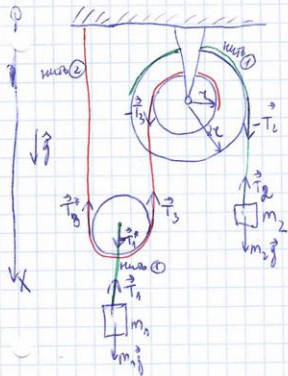
$$6g = \frac{8T_2}{m_1} + \frac{T_2}{2m_2} + \frac{T_2}{2m_3} \Rightarrow T_2 = \frac{6g}{\frac{8m_1 m_2 m_3}{m_1 + 2m_2 + 2m_3} + 1} = \frac{12g m_1 m_2 m_3}{16m_2 m_3 + m_1 m_3 + m_1 m_2}$$

$$\ddot{x}_1 = g - \frac{2T_2}{m_1} = \frac{16m_2 m_3 g + m_1 m_3 g + m_1 m_2 g - 24m_1 m_3 g}{16m_2 m_3 + m_1 m_3 + m_1 m_2} = \frac{-8m_1 m_3 g + m_1 m_3 g + m_1 m_2 g}{16m_2 m_3 + m_1 m_3 + m_1 m_2}$$

$$\ddot{x}_2 = g - \frac{T_2}{2m_2} = \frac{16m_2 m_3 g + m_1 m_3 g + m_1 m_2 g - 6m_1 m_3 g}{16m_2 m_3 + m_1 m_3 + m_1 m_2} = \frac{16m_2 m_3 g - 5m_1 m_3 g + m_1 m_2 g}{16m_2 m_3 + m_1 m_3 + m_1 m_2}$$

$$\ddot{x}_3 = g - \frac{T_2}{2m_3} = \frac{16m_2 m_3 g + m_1 m_3 g - 5m_1 m_2 g}{16m_2 m_3 + m_1 m_3 + m_1 m_2}$$

N 5.



степеней свободы = # координат управл. Ковот -
- # независимых р-ций = 2 - 1 = 1

$$\begin{cases} m_1 \ddot{x}_1 = m_1 g - T_1 \\ m_2 \ddot{x}_2 = m_2 g - T_2 \\ T_1 = 2 T_2 \end{cases}$$

Так как радиусы r_1 и r_2 равны, то $T_3 = 2 T_2$

$$\Rightarrow T_1 = 4 T_2$$

Пусть катушка повернется на угол φ относительно своей оси

$$\Delta l_{\text{шарика 1}} = 2 r_1 \varphi$$

$$\Delta l_{\text{шарика 2}} = r_2 \varphi$$

$$\begin{cases} 2 x_1 + r_1 \varphi = \text{const} \\ x_2 - 2 r_2 \varphi = \text{const} \end{cases} \quad \begin{cases} 2 \dot{x}_1 + r_1 \dot{\varphi} = 0 \\ \dot{x}_2 - 2 r_2 \dot{\varphi} = 0 \end{cases} \quad \begin{cases} r_1 \dot{\varphi} = -2 \dot{x}_1 \\ r_2 \dot{\varphi} = \frac{\dot{x}_2}{2} \end{cases}$$

$$\Rightarrow -2 \dot{x}_1 = \frac{\dot{x}_2}{2} \quad \dot{x}_2 + 4 \dot{x}_1 = 0$$

$$\ddot{x}_2 = -4 \ddot{x}_1$$

$$\Rightarrow \otimes m_2 \cdot (-4 \ddot{x}_1) = m_2 g - T_1/4$$

$$\begin{cases} m_1 \ddot{x}_1 = m_1 g - T_1 \end{cases}$$

$$-16 m_2 \ddot{x}_1 = 4 m_2 g - T_1$$

$$\Rightarrow m_1 \ddot{x}_1 = m_1 g - T_1$$

$$-16 m_2 \ddot{x}_1 - m_1 \ddot{x}_1 = g(4 m_2 - m_1)$$

$$\ddot{x}_1 = \frac{g(4 m_2 - m_1)}{-m_1 - 16 m_2} = \frac{g(m_1 - 4 m_2)}{m_1 + 16 m_2}$$

$$\ddot{x}_2 = \frac{-4 g(m_1 - 4 m_2)}{m_1 + 16 m_2}$$

$$r = \sqrt{x^2 + y^2 + z^2} \quad \lg \theta = \frac{\sqrt{x^2 + y^2}}{z} \quad \lg \varphi = \frac{x}{y} \quad N6$$

$$(\vec{e}_r, \vec{e}_\theta, \vec{e}_\varphi) = (\vec{e}_x, \vec{e}_y, \vec{e}_z) \begin{pmatrix} \sin \theta \cos \varphi & \cos \theta \cos \varphi & -\sin \varphi \\ \sin \theta \sin \varphi & \cos \theta \sin \varphi & \cos \varphi \\ \cos \theta & -\sin \theta & 0 \end{pmatrix}$$

$$\begin{aligned} \dot{\vec{e}}_r &= (\vec{e}_x \cdot \sin \theta \cdot \cos \varphi + \vec{e}_y \cdot \sin \theta \cdot \sin \varphi + \vec{e}_z \cdot \cos \theta)' = \\ &= \vec{e}_x \cdot \cos \theta \cdot \dot{\theta} \cdot \cos \varphi + \vec{e}_x \cdot \sin \theta (-\sin \varphi) \cdot \dot{\varphi} + \vec{e}_y \cdot \cos \theta \cdot \dot{\theta} \cdot \sin \varphi + \\ &+ \vec{e}_y \cdot \sin \theta \cdot \cos \varphi \cdot \dot{\varphi} + \vec{e}_z (-\sin \theta) \cdot \dot{\theta} = \\ &= \dot{\theta} (\vec{e}_x \cdot \cos \theta \cos \varphi + \vec{e}_y \cdot \cos \theta \sin \varphi - \vec{e}_z \cdot \sin \theta) + \\ &+ \dot{\varphi} (\vec{e}_x \cdot \sin \theta \sin \varphi + \vec{e}_y \cdot \sin \theta \cos \varphi) = \\ &= \dot{\theta} \cdot \vec{e}_\theta + \dot{\varphi} \cdot \vec{e}_\varphi \sin \theta \end{aligned}$$

$$\begin{aligned} \dot{\vec{e}}_\theta &= (\vec{e}_x \cdot \cos \theta \cdot \cos \varphi + \vec{e}_y \cdot \cos \theta \cdot \sin \varphi - \vec{e}_z \cdot \sin \theta)' = \\ &= \vec{e}_x \cdot (-\sin \theta) \cdot \dot{\theta} \cdot \cos \varphi + \vec{e}_x \cdot \cos \theta \cdot (-\sin \varphi) \cdot \dot{\varphi} + \\ &+ \vec{e}_y \cdot (-\sin \theta) \cdot \dot{\theta} \cdot \sin \varphi + \vec{e}_y \cdot \cos \theta \cdot \cos \varphi \cdot \dot{\varphi} - \vec{e}_z \cdot \cos \theta \cdot \dot{\theta} = \\ &= \dot{\theta} (-\vec{e}_x \cdot \sin \theta \cos \varphi - \vec{e}_y \cdot \sin \theta \sin \varphi - \vec{e}_z \cdot \cos \theta) + \\ &+ \dot{\varphi} (-\vec{e}_x \cdot \cos \theta \sin \varphi + \vec{e}_y \cdot \cos \theta \cos \varphi) = \\ &= \dot{\theta} \cdot (-\vec{e}_r) + \dot{\varphi} \cdot (\cos \theta) \cdot \vec{e}_\varphi = -\dot{\theta} \cdot \vec{e}_r + \dot{\varphi} \cdot \cos \theta \cdot \vec{e}_\varphi \end{aligned}$$

$$\begin{aligned} \dot{\vec{e}}_\varphi &= (-\vec{e}_x \sin \varphi + \vec{e}_y \cos \varphi)' = -\vec{e}_x \cdot \cos \varphi \cdot \dot{\varphi} + \vec{e}_y \cdot \sin \varphi \cdot \dot{\varphi} = \\ &= -\dot{\varphi} (\vec{e}_x \cdot \cos \varphi - \vec{e}_y \cdot \sin \varphi) = -\dot{\varphi} (\vec{e}_x \cos \varphi (\sin^2 \theta + \cos^2 \theta) + \vec{e}_y \sin \varphi (\sin^2 \theta + \cos^2 \theta)) \\ &= -\dot{\varphi} (\vec{e}_x \cdot \cos \varphi \cdot \sin^2 \theta + \vec{e}_y \cdot \sin^2 \theta \cdot \sin \varphi + \vec{e}_z \cdot \cos \theta \sin \theta + \\ &+ \vec{e}_x \cdot \cos^2 \theta \cos \varphi + \vec{e}_y \cdot \cos^2 \theta \sin \varphi - \vec{e}_z \cdot \sin \theta \cdot \cos \theta) = \\ &= -\dot{\varphi} (\vec{e}_r \cdot \sin \theta + \vec{e}_\theta \cdot \cos \theta) \end{aligned}$$

$$\vec{r} = r \cdot \vec{e}_r$$

$$\begin{aligned} \dot{\vec{r}} &= \dot{r} \cdot \vec{e}_r + r \cdot \dot{\vec{e}}_r = \dot{r} \vec{e}_r + r (\dot{\theta} \cdot \vec{e}_\theta + \dot{\varphi} \cdot \vec{e}_\varphi \sin \theta) = \\ &= \dot{r} \cdot \vec{e}_r + r \cdot \dot{\theta} \cdot \vec{e}_\theta + r \dot{\varphi} \sin \theta \vec{e}_\varphi \end{aligned}$$

$$\begin{aligned}
\vec{\ddot{r}} &= (\dot{r} \cdot \vec{e}_r + r \cdot \dot{\theta} \cdot \vec{e}_\theta + r \cdot \dot{\varphi} \cdot \sin \theta \cdot \vec{e}_\varphi)' = \\
&= \ddot{r} \cdot \vec{e}_r + \dot{r} \cdot \dot{\vec{e}}_r + \dot{r} \cdot \dot{\theta} \cdot \vec{e}_\theta + r \cdot \ddot{\theta} \cdot \vec{e}_\theta + r \cdot \dot{\theta} \cdot \dot{\vec{e}}_\theta + \\
&+ \dot{r} \cdot \dot{\varphi} \cdot \sin \theta \cdot \vec{e}_\varphi + r \cdot \ddot{\varphi} \cdot \sin \theta \cdot \vec{e}_\varphi + r \cdot \dot{\varphi} \cdot \cos \theta \cdot \dot{\theta} \cdot \vec{e}_\theta + r \cdot \dot{\varphi} \cdot \sin \theta \cdot \dot{\vec{e}}_\varphi = \\
&= \ddot{r} \cdot \vec{e}_r + \dot{r} (\dot{\theta} \vec{e}_\theta + \dot{\varphi} \sin \theta \vec{e}_\varphi) + r (\ddot{\theta} \vec{e}_\theta + \dot{\theta} \dot{\vec{e}}_\theta + \ddot{\varphi} \sin \theta \vec{e}_\varphi + \dot{\varphi} \cos \theta \dot{\vec{e}}_\theta + \\
&+ \dot{r} \cdot \dot{\varphi} \cdot \sin \theta \cdot \vec{e}_\varphi + r \cdot \ddot{\varphi} \sin \theta \cdot \vec{e}_\varphi + r \dot{\varphi} \cos \theta \cdot \dot{\theta} \cdot \vec{e}_\theta + \\
&+ r \cdot \dot{\varphi} \cdot \sin \theta \cdot (-\dot{\varphi}) (\vec{e}_r \sin \theta + \vec{e}_\theta \cos \theta) = \\
&= \vec{e}_r (\ddot{r} - r \dot{\theta}^2 - r \dot{\varphi}^2 \sin^2 \theta) + \vec{e}_\theta (2\dot{r} \dot{\theta} + r \ddot{\theta} - r \dot{\varphi}^2 \sin \theta \cos \theta) + \\
&+ \vec{e}_\varphi (2\dot{r} \dot{\varphi} \sin \theta + 2r \dot{\theta} \dot{\varphi} \cos \theta + r \ddot{\varphi} \sin \theta + r \dot{\varphi} \dot{\theta} \cos \theta) = \\
&= \vec{e}_r (\ddot{r} - r \dot{\theta}^2 - r \dot{\varphi}^2 \sin^2 \theta) + \vec{e}_\theta (2\dot{r} \dot{\theta} + r \ddot{\theta} - r \dot{\varphi}^2 \sin \theta \cos \theta) + \\
&+ 2\vec{e}_\varphi (2\dot{r} \dot{\varphi} \sin \theta + 2r \dot{\theta} \dot{\varphi} \cos \theta + r \ddot{\varphi} \sin \theta)
\end{aligned}$$

На \mathbb{R}^3 можно перейти к сферическим координатам или к цилиндрическим, т.к. переход к сферическим координатам называется сферическими координатами, а также, где любой из этих координат отличен от 0.