

Circuit Theory

Problem Set 4

Operational Amplifier Circuits

Xin, Wenkang

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(a) For an ideal op-amp, the input current is zero so that:

$$\frac{V_{\text{IN}} - 0}{R_1} = \frac{0 - V_{\text{OUT}}}{R_2} \quad (1)$$

so that:

$$V_{\text{OUT}} = -\frac{R_2}{R_1} V_{\text{IN}} \quad (2)$$

When $R_2 = 4R_1$ and $V_{\text{OUT}} = 2\text{ V}$, we have $V_{\text{IN}} = -0.5\text{ V}$.

(b) We have:

$$\frac{V_{\text{OUT}} - V_{\text{IN}}}{R_2} = \frac{V_{\text{IN}} - 0}{R_1} \quad (3)$$

so that:

$$V_{\text{OUT}} = \frac{R_1 + R_2}{R_1} V_{\text{IN}} \quad (4)$$

When $R_2 = 4R_1$ and $V_{\text{OUT}} = 2\text{ V}$, we have $V_{\text{IN}} = 0.4\text{ V}$.

(c) We have:

$$\begin{aligned} \frac{V_{\text{ref}} - V}{R_2} &= \frac{V - V_{\text{OUT}}}{R_1} \\ \frac{V_{\text{IN}} - V}{R_1} &= \frac{V}{R_2} \end{aligned} \quad (5)$$

where V is the input voltage of the op-amp.

Solving for V_{OUT} yields:

$$V_{\text{OUT}} = \frac{R_2}{R_1} (V_{\text{IN}} - V_{\text{ref}}) \quad (6)$$

When $R_2 = 4R_1$ and $V_{\text{OUT}} = 2\text{ V}$, we have $V_{\text{IN}} = 1.5\text{ V}$.

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For there to be no current through the op-amp, we have:

$$\frac{V_{\text{IN}}}{R} = \frac{dq}{dt} \quad (7)$$

where $q(t)$ is the charge on left-plate of the capacitor.

Hence the output of the first op-amp satisfies $V'_{\text{OUT}} = -q/C$. Further imposing the no-current condition on the second op-amp yields:

$$\frac{V'_{\text{OUT}}}{R} + \frac{V_1}{R} = \frac{0 - V_{\text{OUT}}}{R} \quad (8)$$

This leads to:

$$V_{\text{OUT}} = -V'_{\text{OUT}} - V_1 = \frac{1}{RC} \int_0^t V_{\text{IN}} dt - V_1 \quad (9)$$

Given that $V_{\text{IN}} = 1 \text{ V}$, we have the numerical value of V_{OUT} to be $(t - 10)$. This grows arbitrarily large as t tends to infinity, which is not physically possible.

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Imposing the no-current condition on the op-amp yields:

$$\frac{V_{\text{IN}}}{R} = \frac{dq_C}{dt} + i_R \quad (10)$$

where q_C is the charge on the capacitor satisfying $V_{\text{OUT}} = -q_C/C$ and i_R is the current through the resistor satisfying $V_{\text{OUT}} = -i_R R$.

This yields a differential equation for $V_{\text{OUT}}(t)$:

$$\frac{dV_{\text{OUT}}}{dt} + \frac{V_{\text{OUT}}}{RC} + \frac{V_{\text{IN}}}{RC} = 0 \quad (11)$$

Now let the input voltage take the complex form $V_{\text{IN}} = \tilde{V}e^{i\omega t}$, where ω is the angular frequency. Applying an integrating factor of $e^{t/CR}$ yields:

$$\begin{aligned} \frac{d}{dt} (e^{t/CR} V_{\text{OUT}}) &= -\frac{\tilde{V}}{CR} e^{(1/CR + i\omega)t} \\ V_{\text{OUT}}(t) &= -\frac{\tilde{V}}{1 + i\omega CR} e^{i\omega t} = -\frac{1}{1 + i\omega CR} V_{\text{IN}}(t) \end{aligned} \quad (12)$$

Taking the ratio leads to $|V_{\text{OUT}}/V_{\text{IN}}| = 1/\sqrt{1 + (\omega CR)^2}$. This equals $1/\sqrt{2}$ when $\omega = 1/(CR)$, which is the usual definition of the resonance frequency.

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First note that the current output by V_{IN} is constant and does not alter when any of the switches changes. Hence we can calculate the voltages V_0, V_1, V_2, V_3 above the switches without ambiguity.

First focus on the node above the last switch S_3 . The two $2R$ resistors combine to give a R resistor, which means $V_3 = V_2/2$. Note that this argument can be made for every node above a switch, which means $V_i = V_{i-1}/2$ for $i = 1, 2, 3$. But V_0 is just the input voltage, and we thus know all the node voltages.

Applying the no-current condition on the op-amp yields:

$$\frac{0 - V_{\text{OUT}}}{R} = I = \sum_{i=0}^3 \frac{S_i}{2R} V_i \quad (13)$$

Therefore:

$$V_{\text{OUT}} = -V_{\text{IN}} \left(\frac{S_0}{2} + \frac{S_1}{4} + \frac{S_2}{8} + \frac{S_3}{16} \right) \quad (14)$$

The range of the output is from 0 V to -9.375 V. To make the output non-inverting, we can use the circuit in Question 23 Part (b), replacing R_1 with the present network and R_2 with R . This will lead to the output expression:

$$V_{\text{OUT}} = V_{\text{IN}} \left(1 + \frac{S_0}{2} + \frac{S_1}{4} + \frac{S_2}{8} + \frac{S_3}{16} \right) \quad (15)$$

(this seems weird...)