

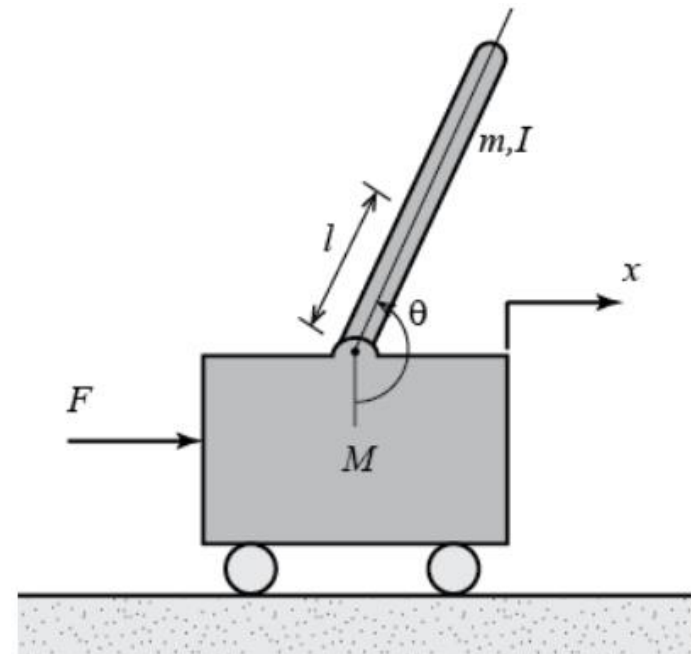


# Inverted Pendulum Modeling, Control and Demo

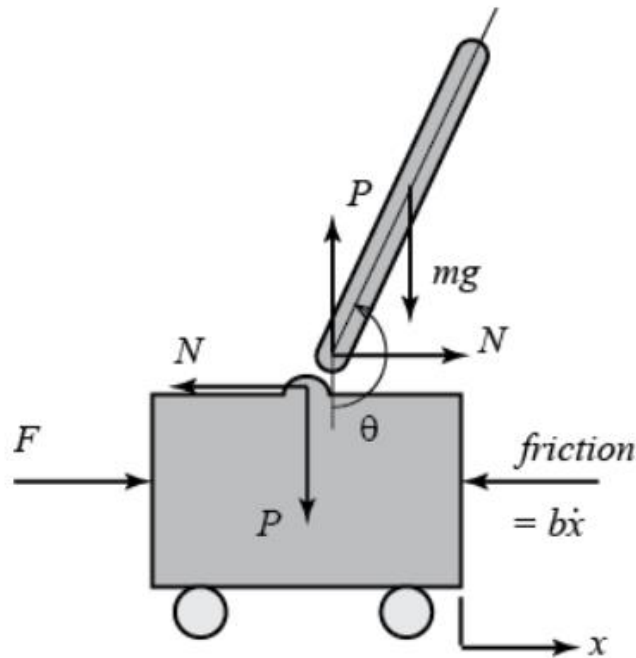


# Overview

- System Modeling
- Various Controllers
- PD Control Demo



# System Modeling



$$\begin{aligned} M\ddot{x} + b\dot{x} + N &= F \\ N &= m\ddot{x} + ml\ddot{\theta}\cos\theta - ml\dot{\theta}^2\sin\theta \\ (M + m)\ddot{x} + b\dot{x} + ml\ddot{\theta}\cos\theta - ml\dot{\theta}^2\sin\theta &= F \end{aligned} \quad (1)$$

$$\begin{aligned} P\sin\theta + N\cos\theta - mg\sin\theta &= ml\ddot{\theta} + m\ddot{x}\cos\theta \\ -Pl\sin\theta - Nl\cos\theta &= I\ddot{\theta} \\ (I + ml^2)\ddot{\theta} + mgl\sin\theta &= -ml\ddot{x}\cos\theta \end{aligned} \quad (2)$$

$$\begin{aligned} \cos\theta &= \cos(\pi + \phi) \approx -1 \\ \sin\theta &= \sin(\pi + \phi) \approx -\phi \\ \dot{\theta}^2 &= \dot{\phi}^2 \approx 0 \end{aligned}$$

Linearize

$$\begin{aligned} (I + ml^2)\ddot{\phi} - mgl\phi &= ml\ddot{x} \\ (M + m)\ddot{x} + b\dot{x} - ml\ddot{\phi} &= u \end{aligned}$$

Linear EOM

# Transfer Function

$$\begin{aligned}(I + ml^2)\ddot{\phi} - mgl\phi &= ml\ddot{x} \\ (M + m)\ddot{x} + b\dot{x} - ml\ddot{\phi} &= u\end{aligned}$$

$$\begin{aligned}(I + ml^2)\Phi(s)s^2 - mgl\Phi(s) &= mlX(s)s^2 \\ (M + m)X(s)s^2 + bX(s)s - ml\Phi(s)s^2 &= U(s)\end{aligned}$$

$$P_{pend}(s) = \frac{\Phi(s)}{U(s)} = \frac{\frac{ml}{q}s}{s^3 + \frac{b(I+ml^2)}{q}s^2 - \frac{(M+m)mgl}{q}s - \frac{bmgl}{q}} \quad \left[\frac{rad}{N}\right]$$

$$P_{cart}(s) = \frac{X(s)}{U(s)} = \frac{\frac{(I+ml^2)s^2 - gml}{q}}{s^4 + \frac{b(I+ml^2)}{q}s^3 - \frac{(M+m)mgl}{q}s^2 - \frac{bmgl}{q}s} \quad \left[\frac{m}{N}\right]$$

Transfer  
Function

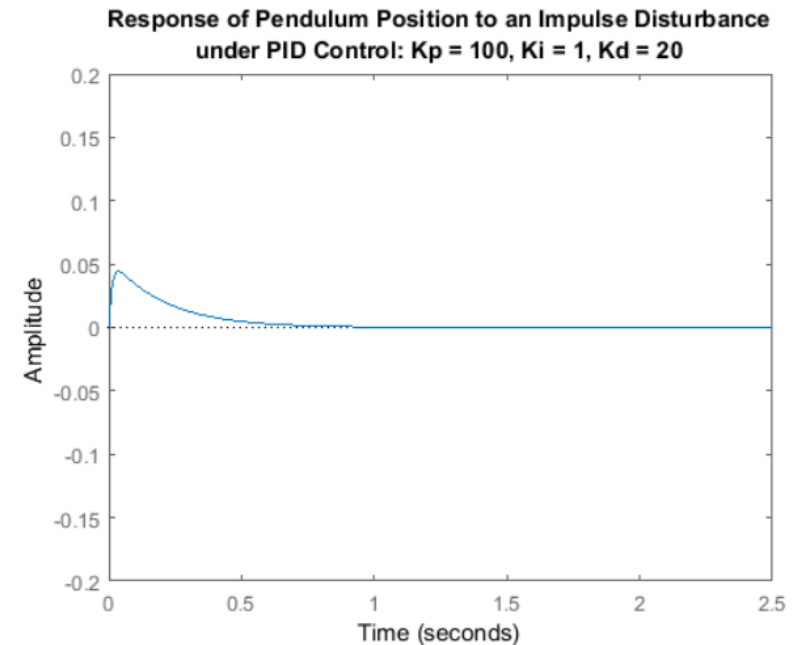
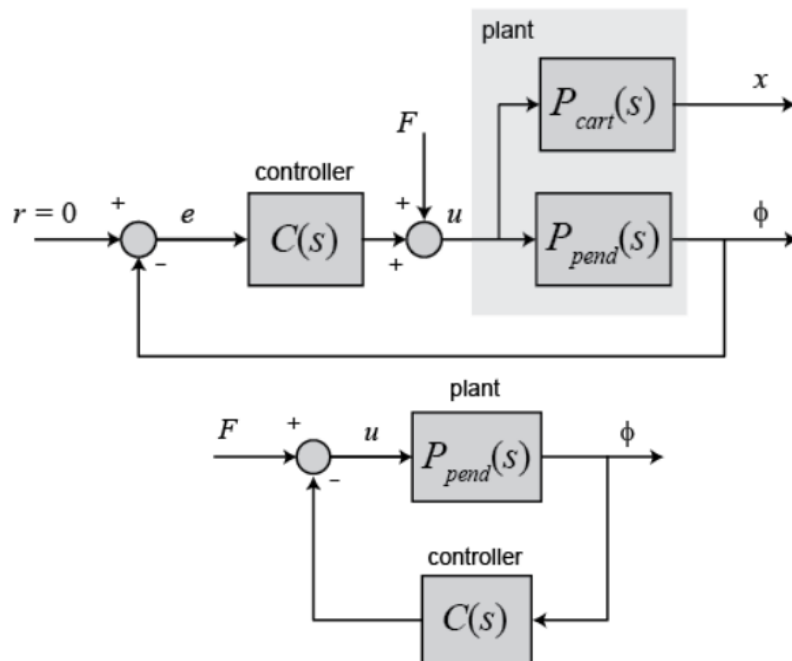
$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\phi} \\ \ddot{\phi} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & \frac{-(I+ml^2)b}{I(M+m)+Mml^2} & \frac{m^2gl^2}{I(M+m)+Mml^2} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & \frac{-mlb}{I(M+m)+Mml^2} & \frac{mgl(M+m)}{I(M+m)+Mml^2} & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{I+ml^2}{I(M+m)+Mml^2} \\ 0 \\ \frac{ml}{I(M+m)+Mml^2} \end{bmatrix} u$$

State  
Space

$$\mathbf{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

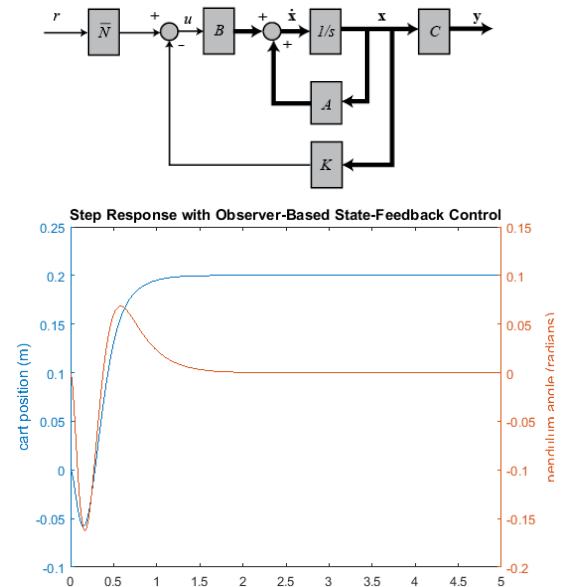
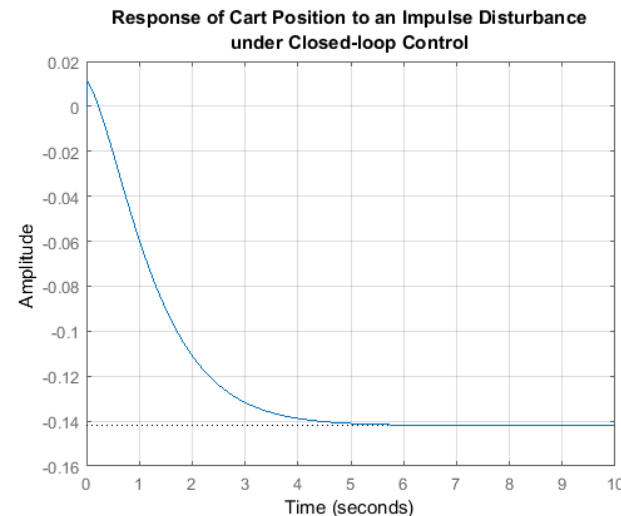
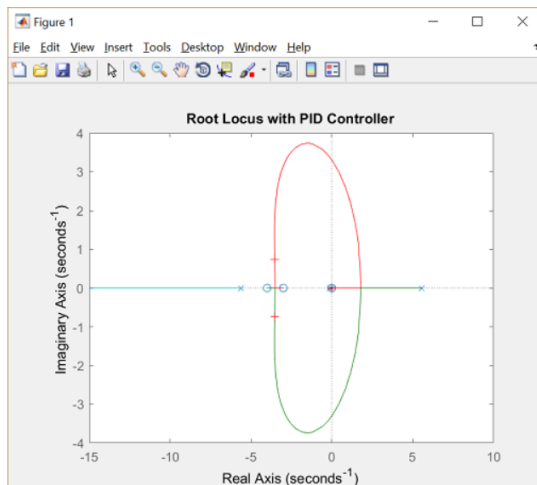
# PID Control for Angle

- Angle PID control can stabilize pendulum but not cart
- Analyze for reference equal to 0 and found impulse response



# Other Control Techniques

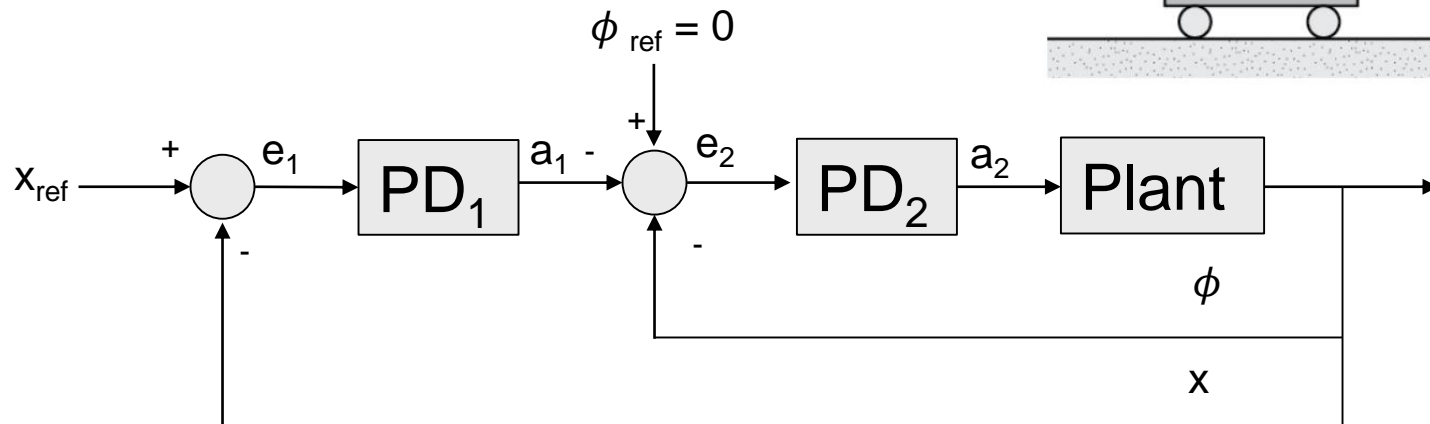
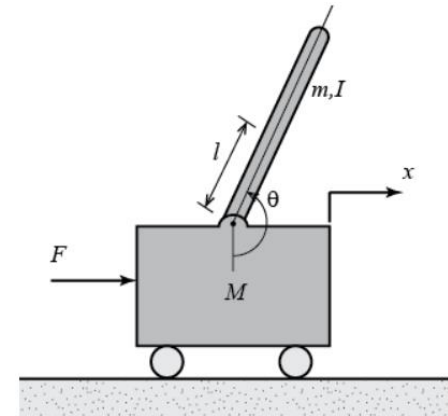
- Root locus for PID design can be used for pole placement
- Frequency domain loop shaping can luckily control cart position
- State space design technique can stabilize both variable



# Double PD Control

- Inner and Outer layer PD control
- Negative feedback from position
- Less intuitive due to 2 layer controller

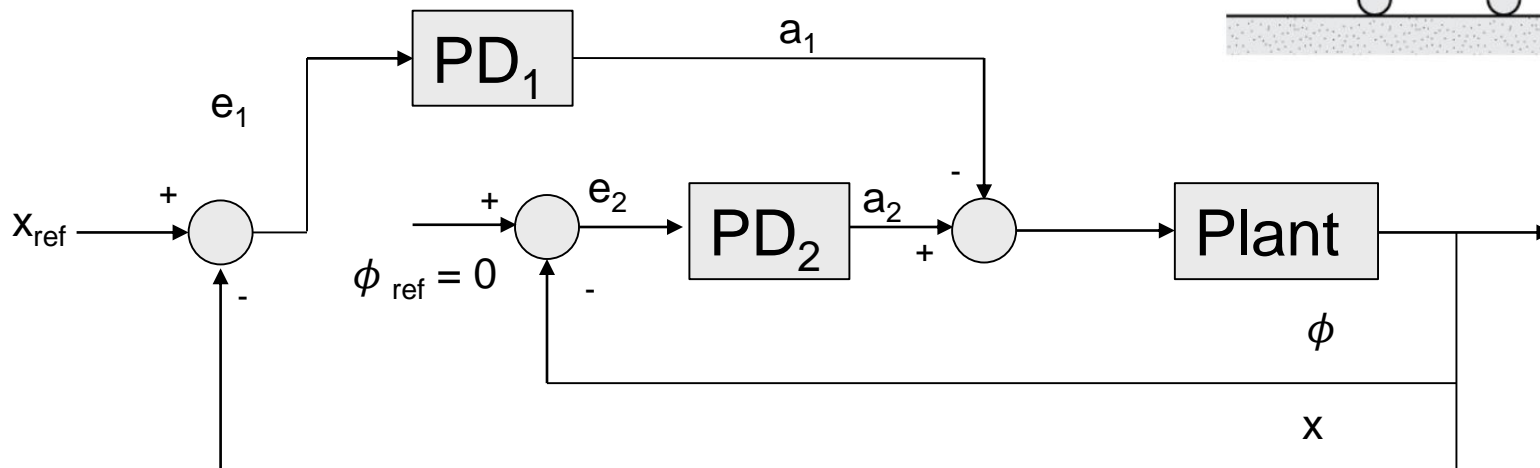
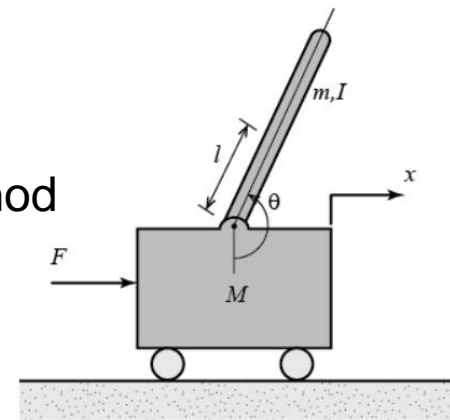
$$a_1 = k_{p1}e_1 + k_{d1}\dot{e}_1 \quad a_2 = k_{p2}e_2 + k_{d2}\dot{e}_2$$



## Parallel PD Control Used in Demo

- Use parallel architecture to simplify system
- No need for double PD on position input
- OK performance but not as good as SS method

$$a_1 = k_{p1}e_1 + k_{d1}\dot{e}_1 \quad a_2 = k_{p2}e_2 + k_{d2}\dot{e}_2$$







# Thank You!