

```

%% William Valentine
% ECE885 Project 2
% H-infinity design for UAV pitch rate controller
clear; clc; close all;
s = tf('s');

```

## Identified plant G\_qde(s)

```

%           Mde(s + Zw)
% G(s) = ----- * e^(-tau*s)
%           s^2 + 2*zeta*wn*s + wn^2

% Nominal parameters
Mde_nom = -120.1;
Zw_nom = 9.24;
wn_nom = 10.9;
zeta_nom = 0.92;
tau_nom = 0.0575;

% Min/Max Parameter Values From Sys ID
Mde_min = -137.43; Mde_max = -105.65;
Zw_min = 8.28; Zw_max = 10.33;
wn_min = 10.11; wn_max = 11.32;
zeta_min = 0.85; zeta_max = 0.99;
tau_min = 0.05; tau_max = 0.06;

% Nominal plant transfer function
G_nom = (Mde_nom*s + Mde_nom*Zw_nom) / ...
    (s^2 + 2*zeta_nom*wn_nom*s + wn_nom^2);

% Approximate time delay with 1st-order pade
[numD,denD] = pade(tau_nom,1); % 1st-order Pade
Gdelay = tf(numD, denD);
G = Gdelay * G_nom; % Construct nominal plant with time delay

disp('Pitch-rate plant G(s) excluding Tau= q/δe:');

```

Pitch-rate plant G(s) excluding Tau= q/δe:

G\_nom

```

G_nom =

    -120.1 s - 1110
    -----
    s^2 + 20.06 s + 118.8

```

Continuous-time transfer function.  
Model Properties

```

disp('Full Pitch-rate plant G(s) = q/δe:');

```

Full Pitch-rate plant  $G(s) = q/\delta_e$ :

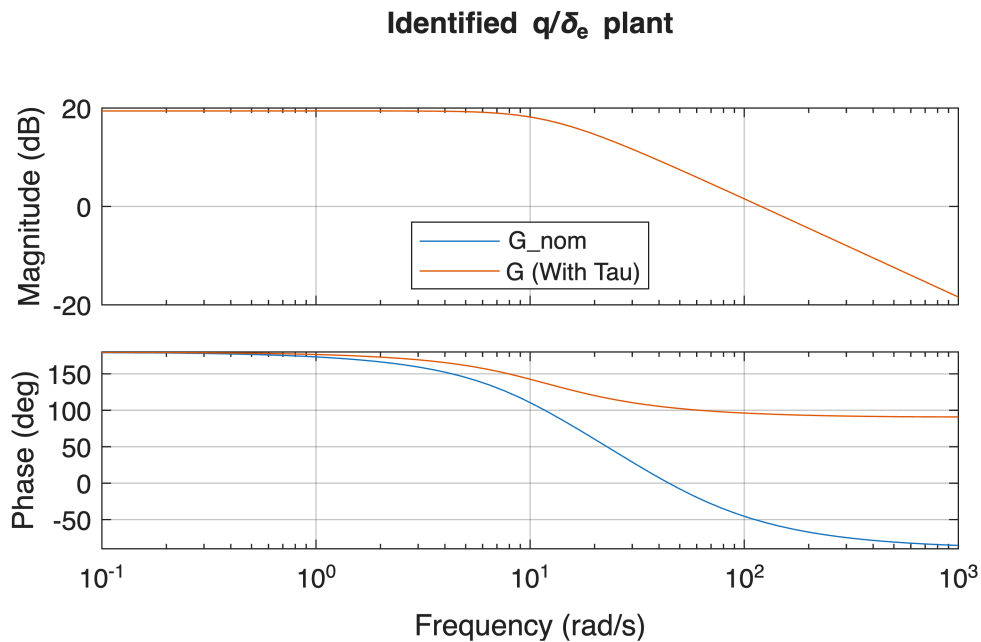
G

G =

$$\frac{120.1 s^2 - 3068 s - 3.86e04}{s^3 + 54.84 s^2 + 816.4 s + 4133}$$

Continuous-time transfer function.  
Model Properties

```
figure; bode(G); grid on;  
hold on;  
bode(G_nom);  
legend('G_nom', 'G (With Tau)', 'Location', 'Best');  
title('Identified q/\delta_e plant');
```



## Performance specs

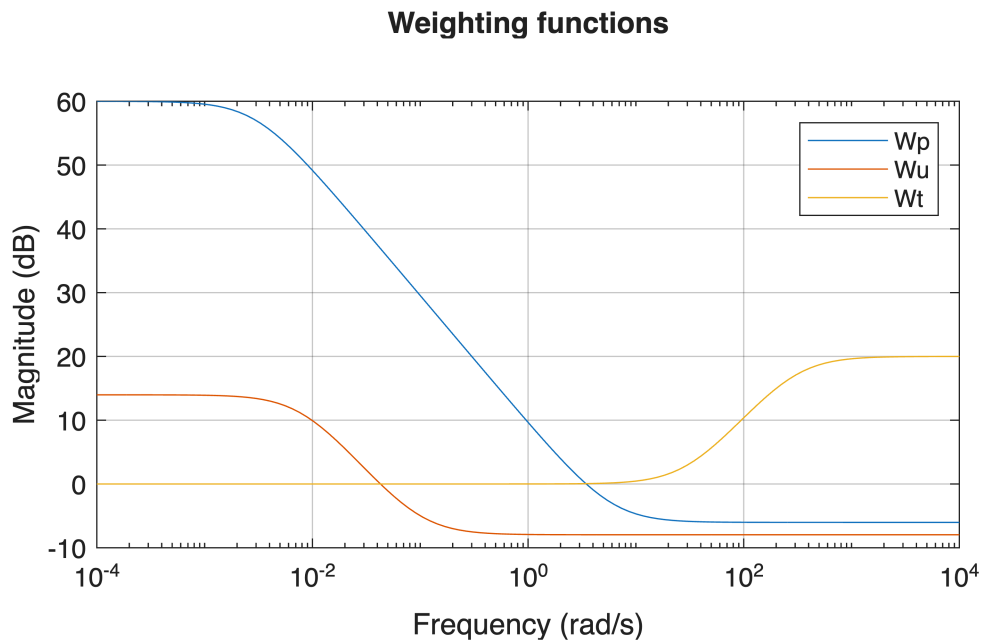
```
wb = 3;      % 3 rad/s desired closed loop bandwidth  
Ms  = 2;      % Desired peak sensitivity  
A   = 0.001;  % Steady state tracking error
```

## Weighting functions for mixed-sensitivity H-infinity design

```
% Wp: shape sensitivity S for tracking / disturbance rejection  
Wp = (s/Ms + wb) / (s + wb*A);  
  
% Wu: penalize control effort  
Wu = 0.4 * (s + 0.1) / (s + 0.008);
```

```
% Wt: penalize high-frequency T for noise & robustness
w_noise = 30; % start penalizing around 30 rad/s
Wt = (s/w_noise + 1) / (s/(10*w_noise) + 1);

figure; bodemag(Wp, Wu, Wt); grid on;
legend('Wp', 'Wu', 'Wt');
title('Weighting functions');
```



## H-infinity mixed-sensitivity synthesis

```
[Kh, CL, gamma_opt] = mixsyn(G, Wp, Wu, Wt);

disp('Optimal H-infinity gamma:');
```

Optimal H-infinity gamma:

gamma\_opt

```
gamma_opt =
1.1419
```

```
disp('H-infinity controller K(s):');
```

H-infinity controller K(s):

Kh

Kh =

```
A =
      x1      x2      x3      x4      x5      x6
x1    -0.003    2.633e-16  -6.166e-16  4.183e-15  -8.601e-15  -5.821e-15
```

x2	-4.621	0.3645	17.7	-43.14	5.018	10.11
x3	-2.267e-17	1.906e-18	-300	480.4	-383.5	-301.6
x4	-295.8	23.84	1133	-2816	295.6	638.8
x5	1.186e-17	-9.97e-19	2.335e-18	32	3.592e-17	2.324e-17
x6	2.837e-17	-2.386e-18	5.586e-18	-3.591e-17	16	5.561e-17

```
B =
      u1
x1      2
x2  9.742e-18
x3  3.215e-18
x4  3.316e-19
x5 -1.682e-18
x6 -4.023e-18
```

```
C =
      x1      x2      x3      x4      x5      x6
y1 -18.48   1.49  70.78 -172.6  20.07  40.43
```

```
D =
      u1
y1      0
```

Continuous-time state-space model.  
Model Properties

## Closed-Loop Sensitivity Functions

```
L = minreal(G*Kh);           % loop transfer
```

3 states removed.

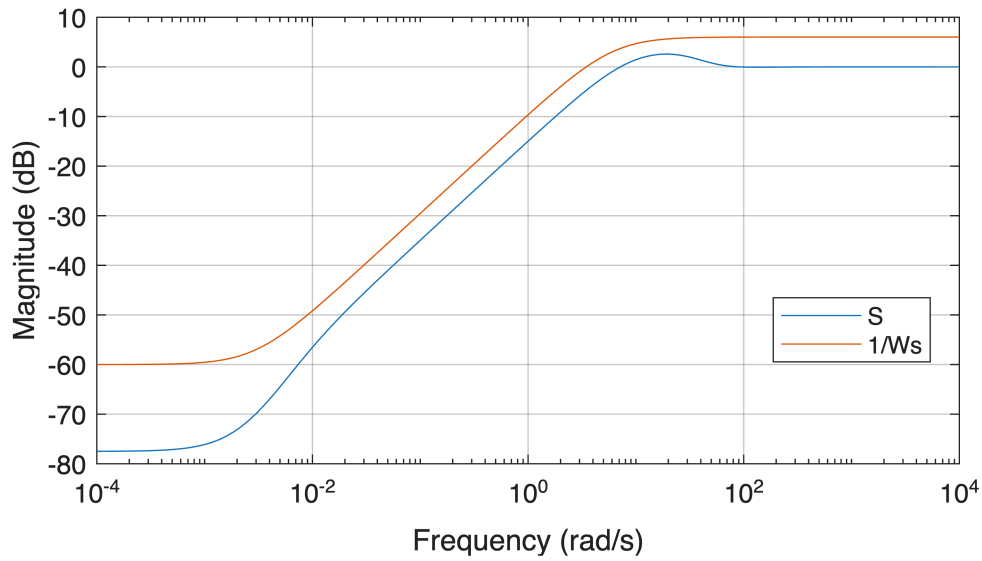
```
S = feedback(1, L);          % sensitivity
T = feedback(L, 1);          % complementary sensitivity
KS = minreal(Kh*S);          % weighted control effort
```

6 states removed.

## Check Frequency-Domain Specs

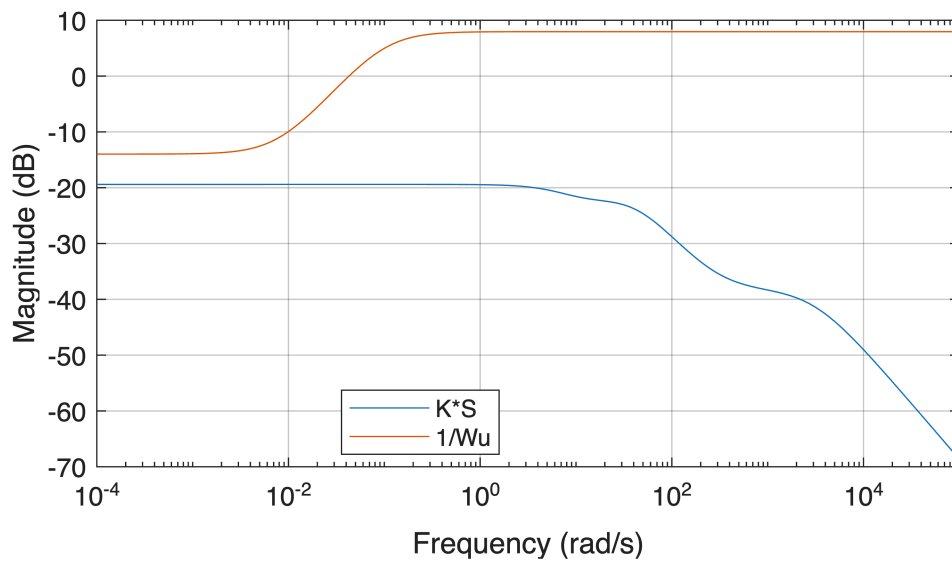
```
% Sensitivity
figure;
bodemag(S, 1/Wp); grid on;
legend('S', '1/Ws', 'Location', 'Best');
title('Sensitivity vs. requirement');
```

**Sensitivity vs. requirement**



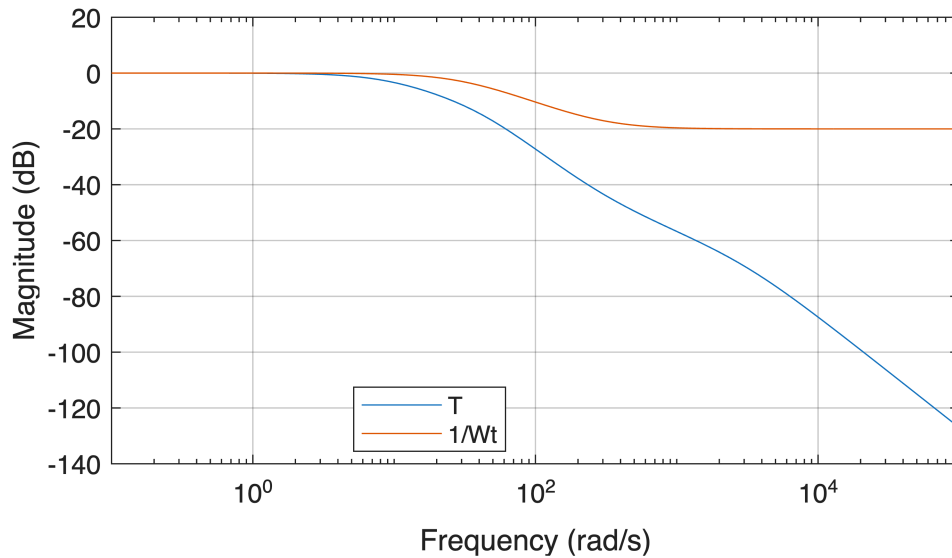
```
% Control Effort
figure;
bodemag(KS, 1/Wu); grid on;
legend('K*S', '1/Wu', 'Location', 'Best');
title('Control effort vs. requirement');
```

**Control effort vs. requirement**



```
% Complementary Sensitivity
figure;
bodemag(T, 1/Wt); grid on;
legend('T', '1/Wt', 'Location', 'Best');
title('Complementary sensitivity vs. requirement');
```

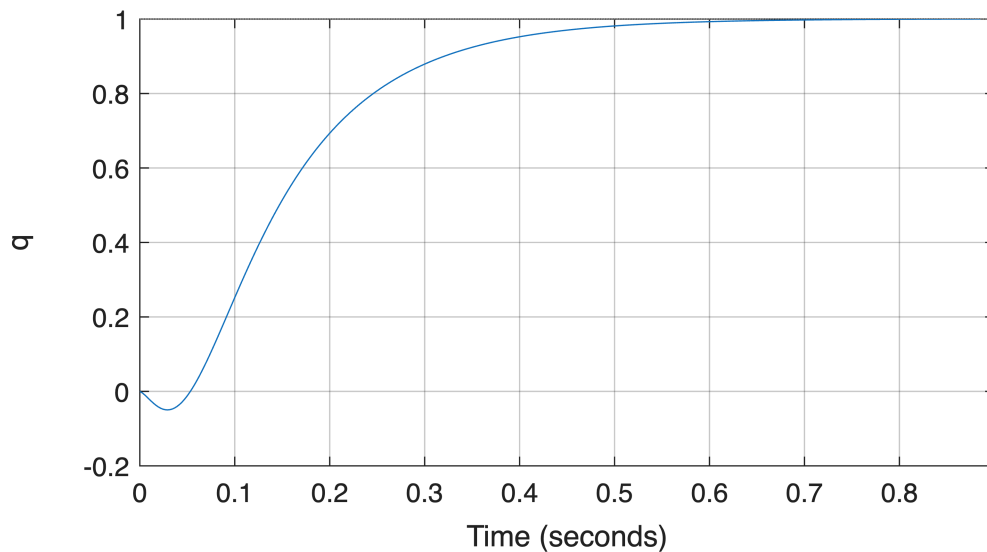
### Complementary sensitivity vs. requirement



### Time-domain simulations

```
% Step in pitch-rate command
figure; step(T); grid on;
title('Closed-loop step response:  $q_c \rightarrow q$ ');
ylabel('q');
```

### Closed-loop step response: $q_c \rightarrow q$



```
stepinfo(T)
```

ans = struct with fields:

```

RiseTime: 0.2464
TransientTime: 0.4862
SettlingTime: 0.4913
SettlingMin: 0.8999
SettlingMax: 1.0002
Overshoot: 0.0379
Undershoot: 4.9693
Peak: 1.0002
PeakTime: 0.9512

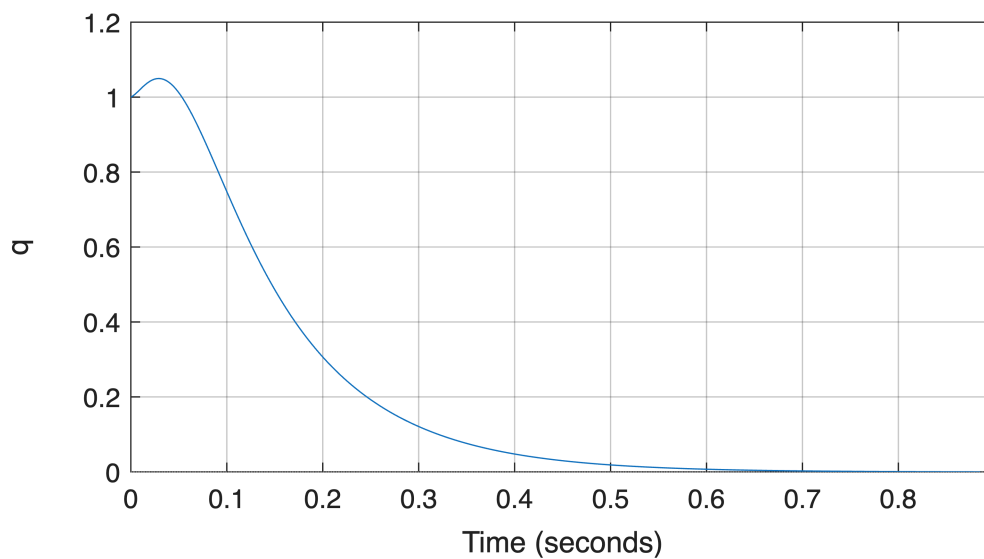
```

```

% Step in Disturbance at plant output
figure; step(S); grid on;
title('Response to output disturbance d \rightarrow q');
ylabel('q');

```

**Response to output disturbance  $d \rightarrow q$**

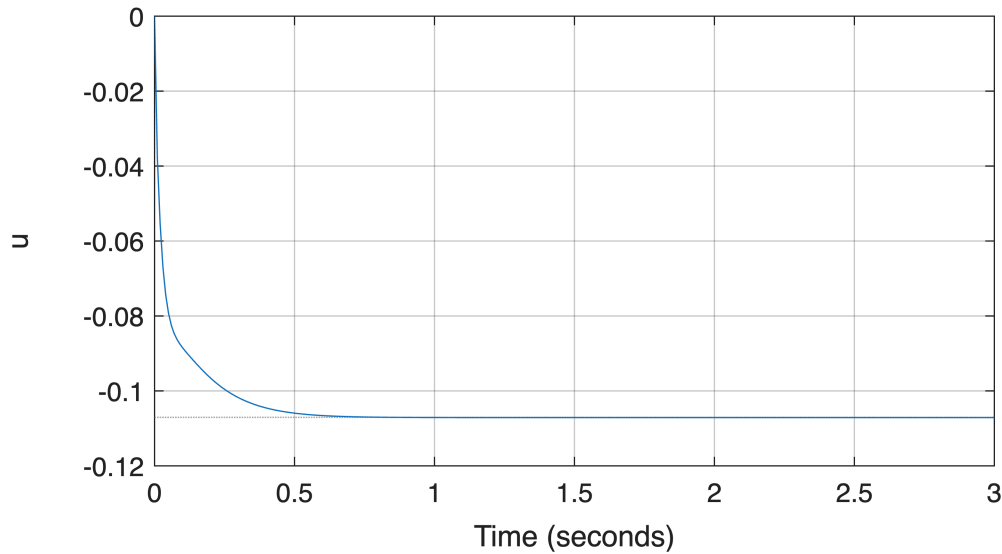


```

%% Control input
figure; step(Kh*S, 3); grid on;
title('Actuator response reference input r \rightarrow u');
ylabel('u');

```

### Actuator response reference input $r \rightarrow u$



## Robust Control Analysis

```
%% Add multiplicative uncertainty Wi
Wi = 0.5 * (s/4 + 1) / (s/25 + 1); %Shape Wi to encompass all uncertain
plants

% Variations for each parameters
Mde_grid = [Mde_min, Mde_nom, Mde_max];
Zw_grid = [Zw_min, Zw_nom, Zw_max];
wn_grid = [wn_min, wn_nom, wn_max];
zeta_grid = [zeta_min, zeta_nom, zeta_max];
tau_grid = [tau_min, tau_nom, tau_max];

% Frequency grid
w = logspace(-1, 2, 400); % 0.1–100 rad/s

% Nominal plant frequency response
G_nom_w = squeeze(freqresp(G, w));

figure; hold on; grid on;
title('Relative error for uncertainty set');
xlabel('Frequency (rad/s)');
ylabel('Relative error |(G_p - G)/G|');

for Mde_i = Mde_grid
    for Zw_i = Zw_grid
        for wn_i = wn_grid
            for zeta_i = zeta_grid
```



```

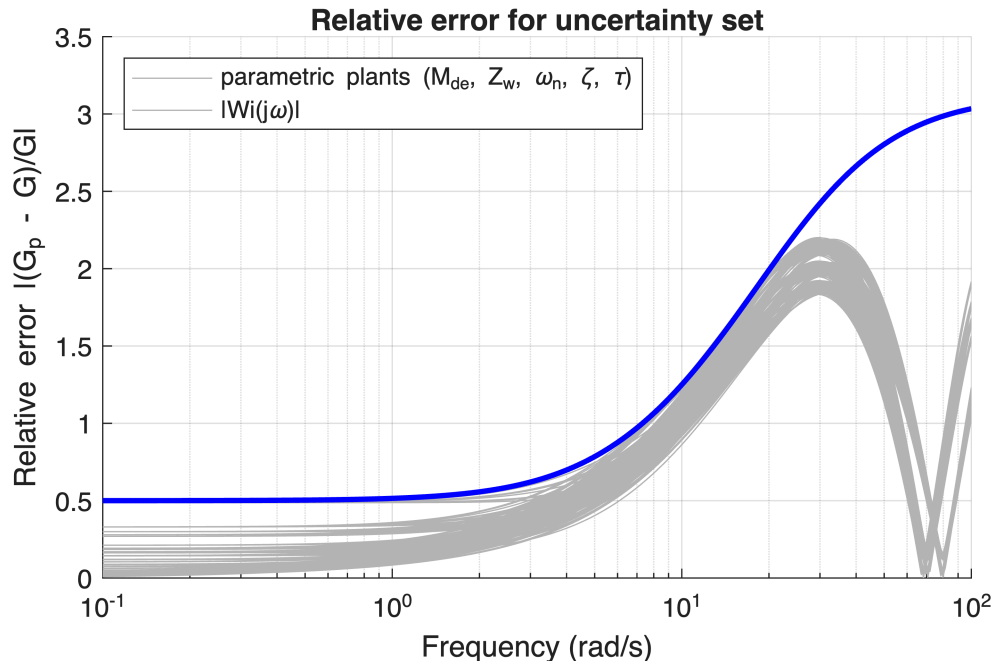
% Plant for this parameter combo
Gp0 = (Mde_i*s + Mde_i*Zw_i) / ...
      (s^2 + 2*zeta_i*wn_i*s + wn_i^2);
Gp0_w = squeeze(freqresp(Gp0, w)); % freq response of
delay-free part

% Sweep tau values
for tau_i = tau_grid
    delay_factor = exp(-1j * w * tau_i); % Pure delay
factor

    Gp_w = Gp0_w .* delay_factor'; % Full plant with delay
    E = abs((Gp_w - G_nom_w) ./ G_nom_w); % Relative error
    loglog(w, E, 'Color', [0.7 0.7 0.7]);
end
end
end
end

% Overlay |Wi(jw)|
Wi_w = squeeze(freqresp(Wi, w));
loglog(w, abs(Wi_w), 'b', 'LineWidth', 2);
set(gca, 'XScale', 'log');
legend('parametric plants (M_{de}, Z_w, \omega_n, \zeta, \tau)', ...
      '|Wi(j\omega)|', 'Location', 'NorthWest');

```



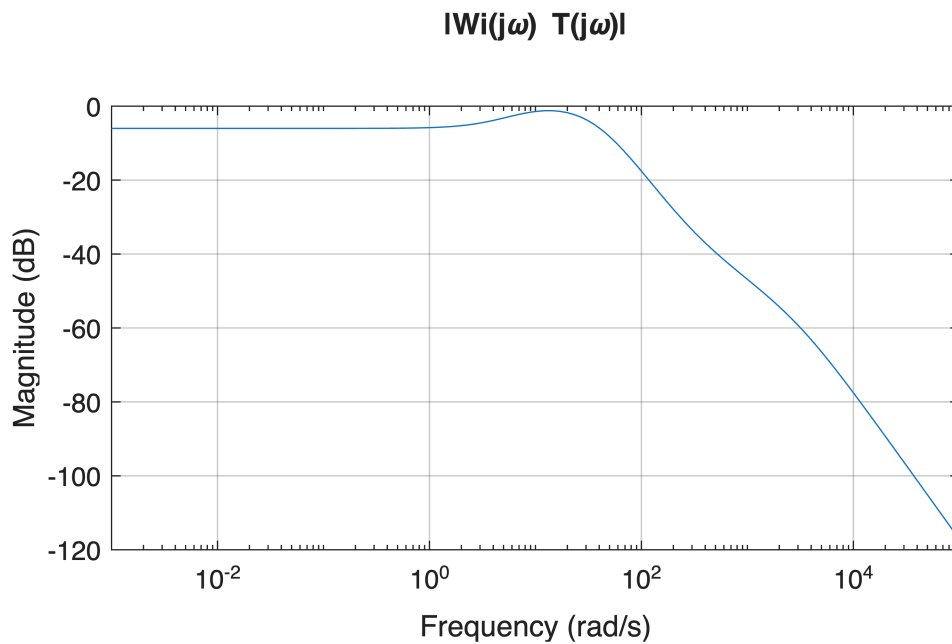
```

%% Check Wi * T < 1
WT = minreal(Wi * T);

figure; bodemag(WT); grid on;
title('|Wi(j\omega) T(j\omega)|');

```

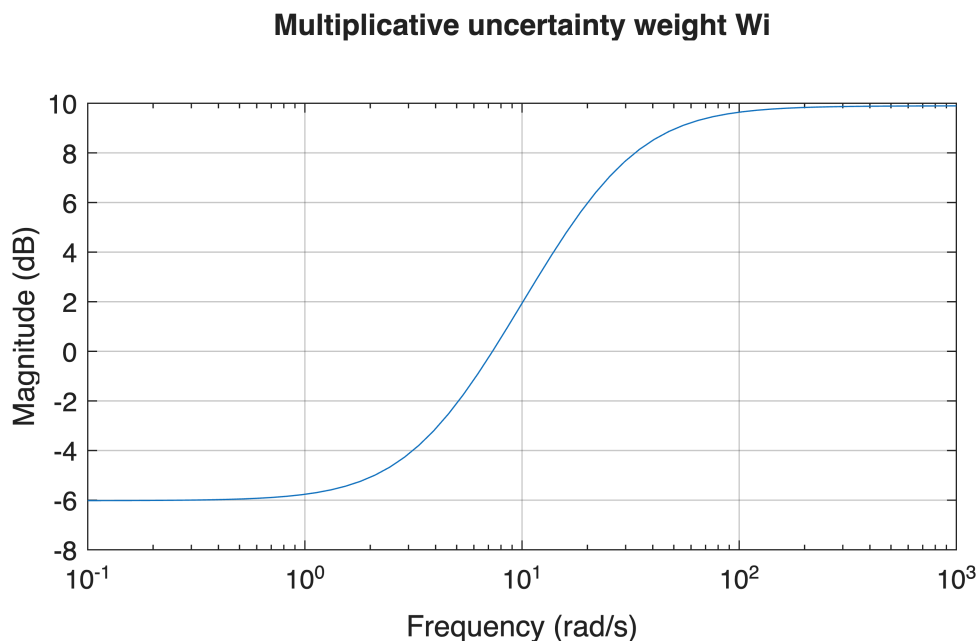
```
ylines(0, '--'); % 0 dB line (|WT| = 1);
```



```
gamma_WT = norm(WT, inf); % Check infinity norm of |Wi*T|
fprintf('||Wi * T||_inf = %.3f\n', gamma_WT);
```

```
||Wi * T||_inf = 0.870
```

```
% Wi Frequency Response
figure; bodemag(Wi); grid on;
title('Multiplicative uncertainty weight Wi');
```



```
% Normalized, unknown stable LTI block with ||Delta||_inf <= 1
Delta = ultidyn('Delta',[1 1]);
```

```

% Multiplicative output uncertainty:
G_unc = G * (1 + Wi * Delta);

% Robust stability analysis with uncertainty

% Closed-loop from reference to output with uncertain plant
CL_unc = feedback(G_unc*Kh, 1);

[stabmarg, destabunc, report_stab] = robuststab(CL_unc);

disp('Robust stability report:');

```

Robust stability report:

```
disp(report_stab);
```

```

System is robustly stable for the modeled uncertainty.
-- It can tolerate up to 115% of the modeled uncertainty.
-- There is a destabilizing perturbation amounting to 115% of the modeled uncertainty.
-- This perturbation causes an instability at the frequency 12.4 rad/seconds.
-- Sensitivity with respect to each uncertain element is:
    100% for Delta. Increasing Delta by 25% decreases the margin by 25%.

```

```
disp('Robust stability margin (lower bound):');
```

Robust stability margin (lower bound):

```
disp(stabmarg.LowerBound);
```

1.1512

## Monte-Carlo sampling of uncertain plants (step responses)

```

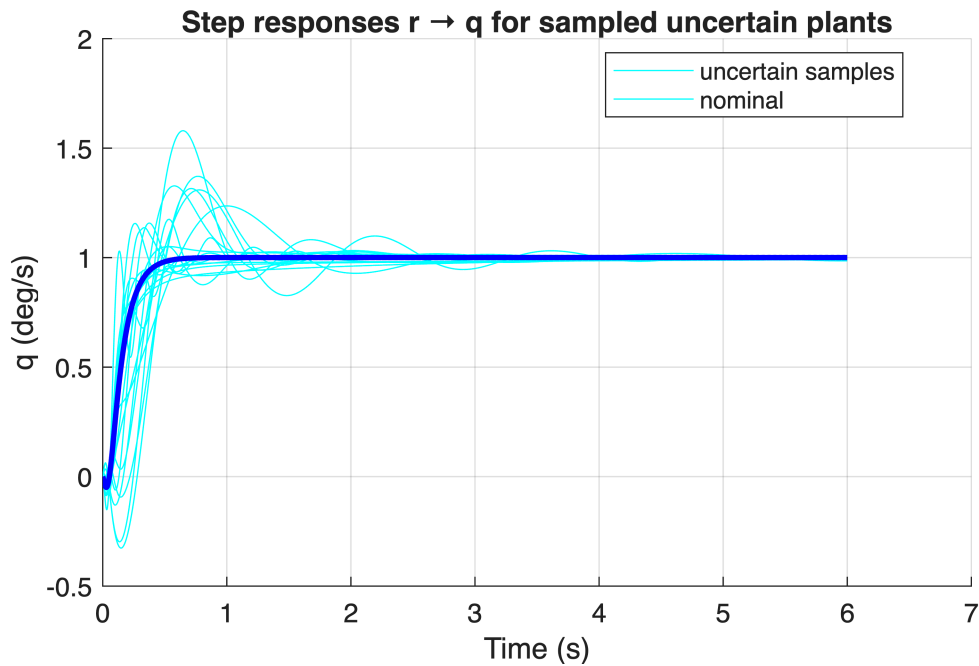
nsamples = 20;
tfinal    = 6;

figure; hold on; grid on;
title('Step responses r → q for sampled uncertain plants');
xlabel('Time (s)'); ylabel('q (deg/s)');

for k = 1:nsamples
    Gk = usample(G_unc); %Sample some random plants within the
    multiplicative uncertainty set
    CLk = feedback(Gk*Kh, 1);
    [y,t] = step(CLk, tfinal);
    plot(t, y, 'c','LineWidth', 0.5);
end

% Plot nominal response on top (thicker line)
[y_nom, t_nom] = step(T, tfinal);
plot(t_nom, y_nom, 'b', 'LineWidth', 2);
legend('uncertain samples','nominal','Location','Best');

```



## Frequency-domain view of uncertain loop

```
% Sample a few plants and plot L bode
figure; hold on;
title('Sensitivity function for sampled uncertain plants');
for k = 1:5
    Gk = usample(G_unc); %Sample some random plants within the
multiplicative uncertainty set
    Lk = minreal(Gk*Kh);
    bodemag(Lk, 'w');
end
```

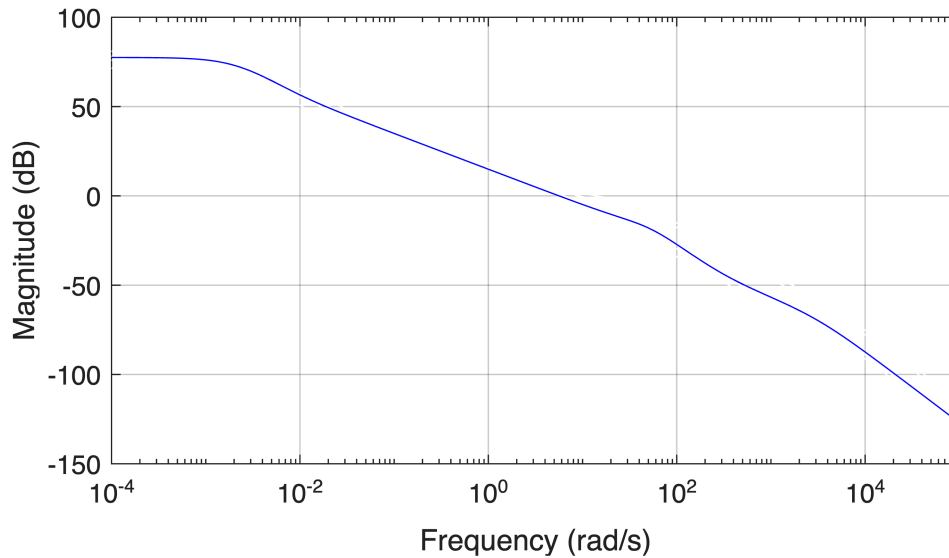
```
3 states removed.
3 states removed.
3 states removed.
3 states removed.
3 states removed.
```

```
L_nom = minreal(G*Kh);
```

```
3 states removed.
```

```
bodemag(L_nom, 'b'); % nominal plant
grid on;
```

## Bode Diagram



## Test controller on UAV

```
%% Discretize controller for 100 hz
Ts = 0.01; % 100 Hz
Kh_d = c2d(Kh, Ts, 'tustin');
disp('Discretized H_infinity controller');
```

Discretized H\_infinity controller

```
Kh_d %Load the discretized controller onto flight controller for testing
```

Kh\_d =

```
A =
      x1      x2      x3      x4      x5      x6
x1      1      2.896e-18  2.527e-18  2.159e-18 -9.199e-17 -5.498e-17
x2 -0.005927      1      0.009079 -0.02725 -0.007466  0.0003741
x3 -0.2432      0.0196      0.1726      0.1642      -2.104      -1.243
x4 -0.2929      0.02361      0.4487      -0.8023      -0.5709      -0.04383
x5 -0.04687      0.003777      0.07179      0.03163      0.9087      -0.007014
x6 -0.003749      0.0003022      0.005743      0.002531      0.1527      0.9994
```

```
B =
      u1
x1      0.02
x2 -5.927e-05
x3 -0.002432
x4 -0.002929
x5 -0.0004687
x6 -3.749e-05
```

```
C =
      x1      x2      x3      x4      x5      x6
y1 -2.371      0.1911      3.632      -10.9      -2.986      0.1496
```

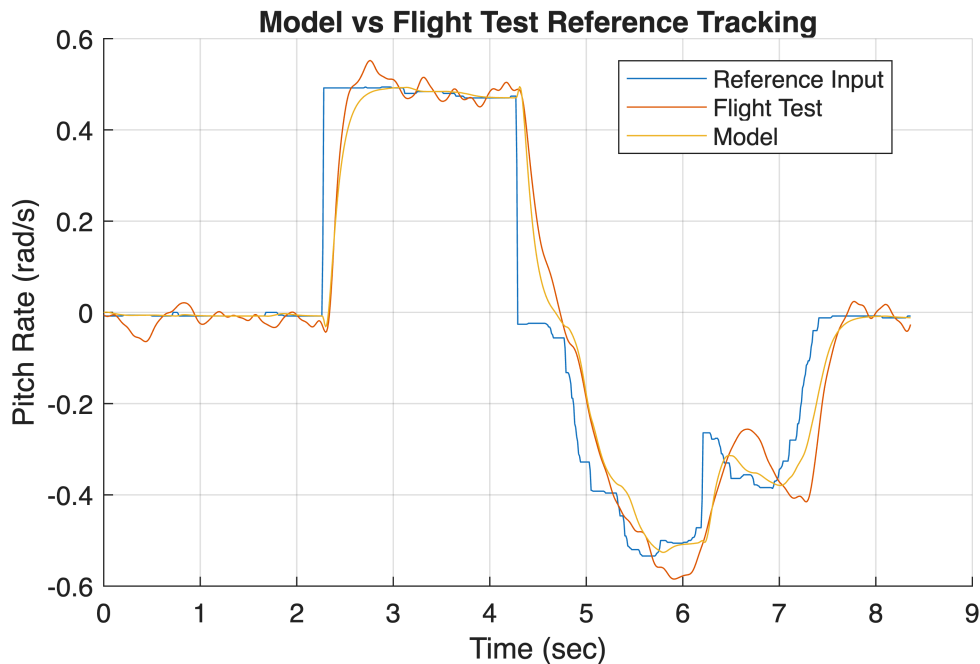
```
D =
```

u1  
y1 -0.02371

Sample time: 0.01 seconds  
Discrete-time state-space model.  
Model Properties

## Flight test step input time histories

```
flightData = load('P_CL_Step_M50D02_run2.mat');  
startIndex = 964;  
stopIndex = 1800;  
  
figure; hold on; grid on;  
  
time = flightData.time(startIndex:stopIndex);  
time = time - time(1);  
q_raw = flightData.q(startIndex:stopIndex);  
input = flightData.lnStkStm(startIndex:stopIndex);  
Fc = 5; %5 hz filter cutoff  
q_filt = lowpass(q_raw, Fc, 100);%Low pass filter measured pitch rate data  
  
% Simulated response  
q_sim = lsim(T,input,time);  
  
plot(time,input);  
plot(time,q_filt);  
plot(time,q_sim);  
legend('Reference Input', 'Flight Test', 'Model','Location','Best');  
xlabel('Time (sec)');  
ylabel('Pitch Rate (rad/s)');  
title('Model vs Flight Test Reference Tracking')
```



## Flight test frequency responses

```
load('PFWUAVCL_COM_ABCDE_ele_blo.mat'); %Import frequency response data
obtained from CIFER

w_cifer = freq(96:923); % Import frequency range (rad/s)

%mag_cifer_dB = mag2db(db2mag(mag(96:923))/2); %%% I DON'T KNOW WHERE THIS
FACTOR OF 2 CAME FROM!!! (BUT IT WORKS)
mag_cifer_dB=mag(96:923);
phase_cifer_deg = phase(96:923);

% Evaluate loop transfer function on the CIFER frequencies
[magL, phaseL] = bode(L, w_cifer);

magL = squeeze(magL);
phaseL = squeeze(phaseL);

magL_dB = 20*log10(magL);
phaseL_deg = phaseL-360; %Phase shift to align with CIFER

% Plot overlay
figure;

% Magnitude plot
subplot(2,1,1);
semilogx(w_cifer, magL_dB, 'b-', 'LineWidth', 1.5); hold on;
semilogx(w_cifer, mag_cifer_dB, 'ro', 'LineWidth', 1.5, 'MarkerSize', 3);
```

```

grid on;
ylabel('Magnitude (dB)');
legend('Model L(j\omega)', 'Flight Test', 'Location', 'Best');

% Phase plot
subplot(2,1,2);
semilogx(w_cifer, phaseL_deg, 'b-', 'LineWidth', 1.5); hold on;
semilogx(w_cifer, phase_cifer_deg, 'ro', 'LineWidth', 1.5, 'MarkerSize', 3);
grid on;
xlabel('\omega (rad/s)');
ylabel('Phase (deg)');
legend('Model L(j\omega)', 'Flight Test', 'Location', 'Best');
sgtitle('Nominal model vs. flight test identified loop transfer function');

```

## Nominal model vs. flight test identified loop transfer function

