# Physics-based Animation: A Mathematical Perspective

# Based on Ladislav Kavan's CS6660 with annotations from wxgopher $\label{eq:July 1, 2019} \text{July 1, 2019}$

# **Contents**

1	Classical Mechanics	2
	1.1 Basics: a harmonic oscillator	2
2	Time Integration	2
3		2
	3.1 Implicit Newmark	2
	3.2 Optimization Problems	2
	3.2.1 Solving unconstrained problems	3
	3.2.2 Newton's method	3
	3.3 Numerical Linear Algebra	4
	3.3.1 Direct solvers	4
	3.3.2 Iterative solvers	5
4	Elastic Materials and Finite Element Simulation	6
	4.1 Kinetic energy	6
	4.2 Elastic energy	7
	4.3 Vectorization	8
	4.4 Material property $\psi$	9
	4.4.1 Linear elasticity	9
	4.4.2 Saint VenantKirchhoff (StVK)	9
	4.4.3 Corotated linear elasticity	10
	4.4.4 Volume preservation term	10
	4.4.5 General corotated linear elasticity	10
5	Fluids and Partial Differential Equations	10
6	Something more	10
7	Papers and books	10

This lecture note is based on Dr. Ladislav Kavan's Physics-based Animation course CS6660, originally taught at the University of Utah. I also try to include some supplementary materials from other resources.

Warning: Although as I strive to make this material useful, there are certain bugs, use this material at your own risk. I would also be grateful to hear feedbacks.

.....

## 1 Classical Mechanics

#### 1.1 Basics: a harmonic oscillator

# 2 Time Integration

# 3 Optimization

# 3.1 Implicit Newmark

$$x_{n+1} = x_n + \frac{h}{2}(v_n + v_{n+1}),$$
 (1a)

$$v_{n+1} = v_n = \frac{h}{2}(f_n + f_{n+1}),$$
 (1b)

where *x* and *v* are positions and velocities, and  $f_n \equiv f(x_n)$ . Thus we have

$$x_{n+1} - x_n - hv_n = \frac{h^2}{4} (f_n + f_{n+1}).$$
 (2)

Let  $y = x_n + h_n v_n + \frac{h^2}{4} f_n$ ,  $x_{n+1} = x$ , note that  $\nabla E = -f$ , then (2) becomes

$$x - y = \frac{h^2}{4}f \Rightarrow x - y + \frac{h^2}{4}f\nabla E = 0.$$
 (3)

Let  $g(x) = \frac{1}{2}||x - y|^2 + \frac{h^2}{4}E$ , then solving g equals to solve x for

$$\min_{x} \quad g(x). \tag{4}$$

# 3.2 Optimization Problems

Problem formulation:

$$\min_{x} \quad g(x), \quad x \in \mathbb{R}^{n}, \quad g \in \mathbb{R}. \tag{5}$$

Optimization problems can be categorized into constrained or unconstrained problems, or convex or non-convex problems.

**Theorem 1.** For a convex problem (where both objective and feasible set are convex), if the objective is  $C^2$ , then the Hessian  $H \succeq 0$ , and the local minimum is the global minimum.

**Definition 1.** A linear programming (LP) is a problem with linear objective and linear equality or inequality constraints. A quadratic programming (QP) is the same as LP except with a quadratic objective.

**Note 1.** Convex QP has polynomial time solver but non-convex QP is NP-hard.

**Example 1.** A non-convex QP:

$$\min_{x} \quad \frac{1}{2} ||Ax||^2, \tag{6a}$$

$$s.t. ||x||_2 = 1.$$
 (6b)

Note 2. Software package for solving non-convex problem: IpOPT, KNITRO, or NEOS-Guide

#### 3.2.1 Solving unconstrained problems

There are two ways to solve an unconstrained problem: descent method or trust-region method.

Descent method refers to pick a descent direction d and do an exact or inexact line search (LS) to determine descent distance  $\alpha d$ .

**Definition 2.** *Descent direction*:  $\forall \alpha \in (0, \alpha_0), \alpha_0 > 0, g(x + \alpha d) < g(x).$ 

**Definition 3.** *Exact LS refers to solving the following problem:* 

$$\underset{\alpha>0}{\arg\min}\,g(x+\alpha d).$$

#### Backtracking LS

#### 3.2.2 Newton's method

A usual descent direction is called **gradient descent** (GD), denoted by  $d = -\nabla g$ . It doesn't work well sometime, for example:

Example 2.

$$\min_{x_1, x_2} g(x_1, x_2) = \frac{1}{2} (x_1^2 + \gamma x_2^2), \quad \gamma > 0.$$
 (7)

If we do exact LS, we get

$$x_1^k = \gamma (\frac{\gamma - 1}{\gamma + 1})^k,\tag{8a}$$

$$x_2^k = (-\frac{\gamma - 1}{\gamma + 1})^k. {(8b)}$$

If gamma becomes huge, we can tell GD converges slowly (as two GD directions are perpendicular).

Newton's method refers to do a quadratic approximation to problem (5), given by

$$g(x+p) = g(x) + \nabla g^{\mathsf{T}}(x)p + \frac{1}{2}p^{\mathsf{T}}\nabla^{2}g(x)p + O(\|p\|^{2}) \equiv \tilde{g}(x) + O.$$
 (9)

Thus we have

$$\frac{\partial \tilde{g}}{\partial p} = 0 \Longleftrightarrow \nabla g + \nabla^2 g p = 0.$$

The **Newton descent direction** is given by

$$p = -(\nabla^2 g)^{-1} \nabla g. \tag{10}$$

**Note 3.** Newton's method is affine invariant. Let x = Ty with T being a nonsingular matrix, so problem (5) is equivalent to problem

$$\min_{y} \tilde{g}(y). \tag{11}$$

We also have

$$\nabla \tilde{g} = T^2 \nabla g, \quad \nabla^2 \tilde{g} = T^T \nabla^2 g T.$$

Newton direction  $\Delta y$  of  $\tilde{g}$  and  $\Delta x$  of g is given by

$$\Delta y = -T^{-1}\nabla^2 g \nabla g = T^{-1}\Delta x.$$

**Definition 4.** Newton decrement: substitute Newton descent direction (10) into (9), we get the Newton decrement

$$\lambda^2 = g - \frac{1}{2} \nabla g^{\mathrm{T}} (\nabla^2 g)^{-1} \nabla g. \tag{12}$$

A stopping criteria for Newton's method would be

$$\frac{\lambda^2}{2} \le \epsilon$$
.

Note that Newton decrement is also affine invariant.

Convergence analysis of the Newton's method is given as follows:

**Theorem 2.** *Kantorovich*: if g is strictly convex and  $\nabla^2 g$  is Lipschitz continuous, then  $\exists \epsilon > 0, \eta > 0, \gamma > 0$ , s.t.

**Damped phase I** *If* 
$$\|\nabla g\| \ge \eta$$
, then  $\|g^{k+1}\| \le \|g^k\| - \gamma$ ;

**Quadratic phase II** If  $\|\nabla g\| < \eta$ , then  $\|g^{k+1}\| \le c\|g^k\|^2$ .

Some cases where Newton's method doesn't work well:

- 1. If *g* is highly nonlinear, the damped phase will be long;
- 2. If *g* is non-convex, solution might not converge to a minimum.

In practical implementations, the Hessian might not always be positive definite. A possible Hessian modification is:

**Note 4.** Hessian modification: Consider  $A = \nabla^2 g + cI$ , where c > 0. It is shown that if  $\nabla^2 g = Q\Lambda Q^T$  ( $\nabla^2 g$  is symmetric, hence it is always diagonalizable), then  $A = Q(\Lambda + cI)Q^T$ , hence A is positive definite given sufficiently large c > 0.

Solving Newton's direction (10) refers to solving a linear system. We introduce several techniques to tackle this.

# 3.3 Numerical Linear Algebra

We consider solving a linear system Ax = b.

#### 3.3.1 Direct solvers

We can prefactor A into  $A = UV^{T}$ , with U and V being low rank matrices.

Common factorization methods are

LU If A is nonsingular, then there exist L, P, U, where they are lower-triangular matrix, permutation matrix (hence orthogonal), and upper-triangular matrix, respectively, s.t. A = PLU.

**Sparse LU**  $A = P_1LUP_2$ , where  $P_1$  and  $P_2$  are permutations to utilize sparse information of A.

**Cholesky** For symmetric positive-definite matrix, we have  $A = LL^{T}$  with unique L. Note that for positive semi-definite matrix, Cholesky is not unique.

LDLT

#### 3.3.2 Iterative solvers

Iterative solvers includes:

- 1. Classical method: Jacobian, Gauss-Seidel, SOR (super over-relaxation), etc.;
- 2. Krylov subspace method: CG (conjugate gradient)<sup>1</sup>, GMRES (generalized minimal residual), etc.;
- 3. multigrid method.

**Classical method** Suppose *P* is easy to invert, let A = P + A - P, then

$$Ax = b \Leftrightarrow Px = (P - A)x + b.$$

P = diag(A) gives us Jacobian method, and it's GPU-friendly; P = lower(A) gives us GS method;  $P = diag(A) + w \cdot lower(A)$  gives us SOR method where w < 2.

The residual term follows

$$r_k \equiv A(x^* - x_k) = b - Ax_k \quad \Leftrightarrow \quad r_{k+1} = (I - P^{-1}A)r_k.$$

To make classical method converge, we need  $\rho(I - P^{-1}A) < 1$ , where  $\rho(\cdot)$  is the spectrum radius.

**Krylov subpace method** Assuming  $A^{T} = A$  and  $A \succeq 0$ , then

$$\arg\min_{x} g(x) = \frac{1}{2} x^{T} A x - x^{T} b \quad \Leftrightarrow \quad solve \ A x = b. \tag{13}$$

Let  $\nabla g_k = Ax_k - b = -r_k^2$  as a descent direction, the line search for (13) is as follows:

- 1. Solve  $\alpha$  from  $\arg\min_{\alpha}(\frac{1}{2}(x+\alpha r)^{\mathrm{T}}A(x+\alpha r)-(x+\alpha r)^{\mathrm{T}}b\equiv\frac{1}{2}\|x+\alpha r\|_{A}^{2}-(x+\alpha r)^{\mathrm{T}}b)$  by letting  $\frac{\partial E}{\partial \alpha}=0$ , where E is the objective;
- 2.  $\alpha$  follows  $\alpha = -\frac{\|r\|^2}{|r||_A^2}$ ;
- 3.  $x_{k+1} = x_k + \alpha_k r_k$ .

This is the gist of CG from gradient descent.

**CG** Assuming solving problem (13).

**Definition 5.** A-conjugate A set of vectors  $\{p_i\}$  are A-conjugate iff  $\forall i, j, i \neq j, p_i^T A p_j = 0$ .

The CG algorithm is as follows:

- 1. We define  $r_k = Ax_k b$ ;
- 2. Let  $p_1 = r_1^3$ ;

3. 
$$p_k = r_k + \beta_k p_{k-1}, \beta_k = \frac{r_k^T A p_{k-1}}{p_{k-1}^T A p_{k-1}};$$

- 4. Do LS along direction  $p_k$ , we have  $\alpha_k = \frac{r_k^T p_k}{p^T A p_k}$ ;
- 5.  $x_{k+1} = x_k + \alpha_k p_k$ .

<sup>&</sup>lt;sup>1</sup>A good reference on CG is [8].

 $<sup>{}^{2}</sup>Ax$  is computed on-fly, we don't need the whole A.

 $<sup>^{3}</sup>r_{1}$  is usually chosen as a GD step

**Preconditioning CG** If *A* is ill-conditioned, we consider adding preconditioner *M* to *A*, s.t. cond(MA) < cond(A).

The Jacobian preconditioner is given by  $M = diag(A)^{-1}$ . The incomplete Cholesky is given by prefactoring A into  $L_aL_a^{\mathrm{T}}$  where  $-L_a$  is an approximation of L of the Cholesky decomposition of A given by  $A = LL^{\mathrm{T}}$ .

## 4 Elastic Materials and Finite Element Simulation

# 4.1 Kinetic energy

Consider kinetic energy

$$k = \frac{1}{2}v^{\mathrm{T}}Mv.$$

Assuming unit mass, we have

$$k = \frac{1}{2} \int_{\Omega} \rho(p) ||v(p)||^2 dp,$$
 (14)

where  $p \in \Omega$  is the material point. We discretize  $\Omega$ , and for every node  $p_i$  we define piece-wise shape function  $s_i : \Omega \mapsto [0,1]$ , s.t.  $\sum_i s_i = 1$ . For every region  $E_t$ , we also define

$$r_t(p) = \begin{cases} 1 & p \in E_t, \\ 0 & otherwise. \end{cases}$$

We have

$$v(p) = \sum_{i} v_i s_i(p), \tag{15a}$$

$$\rho(p) = \sum_{t} \rho_t r_t(p). \tag{15b}$$

The kinetic energy follows

$$k = \frac{1}{2} \int_{\Omega} \sum_{t} \rho_{t} r_{t} \|v(p)\|^{2} dp$$
 (16a)

$$= \frac{1}{2} \sum_{t} \rho_{t} \int_{\Omega} r_{t}(p) \|v(p)\|^{2} dp$$
 (16b)

$$= \frac{1}{2} \sum_{t} \rho_t \int_{E_t} ||v||^2 \mathrm{d}p \tag{16c}$$

$$= \frac{1}{2} \sum_{t} \rho_t \sum_{i,j} v_i^{\mathsf{T}} v_j \int_{E_t} s_i s_j \mathrm{d} p. \tag{16d}$$

(16e)

We define

$$\int_{E_t} s_i s_j \mathrm{d}p = s_{i,j}^t,\tag{17}$$

for different methods of discretization, we have

#### Triangal element (2-dimension)

$$s_{i,j}^{t} = \begin{cases} \frac{Area(t)}{6} & i = j, \\ \frac{Area(t)}{12} & i \neq j. \end{cases}$$

#### Tetrahderal element (3-dimension)

$$s_{i,j}^t = \begin{cases} \frac{Area(t)}{10} & i = j, \\ \frac{Area(t)}{20} & i \neq j. \end{cases}$$

Let's consider practical implementation of FEM. From discussions above, we have

$$\int_{E_t} \|v(p)\|^2 dp = \sum_{i,j} v_i^{\mathrm{T}} v_j \int_{E_t} s_i s_j dp$$
 (18a)

$$= \sum_{i,j} v_i^{\mathrm{T}} v_j s_{i,j}^t \tag{18b}$$

$$= V^{\mathrm{T}} S_t V, \tag{18c}$$

where  $V = (v_1, v_2, \cdots, v_n)^T$ , and

$$S_{t} = \begin{pmatrix} s_{1,1}^{t} \cdot I_{3} & \cdots & s_{1,n}^{t} \cdot I_{3} \\ \vdots & \ddots & \vdots \\ s_{n,1}^{t} \cdot I_{3} & \cdots & s_{n,n}^{t} \cdot I_{3} \end{pmatrix}.$$

The kinetic energy follows

$$k = \frac{1}{2} \sum_{t} \rho_t(V^{\mathrm{T}} S_t V) \tag{19a}$$

$$= \frac{1}{2} V^{\mathrm{T}} \left( \sum_{t} \rho_t S_t \right) V \tag{19b}$$

We denote *mass matrix*  $M_t$  with  $M_t = \sum_t \rho_t S_t$ . For triangle element we have

$$M_t = \sum_t \rho_t S_t = \rho_t Area(t) P \otimes I_3, \tag{20}$$

where *P* is defined by

$$P_{m,n} = \begin{cases} \frac{1}{6} & m = n \in i, j, k \\ \frac{1}{12} & m \neq n \in i, j, k, \\ 0 & otherwise \end{cases}$$

where i, j and k are triangle vertex indices<sup>4</sup>.

# 4.2 Elastic energy

In this section we only consider hyperelastic materials.

#### Pic here

Consider a deformation f from n-points d-dimensional material (rest pose) space  $\Omega$  to world (deformed) space  $f(\Omega) \in \mathbb{R}^{\mathrm{nd} \times \mathrm{nd}}$ , for every spatial point p, the deformation gradient is  $\nabla f(p)$ . Elastic energy can be represented by

$$E = \int_{\Omega} \psi(\nabla f(p)) \nabla f(p) dp, \tag{21}$$

where  $\psi \in \mathbb{R}^{n \times n} \mapsto \mathbb{R}^+$  is the *energy density function*.

The energy density function can be further decomposed into

$$\psi = \psi_{material} \circ \psi_{strain}, \tag{22}$$

<sup>&</sup>lt;sup>4</sup>In practical implementation, sometimes the *mass lumping* technique is used. This technique aggregates matrix element to its diagonal and to facilitate computations.

where  $\psi_{material}$  describes material property and  $\psi_{strain}$  describes geometric measure of distortion of this material.

Let's consider how to use FEM to discretize the elastic energy.

#### elaborate on this

We consider 3-dimensional problem, where  $\psi \in \mathbb{R}^{3\times 3} \mapsto \mathbb{R}^+$  is given. For every tetrahedron (tet), we define  $F = \nabla f \in \mathbb{R}^{3\times 3}$ . For every deformed vertex  $\mathbf{x}$  and material vertex  $\tilde{\mathbf{x}}^5$ , we have  $\mathbf{x} = f(\tilde{\mathbf{x}}) = F\tilde{\mathbf{x}} + b$ , where  $\mathbf{b}$  is a constant. For the whole tet, we have

$$\mathbf{x}_i - \mathbf{x}_4 = F(\tilde{\mathbf{x}}_i - \tilde{\mathbf{x}}_4),\tag{23}$$

where  $i \in 1, 2, 3, 4$  are vertex indices. This can be written as

$$D_{s} = FD_{m_{s}} \tag{24}$$

where

$$D_{s} = \begin{pmatrix} x_{1} - x_{4} & x_{2} - x_{4} & x_{3} - x_{4} \\ y_{1} - y_{4} & y_{2} - y_{4} & y_{3} - y_{4} \\ z_{1} - z_{4} & z_{2} - z_{4} & z_{3} - z_{4} \end{pmatrix}, \quad D_{m} = \begin{pmatrix} \tilde{x}_{1} - \tilde{x}_{4} & \tilde{x}_{2} - \tilde{x}_{4} & \tilde{x}_{3} - \tilde{x}_{4} \\ \tilde{y}_{1} - \tilde{y}_{4} & \tilde{y}_{2} - \tilde{y}_{4} & \tilde{y}_{3} - \tilde{y}_{4} \\ \tilde{z}_{1} - \tilde{z}_{4} & \tilde{z}_{2} - \tilde{z}_{4} & \tilde{z}_{3} - \tilde{z}_{4} \end{pmatrix}, \quad (25)$$

thus

$$F = D_s(x)D_m^{-1}. (26)$$

The elastic energy (21) can be discretized with

$$E = \sum_{t} \int_{E_t} \psi_t(F_t) dt$$
 (27a)

$$=\sum_{t}w_{t}\psi_{t}(F_{t}),\tag{27b}$$

where

$$w_t = \frac{1}{6} det ||D_m||, (28)$$

is the volume of the tet *t*.

#### 4.3 Vectorization

Before we get to the actual material property, we would introduce a vectorization scheme frequently seen in practical implementations.

Recall that  $\nabla f \equiv F$  is linear w.r.t. x, where x is a collection of material space points, we have F = Gx, where  $F \in \mathbb{R}^{3\times 3}$ ,  $x \in \mathbb{R}^{3n\times 1}$ , and G is a tensor.

**Definition 6.** Let  $A \in \mathbb{R}^{m \times n}$ ,  $B \in \mathbb{R}^{k \times l}$ , we denote the **Kronecker product**  $A \otimes B$  (which is an  $mk \times nl$  matrix) with

$$A \otimes B = \begin{pmatrix} a_{11}B & \cdots & a_{1n}B \\ \vdots & \ddots & \vdots \\ a_{m1}B & \cdots & a_{mn}B \end{pmatrix}.$$
 (29)

**Definition 7.** We denote a vectorization of a matrix A with

$$\operatorname{vec}(A) = (a_1, a_2, \cdots, a_n)^{\mathrm{T}}.$$
(30)

We further derives some lemmas:

**Lemma 1.** For any given matrices A, B, C and D, assuming the matrix dimensions agree, we have

 $<sup>^{5}\</sup>mathbf{x} = (x, y, z)$ 

1.  $(A \otimes B) \cdot (C \otimes D) = A \cdot C \otimes B \cdot D$ ;

2. 
$$(A \otimes B)^{\mathsf{T}} = A^{\mathsf{T}} \otimes B^{\mathsf{T}};$$

3.  $\operatorname{vec}(AX) = (I_p \otimes A) \cdot \operatorname{vec}(X) = (X^T \otimes I_m) \cdot \operatorname{vec}(A)$ , where  $A \in \mathbb{R}^{m \times n}$ ,  $x \in \mathbb{R}^{n \times p}$ .

Then for each tet,  $\text{vec}(F) \in \mathbb{R}^{9 \times 1}$ ,  $G \in \mathbb{R}^{9 \times 3n}$ ,  $x \in \mathbb{R}^{3n \times 1}$ , and

$$\operatorname{vec}(F) = \operatorname{vec}(D_s \cdot D_m^{-1}) = (D_m^{-T} \otimes I_3) \cdot \operatorname{vec}(D_s), \tag{31}$$

where<sup>6</sup>

$$\operatorname{vec}(D_s) = \begin{pmatrix} x_1 - x_4 \\ x_2 - x_4 \\ x_3 - x_4 \end{pmatrix} = (S \cdot I_3) \cdot x \in \mathbb{R}^{9 \times 1}, \tag{32}$$

where we define a selector matrix *S* on each tet. *S* is defined by

$$S = \begin{pmatrix} \cdots & 1 & \cdots & -1 & \cdots \\ 1 & \cdots & \cdots & -1 & \cdots \\ \cdots & \cdots & 1 & -1 & \cdots \end{pmatrix}, \tag{33}$$

where the column indices of 1s are from  $x_1$ ,  $x_2$ , and  $x_3$ ; the column index of -1 is from  $x_4$ . To sum up, for each tet:

$$\operatorname{vec}(F) = (D_m^{-\mathsf{T}} \otimes I_3)(S \otimes I_3)x = (D_m^{-\mathsf{T}} \cdot S \otimes I_3)x. \tag{34}$$

## 4.4 Material property $\psi$

The deformation energy function  $\psi$  is a mapping from the deformation gradient to a positive real number:  $\mathbb{R}^{3\times3} \mapsto \mathbb{R}^+$  (or in a vectorized form  $\mathbb{R}^{9\times1} \mapsto \mathbb{R}^+$ ).

#### 4.4.1 Linear elasticity

$$\psi(F) = \|F - I\|_F^2,\tag{35}$$

where  $\|\cdot\|_F$  denotes the Frobenius norm. Linear elasticity is not rotation invariant, i.e.,

$$\psi(RF) \neq \psi(F),\tag{36}$$

where  $R \in SO(3)$ .

#### 4.4.2 Saint VenantKirchhoff (StVK)

To make  $\psi$  rotation invariant, we consider

$$\psi = \|F^{\mathsf{T}}F - I\|_{F}^{2},\tag{37}$$

where  $\psi_{strain} = F^{T}F - I$  is called the *Green tensor*, and  $\psi_{material} = \|\cdot\|_{F}^{2}$ .

However, the StVK model has the reflection problem. For example, consider  $F_1 = \begin{pmatrix} 1 & 1 \\ & 1 \end{pmatrix}$  and

$$F_2=egin{pmatrix}1&&&\\&1&\\&&-1\end{pmatrix}$$
 , it's easy to derive  $\psi(F_1)=\psi(F_2)$  .

 $<sup>^{6}</sup>x_{i}\in\mathbb{R}^{3\times1}.$ 

## 4.4.3 Corotated linear elasticity

Consider SVD decomposition  $F = U\Sigma V^{\mathrm{T}}$ , where  $U, V \in SO(3)$ ,  $\Sigma = \begin{pmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \end{pmatrix}$ ,  $\sigma_1 \geq \sigma_2 \geq \sigma_3$ . The corotated linear elasticity is defined by

$$\psi(F) = \|\Sigma - I\|_F^2 \tag{38a}$$

$$=\sum_{i=1}^{3} (\sigma_i - 1)^2 \tag{38b}$$

$$= \|U\Sigma V^{\mathrm{T}} - UV^{\mathrm{T}}\|_F^2 \tag{38c}$$

$$= \|F - R\|_F^2 \tag{38d}$$

#### why?

where  $R = \operatorname{arg\,min}_{x \in SO(3)} \|F - x\|_F^T$ .

## 4.4.4 Volume preservation term

Corotated linear elasticity does not preserve volume, for example, given  $F_1 = \begin{pmatrix} 1.5 \\ 1.5 \end{pmatrix}$  and  $F_2 = \begin{pmatrix} 1.5 \\ 0.5 \end{pmatrix}$ , it's easy to derive  $\psi_{corot}(F_1) = \psi_{corot}(F_2)$ .

We consider adding a volume preservation term

$$\psi_{vol}(F) = (\det(F) - 1)r \tag{39a}$$

$$= (\prod \sigma_i - 1)^2 \tag{39b}$$

$$\approx (\sum \sigma_i - 3)^2 \tag{39c}$$

$$= [\operatorname{tr}(\Sigma - I)]^2 \tag{39d}$$

.

## 4.4.5 General corotated linear elasticity

Combining 4.4.3 and 4.4.4 together, we have

$$\psi = \mu \|\Sigma - I\|_F^2 + \frac{\lambda}{2} \operatorname{tr}^2(\Sigma - I), \tag{40}$$

where  $\mu$  and  $\lambda$  are Lamé coefficients.

# 5 Fluids and Partial Differential Equations

# 6 Something more...

# 7 Papers and books

Numerical optimization can refer to [2] [6].

[1] and [9] are great references for continuum mechanics and FEM.

An awesome book on fluids simulation is [3]. Vector calculus can be found in [7]. Useful tips of C++ programming can be found in C++ core guidelines, [4], and [5].

## References

- [1] Javier Bonet and Richard D Wood. *Nonlinear continuum mechanics for finite element analysis*. Cambridge university press, 1997.
- [2] Stephen Boyd and Lieven Vandenberghe. Convex optimization. Cambridge university press, 2004.
- [3] Robert Bridson. Fluid simulation for computer graphics. AK Peters/CRC Press, 2015.
- [4] Scott Meyers. *Effective C++: 55 specific ways to improve your programs and designs.* Pearson Education, 2005.
- [5] Scott Meyers. Effective modern C++: 42 specific ways to improve your use of C++ 11 and C++ 14. " O'Reilly Media, Inc.", 2014.
- [6] Jorge Nocedal and Stephen Wright. Numerical optimization. Springer Science & Business Media, 2006.
- [7] Kaare Brandt Petersen, Michael Syskind Pedersen, et al. The matrix cookbook. *Technical University of Denmark*, 7(15):510, 2008.
- [8] Jonathan Richard Shewchuk et al. An introduction to the conjugate gradient method without the agonizing pain, 1994.
- [9] Eftychios Sifakis and Jernej Barbic. Fem simulation of 3d deformable solids: a practitioner's guide to theory, discretization and model reduction. In *Acm siggraph 2012 courses*, page 20. ACM, 2012.