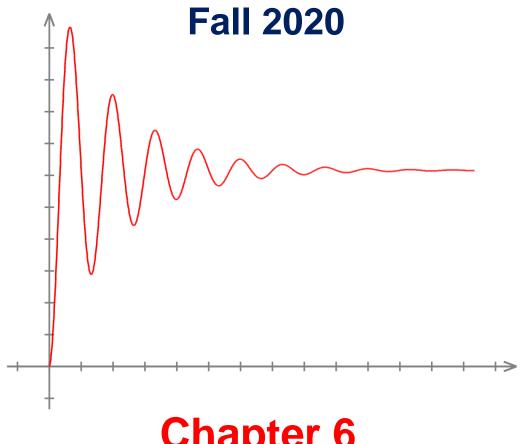
Department of Engineering

ENGR 311: System Dynamics



Chapter 6

Time Domain Analysis of Dynamic Systems

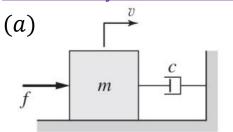
Outline

- Introduction
- Natural and forced response
- □ Transient-response analysis of first-order systems: Analytical and MATLAB
- □ Transient-response analysis of second-order systems: Analytical and MATLAB
- ☐ Transient-response analysis of higher-order systems: Analytical and MATLAB
- ☐ Solution of the state equation

First-order Systems

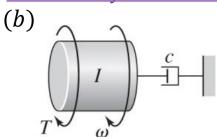
$$a_o \frac{dy}{dt} + a_1 y = bf(t)$$

Mechanical System: Translational



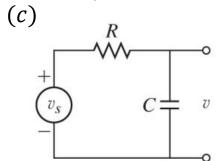
$$m\frac{dv}{dt} + cv = f$$
$$\tau = \frac{m}{c}$$

Mechanical System: Rotational



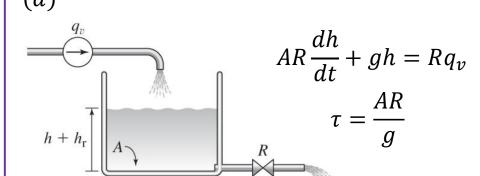
$$I\frac{d\omega}{dt} + c\omega = T$$
$$\tau = \frac{I}{c}$$

Electrical System

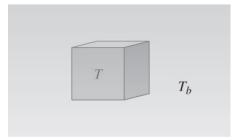


$$RC\frac{dv}{dt} + v = v_{s}$$
$$\tau = RC$$

Fluid System



Thermal System (e)



$$mc_{p}R\frac{dT}{dt} + T = T_{b}$$
$$\tau = mc_{p}R$$

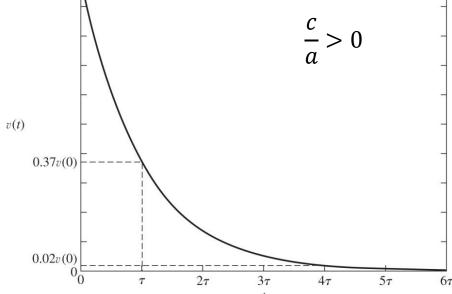
First-order Systems

$$a\frac{dv}{dt} + cv = f(t)$$

$$f(t) = 0$$

$$v(t) = v_{free}(t) = v(0)e^{-ct/a}$$

$$\frac{c}{a} > 0$$



$$c/a > 0$$
: stable $c/a < 0$: unstable $c/a = 0$: neutrally stable

 $f(t) \neq 0$ (e.g., f(t) is step with magnitude F) $v(t) = v_{free}(t) + v_{forced}(t)$ $=v(0)e^{-ct/a}+\frac{F}{c}(1-e^{-ct/a})$ $0.63\frac{F}{a}$ Slope = $\frac{F/c}{\tau}$ $v_{transient}(t) = \left[v(0) - \frac{F}{c}\right]e^{-t/\tau}$ $v_{steady-state}(t) = \frac{F}{c}$ K = 1/c $v(\infty) = v_{ss} = f_{ss}/c = F/c = FK$

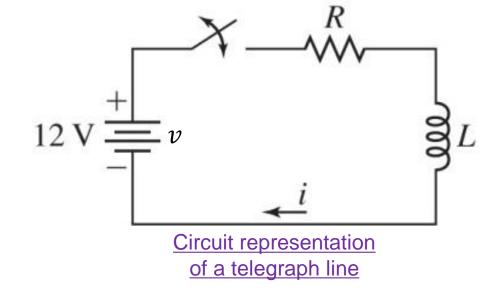
S. K. Armah (PgCAP, Ph.D.)

Example 1

The Figure shows a circuit representation of a telegraph line. The resistance R is the line resistance and L is the inductance of the solenoid that activates the receiver's clicker. The switch represents the operator's key. v(t) represents the input voltage and i(t) is the current passing through the solenoid. Given the model of the system as

$$L\frac{di}{dt} + Ri = v(t)$$

- (a) Determine:
 - the time constant
 - ii. Steady state current
 - iii. the DC gain
 - iv. the transfer function I(s)/V(s)
 - v. state-space model



(b) Assume that when sending a "dot," the key is closed for 0.1 s. Using the values $R = 20 \Omega$ and L = 4 H, obtain the expression for the current i(t) passing through the solenoid. What is the value for i(0+) and $i(\infty)$?

Example 2

Hardness and other properties of metal can be improved by the rapid cooling that occurs during *quenching*, a process in which a heated object is placed into a liquid bath (see the Figures). Consider a lead cube with a side length of d=20 mm. The cube is immersed in an oil bath for which the convection coefficient $h = 200 \,\mathrm{W/}$ (m. °C). The oil temperature is T_b . The density of lead is $1.134 \times 10^4 \text{ kg/m}^3$. Take the specific heat of lead to be $c_p = 129 \, \text{J/kg}$. °C. The model of the cube's temperature as a function of the liquid temperature T_b , which is assumed to be known, is given as:

$$C\frac{dT}{dt} = -\frac{1}{R}(T - T_b), \qquad T > T_b$$

Thermal capacitance: $C = mc_p = \rho V c_p$
 dT

Thermal resistance: $R = \frac{1}{hA}$

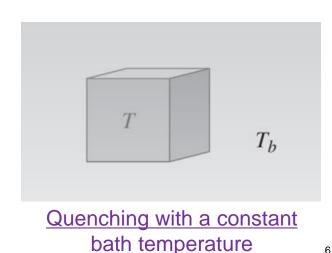
(a) Show that the model can be written as: $24.4\frac{dT}{dt} + T = T_b$

(b) Hence, estimate the time the cube's temperature will

reach T_b



Quenching Process S. K. Armah (PgCAP, Ph.D.)



Second-order Systems

Undamped Response: $\zeta = 0$ (c = 0)

$$a\ddot{x} + bx = f(t)$$

$$a\ddot{x} + bx = f(t)$$
 or $\ddot{x} + \omega_n^2 x = \frac{1}{a}f(t)$

(a)
$$m\frac{d^2x}{dt^2} + kx$$

$$\omega_n = \sqrt{\frac{k}{m}}$$

$$L\frac{d^2\theta}{dt^2} + g\theta = 0$$
$$\omega_n = \sqrt{\frac{g}{L}}$$

$$\begin{pmatrix} c \\ v_s \end{pmatrix} \qquad C \qquad v$$

(b)

$$LC\frac{d^2v}{dt^2} + v = v_s$$

$$\omega_n = \frac{1}{\sqrt{LC}}$$

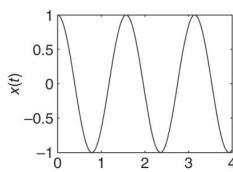
$$m\frac{d^2x}{dt^2} + kx = f(t)$$
 $\omega_n = \sqrt{\frac{b}{a}}$ $f = \frac{1}{2\pi}\sqrt{\frac{b}{a}}$ $T = 2\pi\sqrt{\frac{a}{b}}$

$$x(t) = \frac{\dot{x}(0)}{\omega_n} \sin \omega_n t + x(0) \cos \omega_n t$$

$$x(t) = A\sin(\omega_n t + \emptyset)$$

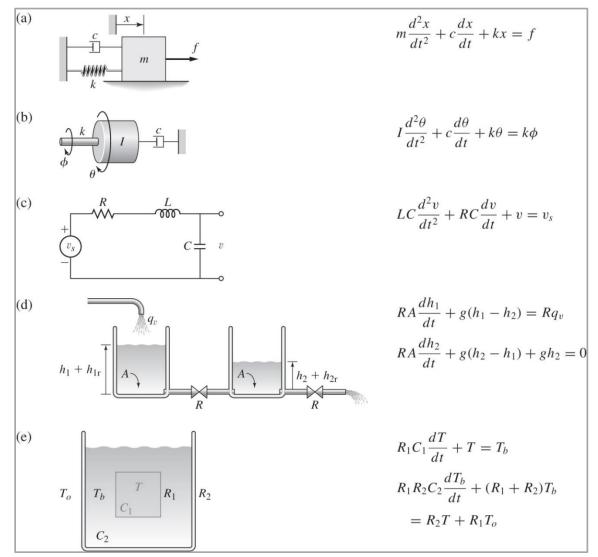
$$A = \sqrt{[x(0)]^2 + \left[\frac{\dot{x}(0)}{\omega_n}\right]^2} \qquad \sin \emptyset = \frac{x(0)}{A}$$

 $\cos\emptyset = \frac{\dot{x}(0)}{4\omega}$ The amplitude and phase angle depends on initial conditions



Second-order Systems

Response with damping: $\zeta \neq 0$ ($c \neq 0$)



$$a\ddot{x} + c\dot{x} + bx = f(t)$$

$$\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = \frac{1}{a}f(t)$$

$$as^{2} + cs + b = 0$$
$$s^{2} + 2\zeta\omega_{n}s + \omega_{n}^{2} = 0$$

$$s = \frac{-c \pm \sqrt{c^2 - 4ab}}{2a}$$

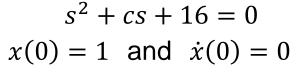
$$s = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

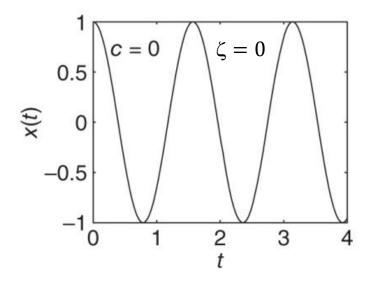
$$\zeta = \frac{c}{c_c} = \frac{c}{2\sqrt{ab}}$$

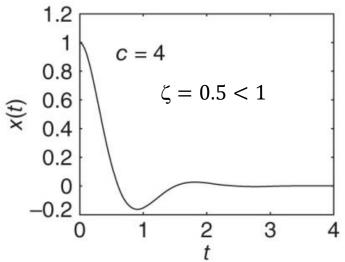
 ζ : Damping ratio/factor c: actual damping value c_c/c_o : critical damping value

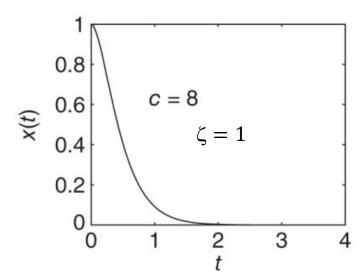
Second-order Systems

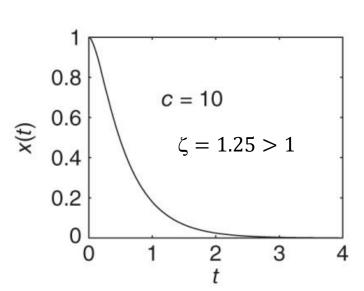
Response with damping: $\zeta \neq 0$ ($c \neq 0$)











Second-order Systems

$$s = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

Response with damping: $\zeta \neq 0$ ($c \neq 0$)

$$c < c_c$$

$$a\ddot{x} + c\dot{x} + bx = 0$$

Underdamped Response

$$0 < \zeta < 1$$

$$\frac{Initial\ conditions}{x(0)\ and\ \dot{x}(0)}$$

$$X(s) = \frac{(s + 2\zeta\omega_n)x(0) + \dot{x}(0)}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$x(t) = e^{-\zeta \omega_n t} \left\{ \left[\frac{\zeta}{\sqrt{1 - \zeta^2}} x(0) + \frac{1}{\omega_d} \dot{x}(0) \right] \sin \omega_d t + x(0) \cos \omega_d t \right\} \quad s = -\zeta \omega_n \pm \omega_d j$$

$$s = -\alpha \pm \omega_d j$$

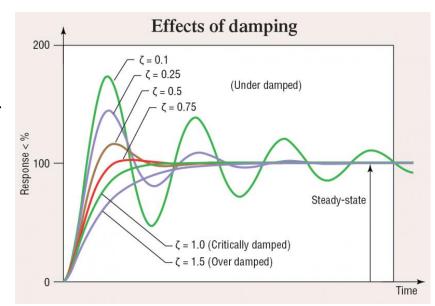
$$x(t) = e^{-\zeta \omega_n t} A \sin(\omega_d t + \emptyset)$$
 $0 \le \zeta < 1$

$$0 \le \zeta < 1$$

$$A = \frac{1}{\omega_d} \sqrt{[\omega_d x(0)]^2 + [\dot{x}(0) + \zeta \omega_n x(0)]^2}$$

$$\sin\emptyset = \frac{x(0)}{A}$$

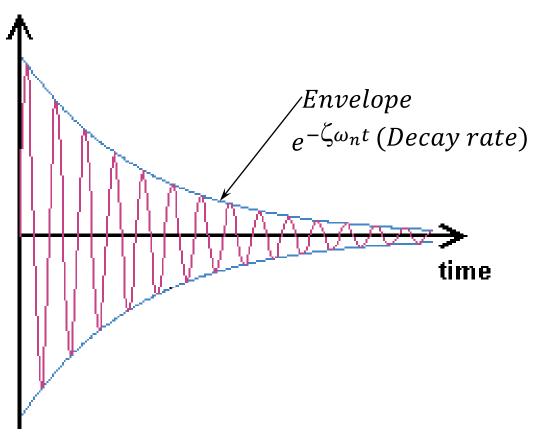
or
$$\cos \emptyset = \frac{\dot{x}(0) + \zeta \omega_n x(0)}{A \zeta \omega_n}$$



Second-order Systems

<u>Underdamped Response</u>

$$c < c_c$$
 or $\zeta < 1$ $s = -\zeta \omega_n \pm \omega_d j$ $x(t) = e^{-\zeta \omega_n t} A \sin(\omega_d t + \emptyset)$



Second-order Systems

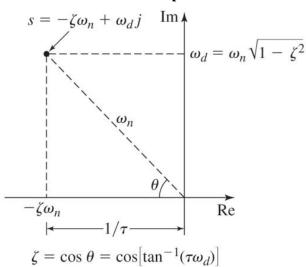
Effect of Root Location: Graphical Interpretation

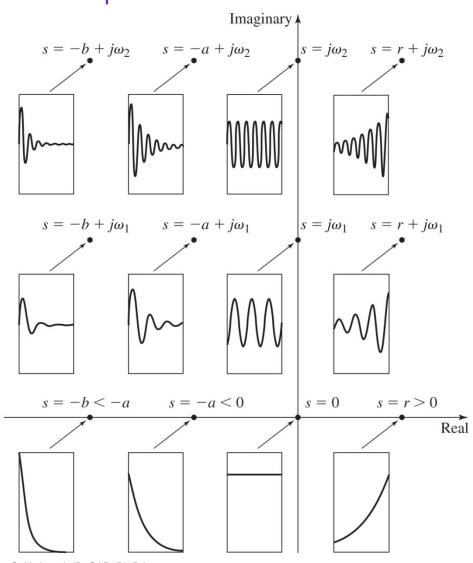
$$as^{2} + cs + b = 0$$
$$s^{2} + 2\zeta\omega_{n}s + \omega_{n}^{2} = 0$$

$$s = \frac{-c \pm \sqrt{c^2 - 4ab}}{2a}$$

$$s = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

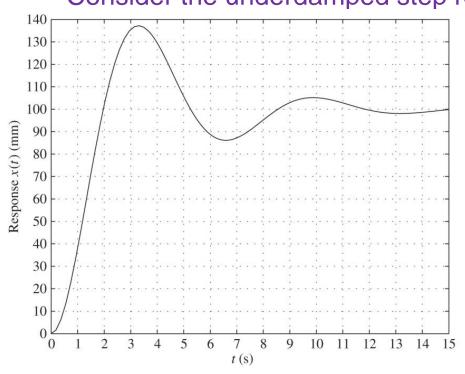
<u>Underdamped</u>

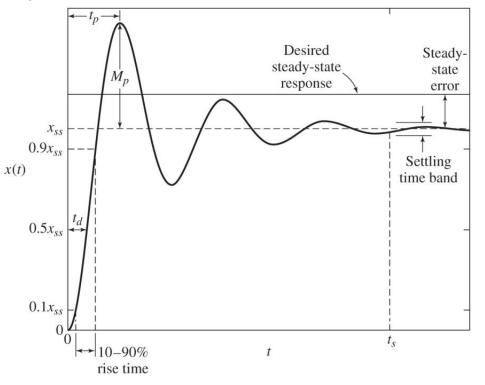




Second-order Systems

Consider the underdamped step response





- Maximum or peak overshoot, M_p
- Percent maximum overshoot, P.O or $M_{\%}$
- Peak value, x_p or x_{max}
- Peak time, t_p
- Rise time, t_r

- Settling time, t_s
- Delay time, t_d
- Steady state value, x_{ss}
- Steady state error, e_{ss}

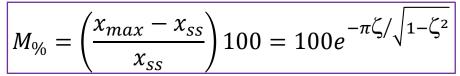
Second-order Systems

- Maximum or peak overshoot, M_p
 - When a signal or function exceeds its target. It is often associated with <u>ringing</u>.

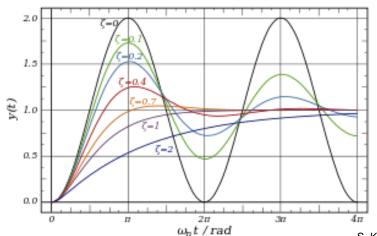
$$M_p = x_{max} - x_{ss}$$

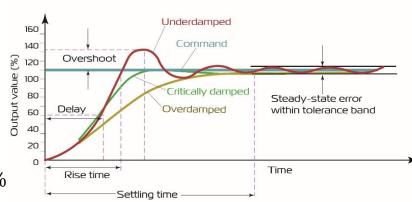
$$M_p = x_p - x_{ss}$$

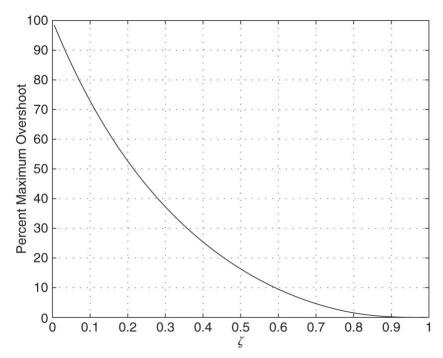
Percent maximum overshoot, P. O or M_%



$$\zeta = \frac{R}{\sqrt{\pi^2 + R^2}} \qquad R = \ln\left(\frac{100}{M_{\%}}\right)$$



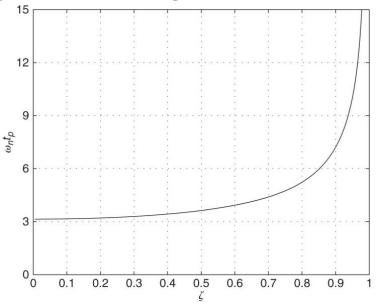




Second-order Systems

- Peak time, t_p
 - Time required for the response to reach the first peak of the overshoot.

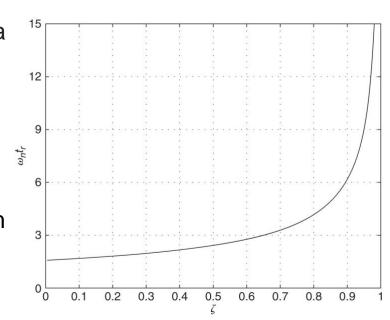
$$t_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = \frac{\pi}{\omega_d}$$



- Rise time, t_r
 - Time required for a signal to change from a specified low value to a specified high value.

$$t_r = \frac{2\pi - \emptyset}{\omega_n \sqrt{1 - \zeta^2}} \quad \emptyset = \tan^{-1} \left(\frac{\sqrt{1 - \zeta^2}}{\zeta}\right) + \pi$$

 This is for 100% rise time. No closed form expression exists for the 10%-90% rise time.



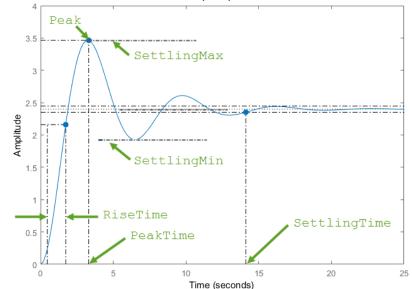
Second-order Systems

- Settling time, t_s
 - Time elapsed from the application of an ideal instantaneous step input to the time at which the output has entered and remained within a specified error band.

$$t_{s} = \frac{4}{\zeta \omega_{n}}$$

$$\tau = \frac{1}{\zeta \omega_n}$$

$$t_s = 4\tau$$



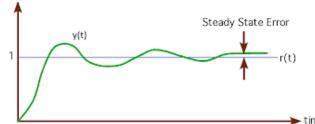
- Delay time, t_d
 - The delay time is the time required for the response to reach half the final value the very first time.

$$t_d \approx \frac{1 + 0.7\zeta}{\omega_n}$$

- Steady-state error, e_{ss}
 - The difference between the desired final output and the actual one when the system reaches a steady state, when its behavior may be expected to continue if the system is undisturbed.

$$e_{ss} = x_{desired} - x_{ss}$$

$$e_{ss} = x_{reference} - x_{ss}$$



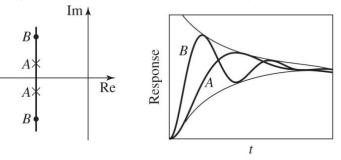
Second-order Systems

$$s = -\zeta \omega_n \pm \omega_d j$$

Effect of Root Location: Graphical Interpretation

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

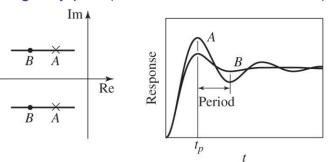
Models A and B have the same real part (on the same vertical line), the same time constant, and the same decay time.



$$\tau = \frac{1}{\zeta \omega_n} \qquad t_s = 4\tau = \frac{4}{\zeta \omega_n}$$

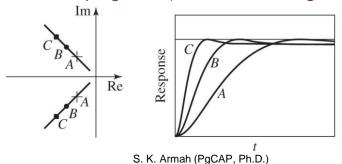
$$Decay\ rate: e^{-\zeta \omega_n t}$$

Models A and B have the same imaginary part (on the same horizontal line), the same period, and same peak time.



$$t_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = \frac{\pi}{\omega_d}$$

Models A, B and C have same damping ratio (on the same diagonal/radial line) and same overshoot.



$$M_{\%} = 100e^{\frac{-\pi\zeta}{\sqrt{1-\zeta^2}}}$$

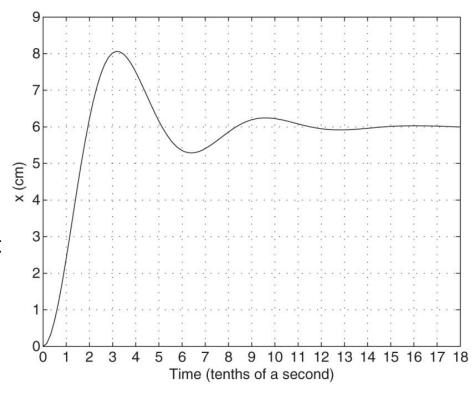
Example 3

The Figure shows the response of a forced spring-mass-damper system to a step input of magnitude $6 \times 10^3 N$.

$$m\ddot{x} + c\dot{x} + kx = f(t)$$

Determine or estimate:

- (a) the peak value
- (b) the peak time
- (c) steady state value
- (d) k
- (e) the maximum percentage overshoot
- (f) the damping ratio
- (g) damped natural frequency
- (h) undamped natural frequency
- (i) m and c



Example 4

The Figure shows the response of an electrical system subjected to a step input voltage of 10 V.

$$LC\frac{d^2v}{dt^2} + RC\frac{dv}{dt} + v = v_s$$
 $R = 400 \Omega$, $C = 20 \mu\text{F}$, $L = 4 \text{ H}$

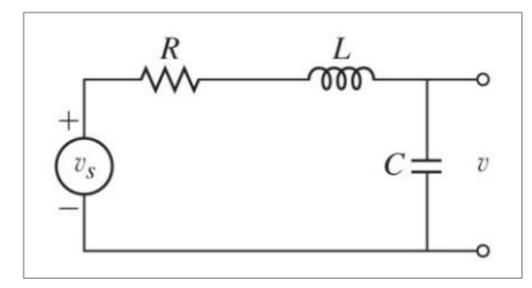
$$R = 400 \Omega$$
,

$$C = 20 \, \mu F$$

$$L = 4 H$$

Determine or estimate the:

- (a) peak value
- peak time (b)
- steady state value (c)
- (d) steady state error
- (e) overshoot
- (f) maximum percentage overshoot
- rise time (g)
- (h) settling time
- delay time (i)
- damping ratio (j)
- damped natural frequency (k)
- **(I)** undamped natural frequency
- R and C, given L = 4 H (m)



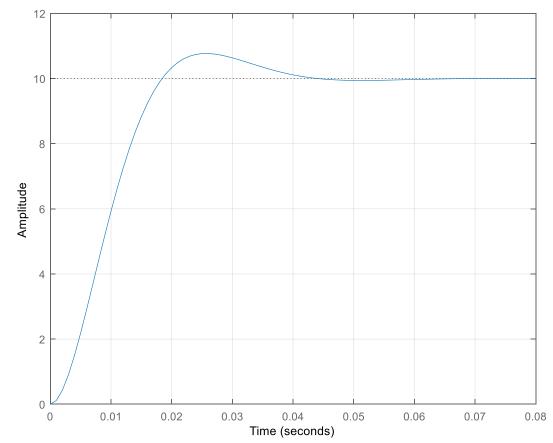
Example 4

The Figure shows the response of an electrical system to a step input

voltage of 10 V.

$$LC\frac{d^2v}{dt^2} + RC\frac{dv}{dt} + v = v_S$$

$$\frac{V(s)}{V_s(s)} = \frac{\frac{1}{LC}}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$



$$R = 400 \,\Omega, \qquad C = 20 \,\mu\text{F}, \qquad L = 4 \,\text{H}$$

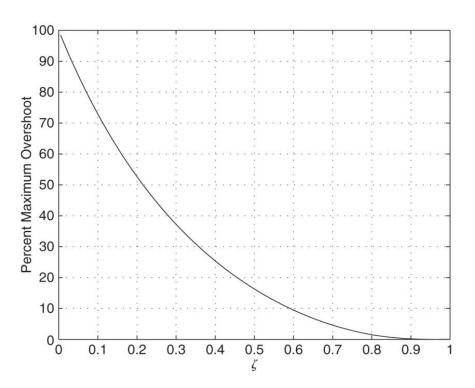
$$C = 20 \, \mu \text{F}$$

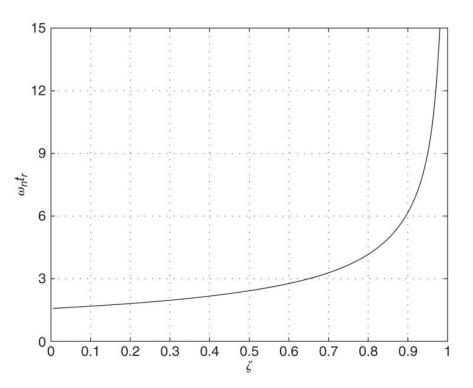
$$L = 4 H$$

Example 5

Compute the maximum percent overshoot, the maximum overshoot, the peak time, the 100% rise time, the delay time, and the 2% settling time for the following model. The initial conditions are zero. Time is measured in seconds.

$$\ddot{x} + 4\dot{x} + 8x = 2u_s(t)$$





Example 6

In the Figure shown, assume that m=1 kg, c=2 N-s/m, and k=100 N/m. The mass is displaced 0.05 m and released without initial velocity. The displacement x is measured from the equilibrium position. Find the frequency observed in the vibration. Hence, find the analytical solution for x(t).

$$X(s) = \frac{(s + 2\zeta\omega_n)x(0) + \dot{x}(0)}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$x(t) = e^{-\zeta \omega_n t} \left\{ \left[\frac{\zeta}{\sqrt{1 - \zeta^2}} x(0) + \frac{1}{\omega_d} \dot{x}(0) \right] \sin \omega_d t + x(0) \cos \omega_d t \right\}$$

$$x(t) = e^{-\zeta \omega_n t} A \sin(\omega_d t + \emptyset) \qquad A = \frac{1}{\omega_d} \sqrt{[\omega_d x(0)]^2 + [\dot{x}(0) + \zeta \omega_n x(0)]^2}$$

$$\sin \emptyset = \frac{x(0)}{A}$$
 or $\cos \emptyset = \frac{\dot{x}(0) + \zeta \omega_n x(0)}{A \zeta \omega_n}$

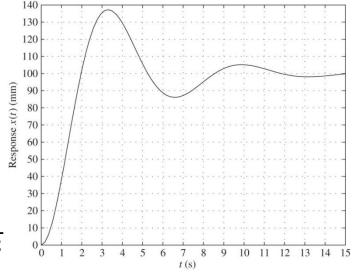
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Second-order Systems

- Experimental determination of Damping ratio, ζ
 - Usually the damping coefficient c is the parameter most difficult to estimate.
 - Logarithmic decrement δ provides a good way to estimate the damping ratio ζ , from which we can compute c ($c = 2\zeta\sqrt{mk}$)..
 - For underdamped system

$$s = -\zeta \omega_n \pm \omega_d j, \qquad \omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$x(t) = Be^{-\zeta\omega_n t} \sin(\omega_d t + \emptyset)$$



$$T = \frac{2\pi}{\omega_d}$$

$$\delta = \ln\left(\frac{x(t)}{x(t+T)}\right) = \ln\left(\frac{Be^{-\zeta\omega_n t}\sin(\omega_d t + \emptyset)}{Be^{-\zeta\omega_n (t+T)}\sin(\omega_d t + \omega_d T + \emptyset)}\right) = \ln e^{\zeta\omega_n T} = \zeta\omega_n T$$

Ratio of two successive amplitudes

$$\zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}}$$

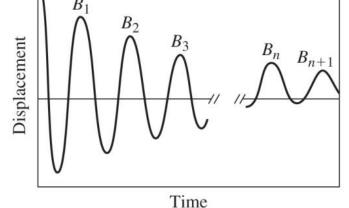
$$\zeta = \frac{\delta}{\sqrt{(2\pi)^2 + \delta^2}}$$

Second-order Systems

- Experimental determination of Damping ratio, ζ
 - The plot of x(t) will contain some measurement error, and for this reason, the preceding method is usually modified to use measurement of two peaks n cycles apart.

$$\ln\left(\frac{B_1}{B_2} \frac{B_2}{B_3} \frac{B_3}{B_4} \dots \frac{B_n}{B_{n+1}}\right) = \ln\left(\frac{B_1}{B_{n+1}}\right)$$

$$\ln\left(\frac{B_1}{B_2}\right) + \ln\left(\frac{B_2}{B_3}\right) + \ln\left(\frac{B_3}{B_4}\right) + \dots + \ln\left(\frac{B_n}{B_{n+1}}\right) = \ln\left(\frac{B_1}{B_{n+1}}\right)$$



$$\delta + \delta + \delta + \dots + \delta = n\delta = \ln\left(\frac{B_1}{B_{n+1}}\right)$$

$$\delta = \frac{1}{n} \ln \left(\frac{B_1}{B_{n+1}} \right)$$

$$\delta = \frac{1}{n} \ln \left(\frac{x_1}{x_{n+1}} \right)$$

 \circ We normally take the first peak to be B_1 , because this is the highest peak and least subject to measurement error, but this is not required. The formula applies to any two points n cycles apart.

Example 7

Measurement of the free response of a certain spring-mass-damper system whose mass is $500 \, \mathrm{kg}$ shows that after six cycles the amplitude of the displacement is 10% of the first amplitude. Also, the time for these six cycles to occur was measured to be $30 \, \mathrm{s}$. Estimate the system's damping c and stiffness k.

$$m\ddot{x} + c\dot{x} + kx = 0$$