

② Then the overall transformation for forward kinematics is:

$$H = H_n^0 = \begin{bmatrix} R_n^0 & \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \\ 0 & \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} \end{bmatrix}$$

and this H is computed from the "chain"

$$H_n^0 = T_n^0 = A_1(q_1) A_2(q_2) \dots A_n(q_n).$$

Denavit-Hartenberg (D-H) convention for forward kinematics

Each A_i is a product of 4 basic transformations:

$$A_i = \text{Rot}_{z, \theta_i} \text{Trans}_{z, d_i} \text{Trans}_{x, a_i} \text{Rot}_{x, \alpha_i}$$

$$= \begin{bmatrix} c\theta_i & -s\theta_i & 0 & 0 \\ s\theta_i & c\theta_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} I & \begin{bmatrix} 0 \\ 0 \\ d_i \end{bmatrix} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} I & \begin{bmatrix} a_i \\ 0 \\ 0 \end{bmatrix} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & c\alpha_i & -s\alpha_i & 0 \\ 0 & s\alpha_i & c\alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_i = \begin{bmatrix} c\theta_i & -s\theta_i c\alpha_i & s\theta_i s\alpha_i & a_i c\theta_i \\ s\theta_i & c\theta_i c\alpha_i & -c\theta_i s\alpha_i & a_i s\theta_i \\ 0 & s\alpha_i & c\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$\theta_i, a_i, d_i, \alpha_i \Rightarrow$ D-H parameters describing the geometry of link i .

③ D-H offers 4 parameters rather than 6 because of how we place the origin and axes of frame i w/r/t frame $i-1$. D-H construction properties:

(DH1) Axis x_i is perpendicular to axis z_0 . (for example)

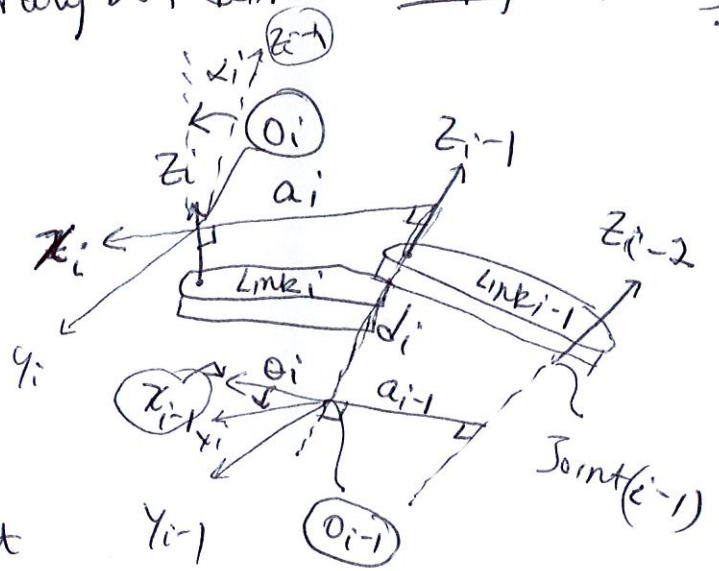
(DH2) Axis x_i intersects axis z_0 .

Coordinate frame assignment.

① Select base frame. (Arbitrary but define as simply as possible) (frame 0)

② Define axes to o_i . 3 cases. Each discussed below.

Case ① z_{i-1}, z_i not coplanar \Rightarrow define unique shortest segment from z_{i-1} to z_i as x_i axis. o_i is point where x_i, z_i intersect. y_i completes right-handed frame.



② z_{i-1} parallel to z_i : choose o_i anywhere on z_i ; extend x_i perpendicular to pass through o_i . y_i completes R.H.S. (typical: choose o_i s.t. normal passes through $o_{i-1} \Rightarrow d_i = 0$)

③ z_{i-1} intersects z_i : x_i is normal to the $z_{i-1}-z_i$ plane. o_i typically chosen at intersection point. $a_i = 0$.

①

Inverse Kinematics

Given a 4×4 homogeneous transformation

$$H = \begin{bmatrix} R & 0 \\ 0 & 1 \end{bmatrix} \in SE(3)$$

find one or more solutions of the equation

$$T_n^0(q_1, q_2, \dots, q_n) = H$$

where

$$T_n^0(q_1, q_2, \dots, q_n) = A_1(q_1) \dots A_n(q_n).$$

The equation for $T_n^0 = H$ represents

12 nonlinear equations

$$T_{ij}(q_1, \dots, q_n) = h_{ij}, \\ i=1,2,3, j=1,2,3,4.$$

Inverse kinematics is typically more

difficult than forward kinematics. we

could use a numerical solver (e.g. in Matlab) to solve these equations, but this would be slow embedded in a control loop and would offer little intuition.

Also, in cases with multiple solutions, a numerical solver would find only one with sensitivity to the initial guess.

Some manipulators can be designed with

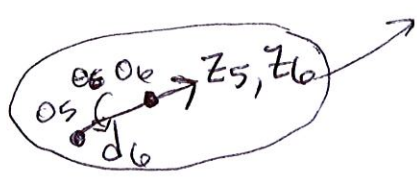
Kinematic decoupling: inverse position kinematics
v. inverse orientation ".

(2) Suppose a revolute arm has 6 DOF. The first three position the "origin" of a "wrist frame" and the last three specify its orientation. (wrist \hat{w} where $\hat{z}_3, \hat{z}_4, \hat{z}_5$ intersect!)

Let $R = R_6^0(q_1, \dots, q_6)$, $o = o_6^0(o_1, \dots, o_6)$.

Let o_c be the wrist frame (sometimes, not always, $o_c = o_3$).

Then $o = o_c + d_6 R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$ so $\boxed{o_c^0 = o - d_6 R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}}$



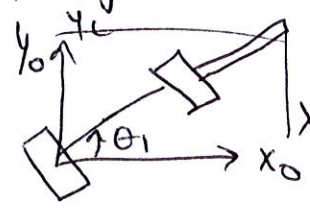
Now note that $R = R_3^0 R_6^3$.

R_3^0 is computed from $o_c = \begin{bmatrix} x_c \\ y_c \\ z_c \end{bmatrix} = \begin{bmatrix} o_x - d_6 r_{13} \\ o_y - d_6 r_{23} \\ o_z - d_6 r_{33} \end{bmatrix}$

$R_6^3 = (R_3^0)^{-1} R = (R_3^0)^T R$

We can also use geometry! The "articulated manipulator" shown in Spong Sec 3.3.4 provides good insight on solving for inverse kinematics geometrically

(1) Project wrist center onto x_0-y_0 plane

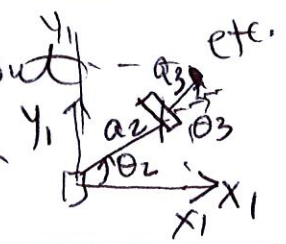


$x_c \Rightarrow \theta_1 = \text{Atan2}(x_c, y_c)$

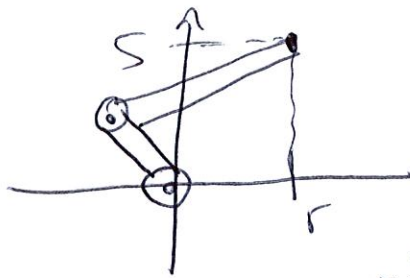
use atan2 to assure correct quadrant



(Spong) shows a case with offsets. without offsets, one can then look @ planar manipulator etc.

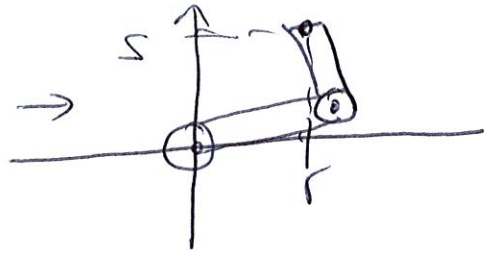


③ Left Configuration

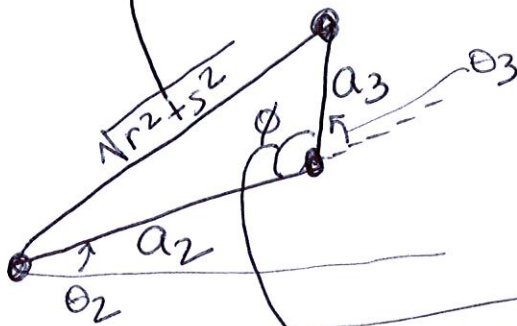
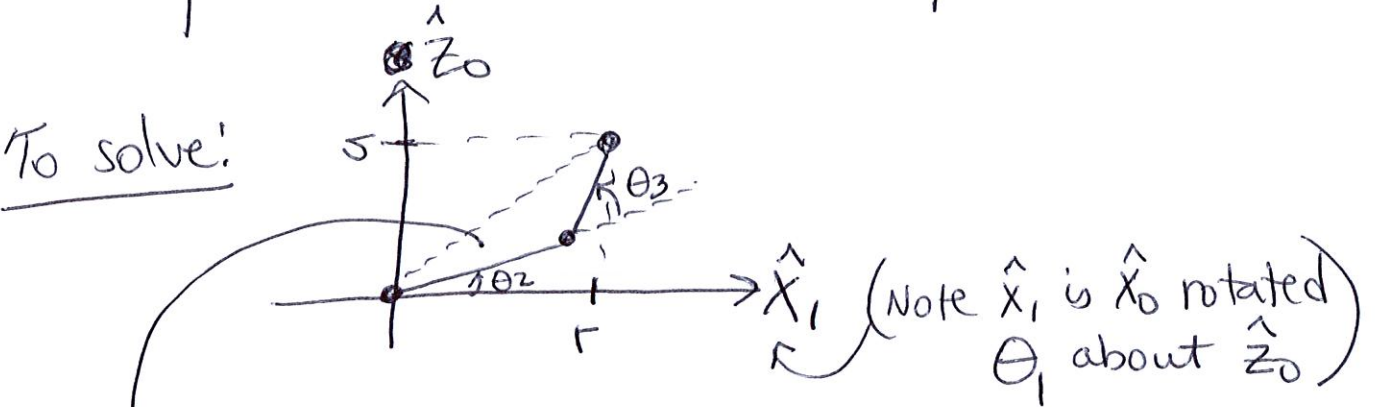


two I.K. solutions to choose from!

Right configuration



To solve:



$$\phi = \pi - \theta_3$$

$$\phi = \tan^{-1}\left(\frac{s}{r}\right) = \text{atan2}(r, s).$$

- Solve for ϕ from the Law of Cosines.
- Then solve for θ_3 .
- Then solve for θ_2 .

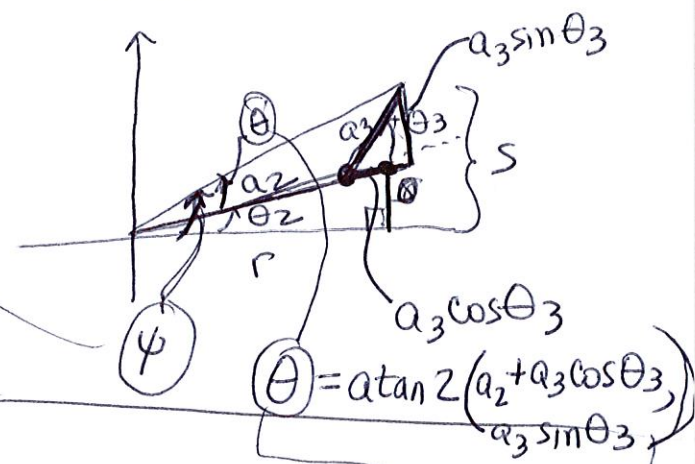
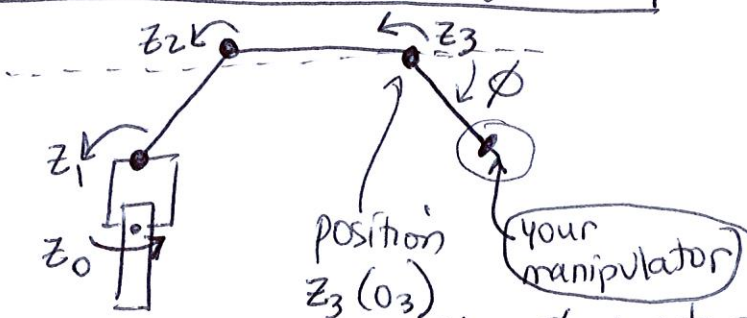


Diagram in the assignment:



w/r/t the horizontal plane.

s.t. rotating ϕ about z_3 gives the illustrated "wrist orientation"