

# Lasers 2022-2023 Exam

Nicolas Le Thomas – nicolas.lethomas@ugent.be

January 9, 2023

## Problem

In the seventieth there was an active search for stable lasers operating in the far-infrared (FIR) range to bridge the gap between the infrared (IR) range and the millimeter-wave range.  $CO_2$  lasers emitting in the IR, namely around  $10\ \mu m$ , were already quite well developed and used to optically pump FIR lasers made of molecular gas. Here, we will study the output power of a FIR laser using the  $570.5\ \mu m$  transition line of methanol vapor  $CH_3OH$ . The laser is described by a four-level system as represented in Fig.1. The level 0 corresponds to some rotational level in the vibrational ground state, 1 and 2 are adjacent rotational levels in a low-lying excited vibrational state and 3 represents the lumped effect of those rotational levels in the upper vibrational manifold, which are not directly involved in the laser transition  $2 \rightarrow 1$ .

The molecules are excited from 0 to 2 at a pumping rate  $w_p$  by a  $CO_2$  laser tuned to the  $0 \rightarrow 2$  absorption line. Collisions between the molecules, occurring at a rate  $w_r$ , are very efficient in establishing thermal equilibrium among the rotational levels of a given vibrational state. The rate  $w_r$  can therefore be assumed to be much larger than the rate  $w_v$  of relaxation back to the vibrational ground state.

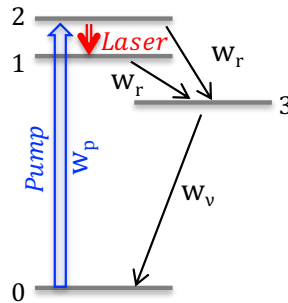


Figure 1: Four-level model for the optically pumped FIR laser

- 1) Briefly explain what are vibrational and rotational states. What are their corresponding wavelength ranges?
- 2) For which energy distance from the ground state, the level 1 and 2 can be considered as unpopulated without the  $CO_2$  pumping. Give an order of magnitude at room temperature. What is the physical effect at play? We will consider in the following that the levels 1 and 2 are sufficiently above the ground state to neglect the impact of this effect.
- 3) Compare the spontaneous emission rate in free space at visible wavelengths, namely for a wavelength around  $\lambda = 0.5 \mu m$  and that in the FIR range  $\lambda = 500 \mu m$ . Considering that the typical spontaneous radiative lifetime is  $1 ns$  at  $\lambda = 0.5 \mu m$ , what is the spontaneous radiative lifetime at  $\lambda = 500 \mu m$ . In view of this result, we will neglect the spontaneous emission in the rate equations governing the laser dynamics.
- 4) Write the rate equations governing the total occupation numbers per unit of volume  $N$  of the various molecular levels, and the FIR photon density  $n$ . Use the Einstein coefficient  $B_{21}$ , the degeneracy  $g_1$  and  $g_2$  of the level 1 and 2, and  $\tau_c$  the photon cavity lifetime. The total number of molecules is  $N$ .
- 5) Show that in the steady state the FIR photon density is given by:

$$n = \frac{g_1}{g_1 + g_2} \frac{w_r}{B_{21}} \left( \frac{NB_{21}\tau_c w_p}{w_r(1 + w_p/w_\nu)} - 1 \right) \quad (1)$$

- 6) Determine the small signal gain per unit length.
- 7) Demonstrate that the saturated intensity is given by:

$$I^{sat} = c \times h\nu \frac{g_1}{g_1 + g_2} \frac{w_r}{B_{21}} \quad (2)$$

We now want to study the impact of the gas pressure  $p$  and of the pump power  $U$  on the laser characteristic, in particular on the FIR photon density  $n$  given in Eq.(1). We assume that the  $1 \rightarrow 2$  transition has a homogeneous linewidth  $\Delta\nu_{12}$  that varies linearly with the pressure  $p$  as  $\Delta\nu_{12} = Cp$  with  $C$  a constant. The spontaneous radiative lifetime of this transition is  $\tau_{sp}$ . The active volume of the laser is  $V$ .

- 1) What is the lineshape of the  $1 \rightarrow 2$  transition in view of the physics at play? The normalized lineshape is noted  $f(\nu)$ .
- 2) Why does the Einstein coefficient  $B_{21}(\nu)$  depend on the pressure?
- 3) Express  $B_{21}(\nu)$  as a function of  $f(\nu)$ ,  $\tau_{sp}$  and  $\Delta\nu_{12}$  and any other relevant parameters. How does  $B_{21}(\nu)$  varies with the pressure  $p$ ?

- 4) Give the equation between the rotational relaxation rate  $w_r$  and the pressure  $p$ .
- 5) The pump power absorbed in the gas is denoted by  $U_{abs}$  and we assume that a fraction  $\xi$  of this power goes into the  $0 \rightarrow 2$  transition. Express  $\xi U_{abs}$  as a function of  $w_p$  and the pump frequency  $\nu_p$ .
- 6) Write the rate equation for the pump intensity  $I$  in the cavity considering that  $\Gamma$  measure the loss rate of the pump radiation.
- 7) The pump rate  $w_p$  is proportional to the intensity  $I$  of the pump radiation in the cavity with  $\zeta$  the coefficient of proportionality. Considering 1) the steady state of the rate equation for the pump intensity found in the previous question, 2) the expression of  $U_{abs}$  versus  $w_p$ , and 3) the ideal gas law, determine  $w_p$  as a function of  $U$  and  $p$ . Introduce the parameters  $p_s = 2\pi kT\xi\Gamma/h\nu_p f_0\zeta V$  and  $U_s = (1 + p/p_s)2\pi\Gamma w_\nu/\zeta$ , where  $k$  is the Boltzmann constant and  $f_0$  the fraction of the total number of molecules being in the 0 state in the absence of pumping.

- 8) Show that

$$\frac{Nw_p}{1 + w_p/w_\nu} = \frac{\xi}{Vh\nu_p} \frac{p/p_s}{1 + p/p_s} \frac{U}{1 + U/U_s} \quad (3)$$

if  $p \ll p_s$  or  $U \ll U_s$ . Show that this expression is also valid if  $U \gg U_s$ .

- 9) Determine the small signal gain and the FIR output power as a function of the pressure  $p$  and the pump power  $U$ . Comment.

I. 2)  $\Delta E_{01} > k_B T$      $\Delta E_{02} > k_B T$     cf. Boltzmann statistics

$$\frac{N_i}{N_0} = \frac{g_i}{g_0} e^{-h\nu/k_B T} \quad \text{at } 300\text{K} \Rightarrow k_B T \approx 25\text{meV}$$

$$h\nu = \Delta E_{0i}$$

$$3) A_{21} \propto \nu \rho(\nu) \quad \& \quad \rho(\nu) = \frac{8\pi\nu^2}{c^3} \Rightarrow A_{21} \propto \frac{1}{\nu^3}$$

$$A_{21}^{\text{FIR}} = \frac{\lambda_{\text{VIS}}^3}{\lambda_{\text{FIR}}^3} A_{21}^{\text{VIS}} \quad A_{21}^{\text{VIS}} = \frac{1}{\tau_{21}^{\text{VIS}}} = 10^9 \text{ s}^{-1} \quad A_{21}^{\text{FIR}} = 1 \text{ s}^{-1}$$

$$4) \frac{dN_2}{dt} = W_p N_0 - n B_{21} \left( N_2 - \frac{g_2}{g_1} N_1 \right) - W_r N_2$$

$$\frac{dN_1}{dt} = n B_{21} \left( N_2 - \frac{g_2}{g_1} N_1 \right) - W_r N_1$$

$$\frac{dN_3}{dt} = W_r N_2 + W_r N_1 - W_v N_3$$

$$\frac{dN_0}{dt} = W_v N_3 - W_p N_0$$

$$N = N_0 + N_1 + N_2 + N_3$$

$$\frac{dn}{dt} = n B_{21} \left( N_2 - \frac{g_2}{g_1} N_1 \right) - \frac{n}{\tau_c}$$

$$5) \frac{dN_2}{dt} = \frac{dN_1}{dt} = \frac{dN_3}{dt} = \frac{dN_0}{dt} = 0 \quad (\text{steady state})$$

$$\frac{dn}{dt} = 0 \quad (\text{gain} = \text{loss})$$

$$\text{from } \frac{dN_0}{dt} = 0 \Rightarrow N_3 = \frac{W_p}{W_v} N_0$$

$$\text{from } \frac{dN_3}{dt} = 0 \Rightarrow N_0 = \frac{W_r}{W_p} (N_1 + N_2)$$

$$N = N_0 + \frac{W_p}{W_r} N_0 + \frac{W_p}{W_v} N_0 = \left( 1 + \frac{W_p}{W_r} + \frac{W_p}{W_v} \right) N_0$$

$$W_r \gg W_v \Rightarrow N \simeq \left(1 + \frac{W_p}{W_v}\right) N_0$$

$$\text{from } g_2 \times \frac{dN_1}{dt} - g_1 \times \frac{dN_2}{dt} = 0$$

$$\Rightarrow -g_1 W_p N_0 + (g_1 + g_2) n B_{21} \left(N_2 - \frac{g_2}{g_1} N_1\right) + W_r g_1 N_2 - W_r g_2 N_1 = 0$$

$$\left[ (g_1 + g_2) n B_{21} + g_1 W_r \right] \left(N_2 - \frac{g_2}{g_1} N_1\right) - g_1 W_p N_0 = 0$$

$$\Downarrow \text{gain} = \text{loss}$$

$$\frac{1}{B_{21} T_c}$$

$$\Rightarrow n = \frac{g_1}{g_1 + g_2} \times \frac{W_r}{B_{21}} \left[ \frac{N B_{21} T_c W_p}{W_r \left(1 + W_p/W_v\right)} - 1 \right]$$

$$6) \quad r = \sigma \left(N_2 - \frac{g_2}{g_1} N_1\right) \quad B_{21} = \frac{\sigma}{h\nu} c$$

$$\left(N_2 - \frac{g_2}{g_1} N_1\right) = \frac{g_1 W_p N_0}{(g_1 + g_2) n B_{21} + g_1 W_r}$$

$$\Rightarrow r = \frac{\frac{h\nu}{c} B_{21} g_1 W_p N_0}{g_1 W_r + (g_1 + g_2) n B_{21}}$$

$$r = \underbrace{\frac{h\nu}{c} B_{21} \frac{W_p}{W_r} \frac{N}{\left(1 + \frac{W_p}{W_v}\right)}}_{Y_0} \times \frac{1}{1 + \underbrace{\frac{(g_1 + g_2) B_{21}}{c h \nu g_1 W_r}}_{\frac{1}{n_{\text{sat}}}}} n$$

$$\text{II. 1) } B_{21}(\nu) = \frac{c^3}{8\pi h \nu^3} A_{21} g(\nu) \quad g(\nu) \rightarrow \text{Lorentzian}$$

$$g(\nu) = \frac{\gamma}{\left(\frac{\gamma}{2}\right)^2 + (\pi(\nu - \nu_0))^2} \quad g(\nu) = \frac{4}{\gamma} f(\nu) \quad \gamma = 2\pi \Delta \nu_{12}$$

2)

$$3) B_{21}(\nu) = \frac{1}{h\nu} \times \frac{c^3}{4\pi^2 \nu^2 T_{sp} \Delta \nu_{12}} f(\nu) \quad \Delta \nu_{12} = c\rho \quad B_{21}(\nu) \propto \frac{1}{\rho}$$

$$4) w_\nu = \frac{1}{2} \gamma = \pi \Delta \nu_{12} = \pi c\rho$$

$$5) \xi U_{abs} = w_p N_0 V h\nu_p = h\nu_p N \frac{w_p}{1 + w_p/w_\nu} \nu$$

$$6) \frac{dI}{dt} = U - 2\pi\Gamma I - U_{abs}$$

$$7) w_p = f(p, U) \quad \frac{dI}{dt} = U - 2\pi\Gamma I - U_{abs} = 0$$

$$U - 2\pi\Gamma \frac{w_p}{\xi} - \frac{h\nu_p}{\xi} \nu \frac{N w_p}{1 + w_p/w_\nu} = 0$$

$$\text{ideal gas law: } N = \frac{P}{kT} \quad P_s = \frac{2\pi kT \xi \Gamma}{h\nu_p \zeta \nu}$$

$$\frac{w_p/w_\nu}{1 + w_p/w_\nu} \times \frac{P}{P_s} + \frac{w_p}{w_\nu} = \frac{\nu}{\nu_s} \left(1 + \frac{P}{P_s}\right)$$

$$\nu_s = \left(1 + \frac{P}{P_s}\right) \frac{2\pi\Gamma w_\nu}{\zeta} \quad \gamma = \frac{w_p}{w_\nu}$$

$$\gamma^2 + \gamma \left(1 + \frac{P}{P_s}\right) \left(1 - \frac{\nu}{\nu_s}\right) - \frac{\nu}{\nu_s} \left(1 + \frac{P}{P_s}\right) = 0$$

$$\Delta = \left(1 + \frac{P}{P_s}\right)^2 \left(1 - \frac{\nu}{\nu_s}\right)^2 + 4 \frac{\nu}{\nu_s} \left(1 + \frac{P}{P_s}\right)$$

$$\gamma = \frac{1}{2} \left[ \left(1 + \frac{P}{P_s}\right) \left(\frac{\nu}{\nu_s} - 1\right) + \sqrt{\Delta} \right]$$

$$① P \ll P_s \Rightarrow \gamma \simeq \frac{(\frac{U}{U_s}-1) + (\frac{U}{U_s}+1)}{2} = \frac{U}{U_s}$$

$$② U \ll U_s \Rightarrow \gamma \simeq \frac{U}{U_s}$$

$$③ U \gg U_s \Rightarrow \gamma \simeq \frac{1}{2} \left(1 + \frac{P}{P_s}\right) \frac{U}{U_s} + \left(1 + \frac{P}{P_s}\right) \frac{U}{U_s} \sqrt{1 + \frac{U_s}{U} \frac{4}{(1+P/P_s)}}$$

$$\gamma \simeq \left(1 + \frac{P}{P_s}\right) \frac{U}{U_s}$$

$$8) \frac{N_{wp}}{1 + w_p/w_v} = w_v \frac{P}{kT} \times \frac{\gamma}{1+\gamma} = w_v \frac{P}{kT U_s} \frac{U}{1+U/U_s}$$

$$= \frac{\xi}{v h \nu_p} \frac{P/P_s}{1+P/P_s} \times \frac{U}{1+U/U_s}$$

$$\frac{N_{wp}}{1 + w_p/w_v} = w_v \frac{P}{kT U_s}$$

$$9) r_o = \frac{h\nu}{c} B_{21} \times \frac{1}{w_r} \frac{N_{wp}}{(1 + \frac{w_p}{w_v})}$$

$$r_o = \frac{\xi B_{21}}{c V} \times \frac{1}{w_v} \times \frac{P/P_s}{1+P/P_s} \times \frac{U/U_s}{1+U/U_s}$$

$$B_{21}(\nu) = \frac{1}{h\nu_p} \frac{c^3}{4\pi^2 \nu^2 T_{sp}}$$