

# 多孔介质污染迁移动力学

Contaminant Transport in Porous Media

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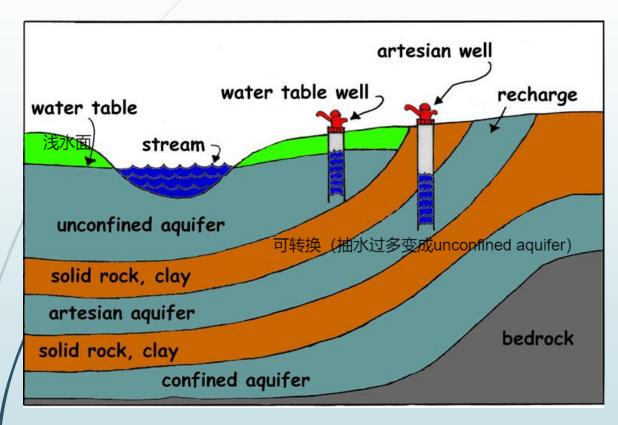
# Lecture 2

**■**1 Subsurface Hydrology

**≠**2 Review of Mathematics and Flow Equation

**■**3 Mass Transport in Saturated Media

## Subsurface Hydrology



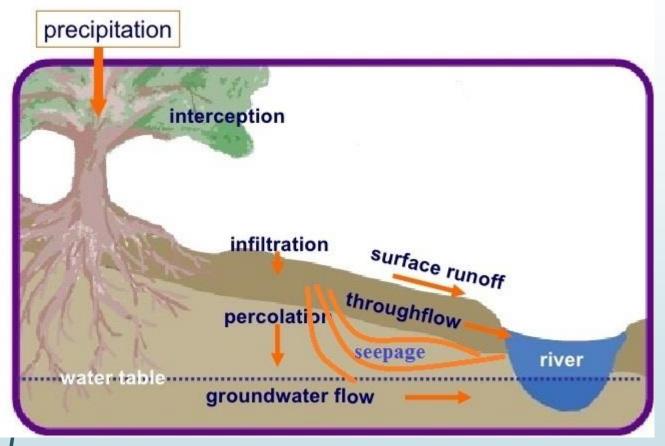
In a **sedimentary basin**, the saturated zone forms a **multiaquifer systems** containing relatively permeable **aquifers** separated by less permeable **confining layers** called **aquitards** or (if having very low permeability) **aquicludes**.

Water table aquifers (or portions thereof) are called **unconfined**.

Aquifers (or portions thereof) enclosed between less permeable strata are called **confined** or **artesian** (the latter term being sometimes reserved for aquifers at sufficiently high pressure for wells to flow spontaneously).

Though **confining beds** and the underlying **bedrock** are sometimes assumed to be impermeable, they are not. Both are sufficiently porous and/or fractured to allow through flow of water, albeit sometimes only locally and at low rates.

## Subsurface Hydrology



**Infiltration** = Rate of flow into unsaturated zone across **soil surface** 

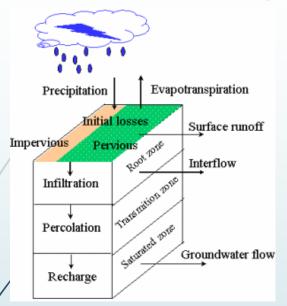
**Deep percolation (net infiltration)** = Rate of downward flow across **bottom of root zone** 

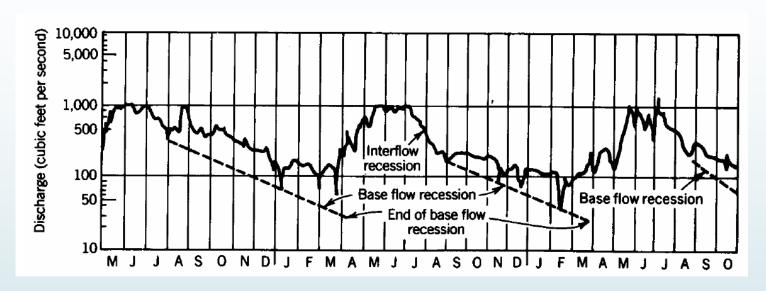
**Recharge** = Rate of flow into saturated zone across water table

The three generally **differ** due to

- Evapotranspiration (ET) from root zone
- Change in water storage within unsaturated zone
- Lateral flow through unsaturated zone (due to sloping topography and layering) that may cause interflow

## Subsurface Hydrology





**Interflow** = component of stream hydrograph contributed by saturated and/or unsaturated flow of **infiltrating water** through the vadose zone.

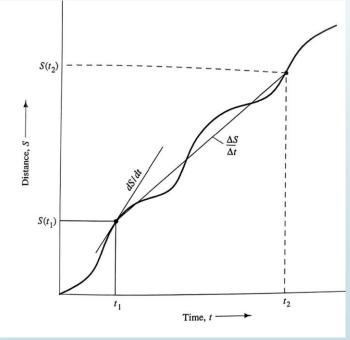
**Baseflow** = component of a stream hydrograph contributed by **groundwater inflow** (the third component being **overland flow**)

**Baseflow Recession** = Decline in stream hydrograph associated with baseflow due to decline in baseflow following an episodic recharge event.

Typically **recession** is near **exponential**, so if a hydrograph is entirely due to baseflow (or interflow), it can be used to estimate the total recharge (or net infiltration) volume.

#### Derivatives

Soil-moisture movement, groundwater flow, transport can be described by means of partial differential equations.



$$\frac{d\left(\frac{dS}{dt}\right)}{dt} \text{ or } \frac{d^2S}{dt^2}$$

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$$\frac{d^2S}{dt^2}$$

$$\frac{d^2S}{dt} \text{ or } \frac{d^2S}{dt^2}$$

$$\frac{\Delta S}{\Delta t} = \frac{S(t_2) - S(t_1)}{t_2 - t_1} \quad \frac{dS(t_1)}{dt} = \lim_{t \to t_1} \frac{S(t) - S(t_1)}{t - t_1}$$

#### Derivatives

In hydrogeology, h=h(x,y,z).

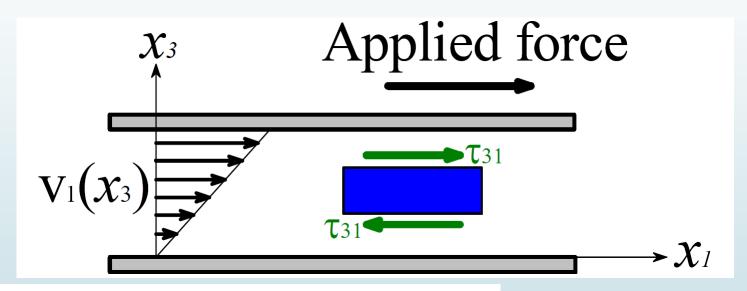
Partial Derivatives: differential head with respect to one of space variables while holding the other two variables constant.

The second derivative of hydraulic head to the space variables:

$$\frac{d^2h}{dx^2} + \frac{d^2h}{dy^2} + \frac{d^2h}{dz^2}$$

#### Water as a Newtonian Fluid

■ Water commonly behaves as a Newtonian fluid in that under laminar flow



$$\tau_{31} = \mu \frac{d\mathbf{v}_1}{dx_3}$$

 $\mu =$ dynamic viscosity

Constitutive relation (law)

$$[\mu] = \frac{[\tau]}{[dv/dx]} = \frac{FL^{-2}}{LT^{-1}L^{-1}} = FTL^{-2} = MT^{-1}L^{-1}$$

剪应力

shear stresses  $\tau$  acting in the planes of the lamina are linearly proportional to the rate of velocity variation (strain rate) normal to the lamina



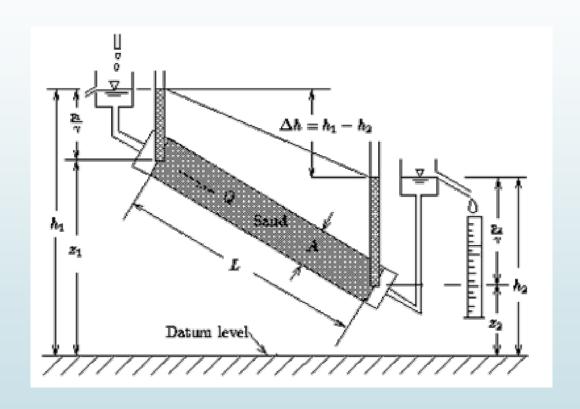




■ Darcy's Law

达西定律

Experiments (starting with *Henry Darcy* 1856) suggest that when a Newtonian fluid fully **permeates** and **flows slowly** and **steadily** through a **porous medium** under **isothermal** conditions it satisfies the **constitutive relation** (<u>Darcy's law</u>)



#### ■ Darcy's Law

$$Q = -KA \frac{dh}{dl}$$

Q = volumetric discharge

K = proportionality constant known as hydraulic conductivity

A = cross-sectional area

dh/dl =gradient of hydraulic head



**K** is a measure of ability of the fractured or porous media to transmit water

specific discharge or Darcy flux

$$q = -K \frac{dh}{dl}$$

$$K = \frac{\gamma}{\mu} k$$

 $\gamma = \rho g =$ **unit weight** of fluid [ $MT^{-2}L^2$ ]

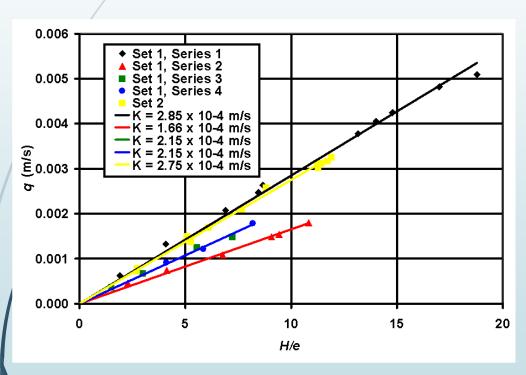
 $K = \frac{\gamma}{\mu} k$   $p = \text{fluid mass density } [M^3/L]$   $g = \text{acceleration due to } \text{gravity}[L/T^2]$  k = intrinsic powersk =**intrinsic permeability** of medium[ $L^2$ ]

k与介质相关

Darcy's law was obtained for one-dimensional flow. However, head is a function of all three dimensions: h=h(x,y,x)

#### ■ Darcy's Law

Darcy's own experimental results look like this:



In other words, for a given fluid at a given pressure and temperature (given  $\mu$ ,  $\rho$ ) flowing slowly through a given porous medium (given k) the flux is linearly proportional to the hydraulic gradient  $\Delta h/\Delta L$ .

Darcy's law is thus equivalent to

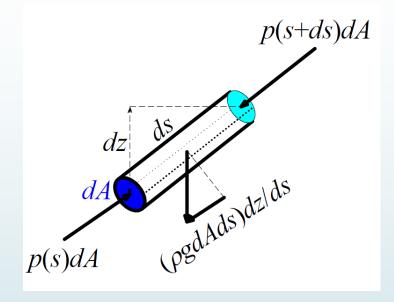
- Fourier's law of heat conduction in solids
- Fick's 1st law of diffusion
- Ohm's law for electrical current.

Darcy's law **does not** apply to non-Newtonian (pseudoplastic, dilatant) fluids and surfactants.

#### **■** Hydraulic Gradient as Force

Consider a **stream tube** having **infinitesimal** crosssectional area *dA* and length *ds*. The fluid is propelled in its motion by the **driving force** 

$$\underbrace{\left[p(s) - p(s + ds)\right]dA}_{\text{differential pressure force}} - \underbrace{\rho g dA ds}_{\text{gravity force}} \frac{dz}{ds}$$



Expanding p(s+ds) in **Taylor series** about s and discarding all but the **two leading terms**,

$$p(s+ds) = p(s) + \frac{dp}{ds}ds$$

$$-\frac{dp}{ds}dAds - \rho g dAds \frac{dz}{ds}$$
differential pressure force gravity force

The driving force per unit volume

$$-\frac{dp}{ds} - \rho g \frac{dz}{ds}$$

#### **Defining hydraulic head**

$$h = \int_{\frac{p_0}{\text{pressure}}}^{p} \frac{dp}{\rho g} + \underbrace{\left(z - z_0\right)}_{\text{elevation or gravity head}}$$

implies that it represents **incremental work** performed by moving a **unit weight** of fluid up-gradient (against the driving force) from a lower to a higher state of **potential energy**. This is why surfaces or curves of equal h are called **equipotentials**.

$$-\frac{dh}{ds} = -\frac{1}{\rho g} \frac{dp}{ds} - \frac{dz}{ds} = \frac{\text{driving force}}{\gamma}$$

$$-\frac{dh}{ds} = -\frac{1}{\rho g} \frac{dp}{ds} - \frac{dz}{ds} = \frac{\text{driving force}}{\gamma} \qquad -\text{grad } h = -\begin{pmatrix} \frac{\partial h}{\partial x} \\ \frac{\partial h}{\partial y} \\ \frac{\partial h}{\partial z} \end{pmatrix} = -\frac{1}{\gamma} \begin{pmatrix} \frac{\partial p}{\partial x} \\ \frac{\partial p}{\partial y} \\ \frac{\partial p}{\partial z} \end{pmatrix} - \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

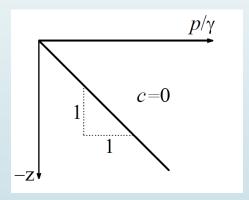
In other words, Darcy's law states that fluid flux is linearly proportional to the driving force per unit weight, the hydraulic conductivity acting as the constant of proportionality, representing flux per unit gradient.

Treating water as an incompressible and homogeneous liquid under **isothermal conditions** implies  $\gamma = \rho g = \text{constant}$ . Setting  $p_0 = 0$  at atmospheric conditions (p thus becoming gauge pressure) and  $z_0$ =0 implies

$$h = \frac{p}{\gamma} + z$$

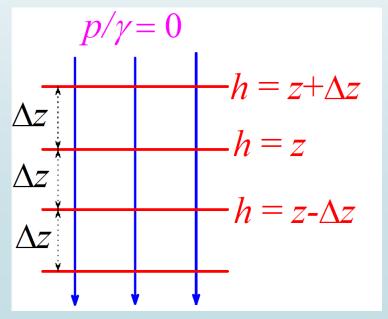
#### **■** Defining hydraulic head

- Flow does not depend on head, only on its gradient. One can therefore set an **arbitrary reference** value for h; we set h = 0 at z = 0.
- If  $h \equiv c$  (constant) then grad  $h \equiv 0$  and so  $q \equiv 0$ , i.e., the fluid is static (does not flow).
- Under static conditions pressure increases linearly with depth:  $p = \gamma (c z)$



#### **■** Defining hydraulic head

- Under horizontal flow (say in an aquifer) the equipotentials are vertical. Setting h=c yields p = $\gamma$  (c-z) along any equipotential, i.e., pressure increases linearly with depth, as in the static case:
- In a domain of equal pressure (say p = 0) there is no pressure force and flow is gravitational under a unit downward force (per unit weight of fluid):



#### ■ Terms relating to tensors:

Scalar: a zero-order tensor, a quantity characterized by its size or magnitude. (e.g., h, C, T)

Vector: a first-order tensor, a quantity has both a magnitude and a direction. (e.g., Discharge, flux)

Tensor: the product of two vectors, requiring nine components to account for all possible products of the three components of each vector.(e.g., hydraulic conductivity, hydrodynamic dispersion)

grad 
$$h = \mathbf{i} \frac{\partial h}{\partial x} + \mathbf{j} \frac{\partial h}{\partial y} + \mathbf{k} \frac{\partial h}{\partial z}$$
 i, j, k are unit vector in x,y,z direction.

h is a scalar, but grad h is a vector

$$\nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z}$$
 vector differential operator

Specific discharge  $\mathbf{q}$  is a vector, three components,  $\mathbf{q}_x, \mathbf{q}_y$ , and  $\mathbf{q}_z$ 

Magnitude of the vector  $\mathbf{q}$ ,  $q = |\mathbf{q}|$ 

■ Terms relating to tensors:

$$\mathbf{K} = \begin{bmatrix} K_{\mathbf{x}\mathbf{x}} & K_{\mathbf{x}\mathbf{y}} & K_{\mathbf{x}\mathbf{z}} \\ K_{\mathbf{y}\mathbf{x}} & K_{\mathbf{y}\mathbf{y}} & K_{\mathbf{y}\mathbf{z}} \\ K_{\mathbf{z}\mathbf{x}} & K_{\mathbf{z}\mathbf{y}} & K_{\mathbf{z}\mathbf{z}} \end{bmatrix}$$

 $\blacksquare$  Three components of the specific discharge vector  $\mathbf{q}$ :

$$q_{x} = -K_{xx} \frac{\partial h}{\partial x} - K_{xy} \frac{\partial h}{\partial y} - K_{xz} \frac{\partial h}{\partial z}$$

$$q_{y} = -K_{yx} \frac{\partial h}{\partial x} - K_{yy} \frac{\partial h}{\partial y} - K_{yz} \frac{\partial h}{\partial z}$$

$$q_{z} = -K_{zx} \frac{\partial h}{\partial x} - K_{zy} \frac{\partial h}{\partial y} - K_{zz} \frac{\partial h}{\partial z}$$

- Dot product/inner product: multiply two vectors together, a scalar.
- Second derivative:  $\nabla \cdot \operatorname{grad} h = \frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial y^2} + \frac{\partial^2 h}{\partial z^2}$

■ Terms relating to tensors:

$$\mathbf{K} = egin{bmatrix} K_{\mathrm{xx}} & K_{\mathrm{xy}} & K_{\mathrm{xz}} \ K_{\mathrm{yx}} & K_{\mathrm{yy}} & K_{\mathrm{yz}} \ K_{\mathrm{zx}} & K_{\mathrm{zy}} & K_{\mathrm{zz}} \end{bmatrix}$$
 均质:k处处相等非均质:k不同位置不同

 $\blacksquare$  Three components of the specific discharge vector  $\mathbf{q}$ :

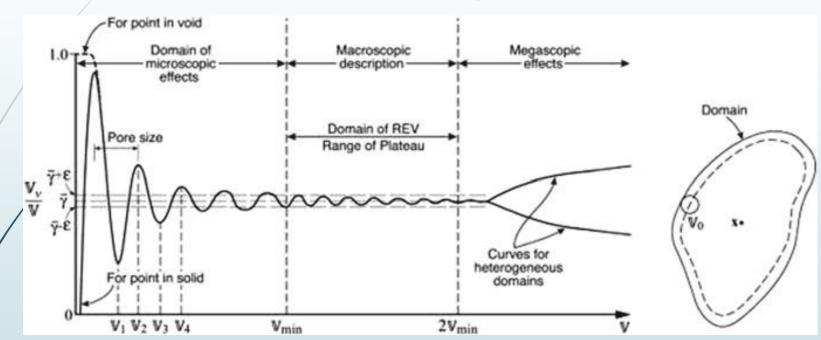
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■ Representative elementary volume (REV)

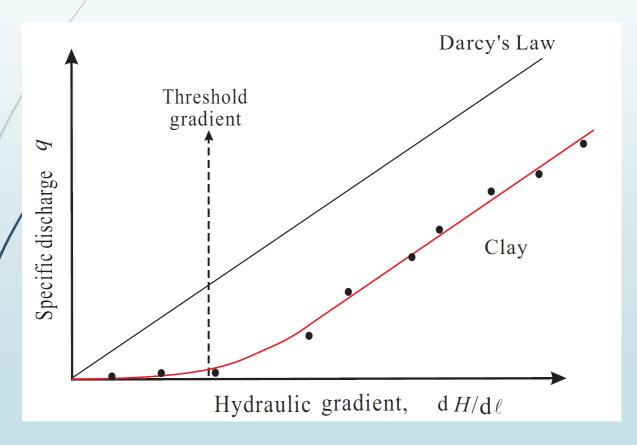


For a considered porous medium, the size of the REV is selected such that:

- The average value of *any relevant geometrical characteristic of the microstructure* of the void space, at any point in a porous medium, will be a unique function of the location of that point only.
- The measured averaged value should be *independent of small variations in the size of the* REV.

VALIDITY OF DARCY'S LAW

#### **Lower Limit**



According to Darcy's law, any hydraulic head gradient, no matter how small, will cause water movement. On the contrary, many experiments have shown that the hydraulic head gradient must exceed some threshold value dh/dl, in order to cause water movement in clayey soils. The failure of Darcy's law in this case can be attributed to the fact that important electrostatic forces exist in the clayey soils, due to electrical charge imbalances within the mineral structure of the soil. At low hydraulic head gradients, these electrostatic forces (or internal energies) cannot be neglected in the derivation of Poiseuille's law.

#### VALIDÍTY OF DARCY'S LAW

The Reynolds Number for Groundwater Flow

**How slowly** must a Newtonian fluid flow for Darcy's law to hold? Experiments done on unconsolidated **granular media** (glass beads, sand, silt) provide the answer in terms of a **dimensionless group** called the **Reynolds number**, generally defined as

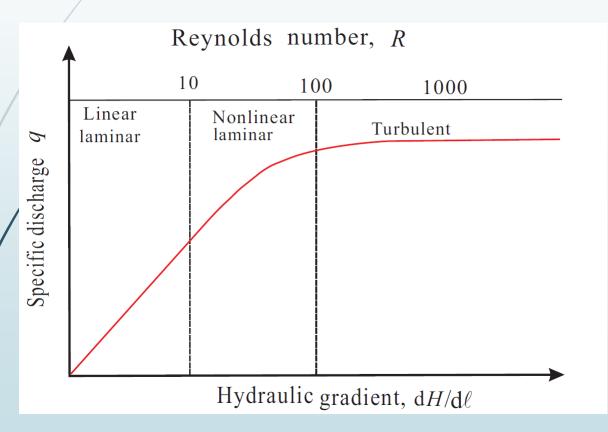
$$Re = \frac{dq}{v}$$

d = mean grain diameter or diameter of 10<sup>th</sup> percentile of grains by weight  $v = \mu / \rho =$  kinematic viscosity [ $L^2/T$ ]

The experiments suggest that the **Darcy regime** (known in fluid mechanics as **Stokes regime**) is valid for Re not exceeding 1-10; beyond that, the flow regime becomes **nonlinear** and (at still higher Re) **turbulent** (otherwise it is **laminar**):

#### VALIDITY OF DARCY'S LAW

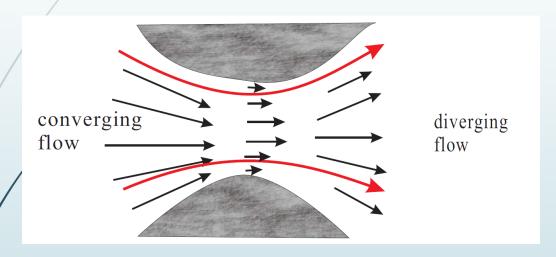
#### **The Upper Limit**



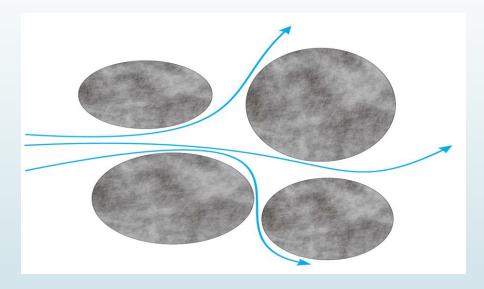
The linear relationship only exists when the hydraulic gradient is relatively small or the Reynolds number is smaller than 10. Flow behaviors deviating from the linear relationship (i.e., Darcian behavior) however have been observed at large dh/dl values (i.e., at  $10 < R_e < 100$ ). Under these conditions, the relation between q and dh/dl is no longer linear, although the flow can still be in the laminar flow regime (or in a transition regime). At  $R_e >> 100$ , turbulent flow with streamlines crossing each other takes place. Under the turbulent flow regime, q is no longer correlated with *dh/dl* and flow exhibits chaotic behavior (random motion). Under this scenario, describing flow behavior quantitatively becomes difficult.

#### ■ VALIDITY OF DARCY'S LAW

#### **The Upper Limit**

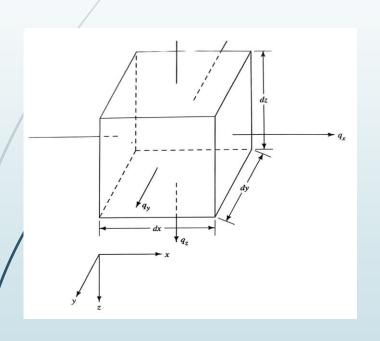


Velocity variation within a pore and converging and diverging flow



Variations in flow velocity among different pores

**■** Derivation of the flow equation in a deforming medium



The law of mass conservation states that there can be no net change in the mass of fluid in a small REV of a porous medium. In other words, the mass entering the REV less the mass leaving the REV is equal to the change in mass storage with time.

The component of mass flux into the REV parallel to the x axis is the fluid density times the flux rate:

Mass influx along x axis = 
$$\rho_w q_x dy dz$$
  
Mass outflow rate parallel to x axis =  $\left[\rho_w q_x + \frac{\partial (\rho_w q_x) dx}{\partial x}\right] dy dz$   
Net mass accumulation = mass inflow- mass outflow  
=  $-\frac{\partial (\rho_w q_x) dx dy dz}{\partial x}$ 

 $\rho_w = \text{fluid density } (M/L^3)$ 

 $q_x$  = specific discharge or volume of flow per cross-sectional area(L/T)

 $dydz = cross-sectional area(L^2)$ 

**■** Derivation of the flow equation in a deforming medium

Net mass accumulation due to the flow component parallel to

the x axis
$$-\frac{\partial(\rho_w q_x) dx dy dz}{\partial x}$$
the y axis
$$-\frac{\partial(\rho_w q_y) dy dx dz}{\partial y}$$
the z axis
$$-\frac{\partial(\rho_w q_y) dy dx dz}{\partial z}$$

the z axis 
$$-\frac{\partial(\rho_w q_z)dzdx\,dy}{\partial z}$$
Total net mass accumulation within REV =  $-\left(\frac{\partial}{\partial x}\left(\rho_w q_x\right) + \frac{\partial}{\partial y}\left(\rho_w q_y\right) + \frac{\partial}{\partial z}\left(\rho_w q_z\right)\right)dxdydz$ 

The change in mass of water to time :  $\frac{\partial M}{\partial t} = \frac{\partial}{\partial t} (\rho_w n \, dx dy dz)$ ; n: porosity

The law of conservation of mass:

$$-\left(\frac{\partial}{\partial x}\left(\rho_{w}q_{x}\right)+\frac{\partial}{\partial y}\left(\rho_{w}q_{y}\right)+\frac{\partial}{\partial z}\left(\rho_{w}q_{z}\right)\right)dxdydz=\frac{\partial}{\partial t}(\rho_{w}n)dxdydz$$

Assume: density is same in REV 
$$\rightarrow -\left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z}\right) = \frac{1}{\rho_w} \frac{\partial}{\partial t} (\rho_w n)$$

#### **■** Derivation of the flow equation in a deforming medium

Substitute Darcy's law for the specific discharge components:

$$\frac{\partial}{\partial x} \left( K_{xx} \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( K_{yy} \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( K_{zz} \frac{\partial h}{\partial z} \right)$$

The change in mass within REV is due to changes in porosity and the density of water as the head changes with time. The change in the volume of water in storage is proportional to the change in head with time:

$$\frac{1}{\rho_w} \frac{\partial}{\partial t} (\rho_w n) = S_s \frac{\partial h}{\partial t}$$

Combine:

$$\frac{\partial}{\partial x} \left( K_{xx} \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( K_{yy} \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( K_{zz} \frac{\partial h}{\partial z} \right) = S_s \frac{\partial h}{\partial t}$$

Derivation of the flow equation in a deforming medium

In del and tensor notation:

$$\nabla \cdot \mathbf{K} \cdot \nabla \mathbf{h} = S_S \frac{\partial h}{\partial t}$$

Einstein's summation notation:

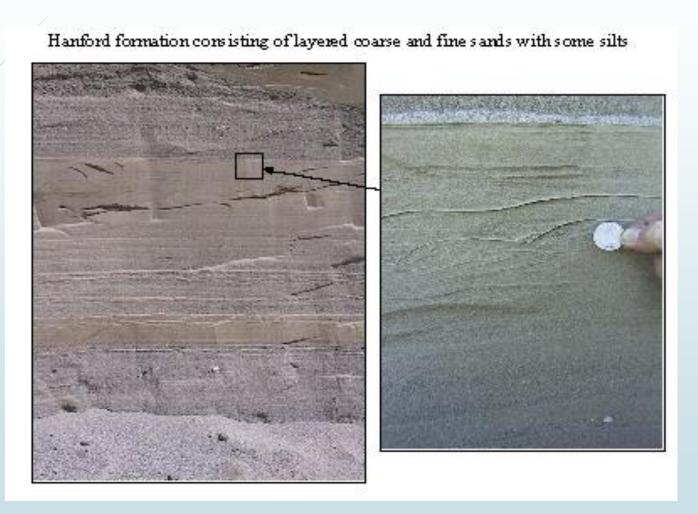
$$q = -\mathbf{K} \frac{dh}{dl}$$

$$q_i = K_{ij}h_j$$

in vector notation : 
$$\mathbf{q} = \mathbf{K} \cdot \operatorname{grad} h$$
  $\mathbf{q} = \mathbf{K} \cdot \mathbf{h}$ 

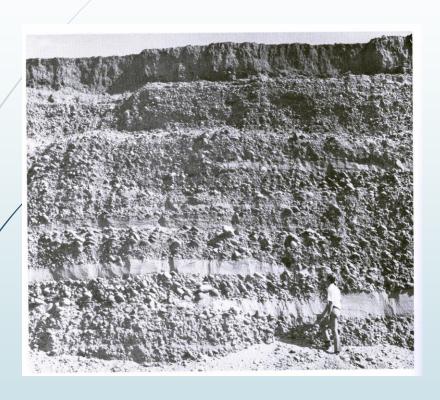
in del notation: 
$$\mathbf{q} = \mathbf{K} \cdot \nabla \mathbf{h}$$

#### Variation in different scale



Multi-scale heterogeneity: stratifications (layers) and lamination

#### Variation in different scale

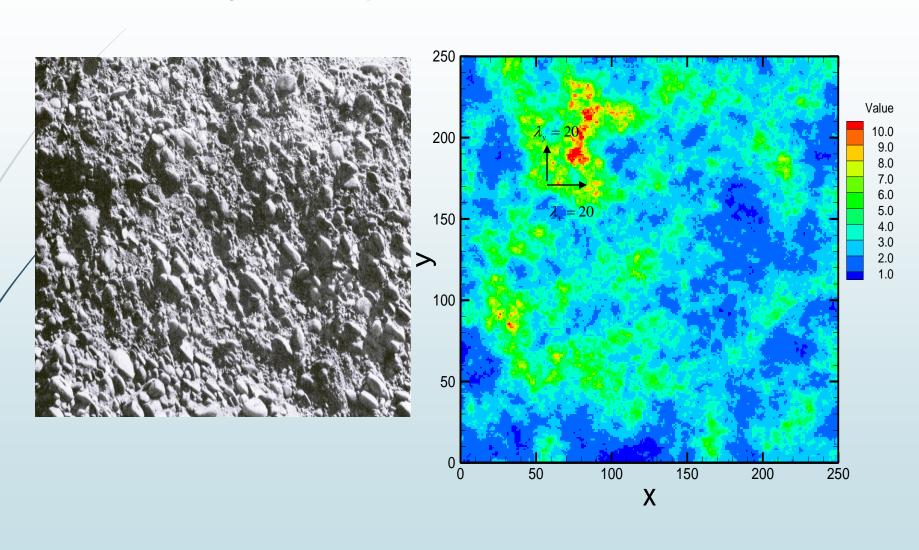


Field-scale heterogeneity meters to hundreds of meters

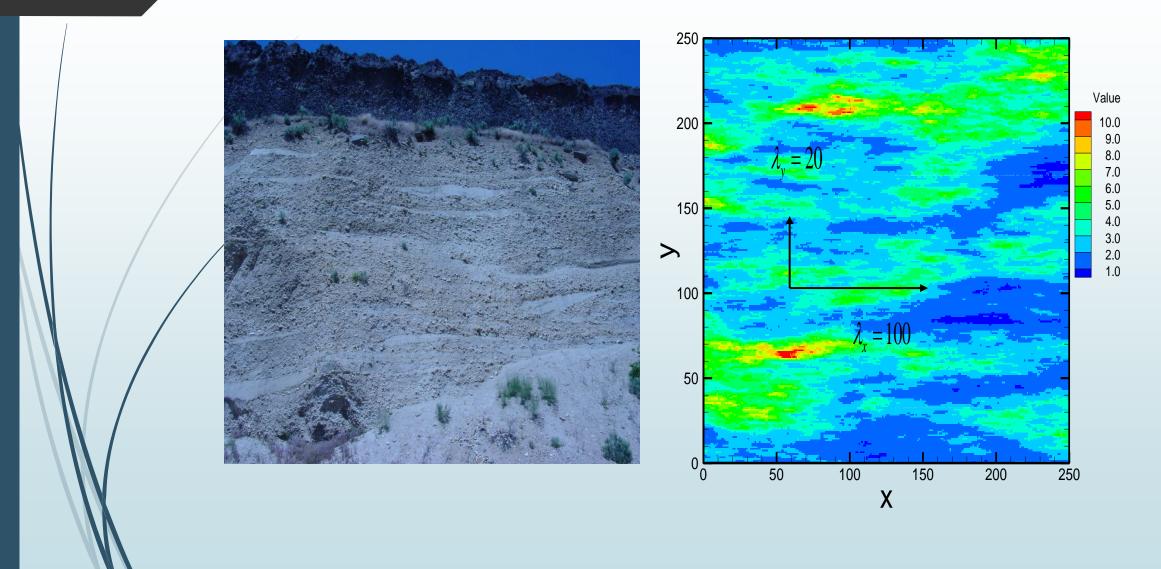


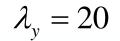
Laboratory-scale heterogeneity Centimeters to meters

# Statistically Isotropic Media

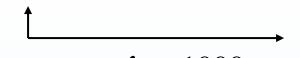


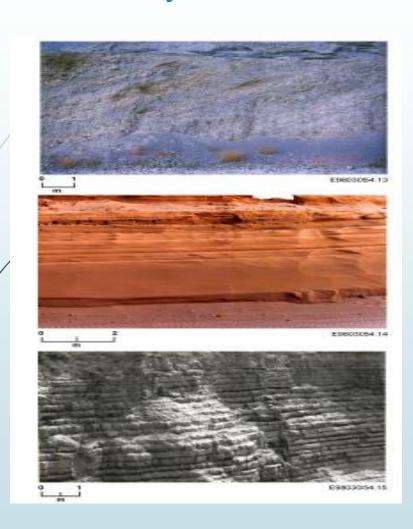
# Statistically anisotropic media

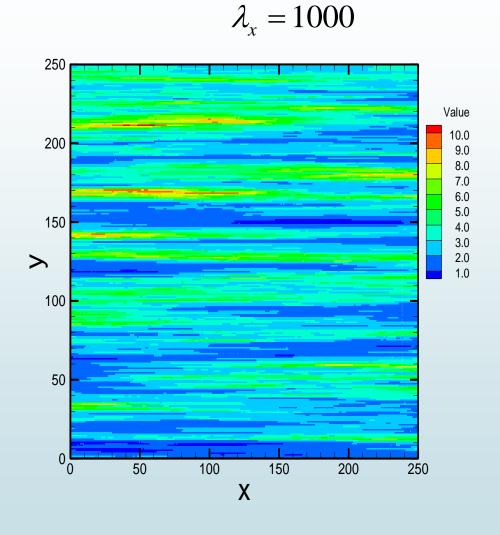




# Perfectly stratified media







# Multi-scale Heterogeneity

- Pore-scale (<<centimeters)</p>
- Laboratory scale (cm to meters)
- Field scale (tens of meters to hundreds of meters)
- ← Basin scale (tens and hundreds of kilometers) 流域尺度
- Regional scale
- Continental scale

