

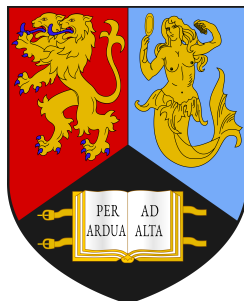
# Kernel-Independent Fast Multipole Method for the computation of large regularized Stokeslet systems

Analysis of the Kernel-independent fast multipole method for use in biofluids

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May 2022

## Acknowledgements

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## Abstract

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# 1 Introduction

$$\begin{aligned} \rho \left( \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right) &= \mathbf{F} - \nabla p + \mu \Delta \mathbf{u} \\ \nabla \cdot \mathbf{u} &= 0 \end{aligned} \tag{1.1}$$

where  $\rho$  is the fluid density,  $\mathbf{u}$  is the velocity of the fluid,  $\mathbf{F}$  is the external force,  $p$  is the pressure and  $\mu$  is the fluid viscosity

## 2 Method of Regularized Stokeslets

### 2.1 Stokes flow

When we look at many physical systems, particularly in biology, we find that the inertial forces withing the fluid are small in comparison to that of the viscous terms. In these cases we can take the limit of the Navier-Stokes equation (eq. (1.1)) where  $Re = \rho u L / \mu \rightarrow 0$  [1]. Within biological system we find that these cases occur when either we are looking at highly viscous fluids where  $\mu$  is large or at small length scales where  $L$  (The typical scale of the system) is very small such as when looking looking at cells, microorganism or flows around small capillaries [2, 3, 4]. As well as biological models we can use it in more general fluid dynamics, where we have stokes flow, with complex boundaries [5, 6].

The steady state Stokes equations in two or three dimensions are

$$\mu \Delta \mathbf{u} = \nabla p - \mathbf{F} \tag{2.1a}$$

$$\nabla \cdot \mathbf{u} = 0 \tag{2.1b}$$

where  $\mathbf{u}$  is the velocity of the fluid,  $\mathbf{F}$  is the external force,  $p$  is the pressure and  $\mu$  is the fluid viscosity. We can derive a singular fundamental solution to the Stokes equations which we will call a *Stokeslet*. The Stokeslet represents the solution for the velocity of the fluid given that the external force  $\mathbf{F}$  acting on the fluid is concentrated at a single point  $\mathbf{F} = \mathbf{f}_0 \delta(\mathbf{x})$  [7, 8, 9]. Through Similar methods to that show later for deriving regularized Stokeslet Equation (eq. (2.18b)) we can derive the singular fundamental solutions to the stokes equations as

$$\begin{aligned} S_{jk}(\mathbf{x}, \mathbf{x}_0) &= \frac{\delta_{jk}}{r} + \frac{(x_j - x_{0,j})(x_k - x_{0,k})}{r^3} \\ P_k(\mathbf{x}, \mathbf{x}_0) &= \frac{x_k - x_{0,k}}{r^3} \\ T_{ijk}(\mathbf{x}, \mathbf{x}_0) &= \frac{-6(x_i - x_{0,i})(x_j - x_{0,j})(x_k - x_{0,k})}{r^5} \end{aligned} \tag{2.2}$$

Where  $r = |\mathbf{x} - \mathbf{x}_0|$ . We find the velocity  $\mathbf{u}$  at a point  $\mathbf{x}$  through the equation

$$\mathbf{u} = (8\pi\mu)^{-1} (S_{1k}, S_{2k}, S_{3k}) f_{0,j}$$

where  $\mathbf{f}_0$  is the force per unit area, exerted by the fluid on the surface, concentrated at the point  $\mathbf{x}_0$ .

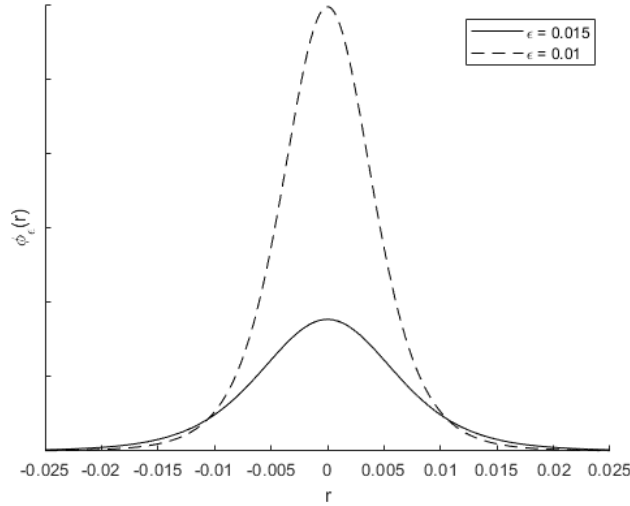


Figure 1: Blob function in equation eq. (2.3) for several values of epsilon

## 2.2 Regularising the Stokeslet

While the singular Stokeslet provides a useful mechanism to solve boundary integral equations, it relies on the surfaces on which they are concentrated on to be smooth such that the velocity is integrable and the fluid bounded in the neighbourhood of the surface. However if we consider non smooth surfaces or curves instead of surfaces then the resulting equations for velocity become non singular and much harder so work with.

In order to remove these singularities we use a "blob function" which instead of approximating at force at a singular point we instead approximate as a sphere centred at the the same point. While the radius of the sphere is often infinite the blob function decays rapidly away from the centre with the largest contribution obtained in the close vicinity of the centre. We introduce a control parameter  $\epsilon$  independent of any discretization which controls the rate of decay. The effect of this control parameter can be seen in Fig.fig. 1. In order to obtain similar results to that of the singular solutions we dictate that  $\int \phi^\epsilon(r) dr = 1$  for all values of  $\epsilon$ . This allows us to preserve the results obtained for the singular kernels for distances away from the point in which the force is exerted and obtains different results close to the point. In order to retain the singular solution we have that as  $\epsilon \rightarrow 0$  our blob function must tend to the Dirac delta. For simplicity of the paper and the application to wider range of problems we will only consider spherically symmetric function such as those in eqs. (2.3) and (2.4) [10, 11, 12].

$$\phi^\epsilon(r) = \frac{15\epsilon^4}{8\pi(r^2 + \epsilon^2)^{7/2}} \quad (2.3)$$

$$\psi_\epsilon(r) = \frac{15\epsilon^6 \left(5 - \frac{2r^2}{\epsilon^2}\right)}{16\pi(r^2 + \epsilon^2)^{9/2}} \quad \psi_\epsilon(r) = \frac{5\epsilon^2 - 2r^2}{2\pi^{3/2}\epsilon^5} e^{-r^2/\epsilon^2} \quad (2.4)$$

For the derivation of the regularized Stokeslets and all further numerical analysis we will use eq. (2.3) due to its popularity in external literature and the simplicity of the kernel it generates.

### 2.2.1 Derivation of the Regularized Stokeslet

By concentrating the force onto a finite area using the blob function rather than a singular point as with the delta function. We therefore convert the stokes equations given in eq. (2.1) to a new set of equation for which we will derive a set of solutions,

$$\mu \Delta \mathbf{u} = \nabla p - \phi_\epsilon(\mathbf{x} - \mathbf{x}_0) \mathbf{f}_0 \quad (2.5a)$$

$$\nabla \cdot \mathbf{u} = 0 \quad (2.5b)$$

where  $f_0$  is the force per unit area as define in the previous section. In order to simplify notation from this point on-wards we will use the Einstein summation convention where repeated indices are summed over. We introduce the regularized Stokeslet function  $S^\epsilon(\mathbf{x}, \mathbf{x}_0)$  which is the Green's function for the velocity  $u^\epsilon(\mathbf{x})$ . We can now write the solution to eq. (2.5) as

$$u_i(\mathbf{x}) = \frac{1}{8\pi\mu} S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0) f_{0,j} \quad (2.6)$$

The pressure and stress tensor associated with that flow can also be also be written as

$$p(\mathbf{x}) = \frac{1}{8\pi} P_j^\epsilon(\mathbf{x}, \mathbf{x}_0) f_{0,j} \quad (2.7)$$

$$\sigma_{ik}(\mathbf{x}) = \frac{1}{8\pi} T_{ijk}^\epsilon(\mathbf{x}, \mathbf{x}_0) f_{0,j} \quad (2.8)$$

By substituting these solutions back into eq. (2.5a) we find that they must obey

$$\Delta S_{kj}^\epsilon(\mathbf{x}, \mathbf{x}_0) = \frac{\partial P_j^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_k} - 8\pi \delta_{kj} \phi^\epsilon(\mathbf{x} - \mathbf{x}_0) \quad (2.9)$$

for all j and k with  $\delta_{kj}$  being the Kronecker delta. The incompressibility condition eq. (2.5b) also gives us that

$$\frac{\partial S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_i} = 0 \quad (2.10)$$

for all j. We next take the derivative of eq. (2.9) with respect to  $x_k$  to get

$$\frac{\partial S_{kj}^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_i \partial x_i \partial x_k} = \frac{\partial^2 P_j^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_k^2} - 8\pi \delta_{kj} \frac{\partial \phi^\epsilon(\mathbf{x} - \mathbf{x}_0)}{\partial x_k}$$

Summing over  $k$  as per the convention and using eq. (2.10) gives us

$$\Delta P_j^\epsilon(\mathbf{x}, \mathbf{x}_0) = 8\pi \frac{\partial \phi^\epsilon(\mathbf{x} - \mathbf{x}_0)}{\partial x_j} \quad (2.11)$$

If we now introduce the following two equations for simplicity

$$\Delta G^\epsilon(\mathbf{x} - \mathbf{x}_0) = \phi^\epsilon(\mathbf{x} - \mathbf{x}_0) \quad (2.12a)$$

$$\Delta B^\epsilon(\mathbf{x} - \mathbf{x}_0) = G^\epsilon(\mathbf{x} - \mathbf{x}_0) \quad (2.12b)$$



Using eqs. (2.11) and (2.12a) we can express the pressure as

$$P_j^\epsilon(\mathbf{x}, \mathbf{x}_0) f_{0,j} = 8\pi \frac{\partial G^\epsilon(\mathbf{x} - \mathbf{x}_0)}{\partial x_j} \quad (2.13)$$

Then finally using eqs. (2.10) and (2.12b) gives us the general for of our Stokeslet.

$$S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0) = 8\pi \left[ \frac{\partial^2 B^\epsilon(\mathbf{x} - \mathbf{x}_0)}{\partial x_i \partial x_j} - \delta_{ij} G^\epsilon(\mathbf{x} - \mathbf{x}_0) \right] \quad (2.14)$$

As the stress tensor is defined as

$$\sigma_{ij}^\epsilon(\mathbf{x}) = -\delta_{ik} p^\epsilon(\mathbf{x}) + \mu \left( \frac{\partial u_i^\epsilon}{\partial x_k} + \frac{\partial u_k^\epsilon}{\partial x_i} \right) \quad (2.15)$$

we find that

$$T_{ijk}^\epsilon(\mathbf{x}, \mathbf{x}_0) = -\delta_{ik} P_j^\epsilon(\mathbf{x}, \mathbf{x}_0) + \mu \left( \frac{\partial S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_k} + \frac{\partial S_{kj}^\epsilon(\mathbf{x}, \mathbf{x}_0)}{\partial x_i} \right) \quad (2.16)$$

### 2.2.2 Specific Blob

If we take the blob equation defined in eq. (2.3) and solve to find  $G^\epsilon$  and  $B^\epsilon$  we get that

$$G^\epsilon(\mathbf{x} - \mathbf{x}_0) = \frac{-2r^2 + 3\epsilon^2}{8\pi(r^2 + \epsilon^2)^{3/2}} + \frac{3}{8\pi\epsilon} \quad (2.17a)$$

$$B^\epsilon(\mathbf{x} - \mathbf{x}_0) = -\frac{\sqrt{\epsilon^2 + r^2}}{8\pi} + \frac{r^2}{16\pi\epsilon} + \frac{\epsilon}{8\pi} \quad (2.17b)$$

$$(2.17c)$$

where  $r = |\mathbf{x} - \mathbf{x}_0|$ . We now substitute eqs. (2.17a) and (2.17b) into eqs. (2.13), (2.14) and (2.16) to obtain our final kernels which will be used for all further analysis.

$$P_j^\epsilon(\mathbf{x}, \mathbf{x}_0) = (x_j - x_{0,j}) \frac{2r^2 + 5\epsilon^2}{(r^2 + \epsilon^2)^{5/2}} \quad (2.18a)$$

$$S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0) = \delta_{ij} \frac{r^2 + 2\epsilon^2}{(r^2 + \epsilon^2)^{3/2}} + \frac{(x_i - x_{0,i})(x_j - x_{0,j})}{(r^2 + \epsilon^2)^{3/2}} \quad (2.18b)$$

$$T_{ijk}^\epsilon(\mathbf{x}, \mathbf{x}_0) = \frac{-6(x_i - x_{0,i})(x_j - x_{0,j})(x_k - x_{0,k})}{(r^2 + \epsilon^2)^{5/2}} \quad (2.18c)$$

$$- \frac{3\epsilon^2[\delta_{jk}(x_i - x_{0,i}) + \delta_{ik}(x_j - x_{0,j}) + \delta_{ij}(x_k - x_{0,k})]}{(r^2 + \epsilon^2)^{5/2}}$$

We can easily check that these provide results consistent with those found by the singular solutions as in the limit  $\epsilon \rightarrow 0$  we obtain the same results stated in eq. (2.2).

### 2.2.3 Boudnary integral equations

The solution to stokes equations

$$\begin{aligned} \mu \Delta \mathbf{u} &= \nabla p \\ \nabla \cdot \mathbf{u} &= 0 \end{aligned} \quad (2.19)$$

and regularized stokes equation

$$\begin{aligned}\mu\Delta\mathbf{u} &= \nabla p - \phi_\epsilon(\mathbf{x} - \mathbf{x}_0)\mathbf{f}_0 \\ \nabla \cdot \mathbf{u} &= 0\end{aligned}\tag{2.20}$$

are linked through the cutoff function and obtain the same results in the limit as  $\epsilon \rightarrow 0$ . It is assumed that the regularized solution is a flow generated by a point force of strength  $\mathbf{f}_0$  located at a point  $\mathbf{x}_0$  while the non-regularized solution is absent of all forces.

We let  $D$  be a solid body and assume the point  $\mathbf{x}$  is outside of  $D$ . Then we have that  $(\mathbf{u}, p)$  satisfies eq. (2.19) with

$$\sigma_{ij}(\mathbf{x}) = -\delta_{ik}p(\mathbf{x}) + \mu \left( \frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right)$$

and  $(\mathbf{u}^\epsilon, p)$  satisfies eq. (2.20) with

$$\sigma_{ij}^\epsilon(\mathbf{x}) = -\delta_{ik}p^\epsilon(\mathbf{x}) + \mu \left( \frac{\partial u_i^\epsilon}{\partial x_k} + \frac{\partial u_k^\epsilon}{\partial x_i} \right)$$

We note that  $\partial\sigma_{ik}^\epsilon(\mathbf{x})/\partial x_k = -f_{0,i}\phi^\epsilon(\mathbf{x} - \mathbf{x}_0)$  and  $\partial\sigma_{ik}(\mathbf{x})/\partial x_k = 0$ . From these two equations we find that

$$\begin{aligned}\frac{\partial}{\partial x_k}(u_i^\epsilon\sigma_{ik} - u_i\sigma_{ik}^\epsilon) &= \\ \frac{\partial u_i^\epsilon}{\partial x_k}\sigma_{ik} + u_i^\epsilon\frac{\partial\sigma_{ik}}{\partial x_k} - \frac{\partial u_i}{\partial x_k}\sigma_{ik}^\epsilon - u_i\frac{\partial\sigma_{ik}^\epsilon}{\partial x_k} &= \\ 0 + 0 - 0 - u_i(-f_{0,i})\phi^\epsilon &= \\ u_j f_{0,j}\psi^\epsilon(\mathbf{x} - \mathbf{x}_0)\end{aligned}$$

where we have replaced the summation over  $i$  with a summation over  $j$  without affecting the result. We now substitute in eq. (2.8) and ?? to obtain

$$\frac{1}{8\pi\mu}\frac{\partial}{\partial x_k}(S_{ij}^\epsilon f_{0,j}\sigma_{ik} - \mu u_i T_{ijk}^\epsilon f_{0,j}) = u_j f_{0,j}\psi_\epsilon(\mathbf{x} - \mathbf{x}_0)$$

as  $f_{0,j}$  is constant we can take it out of the derivative on the left hand side and note that it is now arbitrary and as such  $\mathbf{u}$  and  $p$  obey the relation

$$\frac{1}{8\pi\mu}\frac{\partial}{\partial x_k}(S_{ij}^\epsilon\sigma_{ik} - \mu u_i T_{ijk}^\epsilon) = u_j\psi_\epsilon(\mathbf{x} - \mathbf{x}_0)\tag{2.21}$$

Suppose we now let  $S$  be the area between the solid body  $D$  and a sphere with radius such that all of  $D$  is contained within. We will denote  $\partial S$  to the the surface of  $S$ , note that this contains the surface of the sphere and  $\partial D$ . If we now intergrate the above equation over  $S$  then we get that

$$\int_S \left[ \frac{1}{8\pi\mu}\frac{\partial}{\partial x_k}(S_{ij}^\epsilon\sigma_{ik} - \mu u_i T_{ijk}^\epsilon) \right] dV(\mathbf{x}) = \int_S u_j\psi_\epsilon(\mathbf{x} - \mathbf{x}_0)dV(\mathbf{x})$$

Taking the divergece theorem of the Left hand side we get that

$$\frac{1}{8\pi\mu} \int_{\partial S} [S_{ij}^\epsilon\sigma_{ik} - \mu u_i T_{ijk}^\epsilon] n_k ds(\mathbf{x}) = \int_S u_j\psi_\epsilon(\mathbf{x} - \mathbf{x}_0)dV(\mathbf{x})$$

where  $\mathbf{n}$  is the outwards unit normal vector of the surface of  $S$ . If we take the limit as the radius of the sphere tends to infinity, we find that the only contributions come from  $\partial D$ . We will introduce the traction on the surface of the sphere as  $f_i = -\sigma_{ik}n_k$  and therefore we obtain that

$$\frac{1}{8\pi\mu} \int_{\partial D} S_{ij}^\epsilon f_i ds(\mathbf{x}) - \frac{1}{8\pi} \int_{\partial D} u_i T_{ijk}^\epsilon n_k ds(\mathbf{x}) = \int_S u_j \psi_\epsilon(\mathbf{x} - \mathbf{x}_0) dV(\mathbf{x}) \quad (2.22)$$

Considering the fluid inside of the solid body  $D$  we realise that the velocity must satisfy the zero-deformation condition

$$\frac{\partial u_i}{\partial k} + \frac{\partial u_k}{\partial i} = 0$$

This gives us that  $\sigma_{ik} = -p\delta_{ik}$  so we have that for each  $j$

$$\int_D \frac{\partial}{\partial x_k} [S_{ij}^\epsilon \sigma_{ik}] dV(\mathbf{X}) = -p \int_D \frac{\partial}{\partial x_k} [S_{kj}^\epsilon] dV(\mathbf{X}) = 0$$

from the incompressibility condition eq. (2.10). If we now integrate eq. (2.21) over  $D$  instead of  $S$  and use the above integral we have that

$$\frac{1}{8\pi} \int_{\partial D} u_i T_{ijk}^\epsilon n_k ds(\mathbf{x}) = \int_D u_j \psi_\epsilon(\mathbf{x} - \mathbf{x}_0) dV(\mathbf{x}) \quad (2.23)$$

We note now that the sum over eqs. (2.22) and (2.23) will give us the integral over  $\mathbb{R}^3$ . Using the fact that the velocity is continuous on the boundary  $\partial D$  we obtain the final boundary integral equation

$$\int_{\mathbb{R}^3} u_j(\mathbf{x}) \phi_\epsilon(\mathbf{x} - \mathbf{x}_0) dV(\mathbf{x}) = -\frac{1}{8\pi\mu} \int_{\partial D} S_{ij}^\epsilon(\mathbf{x}, \mathbf{x}_0) f_i ds(\mathbf{x}) \quad (2.24)$$

As the traction  $\mathbf{f}$  denotes the force exerted by the fluid on the body it must have the opposite sign to the Stokeslet strength  $\mathbf{f}_0$  and as such  $\mathbf{f}_0 = -\mathbf{f}$ . The analytical computation of eq. (2.24) is possible for certain cases allowing for the computation of the fluid velocity given prescribed body forces on the fluid, however they are often hard or impossible to do by hand. We can easily discretize the boundary integral equation to obtain a formula for the velocity of the fluid at a point  $\mathbf{x}_0$ . We discretize the integral into the sum over  $N$  Stokeslets located along the surface of  $D$  and obtain

$$u_j(\mathbf{x}_0) = \frac{1}{8\pi\mu} \sum_{n=1}^N \sum_{i=1}^3 S_{ij}^\epsilon(\mathbf{x}_n, \mathbf{x}_0) f_{n,i} A_n \quad (2.25)$$

where  $f_{n,i}$  is the  $i$ th component of the force on the fluid at  $\mathbf{x}_n$  and  $A_n$  is the corresponding quadrature weight of the  $n$ th Stokeslet.

## 3 Nearest

## 4 Kernel-Independent Fast Multipole Method

### 4.1 Hierarchical decomposition of the computational domain

### 4.2 Equivalent surfaces/coronas

### 4.3 Numerical approximation of the force densities

### 4.4 Evaluation

### 4.5 Comparison of KIFMM method vs Direct solver

## 5 Preconditioning

## 6 Numerical Simulations

### 6.1 Cilia

### 6.2 Sperm

## 7 Results

## 8 Discussion

## A Pseudocode

### A.1 Upwards pass

### A.2 Downward pass

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