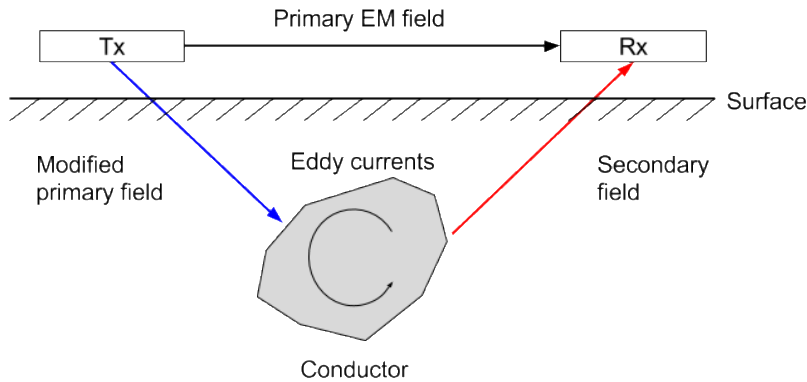


From last time

Circuit model of EM induction

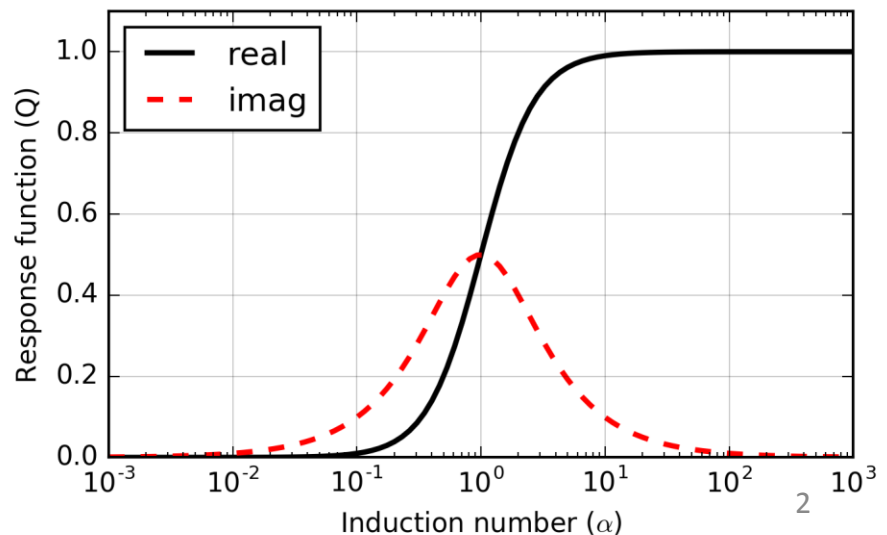


Magnetic field at the receiver

$$\frac{H^s}{H^p} = -\frac{M_{12}M_{23}}{M_{13}L} \underbrace{\left[\frac{\alpha^2 + i\alpha}{1 + \alpha^2} \right]}_Q$$

Induction Number

- Depends on properties of target $\alpha = \frac{\omega L}{R}$



Coupling coefficient:

- Depends on loop geometry

$$M_{12} = \frac{\mu_0}{4\pi} \oint \oint \frac{dl_1 \cdot dl_2}{|\mathbf{r} - \mathbf{r}'|^2}$$

Circuit model of EM induction

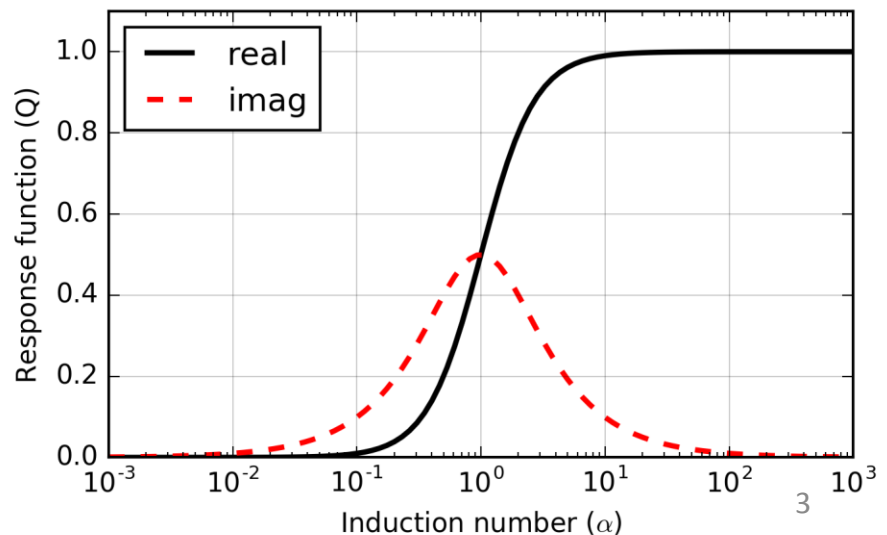
- If coupling between transmitter and target is bad ($M_{12} \sim 0$)
 $\rightarrow H_s \sim 0$
- If coupling between target and receiver is bad ($M_{23} \sim 0$)
 $\rightarrow H_s \sim 0$
- If transmitter frequency is low ($\omega \sim 0$)
 $\rightarrow \alpha \sim 0$
 $\rightarrow H_s \sim 0$
- If L/R is smaller, higher frequencies required for large response

Magnetic field at the receiver

$$\frac{H^s}{H^p} = -\frac{M_{12}M_{23}}{M_{13}L} \underbrace{\left[\frac{\alpha^2 + i\alpha}{1 + \alpha^2} \right]}_Q$$

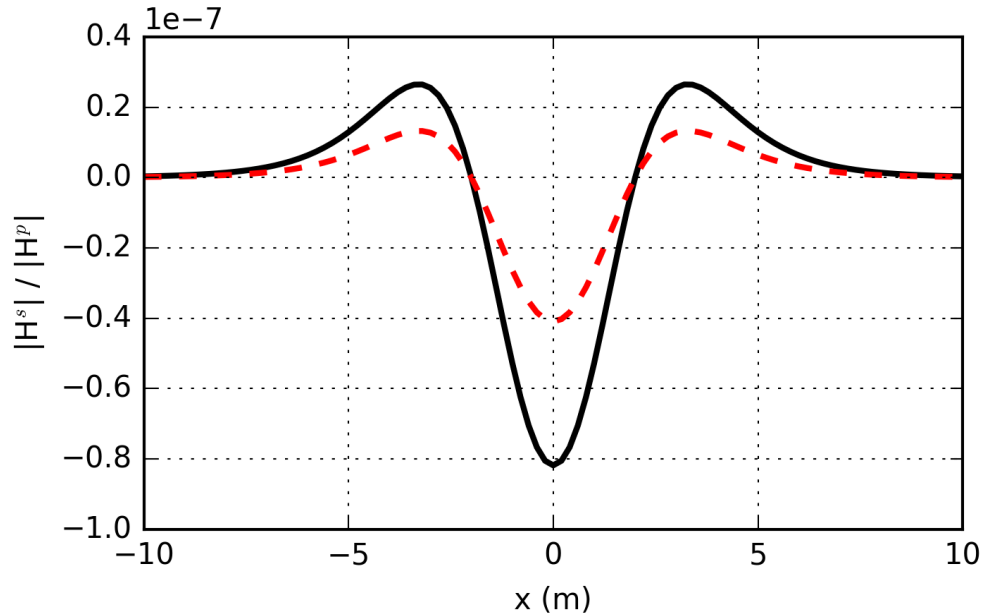
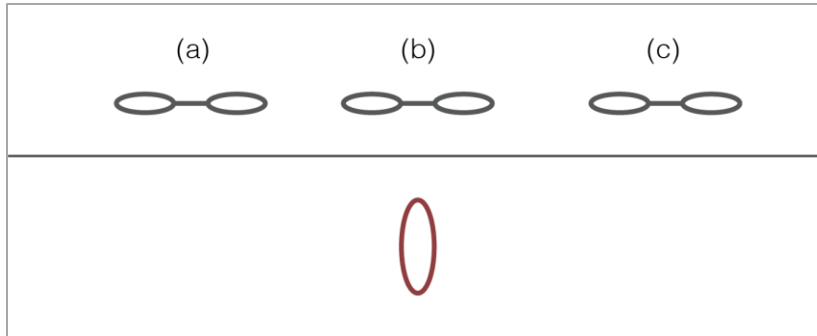
Induction Number

- Depends on properties of target $\alpha = \frac{\omega L}{R}$



Response from conductor in resistive Earth

Profile over the loop

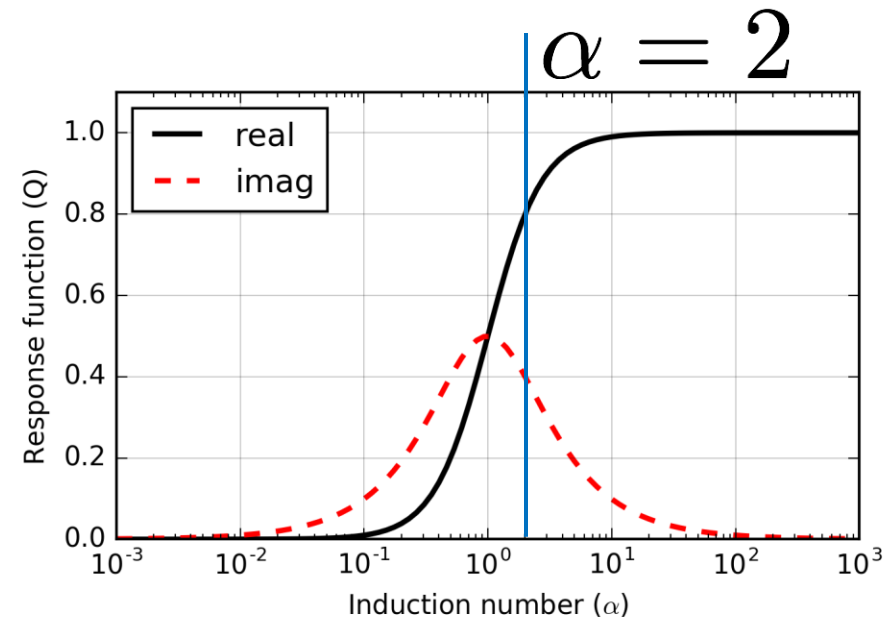


- Induction number

$$\alpha = \frac{\omega L}{R}$$

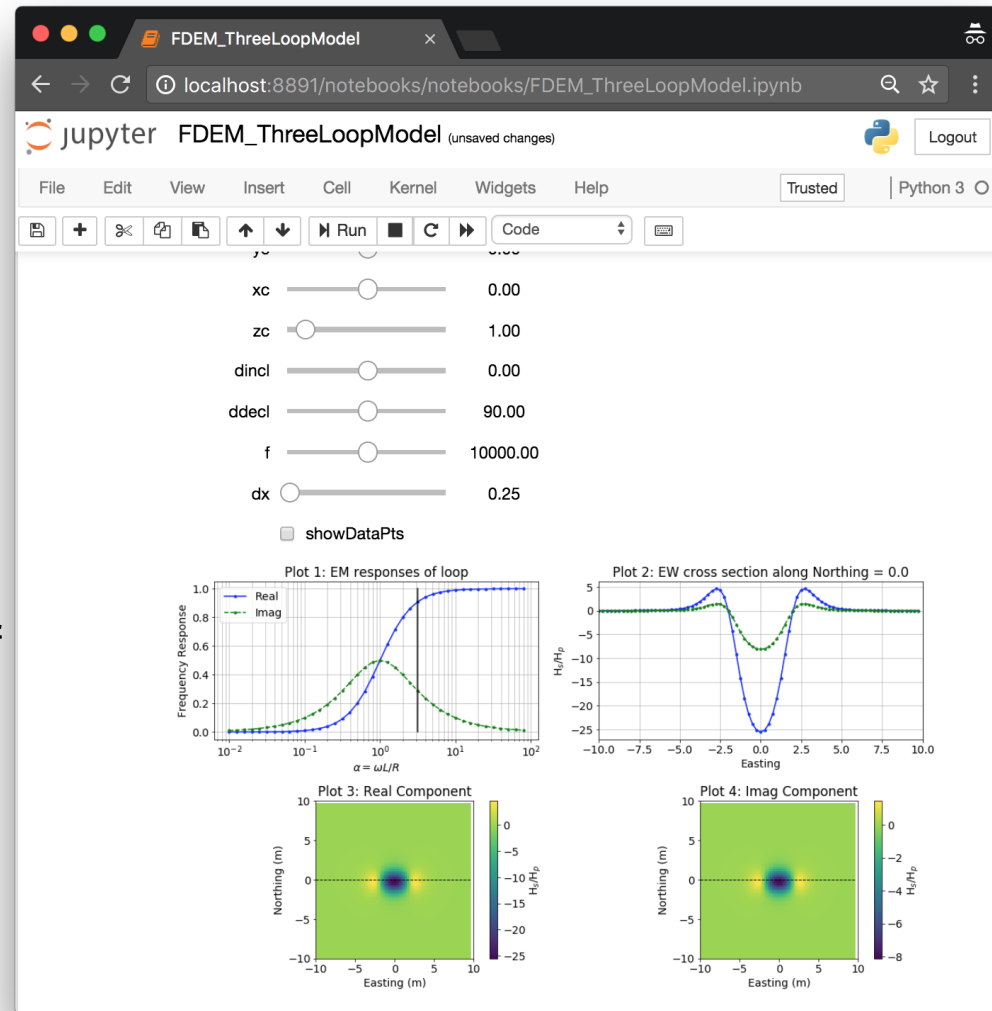
$$\alpha > 1$$

- When Real > Imag



App: Three Loop Model

- FDEM_ThreeLoopModel
- Parameters:
 - Location, separation of transmitter and receiver
 - Number of sounding locations
 - Orientation of target loop
 - Resistance, inductance of target loop
- View:
 - Response function
 - Real and imaginary components (plan view and a profile line)

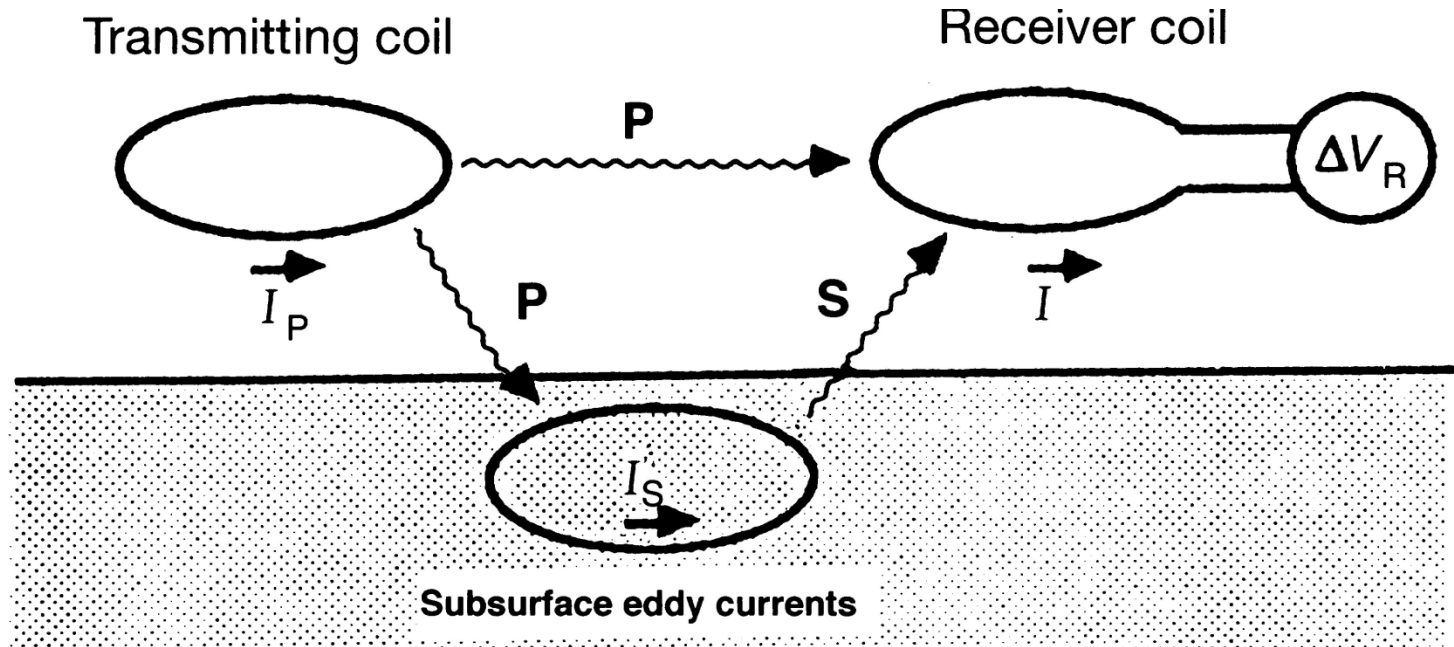


Today's Topics

- Basic Physics:
 - Attenuation and skin depth
 - Conductor in a non-resistive background
 - Basic physics recap
- Survey
 - Sources
 - Receivers
 - Sensitivity

Basic Physics: Attenuation and Skin Depth

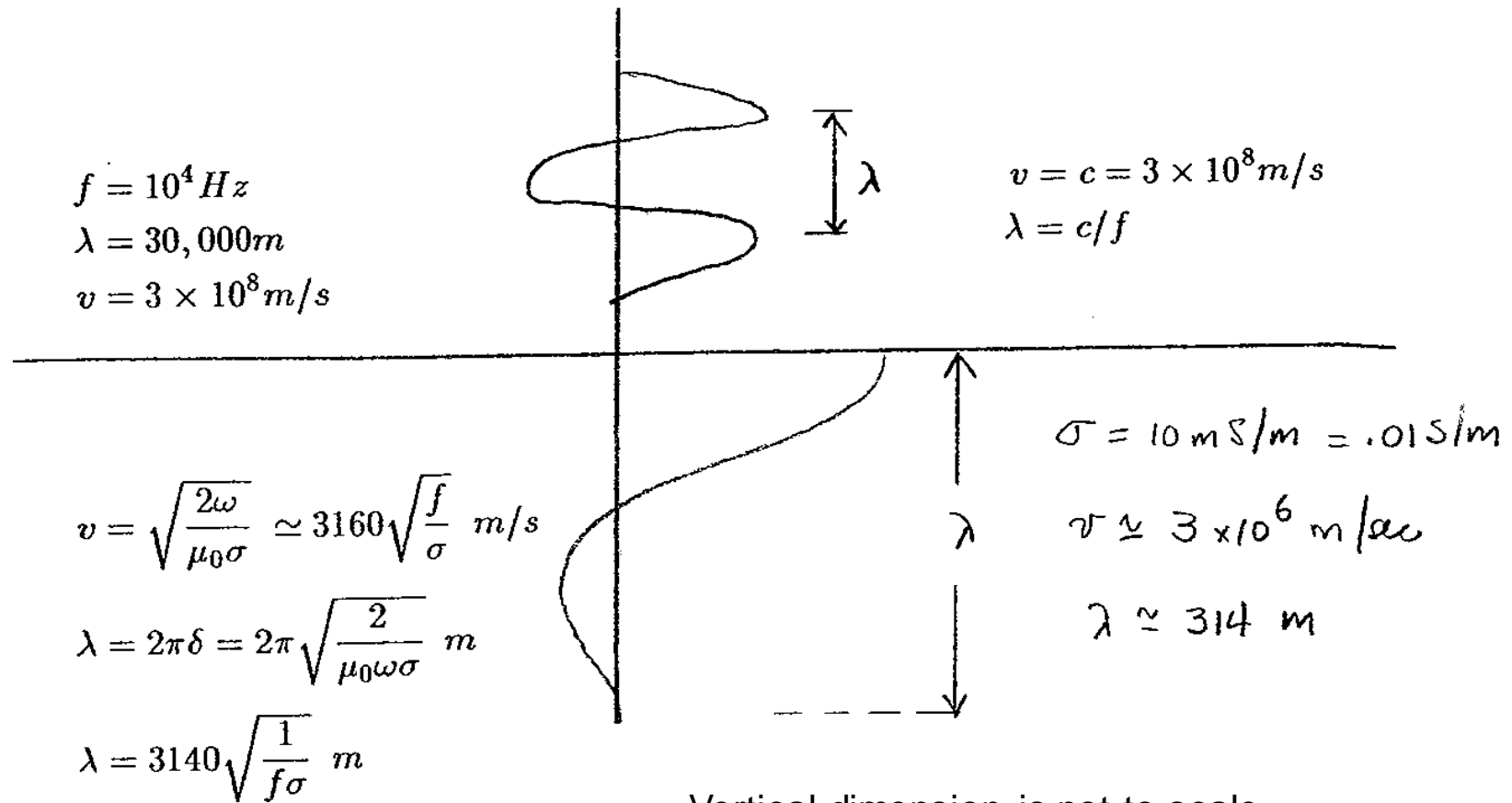
Earth has non-zero conductivity



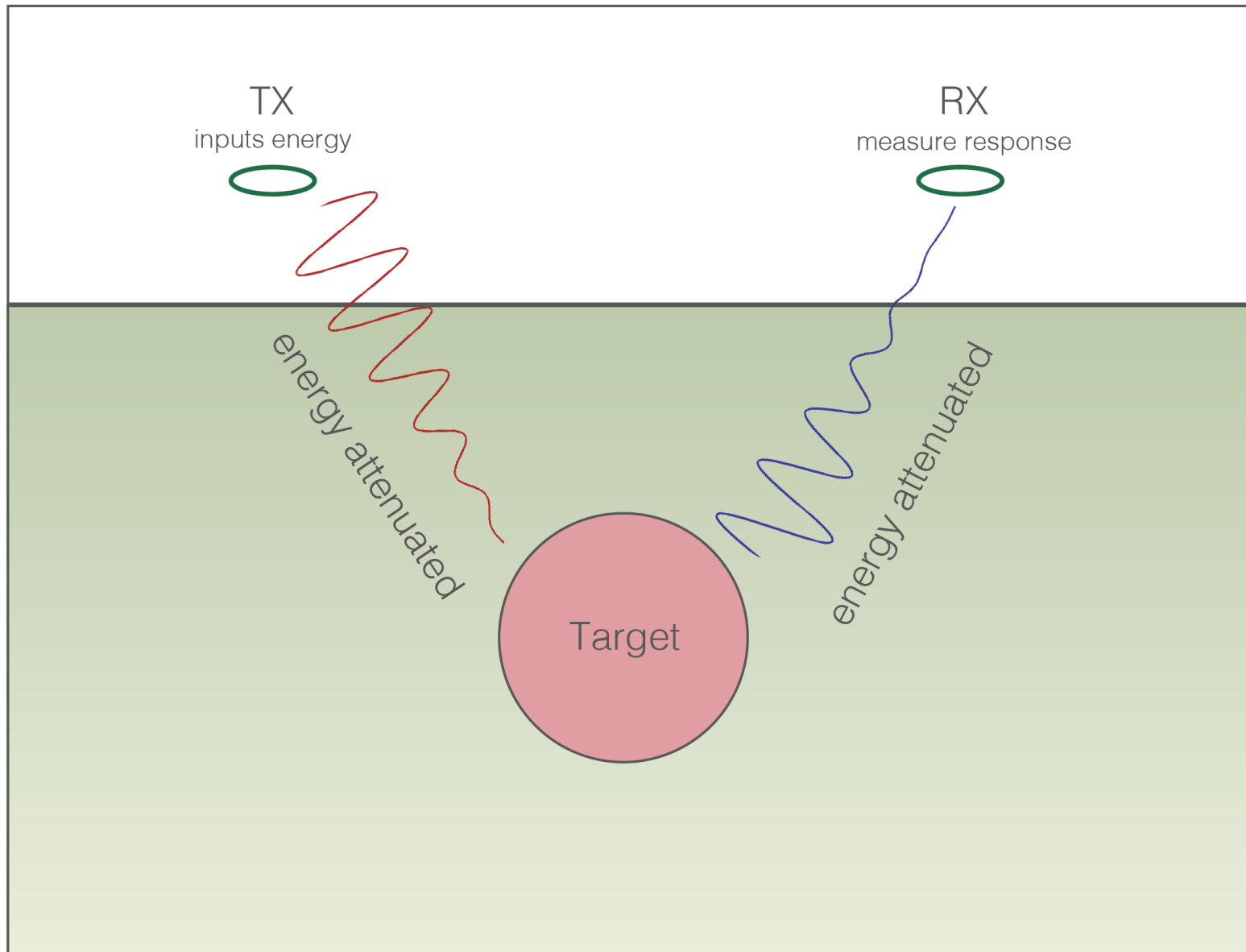
This results in 2 things:

- 1) EM signal attenuates on the way down and on the way up from the conductor
- 2) Currents induced in Earth resulting in secondary fields (we will ignore this effect for now)

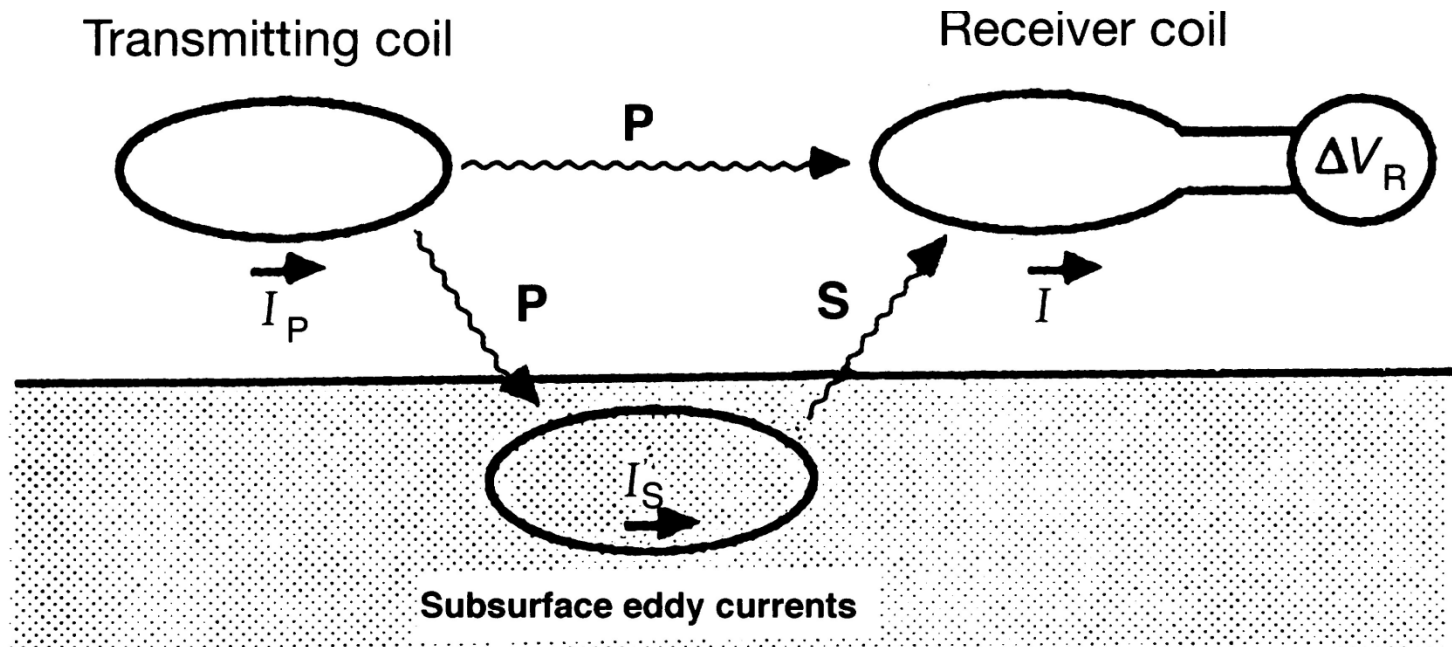
EM waves inside the earth



Attenuation of EM Signal



Depth of Investigation



Depth of investigation depends upon

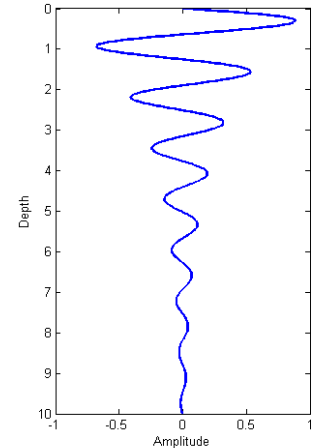
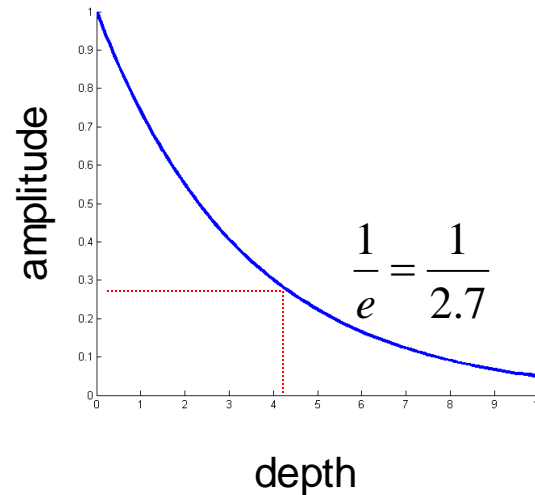
- skin depth
- source receiver geometry

Skin Depth

- EM waves decay when propagating in a conducting earth

- Skin depth

$$\delta \approx 500 \sqrt{\frac{\rho}{f}} \text{ meter}$$



where ρ is resistivity in Ωm
and f is frequency in Hz

Plane Wave apps

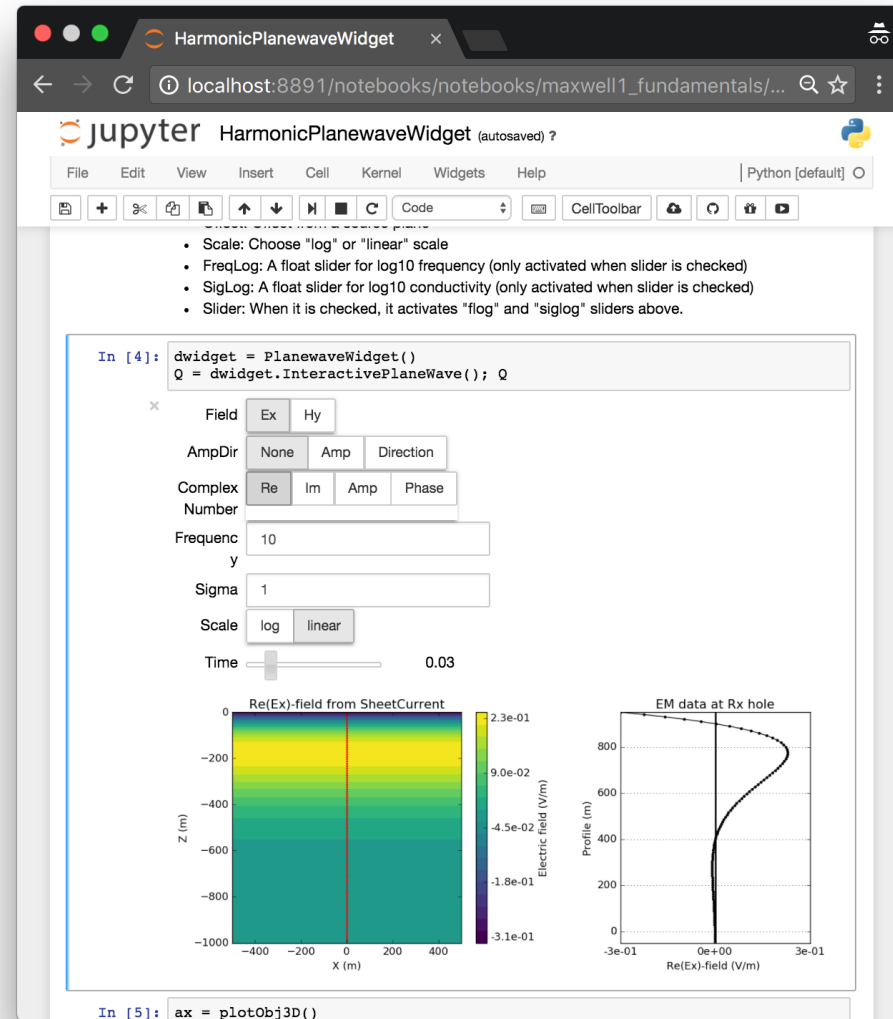
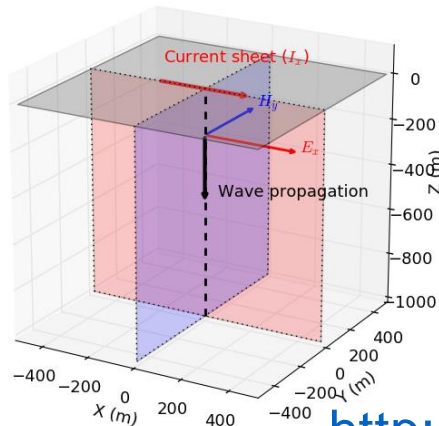
- 2 apps:

- Transient

$$h(t) = -\frac{(\mu\sigma)^{1/2}z}{2\pi^{1/2}t^{3/2}}e^{-\mu\sigma z^2/(4t)}$$

- Harmonic

$$\mathbf{H} = \underbrace{\mathbf{H}_0 e^{-\alpha z}}_{\text{attenuation}} \underbrace{e^{-i(\beta z - \omega t)}}_{\text{phase}}$$

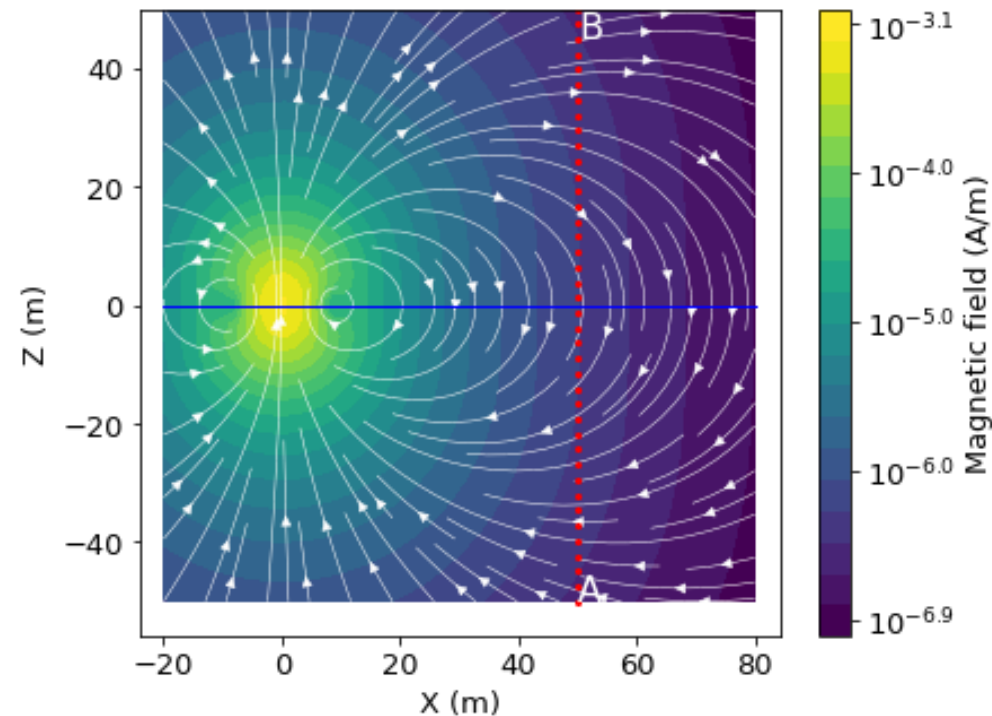


<http://em.geosci.xyz/apps.html>

Geometric Decay: dipole sources

- Primary field has a geometric decay away from the transmitter
 - very different from a plane wave source
- Two principal sources (for small transmitters characteristic of airborne surveys):
 - VMD: vertical magnetic dipole
 - HMD: horizontal magnetic dipole

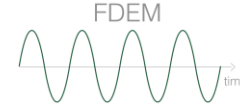
Magnetic field from a vertical magnetic dipole in a whole space



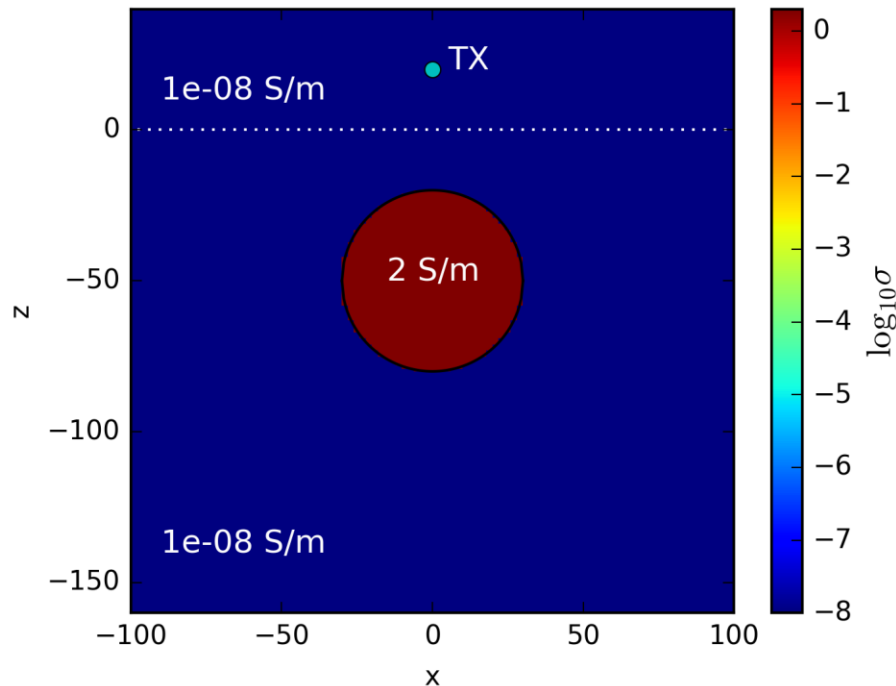
Basic Physics: Conductor in a Non-Resistive Background

Effects of background conductivity (frequency)

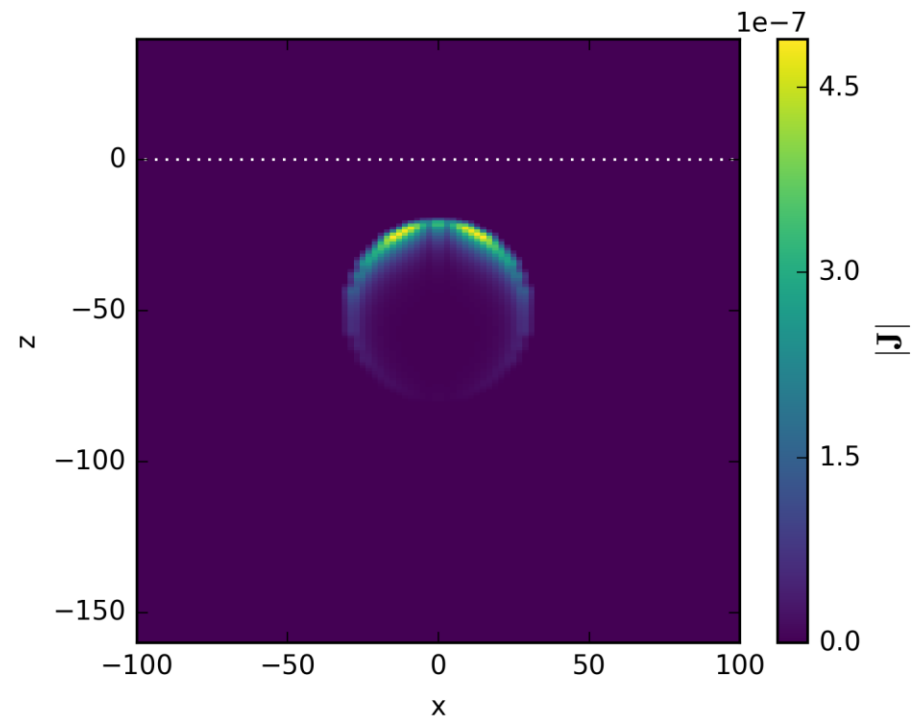
- Buried, conductive sphere
- Vary background conductivity
- Frequency: 10^4 Hz



10^{-8} S/m background



Current Density

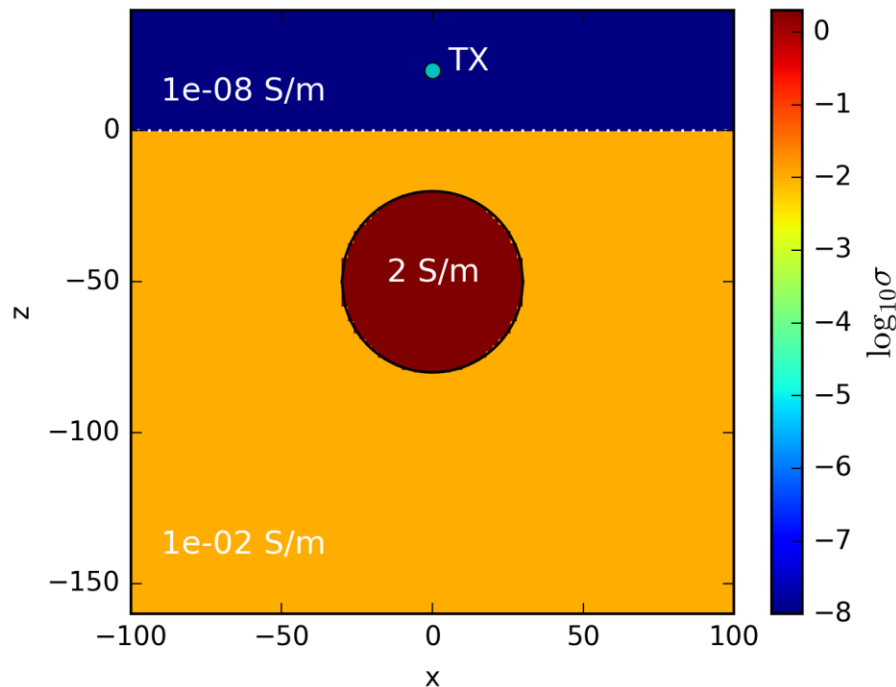


Effects of background conductivity (frequency)

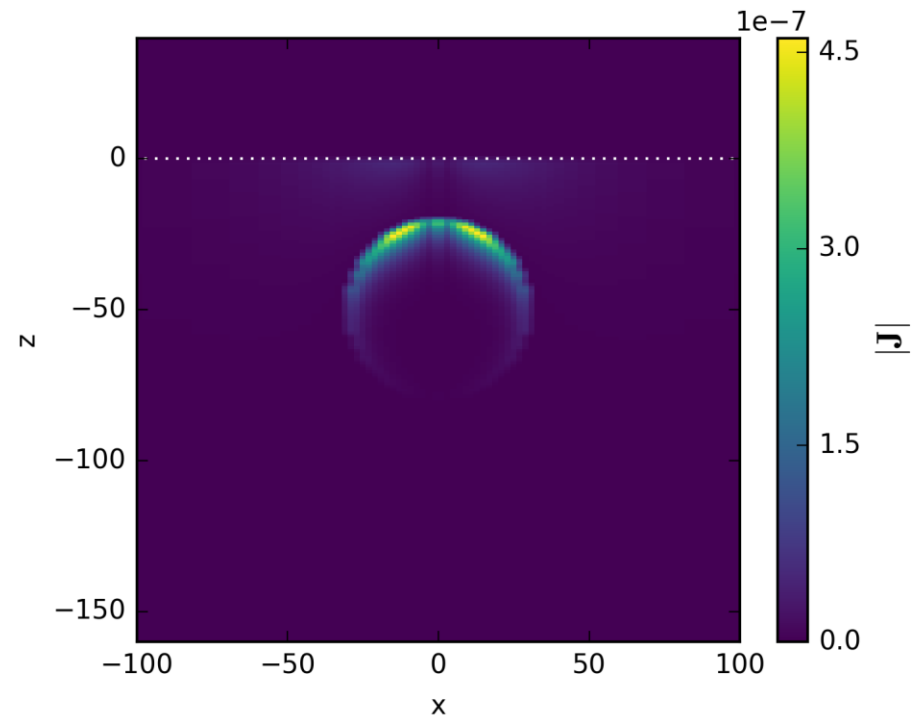
- Buried, conductive sphere
- Vary background conductivity
- Frequency: 10^4 Hz



10^{-2} S/m background



Current Density

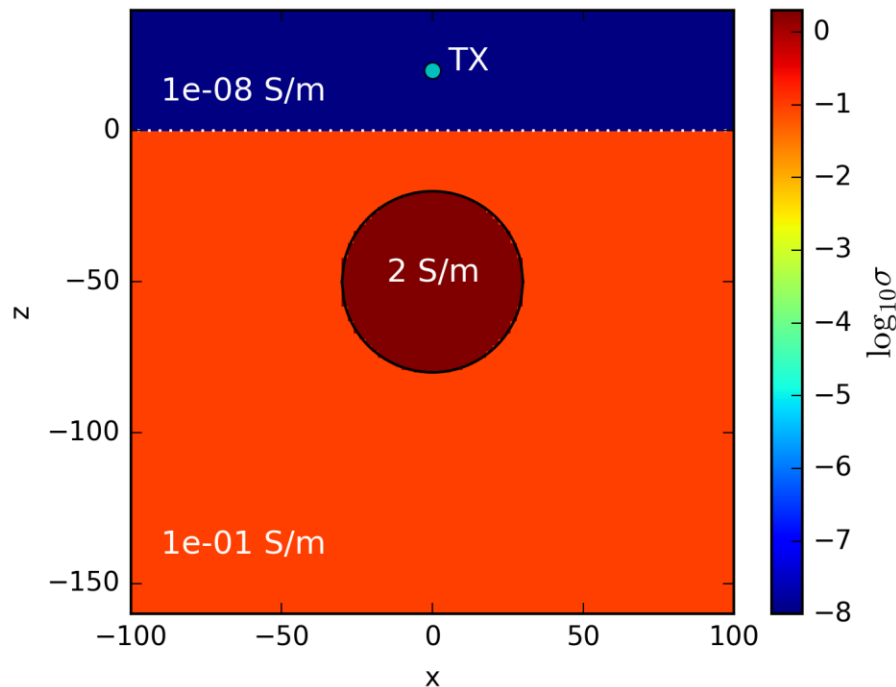


Effects of background conductivity (frequency)

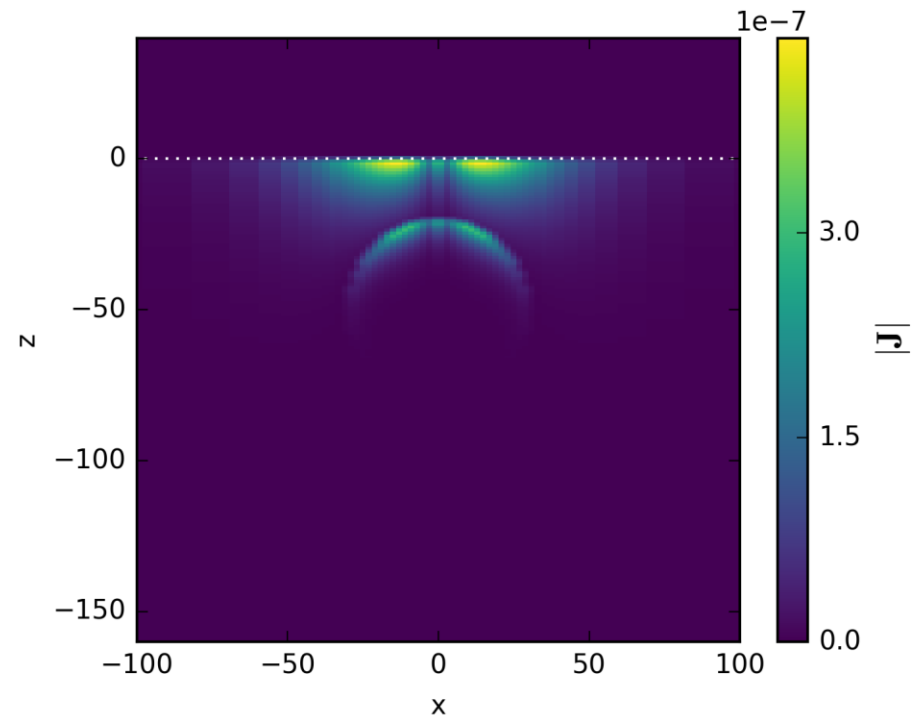
- Buried, conductive sphere
- Vary background conductivity
- Frequency: 10^4 Hz



10^{-1} S/m background



Current Density

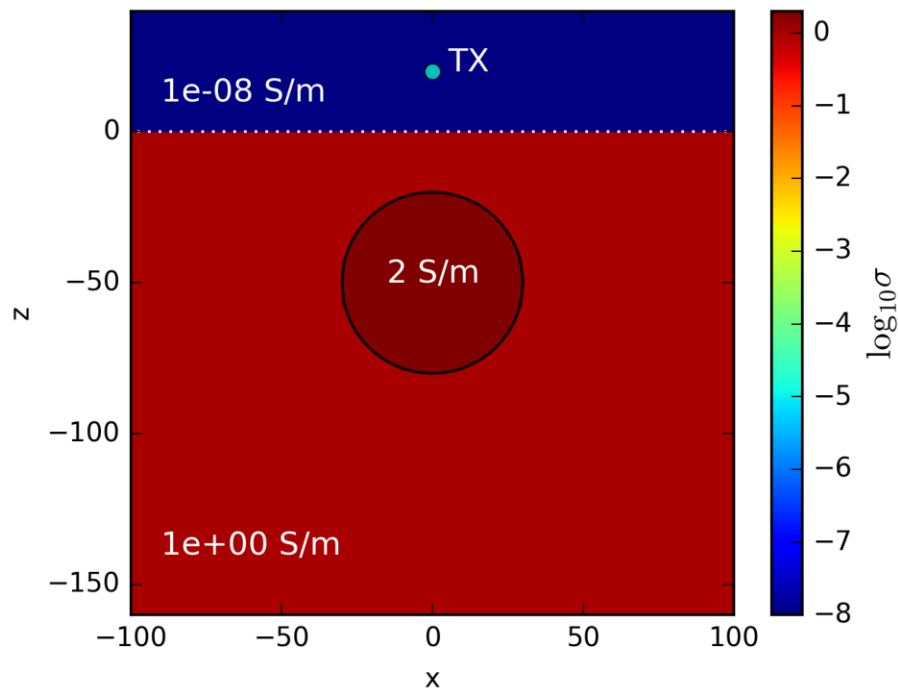


Effects of background conductivity (frequency)

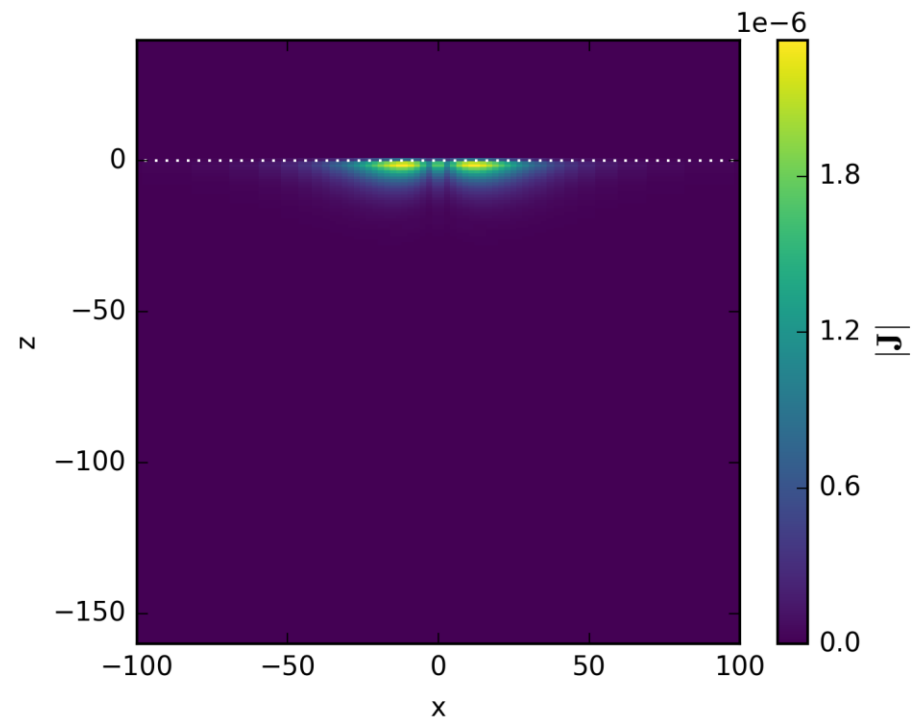
- Buried, conductive sphere
- Vary background conductivity
- Frequency: 10^4 Hz



1 S/m background

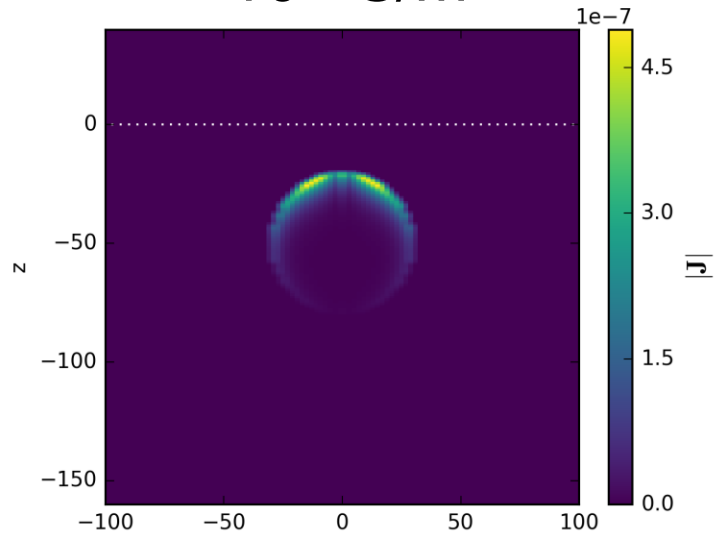


Current Density

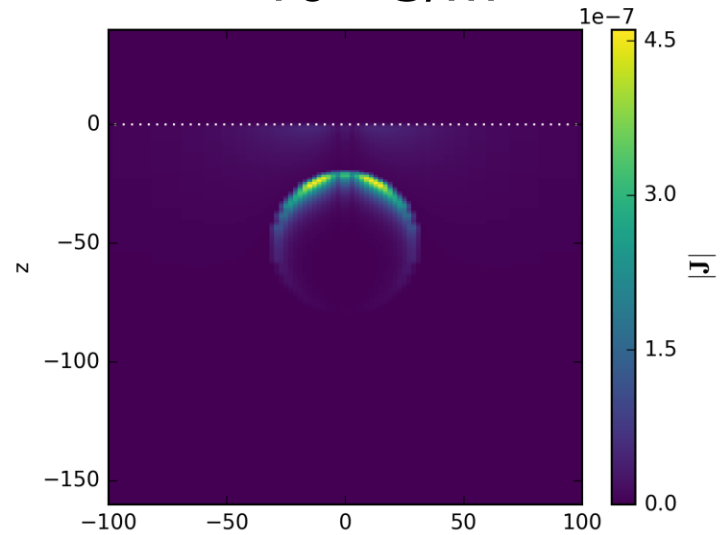


Effects of background conductivity (frequency)

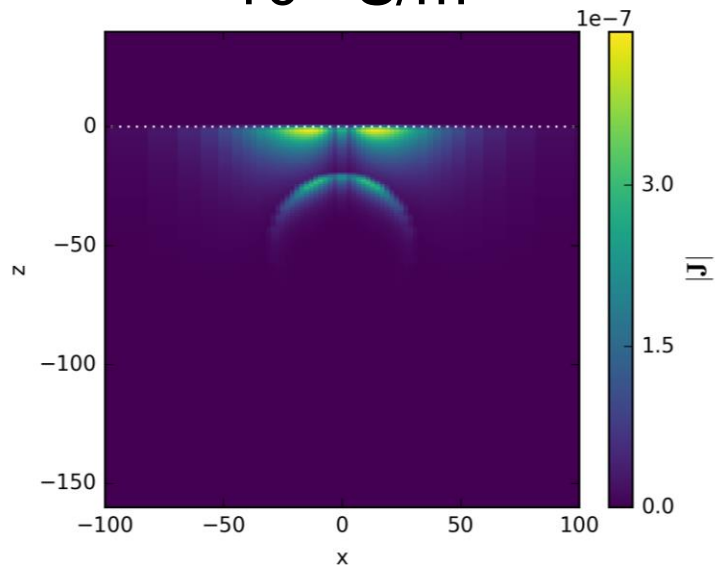
10^{-8} S/m



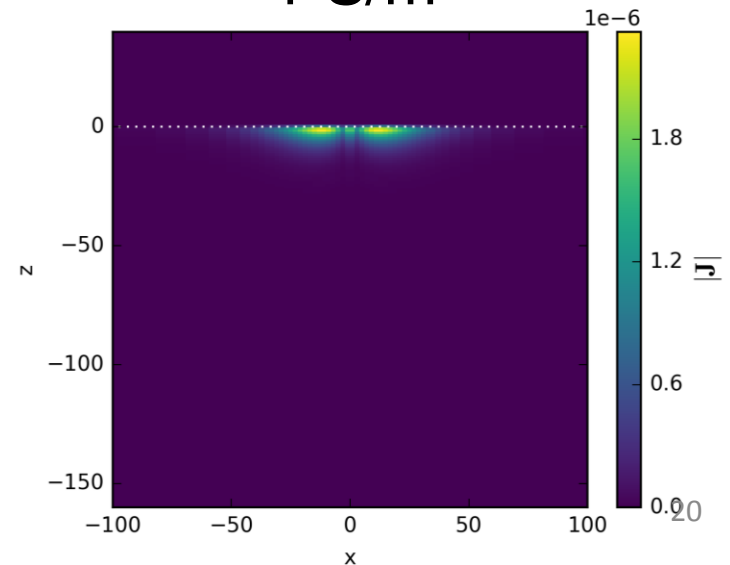
10^{-2} S/m



10^{-1^x} S/m



1 S/m

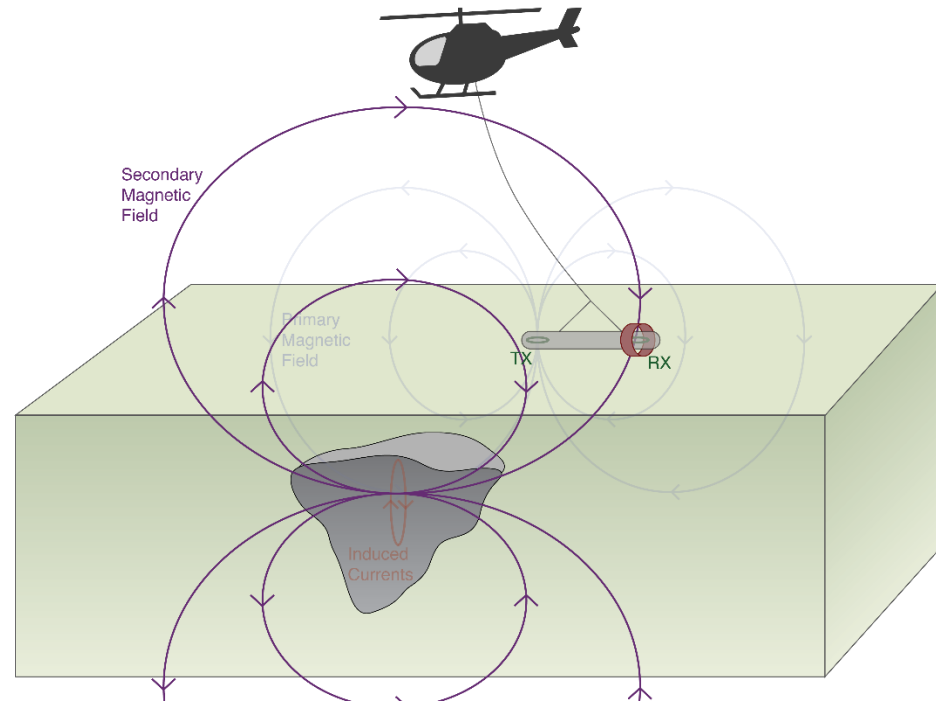


Basic Physics: Recap

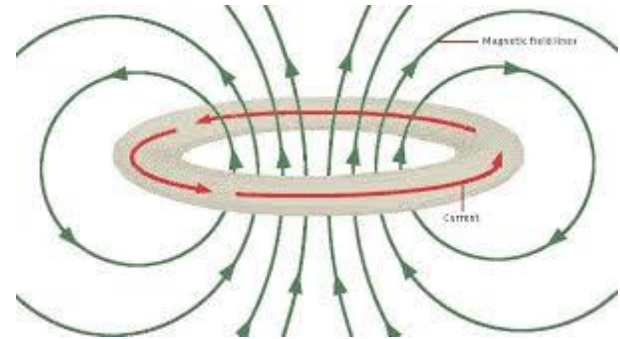
Basic Experiment

- **Source (Tx):**
Current loop makes primary magnetic field
- **Induction:**
Time-varying magnetic fields induce electric fields everywhere

→ Large induced currents in conductors
- **Secondary Fields:**
Induced currents in conductors produce secondary magnetic fields
- **Receiver (Rx):**
Measures magnetic fields



Directions

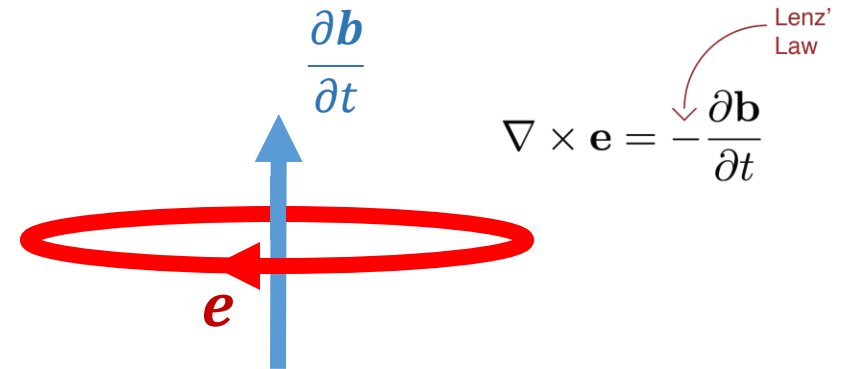


Ampere's Law: $\nabla \times \mathbf{H} = \mathbf{J}$

- Currents produce magnetic fields
- Right-hand rule

Faraday's Law

- Time/frequency varying magnetic fields produce electric fields
- Time/frequency varying magnetic flux generates voltage in wire loops
- Left-hand rule

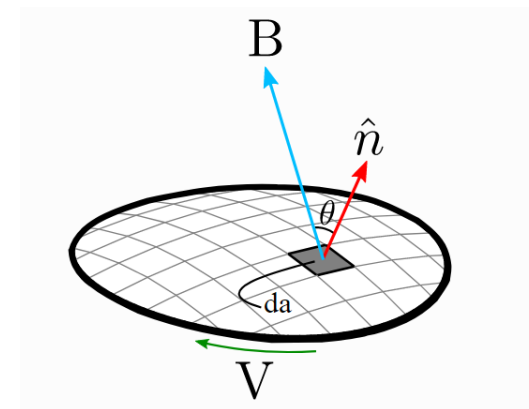


Ohm's Law

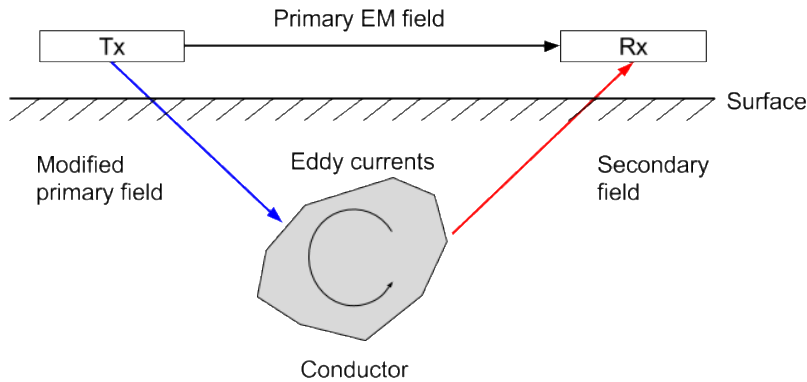
- Current resulting from electric fields depends on conductivity/resistivity

$$\vec{J} = \sigma \vec{E}$$

$$V = EMF = -\frac{d\phi_{\mathbf{b}}}{dt}$$



Circuit model of EM induction

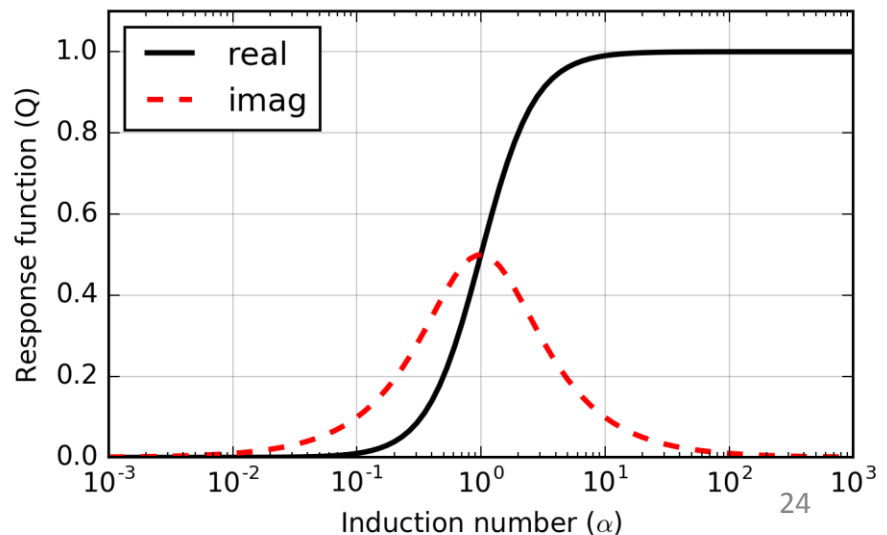


Magnetic field at the receiver

$$\frac{H^s}{H^p} = - \frac{M_{12}M_{23}}{M_{13}L} \underbrace{\left[\frac{\alpha^2 + i\alpha}{1 + \alpha^2} \right]}_Q$$

Induction Number

- Depends on properties of target $\alpha = \frac{\omega L}{R}$



Coupling coefficient:

- Depends on loop geometry

$$M_{12} = \frac{\mu_0}{4\pi} \oint \oint \frac{dl_1 \cdot dl_2}{|\mathbf{r} - \mathbf{r}'|^2}$$

Coupling

- If coupling between transmitter and target is bad ($M_{12} \sim 0$)
 $\rightarrow H_s \sim 0$
- If coupling between target and receiver is bad ($M_{23} \sim 0$)
 $\rightarrow H_s \sim 0$
- If transmitter frequency is low ($\omega \sim 0$)
 $\rightarrow \alpha \sim 0$
 $\rightarrow H_s \sim 0$
- If L/R is smaller, higher frequencies required for large response
- Coupling and EMF

$$EMF = -\frac{\partial \phi_{\mathbf{B}}}{\partial t}$$

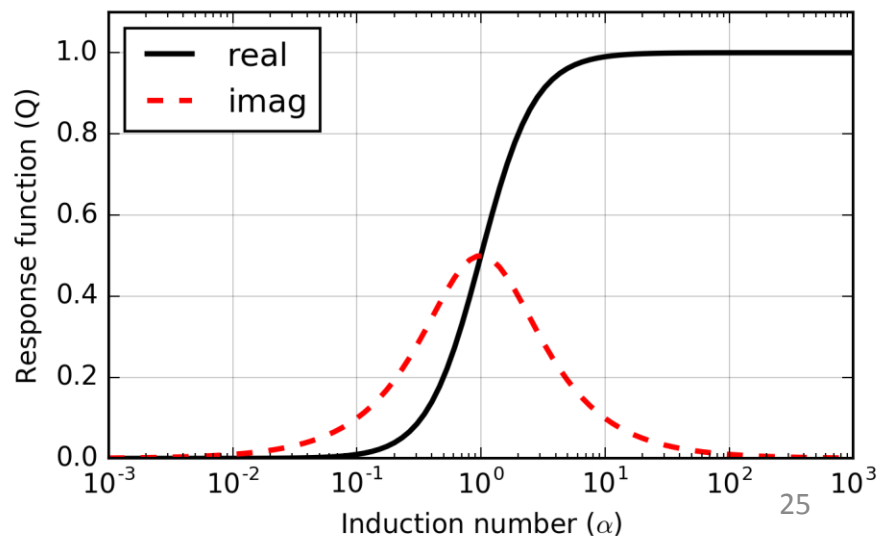
$$= -\frac{\partial}{\partial t} (\mathbf{B}_p \cdot \hat{\mathbf{n}}) A$$

Magnetic field at the receiver

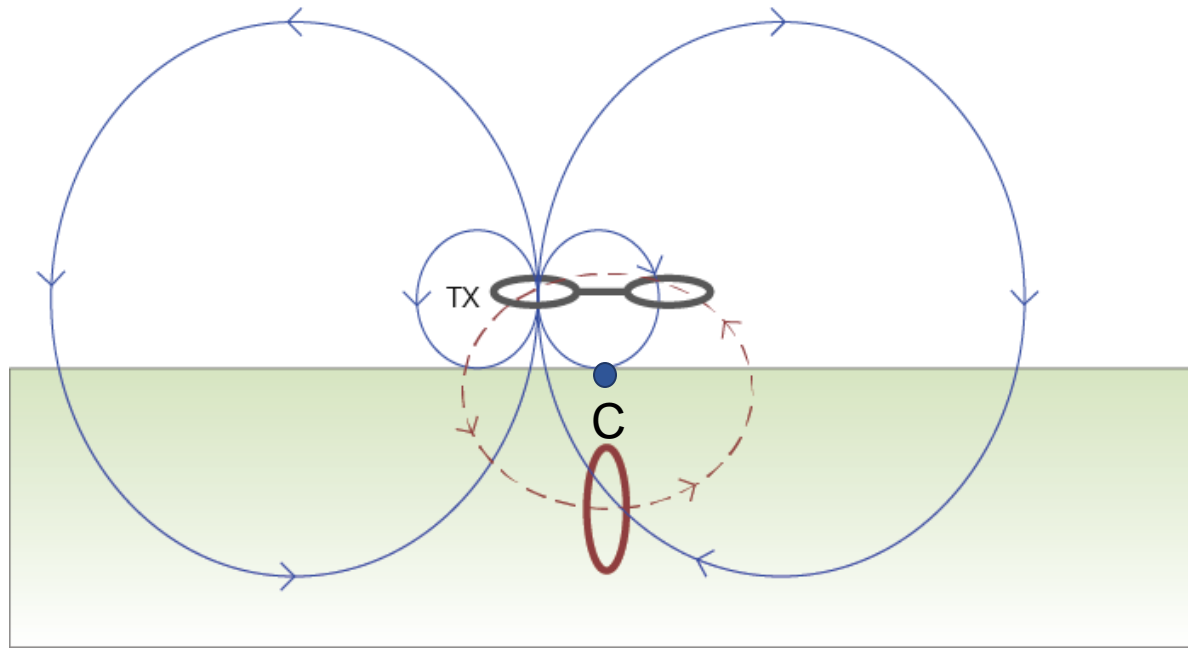
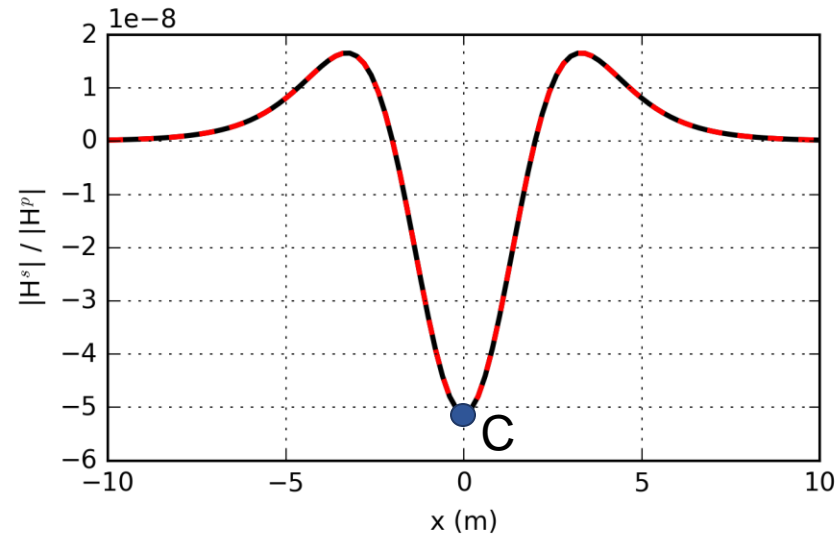
$$\frac{H^s}{H^p} = -\frac{M_{12}M_{23}}{M_{13}L} \underbrace{\left[\frac{\alpha^2 + i\alpha}{1 + \alpha^2} \right]}_Q$$

Induction Number

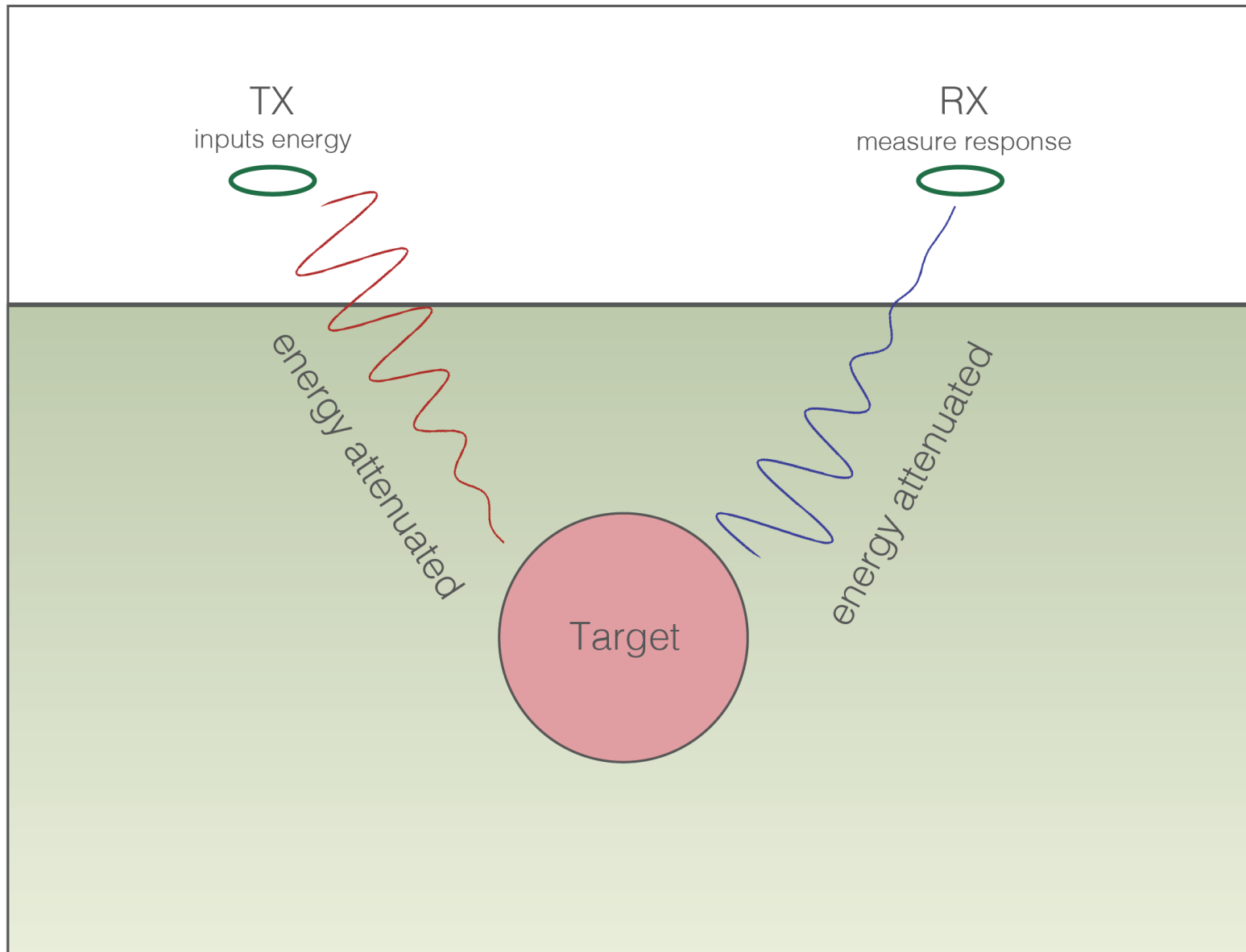
- Depends on properties of target $\alpha = \frac{\omega L}{R}$



Response over target

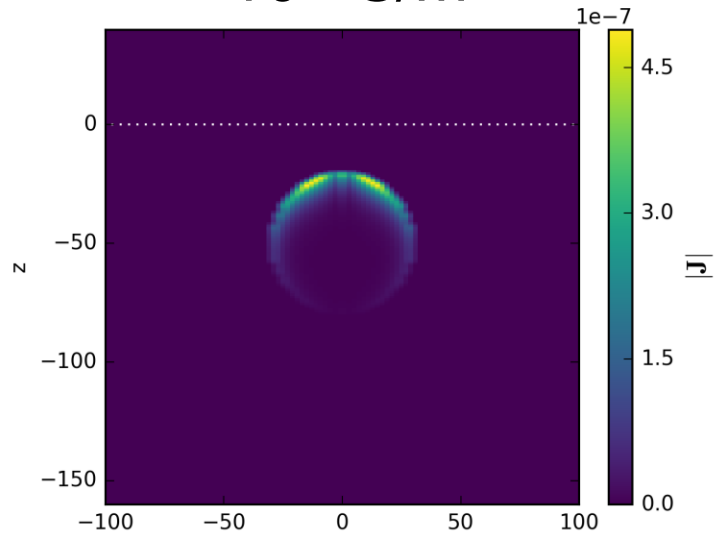


Attenuation of EM Signal

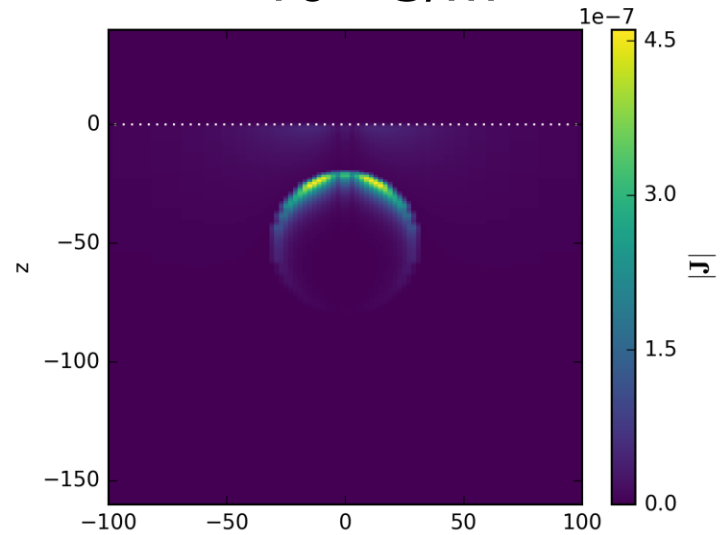


Effects of background conductivity (frequency)

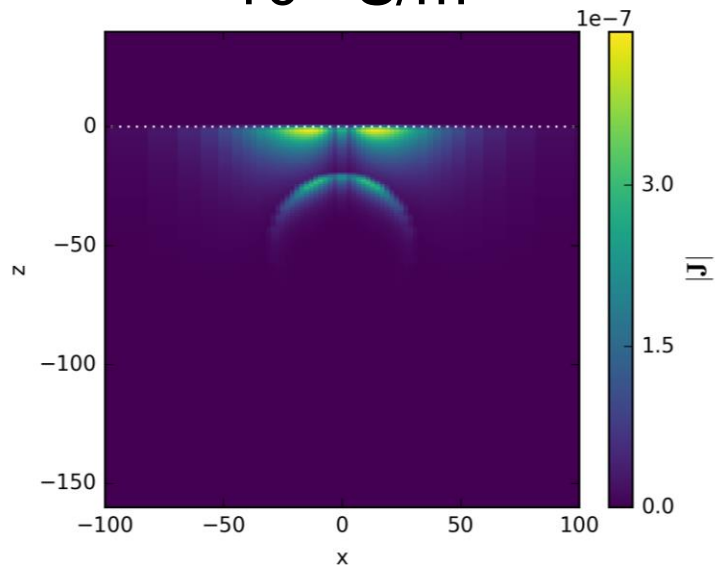
10^{-8} S/m



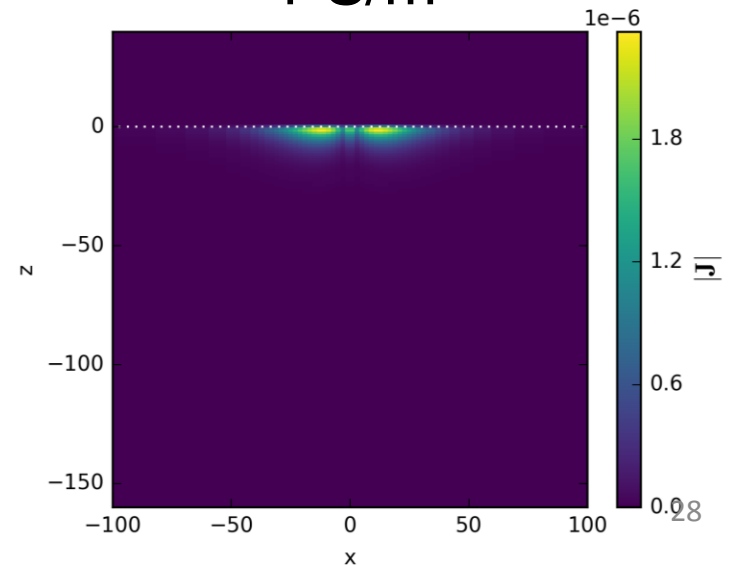
10^{-2} S/m



10^{-1} S/m



1 S/m



Survey

Reading on the GPG:

https://gpg.geosci.xyz/content/DC_resistivity/DC_surveys.html

Sources

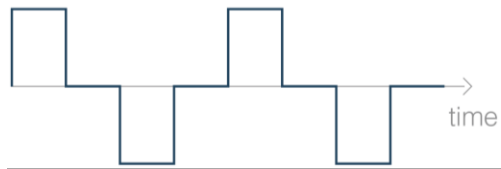
- Type
 - Inductive
 - Grounded

- Waveform

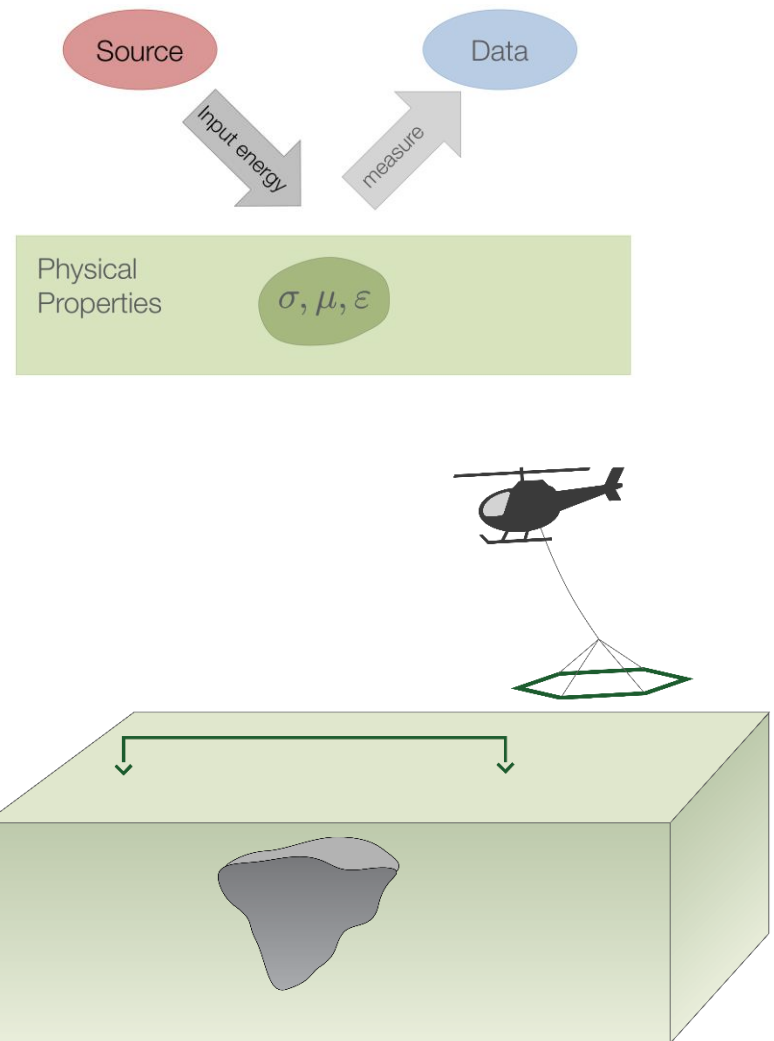
Harmonic
(FDEM)



Transient
(TDEM)

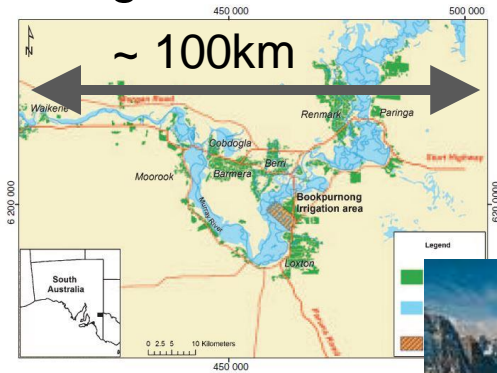


- Location
 - Airborne
 - Ground
 - Borehole



Applications for different sources

Large areas



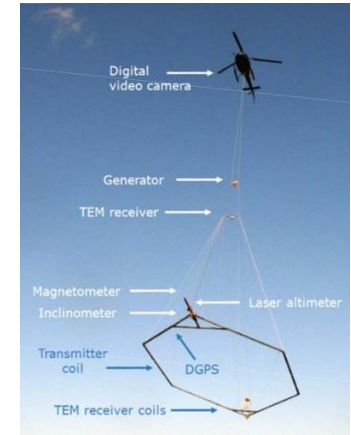
Rugged terrain



Airborne Survey

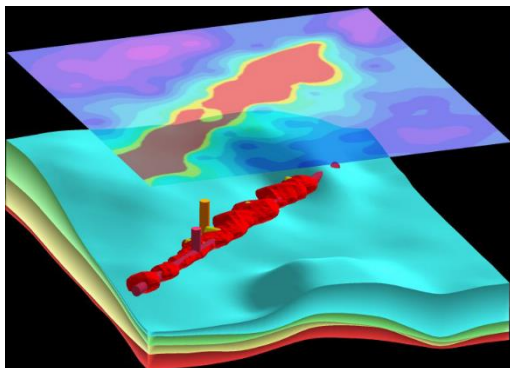


Resolve

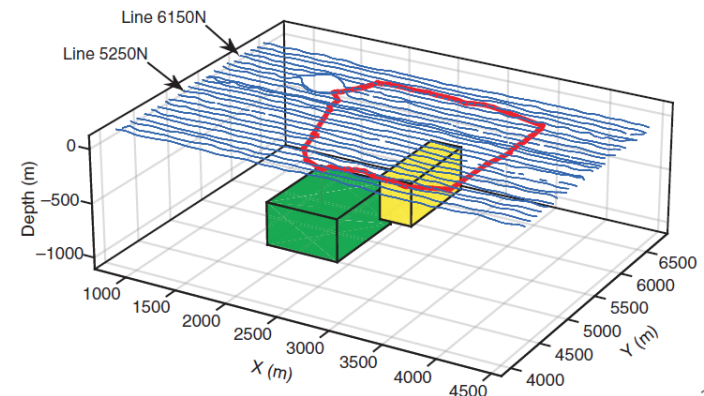


SkyTEM

Deep Targets

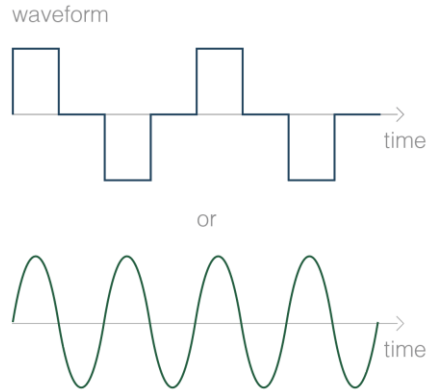


Large Loop



Transmitter considerations

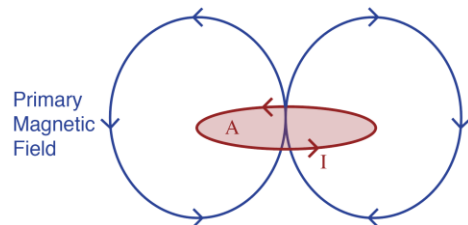
- Time or frequency?



- Key factor is moment

$$m = I \text{ (current)} A \text{ (area)} N \text{ (\# of turns)}$$

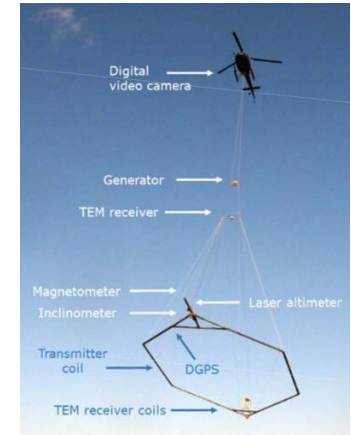
$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0}{4\pi} \left(\frac{3\mathbf{r}(\mathbf{m} \cdot \mathbf{r})}{|\mathbf{r}|^5} - \frac{\mathbf{m}}{|\mathbf{r}|^3} \right)$$



Airborne Survey

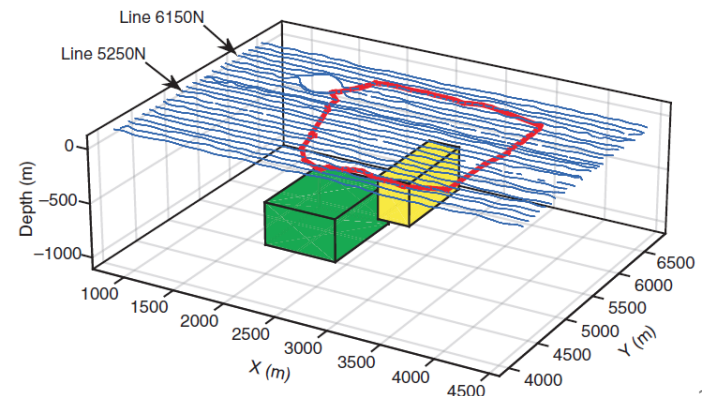


Resolve



SkyTEM

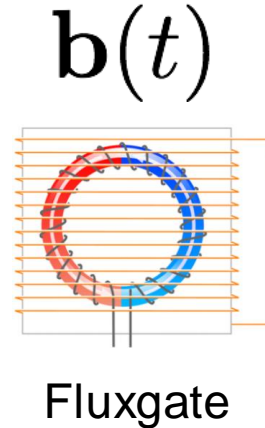
Large Loop



Receivers: Time Domain

Magnetometer

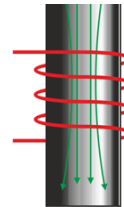
- Measures:
 - Magnetic fields
 - 3 components
- eg. 3-component fluxgate



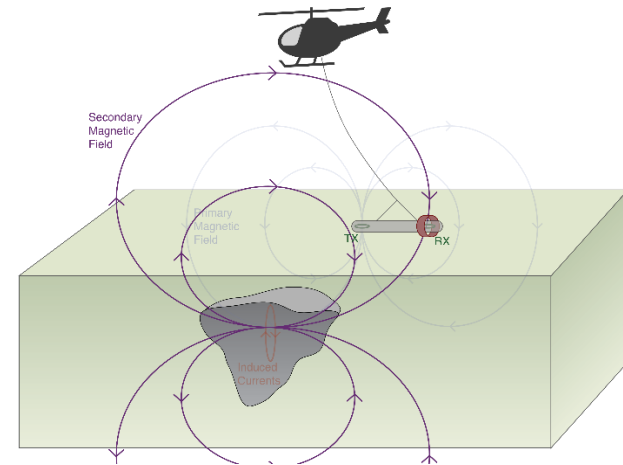
Coil

- Measures:
 - Voltage
 - Single component that depends on coil orientation
 - Coupling matters
- eg. airborne frequency domain
- ratio of H_s/H_p is the same as V_s/V_p

$$\frac{\partial b}{\partial t}$$



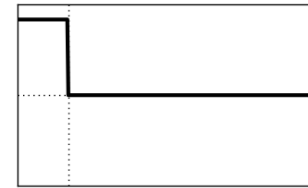
Coil



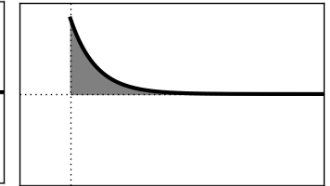
Receivers: Time Domain Data

- Primary field has off-time
- Measure secondary fields
- Receivers can be mounted on transmitter loop or above

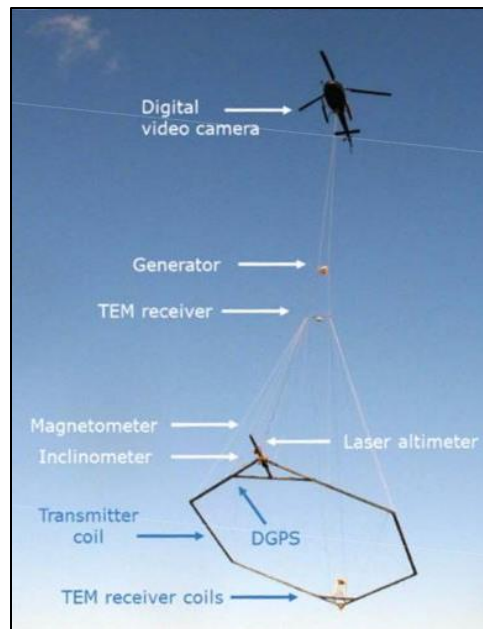
Current



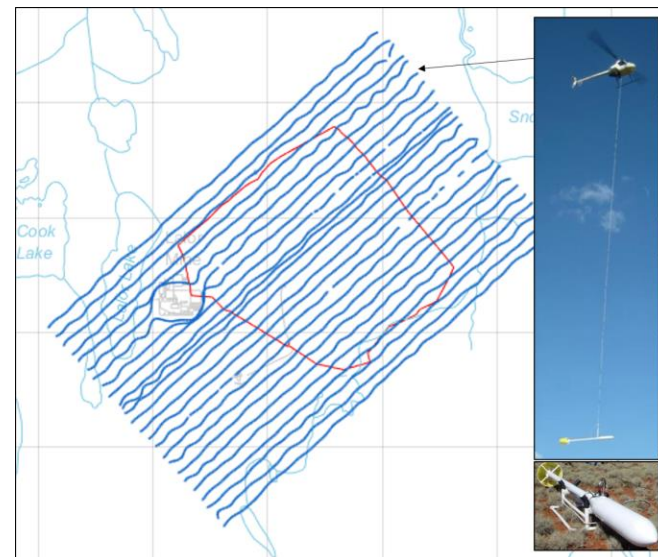
Response



SkyTEM

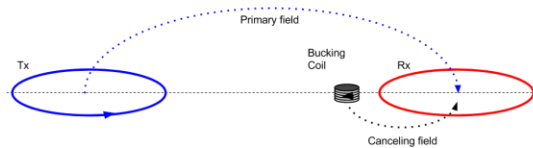


HeliSAM

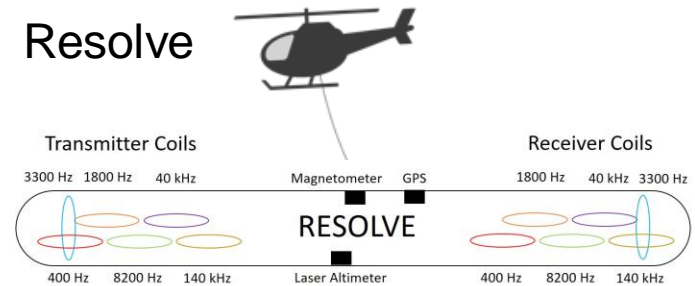
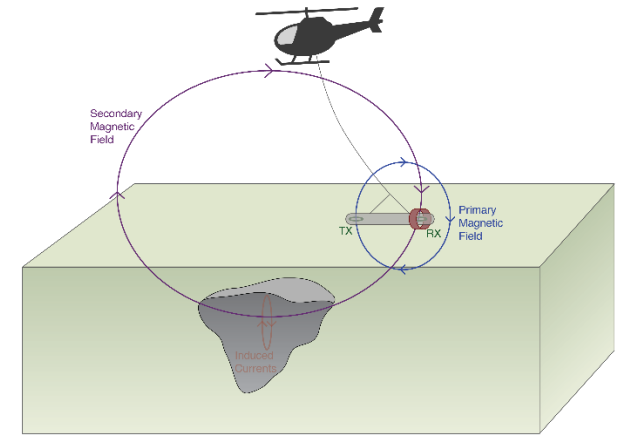


Receivers: Frequency Domain

- Primary field
 - always “on”
 - large compared to secondary fields
- Primary removal
 - Compute and subtract
 - Bucking coil



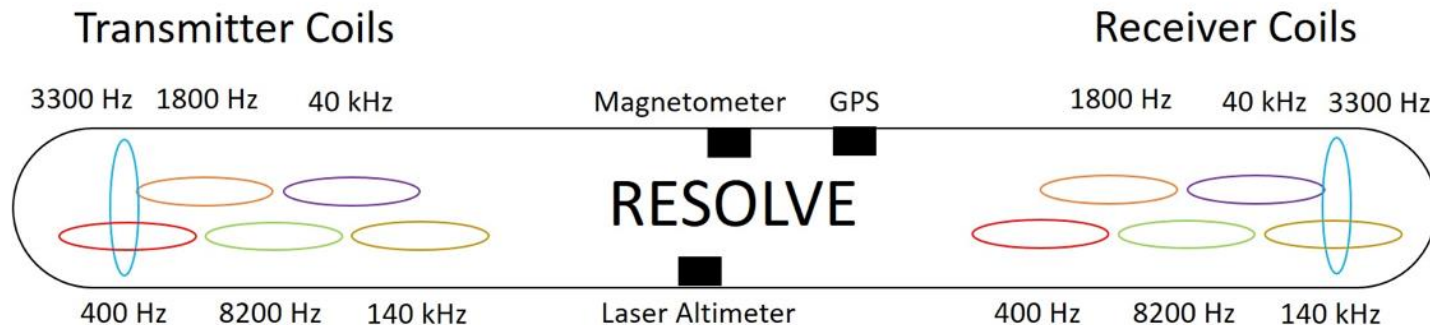
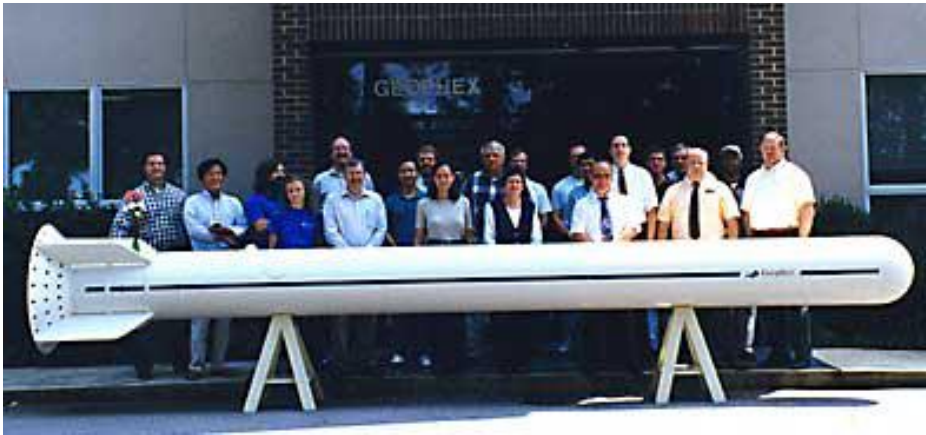
- Main requirement:
 - Know positions of Tx and Rx
 - Keep them in one unit



EM-31

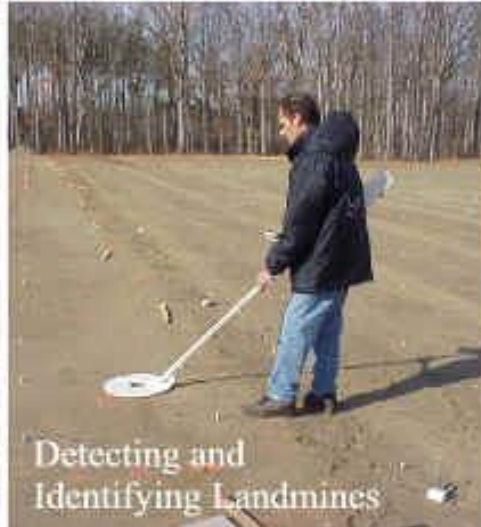


Survey: Airborne EM Resolve System



Skin depth: High frequency for shallow; low frequency for deep

Survey: GEM3



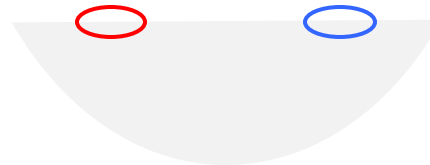
- Concentric Tx-Rx
- Frequency 60 Hz to 24 kHz
- Identify an object based on its spectral fingerprints

Survey: EM-41

Penetration depends upon frequency
and Tx-Rx separation

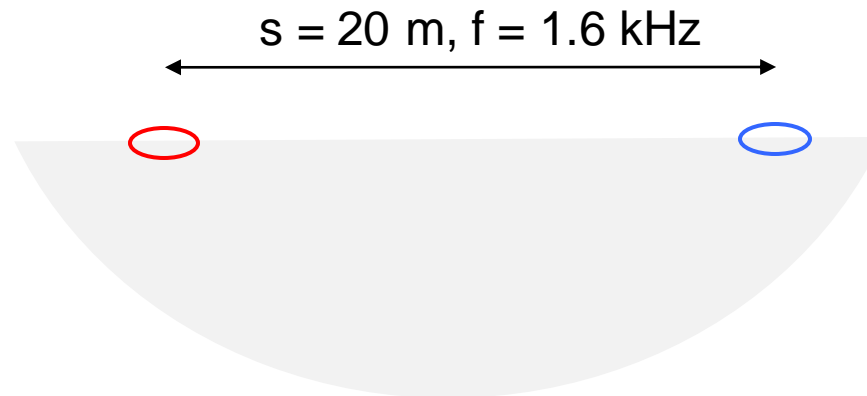


$s = 10 \text{ m}, f = 6.4 \text{ kHz}$



Survey: EM-41

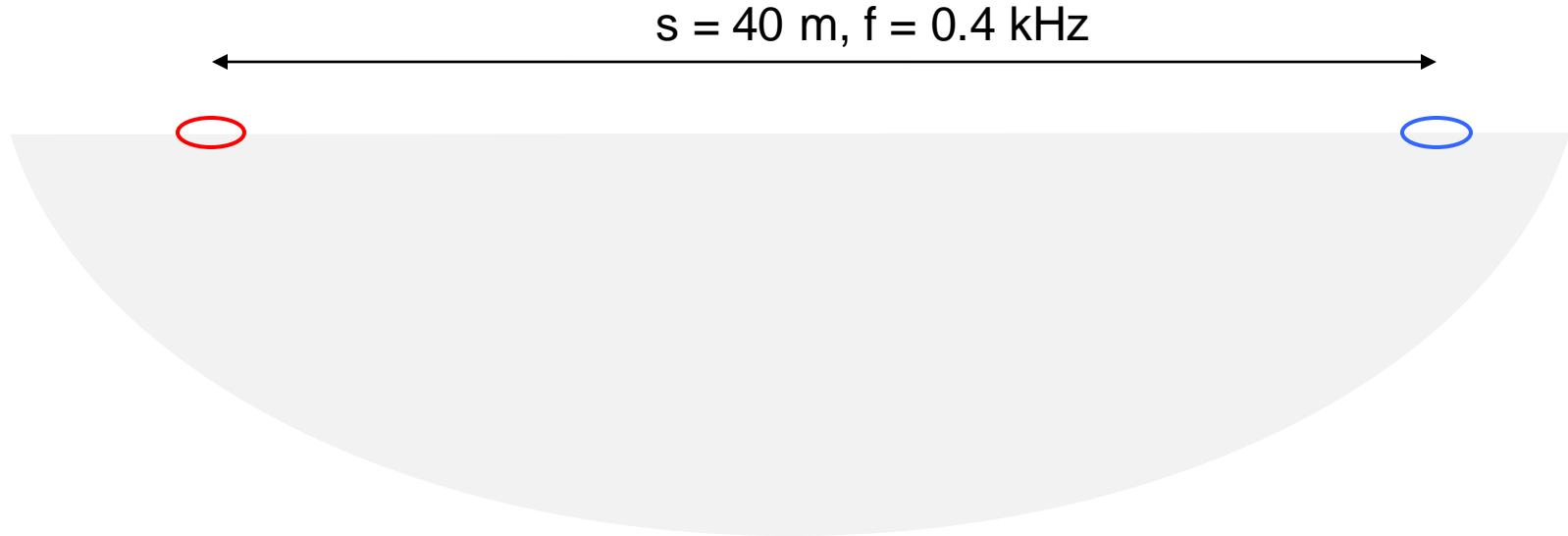
Penetration depends upon frequency
and Tx-Rx separation



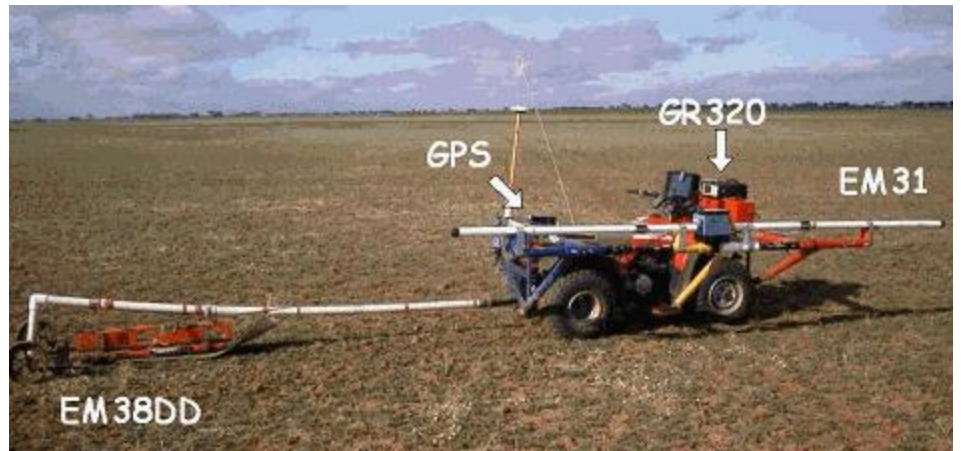
Survey: EM-41

Penetration depends upon frequency
and Tx-Rx separation

- Variable depth of exploration down to 60 m
- HCP or VCP coil configuration
- Groundwater exploration in fractured and faulted bedrock



Survey: EM-41



- Frequency = 9.8 kHz
- Tx-Rx spacing = 3.66 m
- Horizontal or vertical coplanar
- “Ground conductivity meter”

Survey: Recap

- Many FEM and TEM systems for different applications
- Challenging terrain or large scale:
→ Consider airborne survey
- Deep targets and/or conductive overburden:
→ Low frequency and large transmitter dipole moment
- High resolution needed:
→ Ground-based survey and possibly higher frequencies
- Penetration/domain of investigation of ground FEM systems depends on frequency and separation

Unit Activities

- **Labs: (EM I)**
 - Monday, November 4th
 - Tuesday, November 5th
- **Labs: (EM II)**
 - Monday, November 18th
 - Tuesday, November 19th
- **TBL:**
 - Friday, November 15th
- **Quiz:**
 - Wednesday, November 20th