Circuit Theory

Problem Set 3

Complex Impedances and Response of Linear Circuits to AC

Xin, Wenkang June 3, 2023

Complex Impedances and Response of Linear Circuits to AC

14

$$(a) V_{\rm rms} = V_C (1)$$

$$V_{\rm rms} = \frac{V_C}{\sqrt{2}} \tag{2}$$

$$V_{\rm rms} = \frac{V_C}{2} \tag{3}$$

(b) and (c) are different because (b) has a higher extreme absolute value.

(d)
$$V_{\rm rms} = \sqrt{\frac{1}{2T} \int_{-T}^{T} \left(\frac{V_0}{T}\right)^2 t^2 dt} = \frac{V_0}{\sqrt{3}}$$
 (4)

15

For all the networks we have $\tilde{V} = V_0 e^{i(\omega t - \pi/2)}$

(a)
$$Z = R - \frac{j}{\omega C} \tag{5}$$

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{\sqrt{R^2 + (1/\omega C)^2}} e^{i(\omega t - \pi/2 + \phi)}$$

$$\tag{6}$$

where $\phi = \tan^{-1} [1/(\omega CR)] = 0.016 \,\mathrm{rad}.$

The current leads the voltage by ϕ .

$$\tilde{V}_R = R\tilde{I} = V_0 \frac{R}{\sqrt{R^2 + (1/\omega C)^2}} e^{i(\omega t - \pi/2 + \phi)}$$
 (7)

Thus, $V_{R,\text{max}} = V_0 R / (\sqrt{R^2 + (1/\omega C)^2}) = 10 \text{ V}.$

(b)
$$Z = j\omega L - \frac{j}{\omega C} \tag{8}$$

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{\sqrt{(\omega L)^2 + (1/\omega C)^2}} e^{i(\omega t - \pi)}$$
(9)

The current lags the voltage by $\pi/2$.

$$V_{C,\text{max}} = V_0 \frac{(1/\omega C)}{\sqrt{(\omega L)^2 + (1/\omega C)^2}} = 10 \text{ V}$$
 (10)

(c)
$$Z = R + j\omega L - \frac{j}{\omega C}$$
 (11)

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{\sqrt{R^2 + (\omega L)^2 + (1/\omega C)^2}} e^{i(\omega t - \pi/2 + \phi)}$$
(12)

where:

$$\phi = \tan^{-1}\left(\frac{1/(\omega C) - \omega L}{R}\right) = 5.5 \times 10^{-3} \,\text{rad} \tag{13}$$

The current leads the voltage by ϕ .

$$V_{L,\text{max}} = V_0 \frac{\omega L}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}} = 1.3 \times 10^{-3} \,\text{V}$$
 (14)

(d)
$$Z = \frac{1}{1/R + 1/(j\omega L)} = Xe^{i\pi/2}$$
 (15)

where $X = 3.95 \,\Omega$.

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{X} e^{i(\omega t - \pi)} \tag{16}$$

The current lags the voltage by $\pi/2$.

$$V_{R\,\text{max}} = V_0 = 10\,\text{V} \tag{17}$$

(e)
$$Z = \frac{1}{1/(j\omega L) + j\omega C} = Xe^{i\pi/2} \tag{18}$$

where $X = 39.5 \,\Omega$.

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{X} e^{i(\omega t - \pi)} \tag{19}$$

The current lags the voltage by $\pi/2$.

$$V_{C,\text{max}} = V_0 = 10 \,\text{V} \tag{20}$$

(f)
$$Z = \frac{1}{1/R + \frac{1}{j\omega L - j/(\omega C)}} = \frac{R(\omega L - 1/(\omega C))}{\sqrt{R^2 + (\omega L - 1/(\omega C))^2}} e^{i\phi} = Xe^{i\phi}$$
(21)

where:

$$\phi = \tan^{-1}\left(\frac{R}{1/(\omega C) - \omega L}\right) = -1.54 \,\text{rad}$$
(22)

$$\tilde{I} = \frac{\tilde{V}}{Z} = \frac{V_0}{X} e^{i(\omega t - \pi/2 - \phi)} \tag{23}$$

The current lags the voltage by ϕ .

$$V_{L,\text{max}} = V_0 \frac{\omega L}{\omega L - 1/(\omega C)} = 10.3 \,\text{V}$$
(24)

16

For both circuits, $\tilde{V}_1 = V_0 e^{i(\omega t - \pi/2)}$.

(I)
$$\tilde{V}_{2} = \tilde{V}_{1} \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{V_{0}}{\sqrt{1 + (\omega C R)^{2}}} e^{i(\omega t - \pi/2 - \phi)}$$
 (25)

where:

$$\phi = \tan^{-1}(\omega CR) \tag{26}$$

$$\frac{V_{2,\text{max}}}{V_{1,\text{max}}} = \frac{1}{\sqrt{1 + (\omega CR)^2}}$$
 (27)

(II)
$$\tilde{V}_2 = \tilde{V}_1 \frac{j\omega L}{R + j\omega L} = \frac{V_0}{\sqrt{1 + (R/\omega L)^2}} e^{i(\omega t - \pi/2 + \phi)}$$
(28)

where:

$$\phi = \tan^{-1} \left(\frac{R}{\omega L} \right) \tag{29}$$

$$\frac{V_{2,\text{max}}}{V_{1,\text{max}}} = \frac{1}{\sqrt{1 + (R/\omega L)^2}} \tag{30}$$

For both circuits, the ratio is given by:

$$\frac{1}{\sqrt{1 + (\omega/\omega_0)^2}}\tag{31}$$

and the phase is given by:

$$\tan^{-1}\left(\frac{\omega}{\omega_0}\right) \tag{32}$$

17

We have $\tilde{I} = I_0 e^{i(\omega t - \pi/2)}$.

(a) $\tilde{V_C} = \frac{\tilde{I}}{j\omega C} = \frac{I_0}{\omega C} e^{i(\omega t - \pi)}$ (33)

where $\frac{I_0}{\omega C} = 10 \,\text{V}$.

$$\tilde{V}_L = \tilde{I}j\omega L = I_0\omega L e^{i\omega t} \tag{34}$$

where $I_0 \omega L = 20 \text{ V}$.

$$\tilde{V}_R = \tilde{I}R = I_0 R e^{i(\omega t - \pi/2)} \tag{35}$$

where $I_0R = 10 \,\text{V}$.

$$\tilde{V} = I_0 X e^{i(\omega t - \pi/2 + \phi)} \tag{36}$$

where:

$$X = \sqrt{R^2 + (\omega L - 1/(\omega C))^2} = 141 \Omega$$
 (37)

and:

$$\phi = \tan^{-1} \left(\frac{\omega L - 1/(\omega C)}{R} \right) = \pi/2 \tag{38}$$

and $I_0 X = 14.1 \,\text{V}$

(b)
$$P = \operatorname{Re}(\tilde{V}) \operatorname{Re}(\tilde{I}) = I_0^2 X \sin(\omega t + \phi) \sin \omega t$$
 (39)

(c)
$$W_L = \frac{1}{2} L \operatorname{Re}(\tilde{I})^2 = \frac{1}{2} L I_0^2 \sin^2 \omega t$$
 (40)

$$W_C = \frac{1}{2}C \operatorname{Im}(\tilde{V_C})^2 = \frac{1}{2} \frac{1}{\omega^2 C} I_0^2 \cos^2 \omega t$$
 (41)

- (d) Their maximum values are $\frac{1}{2}LI_0^2$ and $\frac{1}{2}\frac{1}{\omega^2C}I_0^2$ respectively.
- (f) For the sum to be constant, $L = 1/(\omega^2 C) = 0.1 \,\text{mH}$.

18

For this circuit:

$$Z = R + j\omega L - \frac{j}{\omega C} = \sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2} e^{i\phi}$$
(42)

For the amplitude to be minimum:

$$\frac{\mathrm{d}}{\mathrm{d}\omega} \left[\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2} \right] = \frac{2(\omega L - \frac{1}{\omega C})(L + \frac{1}{\omega^2 C})}{2\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}} = 0$$
(43)

This happens when $\omega L - \frac{1}{\omega C} = 0$ or $\omega = \frac{1}{\sqrt{LC}}$. Then $Z = Re^{i\phi}$, and $V_{C,\text{max}} = V_0/(\omega CR) = 3.16 \,\text{V}$.

19

$$Z = j\omega L - \frac{j}{2\omega C} + \frac{1}{j\omega C + \frac{1}{\frac{1}{2j\omega C} + j\omega L}} = j\left(\omega L - \frac{1}{2\omega C} - \frac{1}{\omega C + \frac{2\omega C}{1 - 2\omega^2 CL}}\right) = 0 \tag{44}$$

Solving this equation (avoiding the asymptote) gives $\omega = \sqrt{5/(2LC)}$. The other root $\omega = \sqrt{1/(2LC)}$ is obtained by substituting the asymptote value directly into the original expression.

20

(a) For the bridge to be balanced:

$$Z_1 \frac{1}{\frac{1}{R_4} + j\omega C_4} = \frac{1}{j\omega C_3} R_2 \tag{45}$$

Solving for Z_1 yields:

$$Z_1 = R_2 \frac{C_4}{C_3} - j \frac{R_2}{R_4} \frac{1}{\omega C_3} \tag{46}$$

(b) For a series combination:

$$R_1 - j\frac{1}{\omega C_1} = R_2 \frac{C_4}{C_3} - j\frac{R_2}{R_4} \frac{1}{\omega C_3}$$

$$\tag{47}$$

so that $R_1 = R_2C_4/C_3$ and $C_1 = C_3R_4/R_2$.

(c) For a parallel combination:

$$\frac{1}{\frac{1}{R_1} + j\frac{1}{\omega C_1}} = R_2 \frac{C_4}{C_3} - j\frac{R_2}{R_4} \frac{1}{\omega C_3}$$
(48)

Solving this equation yields:

$$R_{1} = \frac{R_{2} \left[1 + (\omega C_{4} R_{4})^{2} \right]}{\omega^{2} C_{3} C_{4} R_{4}^{2}}$$

$$C_{1} = \frac{C_{3} R_{4}}{R_{2} \left[1 + (\omega C_{4} R_{4})^{2} \right]}$$
(49)

21

(a) Note that $\omega_0 L = 1/(\omega_0 C) = \sqrt{3}R$

$$Z = R + \frac{1}{\frac{1}{R + j\omega_0 L} + \frac{1}{R - j/(\omega_0 C)}} = R + \frac{(R + j\sqrt{3}R)(R - j\sqrt{3}R)}{2R} = 3R$$
 (50)

(b)

$$\tilde{V_{AX}} = \frac{R}{3R}\tilde{V_{AB}} = \frac{\tilde{V_{AB}}}{3} \tag{51}$$

$$\tilde{V}_{XY} = \frac{2}{3}\tilde{V}_{AB}\frac{R}{R+i\sqrt{3}R} = \frac{\tilde{V}_{AB}}{3}e^{i\pi/3}$$
 (52)

$$\tilde{V_{XZ}} = \frac{1}{3}\tilde{V_{AB}}\frac{R}{R - i/(\sqrt{3}R)} = \frac{\tilde{V_{AB}}}{3}e^{-i\pi/3}$$
(53)

•

22

We have:

$$V_{xy} = \left(\frac{1}{2} - \frac{1}{1 + j\omega RC}\right)V = \frac{j\omega RC - 1}{j\omega RC + 1}\frac{V}{2}$$

$$\tag{54}$$

so the amplitude is $|V_{xy} = V/2|$ which is independent of R and the phase is $\pi - 2\phi$ where $\phi = \tan^{-1}(\omega RC)$.

Therefore, when $R = 1/(\omega C)$, $\pi - 2\phi = \pi/2$.