



Introduction to Feedback Control and Simulation



Outline

- System Modeling
 - ODE functions for system dynamics
 - Laplace transformation and transfer function
- System Characterization
 - Step response
 - Frequency response and bode plot
- Closed Loop Control Algorithm
 - Closed loop control overview
 - PID controller
 - Loop shaping design
- System Identification Methods
 - Frequency response identification

System Modeling

- Using physical laws, the behavior of certain systems can be described using ordinary differential equation(s)
- First and second order ODEs are easy to solve and correspond to many physical models such as RLC circuit, mass-spring-damper model for mechanical systems as shown below

$$m\ddot{x} + c\dot{x} + kx = u$$

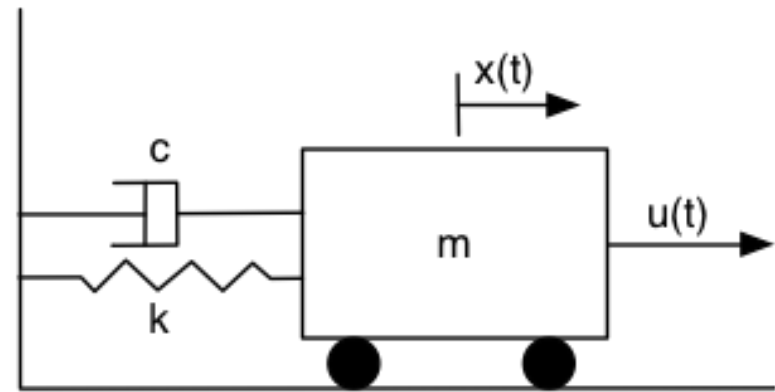
x : position of mass [m] at time t [s]

m : mass [kg]

c : viscous damping coefficient [N s / m]

k : spring constant [N / m]

u : force input [N]



Laplace Transformation

- Laplace transformation simplifies the analysis process for ODES
- Easy representation
- Solving with partial fraction expansion and lookup tables
- Definition

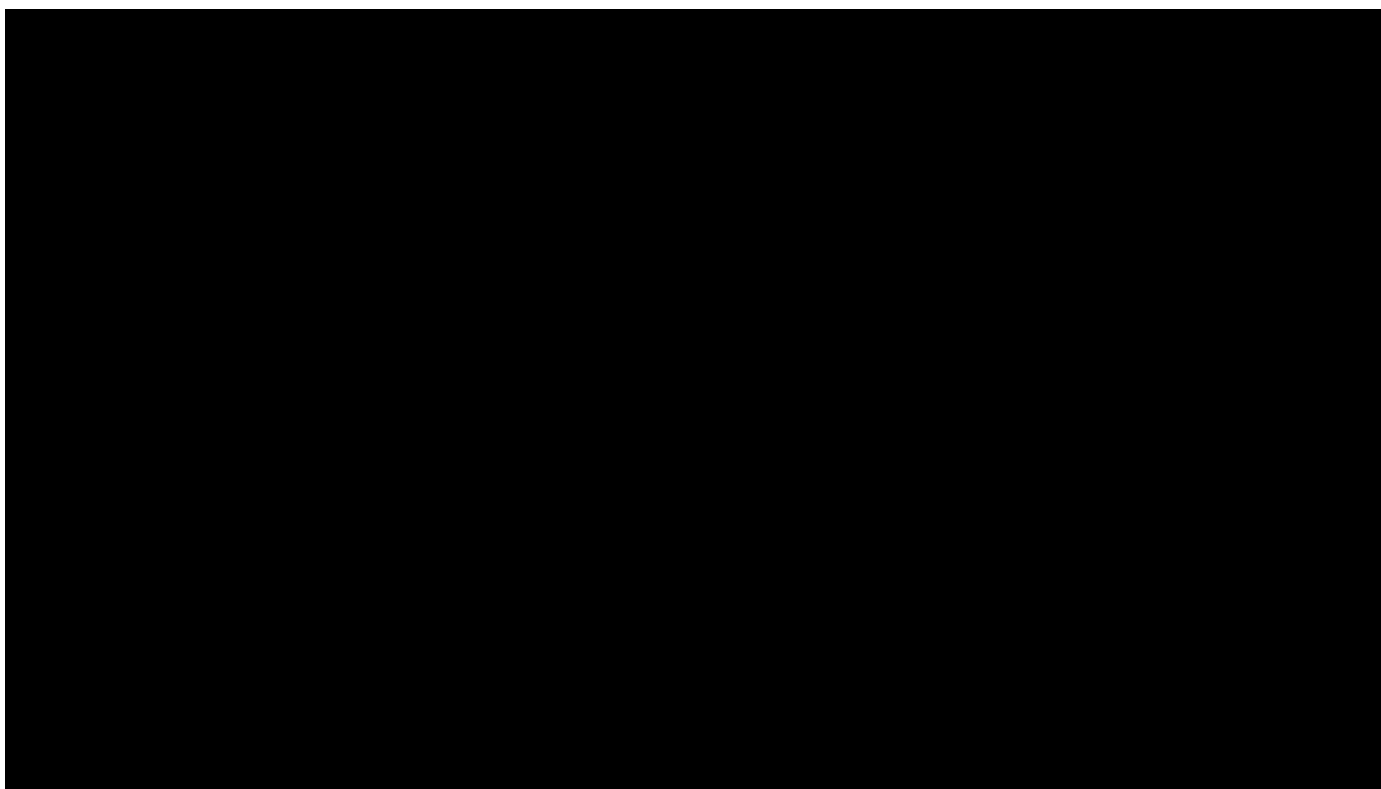
$$F(s) = \int_0^{\infty} f(t)e^{-st} dt$$

First Derivative	$\frac{df(t)}{dt} \xrightarrow{L} sF(s) - f(0^-)$
Second Derivative	$\frac{d^2 f(t)}{dt^2} \xrightarrow{L} s^2 F(s) - sf(0^-) - \dot{f}(0^-)$

Common Laplace Transform Pairs

Time Domain Function		Laplace Domain Function
Name	Definition*	
Unit Impulse	$\delta(t)$	1
Unit Step	$\gamma(t)^\dagger$	$\frac{1}{s}$
Unit Ramp	t	$\frac{1}{s^2}$
Parabola	t^2	$\frac{2}{s^3}$
Exponential	e^{-at}	$\frac{1}{s+a}$
Asymptotic Exponential	$\frac{1}{a}(1 - e^{-at})$	$\frac{1}{s(s+a)}$
Dual Exponential	$\frac{1}{b-a}(e^{-at} - e^{-bt})$	$\frac{1}{(s+a)(s+b)}$
Asymptotic Dual Exponential	$\frac{1}{ab}\left[1 + \frac{1}{a-b}(be^{-at} - ae^{-bt})\right]$	$\frac{1}{s(s+a)(s+b)}$
Time multiplied Exponential	te^{-at}	$\frac{1}{(s+a)^2}$
Sine	$\sin(\omega_0 t)$	$\frac{\omega_0}{s^2 + \omega_0^2}$
Cosine	$\cos(\omega_0 t)$	$\frac{s}{s^2 + \omega_0^2}$
Decaying Sine	$e^{-at} \sin(\omega_0 t)$	$\frac{\omega_0}{(s+a)^2 + \omega_0^2}$
Decaying Cosine	$e^{-at} \cos(\omega_0 t)$	$\frac{s+a}{(s+a)^2 + \omega_0^2}$
Generic Oscillatory Decay	$e^{-at}\left[B\cos(\omega_0 t) + \frac{C-aB}{\omega_0}\sin(\omega_0 t)\right]$	$\frac{Bs+C}{(s+a)^2 + \omega_0^2}$
Prototype Second Order Lowpass, underdamped	$\frac{\omega_0}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_0 t}\sin(\omega_0\sqrt{1-\zeta^2}t)$	$\frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$
Prototype Second Order Lowpass, underdamped Step Response	$1 - \frac{1}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_0 t}\sin(\omega_0\sqrt{1-\zeta^2}t + \phi)$ $\phi = \tan^{-1}\left(\frac{\sqrt{1-\zeta^2}}{\zeta}\right)$	$\frac{\omega_0^2}{s(s^2 + 2\zeta\omega_0 s + \omega_0^2)}$

Transfer Function

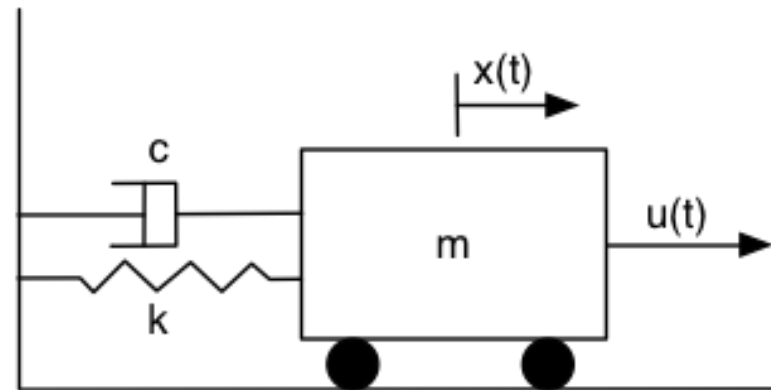


Transfer Function

- Transfer function ignore initial conditions and represent the system response with zero initial conditions
- Transfer function can be cascaded into block diagram form and multiplied to represent complex systems

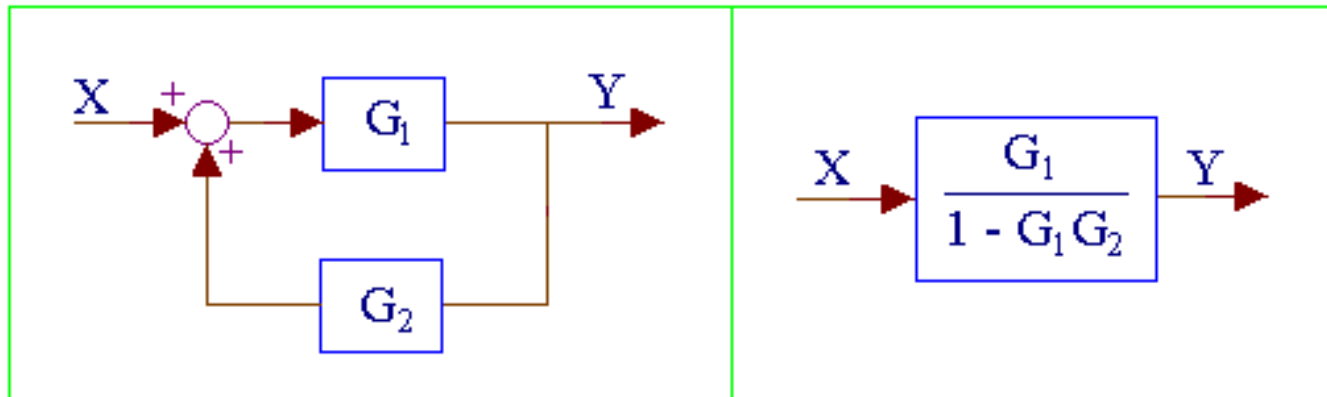
$$m\ddot{x} + c\dot{x} + kx = u$$

$$\frac{X(s)}{U(s)} = \frac{1}{ms^2 + cs + k}$$



Block Diagram Representation

$$Y = G_1 X + G_2 G_1 Y = \frac{G_1}{1 - G_1 G_2} X$$

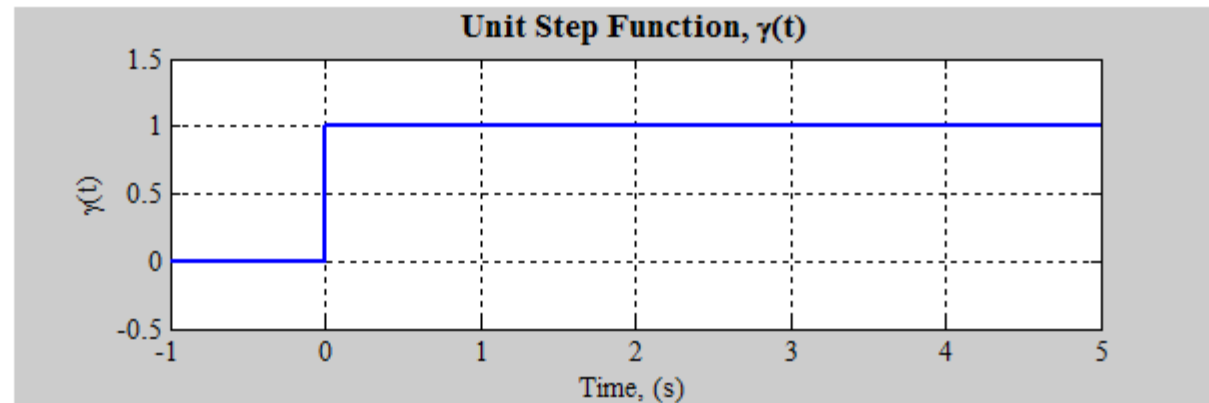


Step Response

- Definition: System response to a unit step function input with zero initial conditions

$$\gamma(t) = \begin{cases} 0, & t < 0 \\ 1, & t \geq 0 \end{cases}$$

$$\Gamma(s) = \frac{1}{s}$$



1st Order System Step Response Example

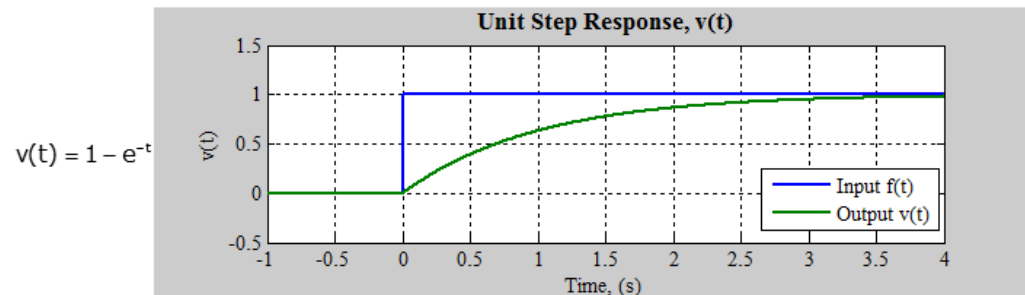
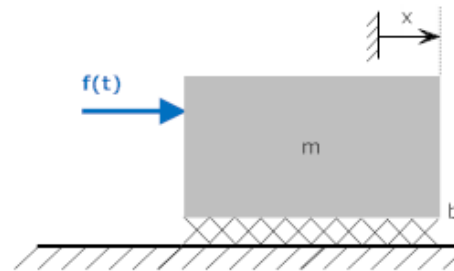
$$m\dot{v} + bv = f(t)$$

$$msV(s) + bV(s) = F(s)$$

$$\frac{V(s)}{F(s)} = H(s) = \frac{1}{ms + b} = \frac{1/m}{s + b/m}$$

$$V(s) = F(s)H(s) = \frac{1}{s} \frac{1/m}{s + b/m}$$

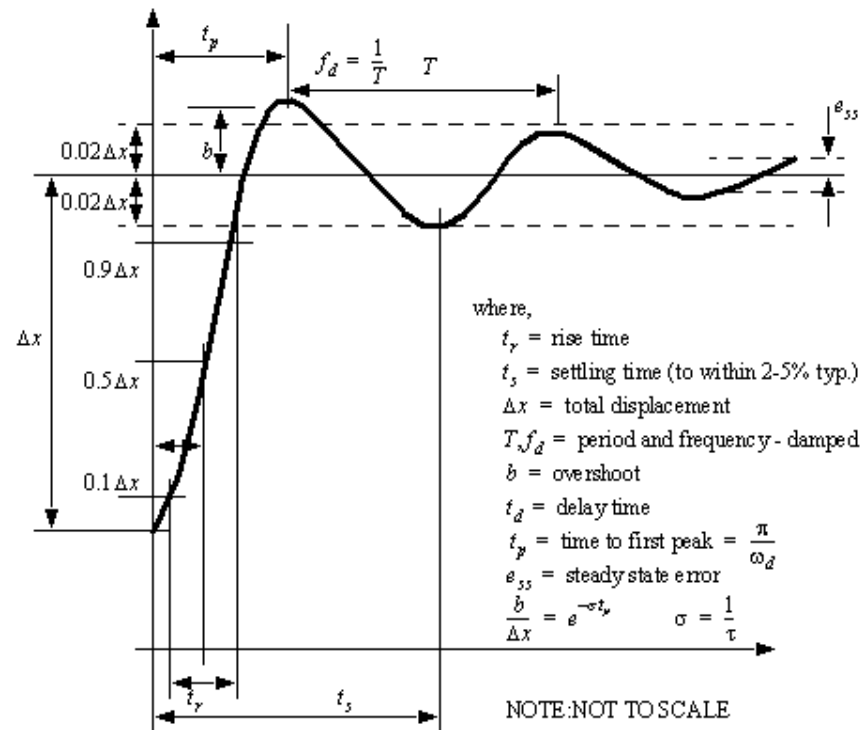
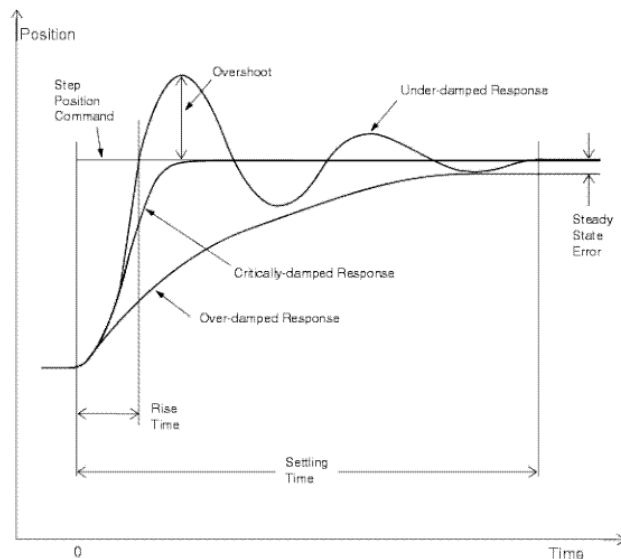
$$v(t) = \frac{1}{b} \left(1 - e^{-(b/m)t} \right)$$



2nd Order System Step Response Example

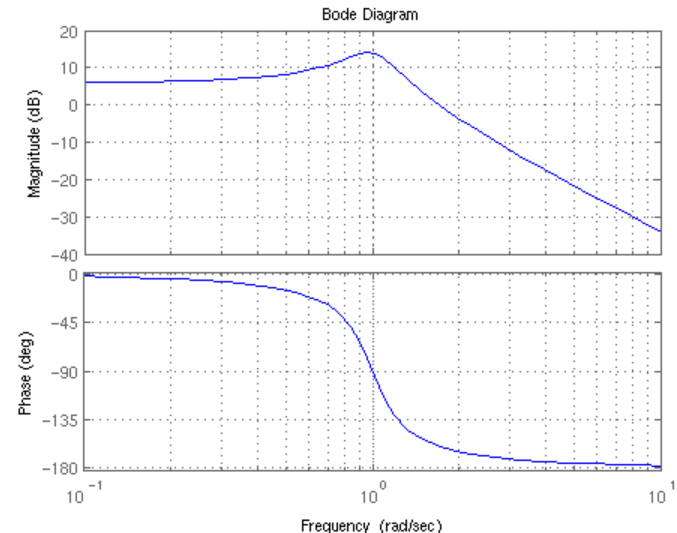
$$Y(s) = \frac{\omega_n^2}{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}$$

$$y(t) = \left[1 - \frac{1}{\sqrt{1-\zeta^2}} \exp(-\zeta\omega_n t) \sin\left(\omega_d t + \text{atan2}\left(\sqrt{1-\zeta^2}, \zeta\right)\right) \right] U_s(t)$$



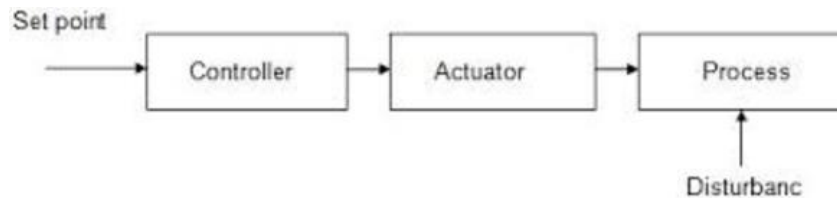
Frequency Response

- Definition: Frequency response characterize the output amplitude and phase with sinusoidal input
- Bode plot is used to give frequency response information
- Bode plot gain and phase can be calculated by substituting the s variable with $j\omega$ and compute the complex number amplitude and phase
- Bode plot plays an important role in classical control theory



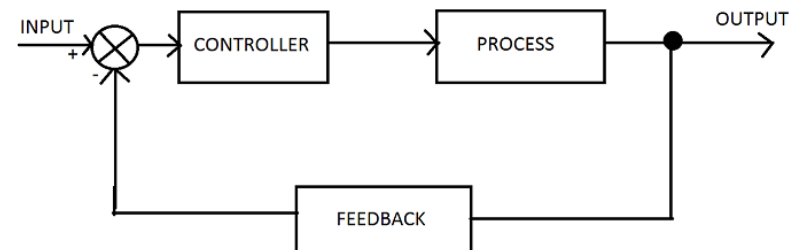
Closed Loop Control Overview

- Open loop controller utilize physical model of system
- Closed loop controller requires sensor to provide feedback signal
- Closed loop controller is more robust to external disturbance



Block Diagram of the Open Loop System

Open loop system



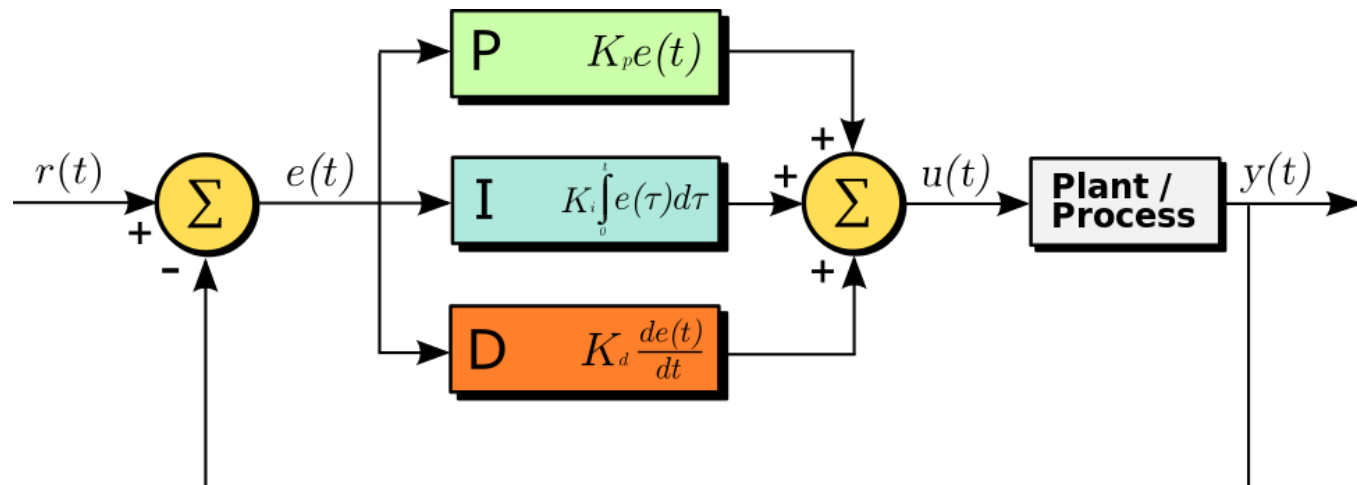
Closed loop system

Control Algorithm Overview

- Poles are roots of the denominator of the transfer function
- Zeros are roots of the numerator of the transfer function
- Closed loop control aims to stabilize the system and place the dominant poles at the desired location
- Common closed loop control tools go as the following
 - PID controller
 - Root-locus design
 - Loop shaping design and Nyquist plot
 - State space model
- Advanced control techniques
 - Adaptive control and learning
 - Robust control
 - Non-linear system control

PID Controller

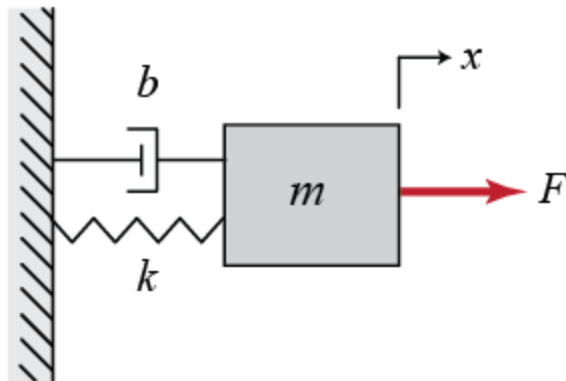
- Proportional, Integral and Derivative Controller



PID Controller

-
- When you are designing a PID controller for a given system, follow the steps shown below to obtain a desired response.
 - Obtain an open-loop response and determine what needs to be improved
 - Add a proportional control to improve the rise time
 - Add a derivative control to improve the overshoot
 - Add an integral control to eliminate the steady-state error
 - Adjust each of K_p , K_i , and K_d until you obtain a desired overall response. You can always refer to the table shown in this "PID Tutorial" page to find out which controller controls what characteristics.
 - Not all PID terms are necessary

PID Controller Design Example

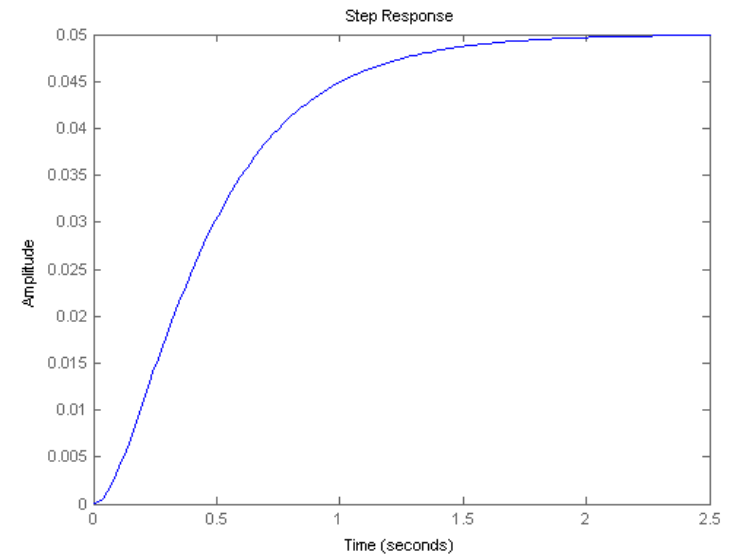


$$M\ddot{x} + b\dot{x} + kx = F$$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + bs + k}$$

$$\frac{X(s)}{F(s)} = \frac{1}{s^2 + 10s + 20}$$

$$\begin{aligned} M &= 1 \text{ kg} \\ b &= 10 \text{ N s/m} \\ k &= 20 \text{ N/m} \\ F &= 1 \text{ N} \end{aligned}$$



System Step Response

```
s = tf('s');
P = 1/(s^2 + 10*s + 20);
step(P)
```

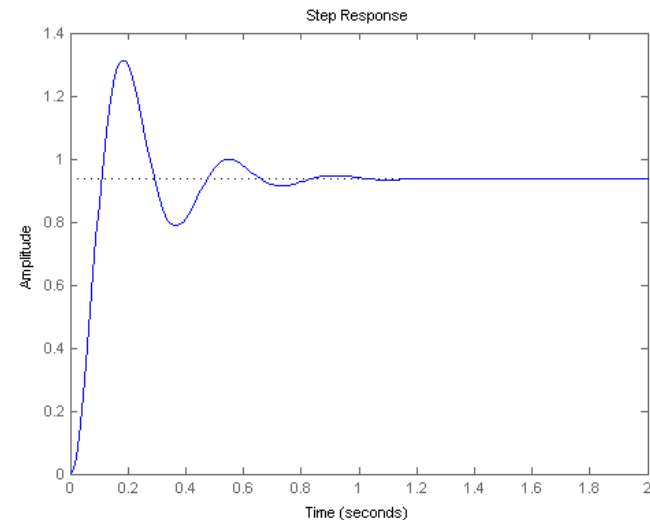

P Controller Example

$$\frac{X(s)}{F(s)} = \frac{K_p}{s^2 + 10s + (20 + K_p)}$$

- The proportional controller reduced both the rise time and the steady-state error, increased the overshoot, and decreased the settling time by small amount.

```
Kp = 300;
C = pid(Kp)
T = feedback(C*P,1)

t = 0:0.01:2;
step(T,t)
```



P Controller Step Response

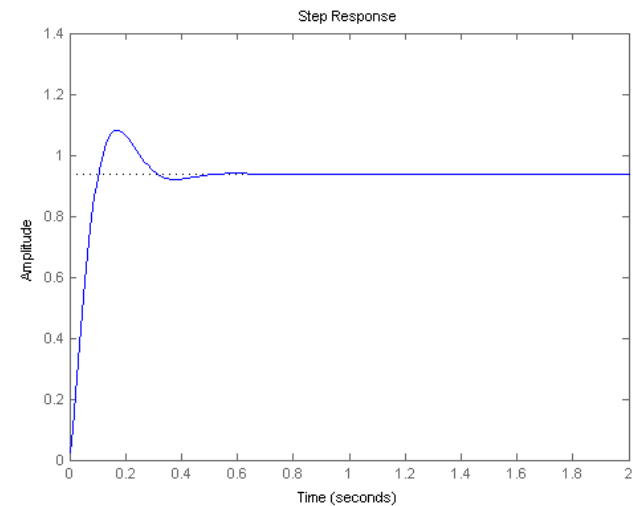
PD Controller Example

$$\frac{X(s)}{F(s)} = \frac{K_d s + K_p}{s^2 + (10 + K_d)s + (20 + K_p)}$$

- The derivative controller reduced both the overshoot and the settling time, and had a small effect on the rise time and the steady-state error.

```
Kp = 300;
Kd = 10;
C = pid(Kp,0,Kd)
T = feedback(C*P,1)

t = 0:0.01:2;
step(T,t)
```



PD Controller Step Response

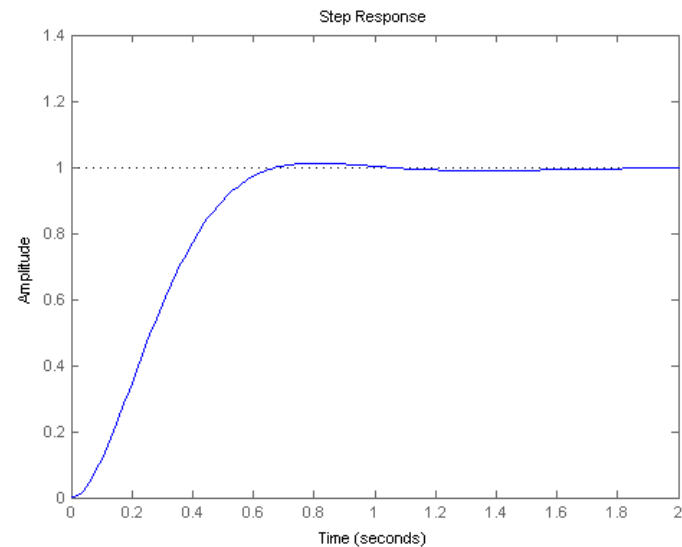
PI Controller Example

$$\frac{X(s)}{F(s)} = \frac{K_p s + K_i}{s^3 + 10s^2 + (20 + K_p s + K_i)}$$

- The derivative controller reduced both the overshoot and the settling time, and had a small effect on the rise time and the steady-state error.

```
Kp = 30;
Ki = 70;
C = pid(Kp,Ki)
T = feedback(C*P,1)

t = 0:0.01:2;
step(T,t)
```



PI Controller Step Response

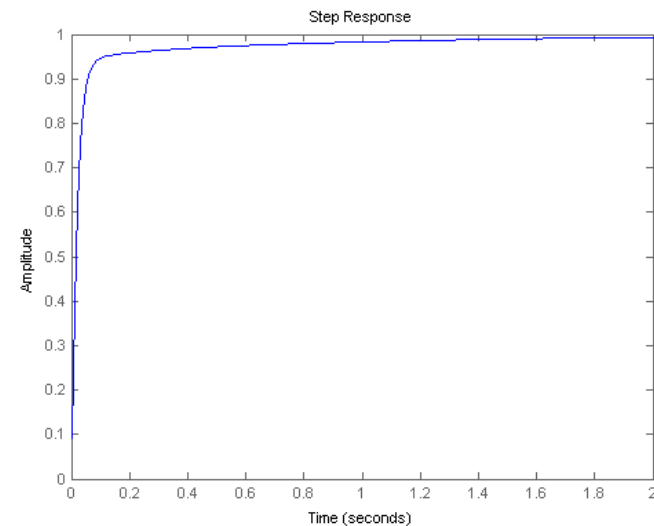
PID Controller Example

$$\frac{X(s)}{F(s)} = \frac{K_d s^2 + K_p s + K_i}{s^3 + (10 + K_d)s^2 + (20 + K_p)s + K_i}$$

- We have obtained a closed-loop system with no overshoot, fast rise time, and no steady-state error.

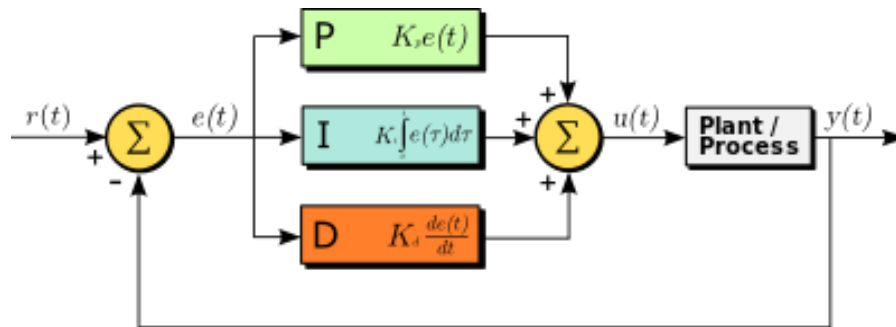
```
Kp = 350;
Ki = 300;
Kd = 50;
C = pid(Kp,Ki,Kd)
T = feedback(C*P,1);

t = 0:0.01:2;
step(T,t)
```

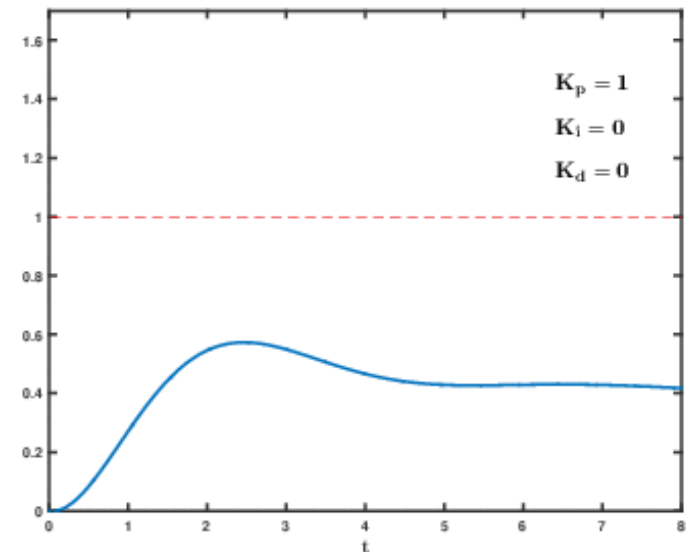


PID Controller Step Response

PID Controller Summary

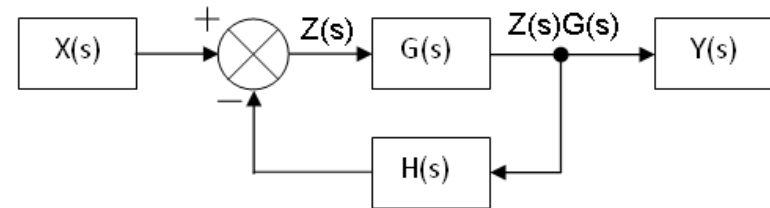


Parameter	Rise time	Overshoot	Settling time	Steady-state error	Stability
K_p	Decrease	Increase	Small change	Decrease	Degrade
K_i	Decrease	Increase	Increase	Eliminate	Degrade
K_d	Minor change	Decrease	Decrease	No effect in theory	Improve if K_d small



Loop Shaping Design

- Closed loop transfer function can be derived directly from block diagram
- Loop transfer function is different from closed loop transfer function as it just captures the feedback loop (in this case $G(s)H(s)$ is the loop transfer function)



Using this figure we write:

$$Y(s) = Z(s)G(s)$$

$$Z(s) = X(s) - Y(s)H(s)$$

$$X(s) = Z(s) + Y(s)H(s)$$

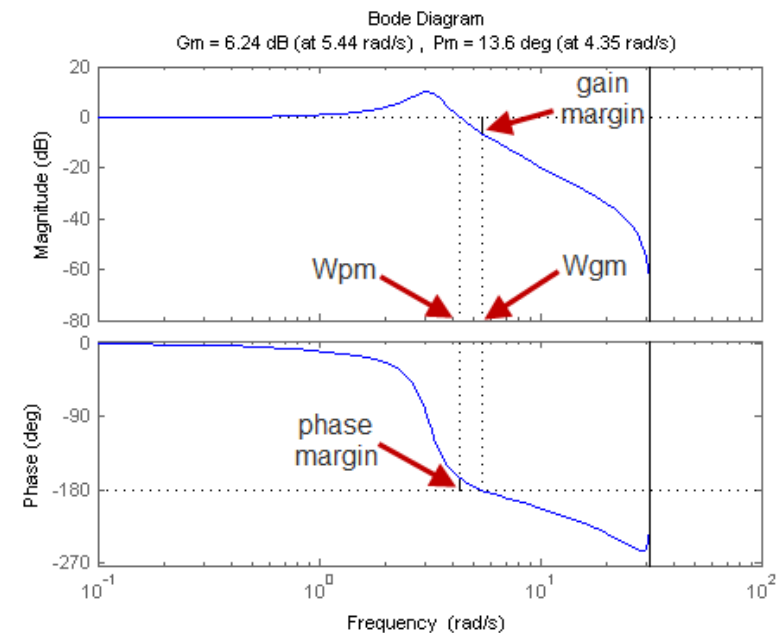
$$X(s) = Z(s) + Z(s)G(s)H(s)$$

$$\Rightarrow \frac{Y(s)}{X(s)} = \frac{Z(s)G(s)}{Z(s) + Z(s)G(s)H(s)}$$

$$\frac{Y(s)}{X(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

Loop Shaping Design

- Phase Margin and Gain Margin definition
- Design for target unit gain cross over frequency with reasonable phase margin (30 to 60 degree)
- Phase margin = 100 damping ratio approximately
- Closed loop system behavior related to loop transfer function



Phase Margin and Damping Ratio

- Loop transfer function

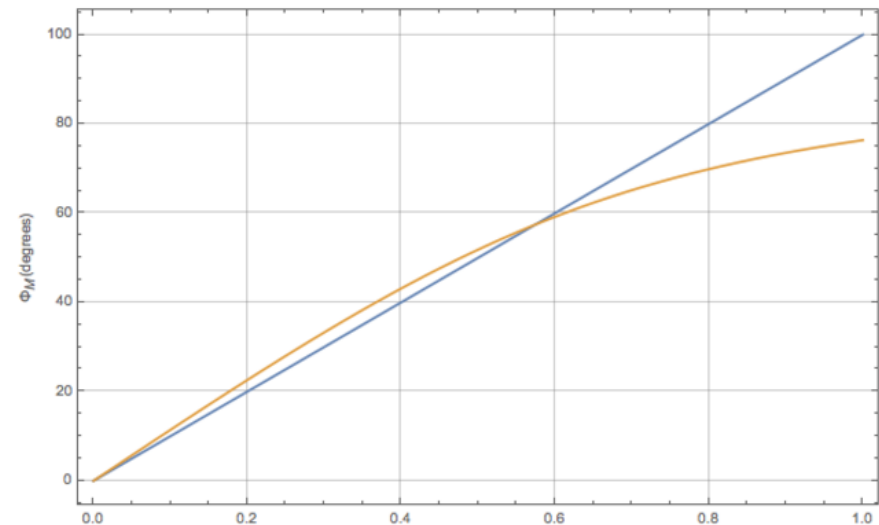
$$G(s) = \frac{\omega_n^2}{s(s+2\zeta\omega_n)}$$

- Closed loop transfer function

$$T(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

- Phase Margin

$$\begin{aligned}\Phi_M &= 90 - \tan^{-1} \frac{\sqrt{-2\zeta^2 + \sqrt{1+4\zeta^4}}}{2\zeta} \\ &= \tan^{-1} \frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{1+4\zeta^4}}}\end{aligned}$$



— 100ζ

— $\tan^{-1} \left(\frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{1+4\zeta^4}}} \right)$

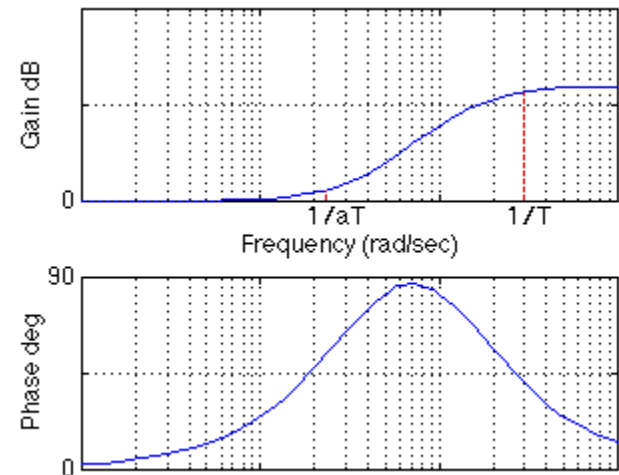
Lead Compensator

- Derivative term in PID controller is hard to implement and subject to noise
- A lead compensator is a good substitution for derivative control term
- Lead compensator helps to improve transient response

$$C(s) = \frac{1 + aTs}{1 + Ts}$$

$$\omega_m = \frac{1}{T\sqrt{a}}$$

$$\sin \phi = \frac{a - 1}{a + 1}$$



Lead Compensator Example

- Design a lead compensator to have the following character
 - Crossover frequency at 1000 rad/s
 - 55° phase lead

$$C(s) = \frac{1 + aTs}{1 + Ts}$$

$$\omega_m = \frac{1}{T\sqrt{a}}$$

$$\sin \phi = \frac{a - 1}{a + 1}$$

$$\phi_{max} = \sin^{-1}\left(\frac{\alpha - 1}{\alpha + 1}\right) = 55^\circ \text{ for } \alpha = 10$$

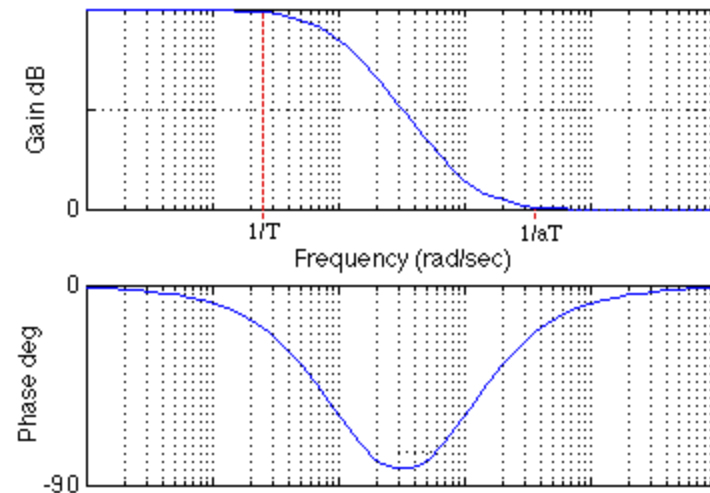
$$\omega_c = 1000 \quad \frac{1}{\sqrt{\alpha} \tau} = 1000 \Rightarrow \tau = \frac{1}{\sqrt{\alpha} \cdot 1000} \Rightarrow \boxed{\tau = 0.316 \text{ msec}}$$

Lag Compensator

- Lag compensator is similar to integral control and improves the steady state behavior of the system by reducing the steady state tracking error
- Not used as often as lead compensator since PI controller can in many case be implemented easily

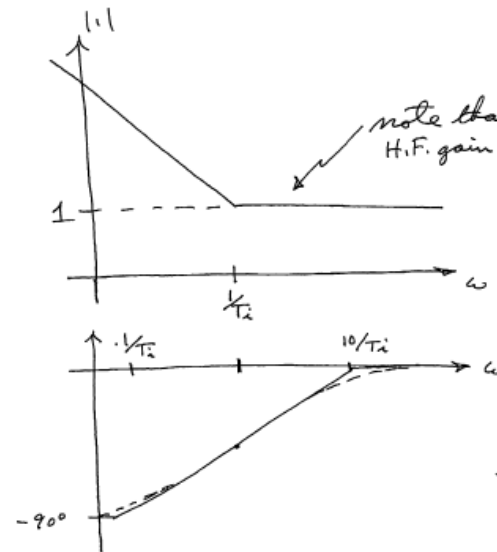
$$C(s) = \frac{1}{a} \left(\frac{1 + aTs}{1 + Ts} \right) \quad [a < 1]$$

$$\omega_m = \frac{1}{T\sqrt{a}}$$



Lag Compensator

lag compensator $\frac{T_i s + 1}{T_i s}$



Because we have lag
H.F. gain = 1,
 K is unchanged

$$\phi = -90^\circ + \tan^{-1} T_i \omega$$

need 80° at $\omega = \omega_c$
to only lose -10° in ϕ_m

$$\Rightarrow \tan^{-1} T_i \omega_c = 80^\circ$$

$$\Rightarrow T_i = \frac{1}{\omega_c} \cdot \tan 80^\circ = \frac{5.7}{\omega_c}$$

$$\Rightarrow \boxed{T_i = 5.7 \text{ msec}}$$

Conclusion

- Start with system physical model (differential equations)
- Linearize about operation point if needed (Taylor series)
- Convert to frequency domain (Laplace transformation)
- Obtain step response with overshoot and rise/settling time
- Draw Bode plot with phase and gain margin (replace s with $j\omega$)
- Draw closed loop control block diagram
- Specify desired system response parameter
- Apply PID control to obtain desired behavior
 - Use proportional control to decrease rise time
 - Use integral control to eliminate steady state error
 - Use derivative control to improve transient response (reduce overshoot)
- Do more detailed analysis with other control algorithm if needed

Homework Problem

- Design a PI controller with lead compensator to meet the specified requirement
- Use Matlab to simulate the system behavior and controller performance and record the plots



Thank You!