

Circuit Theory

Problem Set 2

Response of Linear Circuits to Transients

Xin, Wenkang

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Response of Linear Circuits to Transients

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Let $q(t)$ be the (positive) charge on the upper plate of the capacitor. By KVL, we have:

$$\begin{aligned}
 V - R \frac{dq}{dt} - \frac{q}{C} &= 0 \\
 \int_0^q \frac{1}{VC - q} dq &= \int_0^t \frac{1}{RC} dt \\
 q(t) &= VC(1 - e^{-t/RC}) \\
 i(t) &= \frac{dq}{dt} = \frac{V}{R} e^{-t/RC}
 \end{aligned} \tag{1}$$

For the energy dissipation:

$$Q_R = \int P dt = \int_0^\infty i^2 R dt = \frac{V^2}{R} \int_0^\infty e^{-2t/RC} dt = \frac{CV^2}{2} = Q_C \tag{2}$$

Thus the total energy supplied by the battery is CV^2 .

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Conduct a mesh analysis with the first loop on the left going clockwise and the second loop on the right going anticlockwise. We have the equations:

$$\begin{aligned}
 V - i_1 R_1 - \frac{q}{C} &= 0 \\
 -i_2 R_2 - \frac{q}{C} &= 0 \\
 i_1 + i_2 &= \frac{dq}{dt}
 \end{aligned} \tag{3}$$

Solving this system for $q(t)$ yields the equation:

$$\frac{R_2}{R_1 + R_2} V - \frac{q}{C} = \frac{R_1 R_2}{R_1 + R_2} \frac{dq}{dt} \tag{4}$$

Solving this differential equation gives:

$$\begin{aligned} q(t) &= CV_0(1 - e^{-t/\tau}) \\ V_C(t) &= V_0(1 - e^{-t/\tau}) \end{aligned} \quad (5)$$

where $V_0 = R_2V/(R_1 + R_2) = 4.125 \text{ V}$ and $\tau = CR_1R_2/(R_1 + R_2) = 137.5 \mu\text{s}$.

At steady state, $I = V/(R_1 + R_2)$. Thus:

$$\begin{aligned} P_1 &= I^2R_1 = 3.5 \times 10^{-4} \text{ W} \\ P_2 &= I^2R_2 = 7.7 \times 10^{-4} \text{ W} \\ Q &= \frac{1}{2}CV_0^2 = 1.7 \times 10^{-4} \text{ J} \end{aligned} \quad (6)$$

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Let $i(t)$ be the current flowing in the circuit. By KVL, we have:

$$V - Ri - L\frac{di}{dt} = 0 \quad (7)$$

Solving this differential equation yields:

$$i(t) = \frac{V}{R}e^{-t/\tau} \quad (8)$$

where $\tau = L/R$.

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Let $q(t)$ be the (positive) charge on the upper plate of the capacitor. By KVL, we have:

$$-\dot{q}R - \ddot{q}L - \frac{q}{C} = 0 \quad (9)$$

or:

$$\ddot{q} + \frac{R}{L}\dot{q} + \frac{1}{RC}q = 0 \quad (10)$$

Note that $1/(LC) \gg (R/2L)^2$. Thus for the characteristic equation:

$$r = -\frac{R}{2L} \pm \sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}} \equiv -\beta \pm i\omega \quad (11)$$

where $\beta \equiv (R/2L)$ and $\omega \equiv \sqrt{1/(LC) - \beta^2} \approx \omega_0 = \sqrt{1/(LC)}$

Then the solution is:

$$\begin{aligned} q(t) &= Ae^{-\beta t} \cos(\omega t + \phi) \\ i(t) &= -A [\beta e^{-\beta t} \cos(\omega t + \phi) + \omega e^{-\beta t} \sin(\omega t + \phi)] \end{aligned} \quad (12)$$

With the initial conditions $q(0) = V_0/C$ and $i(0) = 0$, we have $\tan \phi = -\beta/\omega \ll 1$ and $A \approx V_0/C$. •

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Conduct a mesh analysis with the first loop on the left going clockwise and the second loop on the right going anticlockwise. We have the equations:

$$\begin{aligned} V - i_1 R_1 - \frac{q}{C} &= 0 \\ -L \dot{i}_2 - \frac{q}{C} &= 0 \\ i_1 + i_2 &= \dot{q} \end{aligned} \quad (13)$$

Solving this system for $q(t)$ yields the equation:

$$\ddot{q} + \frac{1}{RC} \dot{q} + \frac{1}{LC} q = 0 \quad (14)$$

Note that $\Delta = 1/(RC) - 4/(LC) < 0$ so the system is oscillatory. The solution is:

$$q(t) = Ae^{-\beta t} \cos(\omega t + \phi) \quad (15)$$

where $\beta = 1/(2RC)$ and $\omega = \sqrt{1/(LC) - \beta^2}$.

Thus the decay constant is $t_0 = 1/\beta = 2RC$.

The resonant (natural) frequency is $\omega_0 = \sqrt{1/(LC)} = 1.6 \times 10^5 \text{ rads}^{-1}$. •

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Before the switch is closed, as the circuit has reached steady state, R_2 is shorted by the inductor and thus $V_A = V_B = 0$. The current in the steady state is V_0/R_1

When the switch is closed, there is current only in the loop (clockwise) between A and B. KVL yields:

$$\begin{aligned} -L\dot{i}_2 - i_2 R_2 &= 0 \\ \int_{V_0/R_1}^{i_2} \frac{1}{i_2} di_2 &= \int_0^t -\frac{R}{L} dt \end{aligned} \quad (16)$$

which leads to the solution:

$$i_2(t) = \frac{V_0}{R_1} e^{-t/\tau} \quad (17)$$

where $\tau = L/R_2 = 10 \mu\text{s}$.

At all times, $V_A = V_0 = 10 \text{ V}$. For V_B , note the relationship:

$$V_B(t) = V_A + i_2 R_2 = V_0 \left[\frac{R_2}{R_1} e^{-t/\tau} + 1 \right] \quad (18)$$

Thus, $V_B(0) = 1010 \text{ V}$ and $V_B(\infty) = 10 \text{ V}$.

When the switch is again closed, there is an additional clockwise loop. A mesh analysis yields:

$$\begin{aligned} V_0 - i_1 R_1 - (i_1 - i_2) R_2 &= 0 \\ -L\dot{i}_2 - (i_1 - i_2) R_2 &= 0 \end{aligned} \quad (19)$$

Solving for i_1 yields:

$$V - i_1 R_1 - L \frac{R_1 + R_2}{R_2} \dot{i}_1 = 0 \quad (20)$$

This differential equation has the solution:

$$i_1(t) = \frac{V_0}{R_1} (1 - e^{-t/\kappa}) \quad (21)$$

where $\kappa = L(R_1 + R_2)/(R_1 R_2) = 1 \text{ ms}$.

Thus the voltage across R_1 , which is $i_1 R_1$, also rises exponentially.

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