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Macroscopic Two-Pump Two-Vasculature Cardiovascular Model to Support Treatment of Acute Heart Failure

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Abstract— **Comprehensive understanding of hemodynamics remains a challenge even for expert cardiologists, partially due to a lack of an appropriate macroscopic model. We attempted to amend three major problems of Guyton's conceptual model (unknown left atrial pressure, unilateral heart damage, blood redistribution) and developed a comprehensive macroscopic model of hemodynamics that provides quantitative information. We incorporated a third axis of left atrial pressure, resulting in a 3D coordinate system. Pump functions of left and right heart are expressed by an integrated cardiac output curve, and the capacitive function of total vasculature by a venous return surface. The equations for both the cardiac output curve and venous return surface would facilitate precise diagnosis (especially evaluation of blood volume) and choice of appropriate treatments, including application to autopilot systems.**

I. Introduction

COMPREHSNSIVE understanding of hemodynamics remains a challenge even for specialist clinicians including cardiologists. This is in part attributed to a lack of an appropriate macroscopic model of hemodynamics that would facilitate reasoning. Most cardiologists relied only on, if at all, the classical Guyton's circulatory equilibrium framework [1].

Guyton's model consists of only two subdivisions of the whole circulation: the cardiopulmonary component (in which both hearts and pulmonary vasculature are lumped) and the systemic vascular bed. These two subdivisions are characterized by the 'cardiac output curve' and 'venous return curve', respectively. The 'cardiac output curve' approximated the (total) pump function, and the 'venous return curve' approximated the capacitive function of systemic vasculature. The intersection of these curves coincides with the operating point of the circulation.

Guyton's model is, however, inappropriate (see MODEL AND METHODS) for the understanding of hemodynamics in patients with, for example, acute myocardial infarction, where only one ventricle is preferentially damaged. That is why many cardiologists gradually abandoned using Guyton's model for their reasoning.

If we can amend the shortcomings of Guyton's model and develop a more appropriate model, the new model would obviously help diagnosis procedures and treatment selection. Furthermore, the model may be able to quantify the hemodynamic abnormalities rather than just to identify them.

Therefore, the aim of this study was to develop a comprehensive macroscopic model of hemodynamics that would provide quantitative information and aid diagnosis and treatments.

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II. Model and Methods

A. Shortcomings of Guyton's Model

Guyton's model has a number of problems when used in patients with unilateral heart failure.

First, the model does not provide left atrial pressure (LAP) values directly. LAP indicates the degree of pulmonary congestion and blood desaturation, and is as important as cardiac output (CO) and blood pressure.

Second, it is impossible to precisely model unilateral heart failure, which is frequently seen in patients with ischemic heart disease.

Third, in unilateral heart failure, the relative blood volumes in pulmonary and systemic vascular beds vary. As Guyton's model assumes only blood volume within the systemic vascular bed, such redistribution would shift the venous return curve even though the total blood volume remains the same.

B. Development of Comprehensive Cardiovascular Model

To solve the above problems, we extended Guyton's model.

First, a third axis of LAP was introduced in our new model (Fig. 1) [2], [3], so that LAP can be obtained directly. The pumping ability of the heart and the capacitive function of the vasculature are expressed simultaneously in the 3D space (RAP-LAP-CO coordinate system).

Second, the pumping abilities of the left and right heart are expressed separately by the respective cardiac output surfaces that are independent of each other. In an equilibrium state, by matching the cardiac output of both sides, the pumping ability of the whole heart can be integrated and expressed by a curve

expressing the intersection of the two surfaces (integrated cardiac output curve, Fig. 1, thick curve).

Third, the capacitive function of total vasculature (including both systemic and pulmonary vasculatures) is expressed by the venous return surface (Fig. 1, shaded surface), which is an extension of the venous return curve. This surface expresses the changes in LAP and right atrial pressure (RAP) in response to CO change, while the total intravascular blood volume remains constant. In addition, blood redistribution between systemic and pulmonary vasculatures (without change in total blood volume) will be expressed by movement within the surface rather than by deviation from the surface.

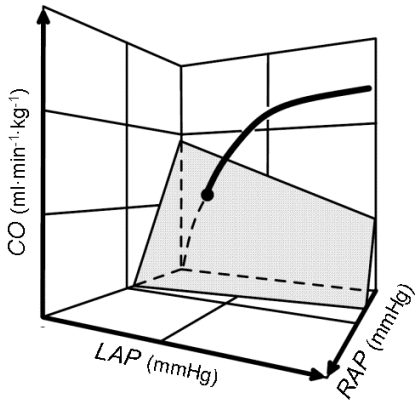

Fig. 1. An original macroscopic model of hemodynamics (an extended Guyton's model). The curve expresses the integrated pumping ability of left and right heart. The shaded surface characterizes the capacitive function of the total (systemic + pulmonary) vasculatures. The surface remains constant as long as the total intravascular blood volume remains the same. CO, cardiac output; LAP, left atrial pressure; RAP, right atrial pressure.

C. Animal Experiments to Characterize Venous Return Surface

Figure 2 depicts the scheme of an experiment to characterize the venous return surface. We replaced the left and right heart with roller pumps, which allows us to change CO of the right heart or left heart independently.

By adjusting the flow (i.e., CO) of the two pumps to the same level, the changes in RAP and LAP in response to a change in CO can be observed. Blood redistribution between systemic and pulmonary vasculatures can be reproduced by transiently unbalancing the flow of the two pumps.

From each dog (n = 6), we obtained 6 different sets of data (CO, RAP, LAP). These data were subjected to bivariate linear regression using RAP and LAP as independent variables and CO as the dependent variable.

III. Results

Figure 3 illustrates the venous return surfaces obtained from 6 dogs. Bivariate linear regression in each animal yielded a flat surface in 3D space. The surface is shown as a line in Fig. 3, because we have projected the surface in a

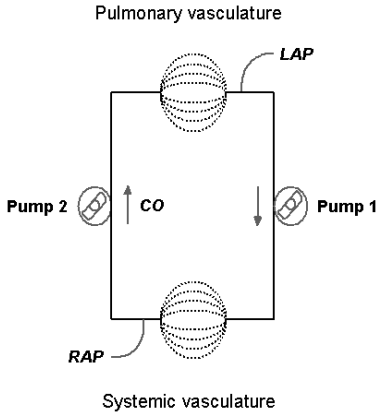

Fig. 2. An experimental scheme to characterize venous return surface. By replacing the left and right heart with roller pumps, one can change cardiac output of the right heart or left heart independently.

direction parallel to the surface. The experimental data obtained from each of the 6 animals showed good fit with the surface. In addition, the surfaces obtained from 6 animals were almost parallel, as shown by the nearly parallel 3D coordinate axes. These experimental results indicated that the venous return surface is linear and can be expressed by a common equation for all animals.

Further, by infusing or withdrawing known amounts of blood, we were able to derive an equation for the venous return surface as follows:

$$CO = V / 0.129 - 19.61\ RAP - 3.49\ LAP$$

where V is total intravascular stressed blood volume. This formula [$V = (CO + 19.61\ RAP + 3.49\ LAP) \times 0.129$] can be used to quantify V from CO, RAP and LAP.

We also succeeded to quantify the integrated cardiac output curve by logarithmic functions as follows:

$$CO = S_L\ [\ln(LAP-2.03)+0.80]$$

$$CO = S_R\ [\ln(RAP-2.13)+1.90]$$

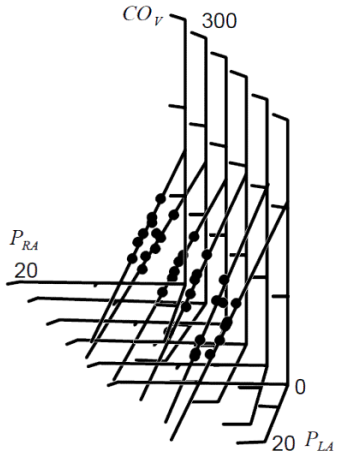

Fig. 3. Superimposed venous return surfaces obtained from 6 dogs. For each dog, the venous return surface (RAP-LAP-CO relationship) in 3D coordinate system was projected in a direction parallel to the surface, and was superimposed with each other.

where S_L and S_R are parameters expressing the pumping ability of the left and right heart, respectively. These equations are also useful for quantifying the pumping ability of right and left heart (S_L = CO / [ln(LAP - 2.03) + 0.80], S_R = CO / [ln(RAP - 2.13) + 1.90]).

Using this model, we are able to predict with acceptable precision the hemodynamics after infusion or withdrawal of known amounts of blood (CO: y = 0.93x + 6.5, r^2 = 0.96, SEE = 7.5 ml·min^{-1}·kg^{-1}; LAP: y = 0.90x + 0.5, r^2= 0.93, SEE = 1.4 mmHg; RAP: y = 0.87x + 0.4, r^2= 0.91, SEE = 0.4 mmHg) (Fig. 4) [3].

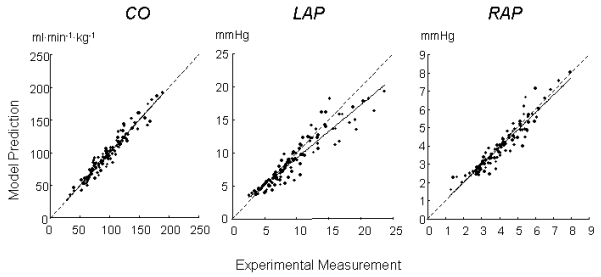

Fig. 4. Prediction of CO, LAP, and RAP based on our comprehensive macroscopic model of hemodynamics.

IV. Discussion

A. Difficulty in Decision Making of Heart Failure Treatment

Three hemodynamic variables: blood pressure, CO and LAP, appear to be the most essential factors influencing the survival of patients with heart failure. Our model clearly indicates that pump functions of left and right heart and total intravascular blood volume are determinants of CO and LAP. Systemic vascular resistance is an additional determinant of blood pressure.

For clinicians, the evaluation of blood volume is relatively difficult compared to pump functions and vascular resistance. In practice, clinicians have been using RAP as a proxy for blood volume. It is clear from our results [V = (CO + 19.61 RAP + 3.49 LAP) × 0.129] that blood volume (V) is not solely determined by RAP. Rather, all three parameters of CO, RAP and LAP are necessary to evaluate blood volume. The equation indicates that an increase of RAP by 1 mmHg is equivalent to an LAP increase of 5.6 mmHg, and a CO increase of 19.61 mL/min/kg (ca. 0.98 L/min for a 50-kg patient).

B. Application of the Model: Autopilot System

The biggest benefit of our comprehensive visual model of hemodynamics is that it enables us to diagnose the abnormality of cardiovascular system in a quantitative manner. This would lead to appropriate selection of drugs and their doses.

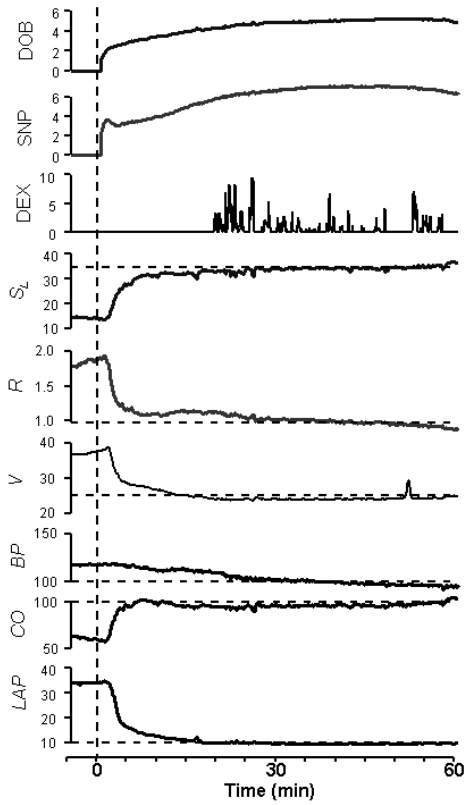

Fig. 5. An example of correction of hemodynamics with an autopilot system. By normalizing cardiovascular properties [pump function (S_L), resistance (R), blood volume (V)] with the administration of dobutamine (DOB), sodium nitroprusside (SNP), and dextran 40 solution (DEX), all the abnormal hemodynamic variables (increased blood pressure [BP], decreased cardiac output [CO], and elevated left atrial pressure [LAP]) were resolved rapidly, sufficiently, and stably.

As shown in Fig. 5, by translating hemodynamic variables into cardiovascular properties (pump function, vascular resistance, and blood volume), and by controlling each of these parameters with individual drug with preferential effect on the parameter, we are able to correct automatically all the parameters of blood pressure, CO and LAP rapidly, stably, and simultaneously.

Using an autopilot system to administer dobutamine (DOB at 5 ± 3 mg·kg^{-1}·min^{-1}), nitroprusside (SNP at 4 ± 2 mg·kg^{-1}·min^{-1}), dextran infusion (DEX at 2 ± 2 ml·kg^{-1}), and furosemide (10 mg in one, 20 mg in one) in 12 dogs with acute heart failure rapidly normalized blood pressure, CO, and LAP in 5 ± 7, 7 ± 5, and 12 ± 10 minutes, respectively. The normalized values remained stable thereafter (RMS values, blood pressure = 4 ± 3 mmHg, CO = 5 ± 2 ml·min^{-1}·kg^{-1}, LAP = 0.8 ± 0.6 mmHg).

V. Conclusion

We have successfully developed a comprehensive macroscopic model of hemodynamics that provides quantitative information. Using a 3D coordinate system, the pump functions of left and right heart are expressed by an

integrated cardiac output curve, and the capacitive function of total vasculature by a venous return surface. The equations of both the cardiac output curve and venous return surface would facilitate accurate diagnosis (especially evaluation of blood volume) and choice of appropriate treatments, including application to autopilot systems.

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