Fluids

Problem Set 2

Dynamics of Fluids

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1 Poiseuille flow in a cylindrical tube

(a) For the current problem, we the Navier-Stokes equation:

$$\frac{\mathbf{D}\mathbf{v}}{\mathbf{D}t} = -\frac{1}{\rho}\nabla p + \nu\nabla^2\mathbf{v} \tag{1}$$

We only have $\mathbf{v} = v_z(r)\hat{z}$ and consider steady-state flow, so the equation reduces to:

$$0 = -\frac{1}{\rho} \frac{\partial p}{\partial z} + \nu (\nabla^2 \mathbf{v})_z \tag{2}$$

Note the vector calculus identity:

$$\nabla^{2}\mathbf{v} = \nabla(\nabla \cdot \mathbf{v}) - \nabla \times (\nabla \times \mathbf{v})$$

$$= -\nabla \times (\nabla \times \mathbf{v})$$

$$= \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_{z}}{\partial r} \right) \hat{z}$$
(3)

Letting $\partial p/\partial z = \Delta p/L$ and solving the equation, we have:

$$v_z(r) = \frac{\Delta p}{L} \frac{1}{4n} (R^2 - r^2) \tag{4}$$

where we have used the boundary condition $v_z(R) = 0$.

(b) The flow rate across a cross section of the tube is given by:

$$Q = \oint v_z dA$$

$$= \int_0^R \frac{\Delta p}{L} \frac{1}{4\eta} (R^2 - r^2) 2\pi r dr$$

$$\propto R^4 \Delta p$$
(5)

which implies $\Delta p \propto Q R^{-4}$.

If the flow rate reduces to half $Q \to Q/2$, the radius should change according to $R \to 2^{-1/4}R$ with constant pressure difference; the pressure should decrease according to $\Delta p \to 2^{-1}\Delta p$ with constant radius.

(c) The viscous friction force is given by:

$$f_{z} = \frac{d\sigma_{zr}}{dr}$$

$$= \eta \frac{d}{dr} \left(\frac{\partial v_{z}}{\partial r} \right)$$

$$= \eta \frac{d}{dr} \left(-\frac{\Delta p}{L} \frac{1}{2\eta} r \right)$$

$$= -\frac{\Delta p}{2L}$$
(6)

The energy loss due to viscous friction is given by the integral:

$$D = \int_{V} \sigma_{ij} \frac{\partial v_{i}}{\partial x_{j}} dV$$

$$= \int_{0}^{L} \int_{0}^{2\pi} \int_{0}^{R} \sigma_{zr} \frac{\partial v_{z}}{\partial r} r dr d\theta dz$$

$$= \eta \left(\frac{\Delta p}{L} \frac{1}{2\eta}\right)^{2} \frac{R^{4}}{4} 2\pi L$$

$$= 2\pi L v_{\text{max}}^{2} \eta$$
(7)

2 Couette ow between rotating cylinders

(a) Since there is longitudinal symmetry, we can write the velocity field as $\mathbf{v} = v_r(r)\hat{r} + v_{\theta}(r)\hat{\theta}$. Neglecting any external pressure, the Navier-Stokes equation reduces to $\nabla^2 \mathbf{v} = 0$. This gives:

$$\nabla^{2}\mathbf{v} = -\nabla \times (\nabla \times \mathbf{v})$$

$$= \frac{\partial}{\partial r} \left[\frac{1}{r} \frac{\partial}{\partial r} (rv_{\theta}) \right] \hat{\theta}$$

$$= \mathbf{0}$$
(8)

This can be solved by integrating the equation to yield $v_{\theta}(r) = C_1 r + C_2/r$ and $\Omega = C_1 + C_2/r^2$. The boundary conditions are $v_{\theta}(R_{1,2})/R_{1,2} = \Omega_{1,2}$, which gives:

$$C_{1} = \frac{\Omega_{1} - \Omega_{2}}{1/R_{1}^{2} - 1/R_{2}^{2}}$$

$$C_{2} = \frac{\Omega_{1}R_{1}^{2} - \Omega_{2}R_{2}^{2}}{R_{1}^{2} - R_{2}^{2}}$$
(9)

For the case $\Omega_1 = \Omega_2 = \Omega$, we have $C_1 = 0$ and $C_2 = \Omega$. This is just co-rotation with the two cylinders rotating at the same angular velocity. For the case $\Omega_2 = 0$ and $R_2 \to \infty$, we have

 $C_1 = \Omega_1 R_1^2$ and $C_2 = 0$. This is just the case of a rotating cylinder in an otherwise stationary fluid. For $R_{1,2} \gg R_2 - R_1$

(b) The viscous friction force is given by:

$$f_{\theta} = \frac{d\sigma_{\theta r}}{dr}$$

$$= \eta \frac{d}{dr} \left(\frac{\partial v_{\theta}}{\partial r} \right)$$

$$= \frac{2C_2 \eta}{r^3}$$
(10)

This is a force per unit area, so the viscous torque on either cylinder is given by:

$$\tau = R \int f_{\theta} dA$$

$$= RL \int f_{\theta} R d\theta$$

$$= 2\pi R^{2} L f_{\theta}(R)$$

$$= 4\pi C_{2} \eta \frac{L}{R}$$
(11)

where $R = R_1$ or R_2 .

3 Motion of a sphere in a very viscous fluid: Stokes law

(a) Given the velocity field $\mathbf{v} = \mathbf{v}_r \hat{r} + \mathbf{v}_{\theta} \hat{\theta}$, where:

$$v_r = \frac{1}{r^2 \sin \theta} \frac{\partial \psi}{\partial \theta}$$

$$v_\theta = -\frac{1}{r \sin \theta} \frac{\partial \psi}{\partial r}$$
(12)

we have the curl of the velocity field:

$$\omega_{\phi} = \frac{1}{r} \left[\frac{\partial}{\partial r} (r v_{\theta}) - \frac{\partial v_{r}}{\partial \theta} \right]$$

$$= \frac{1}{r \sin \theta} \left[-\frac{\partial^{2} \psi}{\partial x^{2}} + \frac{\sin \theta}{r^{2}} \frac{\partial}{\partial \theta} \left(\frac{1}{\theta} \frac{\partial \psi}{\partial \theta} \right) \right]$$

$$= \frac{1}{r \sin \theta} \left[-\mathcal{O}_{1}(\psi) + \mathcal{O}_{2}(\psi) \right]$$
(13)

The Navier-Stokes equation gives $0 = -\nabla p + \eta \nabla^2 \mathbf{v}$. But:

$$\nabla^2 \mathbf{v} = -\nabla \times (\nabla \times \mathbf{v}) = -\nabla \times \omega \tag{14}$$

which gives:

$$\nabla p = -\eta \nabla \times \omega \tag{15}$$

This implies that the curl of this equation is zero. Consider the ϕ component of $\nabla \times (\nabla \times \omega)$:

$$0 = \frac{\partial}{\partial r} \left[-\frac{\partial (r\omega_{\phi})}{\partial r} - \frac{\partial}{\partial \theta} \left(\frac{1}{r \sin \theta} \frac{\partial (\sin \theta \omega_{\phi})}{\partial \theta} \right) \right]$$

$$= \mathcal{O}_1(r\omega_{\phi}) - \frac{1}{\sin \theta} \mathcal{O}_2(\sin \theta \omega_{\phi})$$
(16)

But given the previous results, we have:

$$\mathcal{O}_1(r\omega_\phi) = \frac{1}{\sin\theta} \left[-\mathcal{O}_1\mathcal{O}_1(\psi) + \mathcal{O}_1\mathcal{O}_2(\psi) \right]$$
 (17)

and:

$$\mathcal{O}_2(\sin\theta\omega_\phi) = \frac{1}{r} \left[-\mathcal{O}_2\mathcal{O}_1(\psi) + \mathcal{O}_2\mathcal{O}_2(\psi) \right]$$
 (18)

which eventually gives:

$$\left[\mathcal{O}_1 + \mathcal{O}_2\right]^2 \psi = 0 \tag{19}$$

Consider a solution of the form $\psi(r) = f(r) \sin^2 \theta$. We have:

$$(\mathcal{O}_1 + \mathcal{O}_2)f = \sin^2 \theta (n^2 - n - 2)r^{n-2}$$
(20)

and thus:

$$(\mathcal{O}_1 + \mathcal{O}_2)^2 f = \sin^2 \theta (n^2 - n - 2)^2 (n^2 - 5n + 4) r^{n-4}$$
(21)

This means that n = -1, 1, 2, 4 are the only possible values for n, meaning:

$$\psi = \sin^2\theta \left(Ar^{-1} + Br + Cr^2 + Dr^4 \right) \tag{22}$$

For finite velocity, D = 0, and we have, upon substituting $v_r(R) = v_{\theta}(R) = 0$:

$$v_r = U\left(1 - \frac{3R}{2r} + \frac{R^3}{2r^3}\right)\cos\theta$$

$$v_\theta = -U\left(1 - \frac{3R}{4r} - \frac{R^3}{4r^3}\right)\sin\theta$$
(23)

(b) For an incompressible fluid, the stress tensor is given by:

$$\sigma_{ij} = \eta \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right) \tag{24}$$

The only non-zero component is:

$$\sigma_{r\theta} = -\eta U \sin \theta \frac{3}{2R} \tag{25}$$

(c) Balancing the viscous force with the gravitational force, we have:

$$U = \frac{1}{9} \frac{\rho g R^2}{\eta} = 6.48 \times 10^{-3} \,\text{ms}^{-1} \tag{26}$$

4 Coriolis force and vorticity

(a) In the fixed frame, the Navier-Stokes equation is given by:

$$\left(\frac{\mathrm{d}\mathbf{v}_f}{\mathrm{d}t}\right)_f = -\frac{1}{\rho}\nabla p + \nu\nabla^2\mathbf{v}_f + \mathbf{g}$$
(27)

In the rotating frame, the Navier-Stokes equation is given by:

$$\left(\frac{\mathrm{d}\mathbf{v}_r}{\mathrm{d}t}\right)_r + 2\mathbf{\Omega} \times \mathbf{v}_r + \mathbf{\Omega} \times (\mathbf{\Omega} \times \mathbf{r}) = -\frac{1}{\rho}\nabla p + \nu \nabla^2 \mathbf{v}_r + \mathbf{g}$$
(28)

Consider the third term on the left-hand side of the equation. We have:

$$\nabla(\mathbf{\Omega} \times \mathbf{r})^2 = 2(\mathbf{\Omega} \times \mathbf{r}) \cdot \nabla(\mathbf{\Omega} \times \mathbf{r}) + (\mathbf{\Omega} \times \mathbf{r}) \times [\nabla(\mathbf{\Omega} \times \mathbf{r})]$$

$$= (\mathbf{\Omega} \times \mathbf{r}) \times (2\mathbf{\Omega})$$
(29)

which gives:

$$\mathbf{\Omega} \times (\mathbf{\Omega} \times \mathbf{r}) = -\frac{1}{2} \nabla (\mathbf{\Omega} \times \mathbf{r})^2$$
(30)

so that the centrifugal force can be subsumed into the gravitational force.

(b) For inviscid flow, we have:

$$\left(\frac{\mathrm{d}\mathbf{v}_r}{\mathrm{d}t}\right)_r = -2\mathbf{\Omega} \times \mathbf{v}_r - \frac{1}{\rho}\nabla p + \mathbf{g}'$$
(31)

Consider the rate of change of circulation:

$$\frac{\partial \Gamma}{\partial t} = \oint \frac{\partial \mathbf{v}_r}{\partial t} \cdot d\mathbf{l}$$

$$= \oint \left[-2\mathbf{\Omega} \times \mathbf{v}_r - \frac{1}{\rho} \nabla p + \mathbf{g}' - (\mathbf{v}_r \cdot \nabla) \mathbf{v}_r \right] \cdot d\mathbf{l}$$
(32)

The curl of a gradient is zero, so the pressure term does not contribute to the circulation. $(\mathbf{v}_r \cdot \nabla)\mathbf{v}_r$ is along the direction of the flow, so its curl vanishes too. The contributing term is the Coriolis force.

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5 Rankine vortex

(a) Given the velocity field:

$$v_{\theta} = \begin{cases} \Omega r & r < R \\ \frac{\Omega R^2}{r} & r > R \end{cases} \tag{33}$$

we have the vorticity:

$$\omega_z = \begin{cases} 2\Omega & r < R \\ 0 & r > R \end{cases} \tag{34}$$

(b) By Bernoulli's equation and ignoring gravity, we have $p + \frac{1}{2}\rho v^2 = \text{const.}$ This gives:

$$p_{\infty} = p(r) + \frac{1}{2}\rho v_{\theta}^2 = p_0 \tag{35}$$

Thus, the pressure is given by:

$$p(r) = \begin{cases} p_{\infty} - \frac{1}{2}\rho\Omega^{2}r^{2} & r < R\\ p_{\infty} - \frac{1}{2}\rho\frac{\Omega^{2}R^{4}}{r^{2}} & r > R \end{cases}$$
 (36)

(c)