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A Magnetic Microsystem on a Chip

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**Abstract**

A magnetic microsystem has been designed on a chip to demonstrate the improved performance of an integrated Hall element. The major deficiencies of relatively poor performance of an integrated Hall element has been upgraded through the use of a high efficiency, integrated micro coil, which has been optimized using multiphysics finite element tools. An extensive characterization of the integrated Hall element has allowed the creation of the most complete simulation model, which is usable both in a high level system simulator as well as in a detailed circuit simulation. All results were verified by measuring the fabricated ASIC.

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*Keywords:* magnetic microsystem; self calibation of magnetic microsystem; integrated micro coil

# Introduction

Magnetic Microsystems are used in various applications where the magnetic field carries information about the current, the magnetic force, or the position. In all cases the required measurement needs to be extremely accurate and independent of any environmental condition.

For current measurements the typical requirement is a linearity range extending over five or six decades. The required linearization and absolute accuracy for a magnetic force measurement is in the range of 0.1% /1/, and for the position or rotation angle a 12-bit resolution is a typical specification /2/. There are two or three

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possible sensor types of magnetic field available for integration on a chip. There are: Hall-effect sensors, Hall elements near field micro coils, and large, integrated coils for AC field generation /3/. The Hall element and near field micro coil are investigated in the paper.

# Integrated Hall element

The key parameters of an integrated Hall element are the following:

* + Sensitivity. It is well known that the sensitivity of a Hall element is poor compared to MR or GMR sensors, which prevent many designers from using them in their magnetic circuits. However, we will demonstrate that in most cases it is possible to effectively compensate for this deficiency. The typical sensitivity of an integrated Hall element is around 100μV/1mAmT (100V/AT) in a standard CMOS process, while its noise is about 10nV/¥Hz. This means that the equivalent noise is §10nT¥Hz at 1mA Hall element bias current. The achievable dynamic range in a 1Hz frequency bandwidth is over 100dB.
  + An important parameter is also the temperature coefficient of the Hall element sensitivity, which is highly non-linear and very process dependent. Unfortunately, the sensitivity is also dependent on the mechanical stress caused by the plastic package. There are few possibilities of converting such an inaccurate sensor element into a high precision sensor system. The most promising approach is an alive sensor sensitivity calibration using a near field micro coil.
  + Last but not least, the residual offset of the Hall element is an issue to be considered. The root cause of it is the asymmetry of the four terminal devices, which can be modeled as a resistor bridge. A well-known spinning technique /4/ is the way to minimize the offset. Less known is a requirement that the spinning needs to rotate around a fixed voltage potential of a central sensor point, as shown in Figure 1.

Vdd

Hall element



VHall

R

+

Vcenter −

R

Vb – variable bias current

Vss

Fig.1. Central geometrical point of Hall element stabilized during spinning at various Hall element bias currents

Finally, the remaining offset voltage is trimmed with both a DC value and its temperature coefficient. With such arrangements the achievable offset can be reached in the range of ±10μT. An important issue to design a Hall-element sensor is to have an extensive and well characterized simulation model. The complexity of the model is seen in Figure 2.

R

U D



2

k6I

2

5 off

5 off

rdl

k1Bint

k2Bext

k2Bext k1Bint

rl

voff

k6I2

vs

Off

VCR

roff

rcoil

k6I2

hOut

L

6

BIn

rm

hIn

k6I2

rdr

k2Bext

rr

k2Bext k1Bint

rur

k5Voff

VCR

k5Voff

VCR

k6I2 k6I2

k1Bint

VCR

VCR

VCR

VCR

ru

rd

VCR

k V

VCR

VCR

VCR

VCR

VCR

VCR

VCR

VCR

vm

rul

k V

k6I

k I2

Fig.2. Model elements of integrated Hall element for 0.35μm mixed signal CMOS technology

As can be seen, the model is very complex with 20 voltage controlled resistors, 8 voltage controlled current sources, 8 current controlled current sources, 7 measuring resistors, 3 voltage sources for current measuring and four non-linear and voltage-dependent well resistors.

# Near-field micro coil

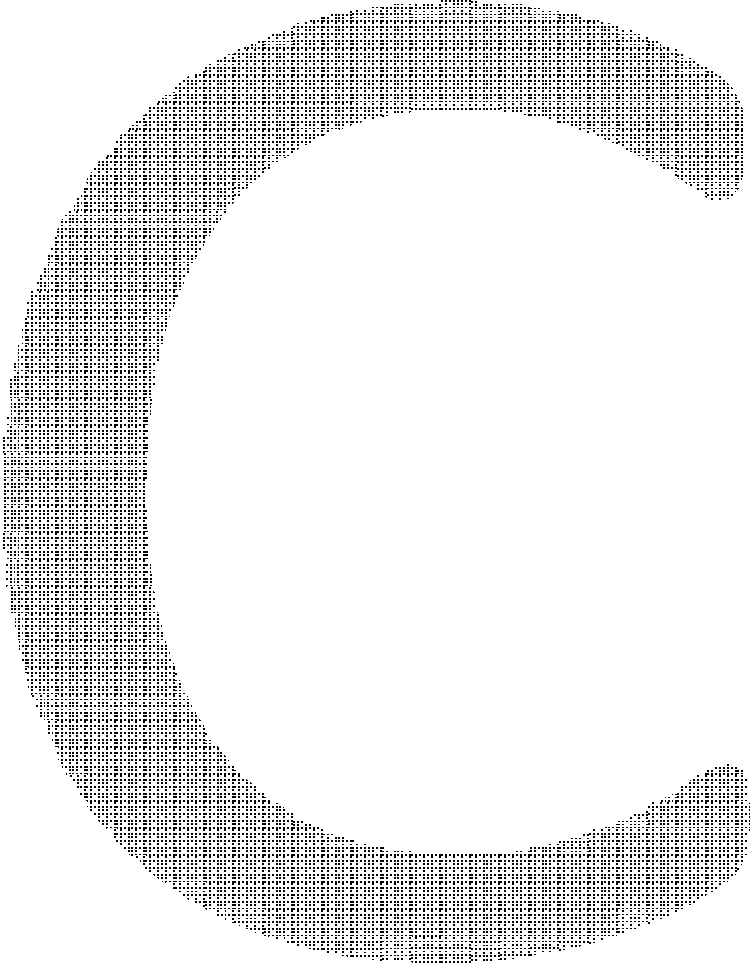
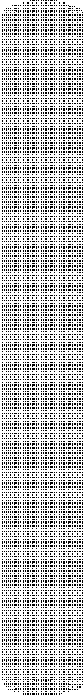
The key function of near-field micro coil is to generate a relative strong reference magnetic field on board to be used for either online or offline Hall element sensitivity adjustment. The offline adjustment can be performed either at wafer sorting or final testing of the device by applying a reference current to the coil and measuring and trimming the Hall element response to the desired value. The application of this method is simple, however it does not cover the temperature effect of the sensitivity, nor the sensitivity variation due to package pressure effect.

It is advisable to use a bipolar coil current for the magnetic field excitation and observing the response as a difference in both coil current directions as follows:

*Vout + Voff - (- Vout + Voff ) = 2 Vout*

which eliminates the offset voltage and any external magnetic field which is not in phase of the coil current alternation. Figure 3 shows the application of this principle.

External resistor Rext is used as accurate voltage to current conversion. The voltage is adjustable according to the evaluation circuit as shown in figure 3

A study of the efficiency of the reference micro coil has been performed to maximize the generated magnetic field versus the coil current.

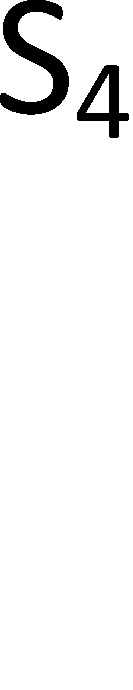
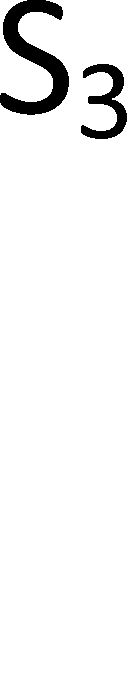
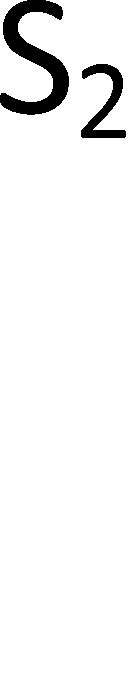
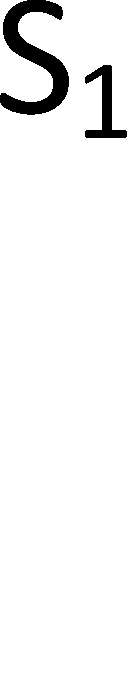
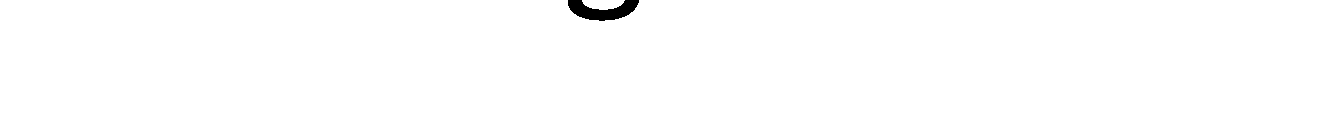
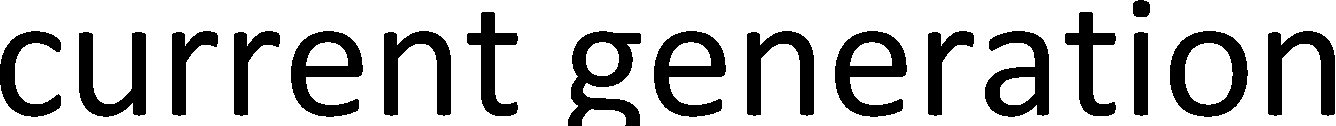
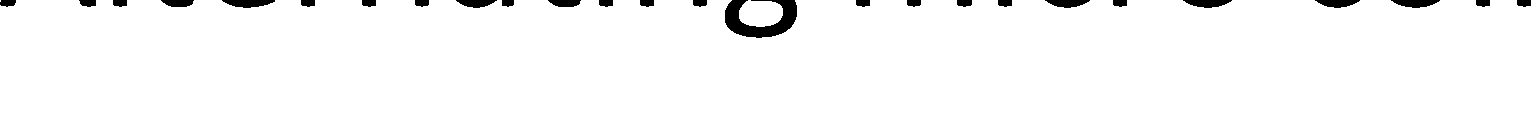
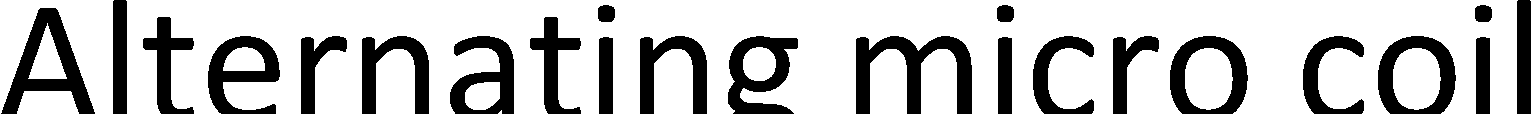
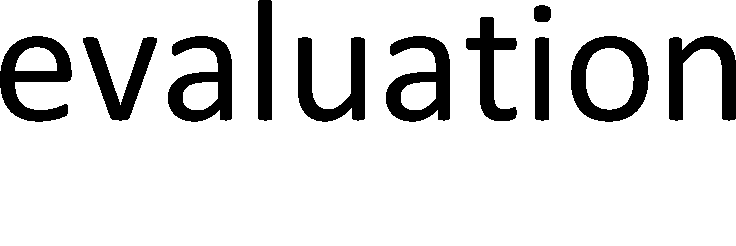
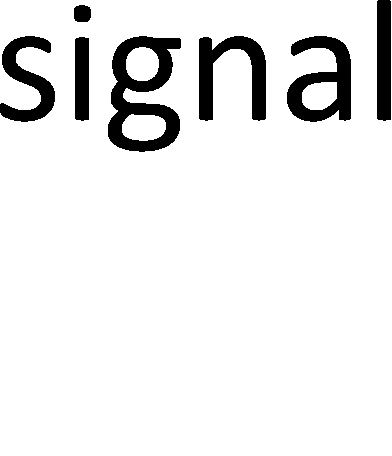
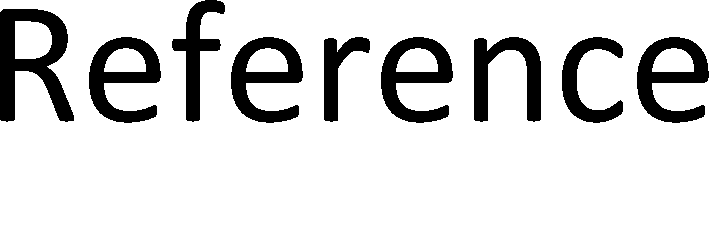
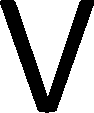
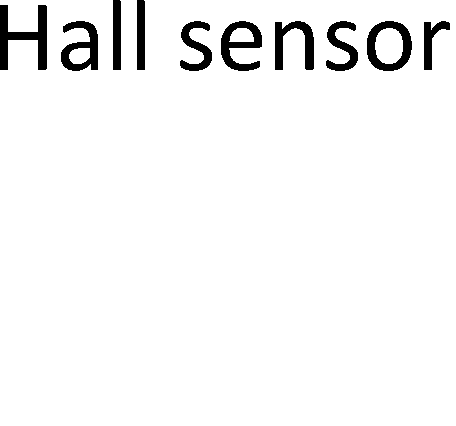
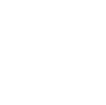
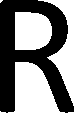
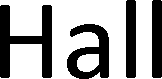
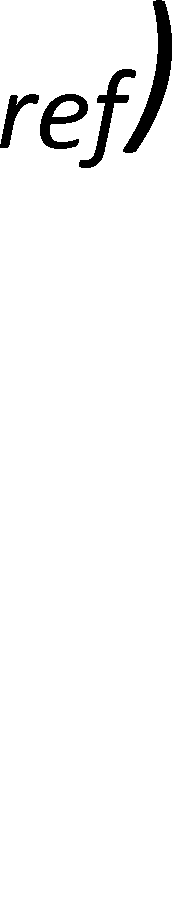
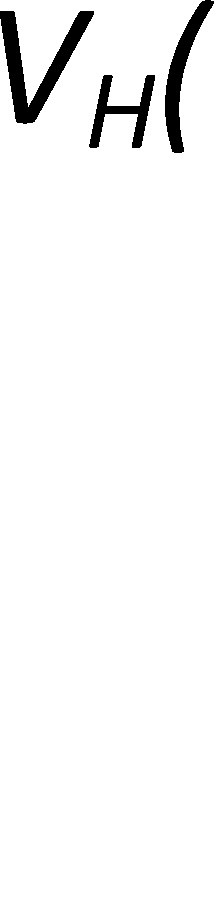
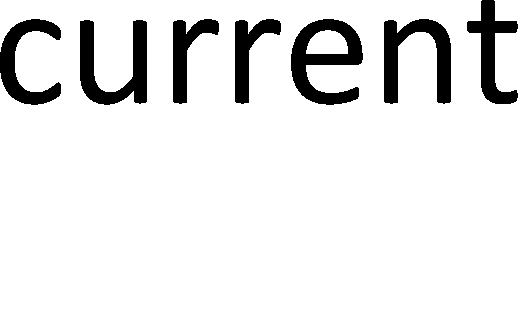
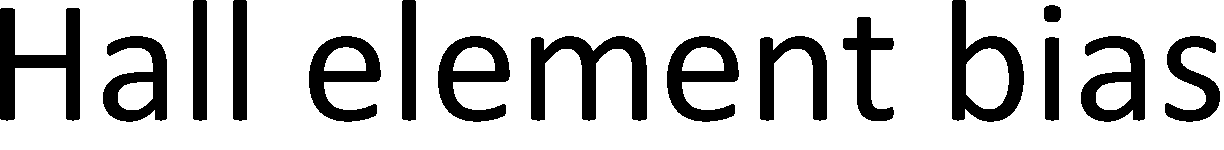


Fig.3. Bipolar reference coil current generation

The most important parameters affecting the efficiency parameters are: numbers of coil turns per metal level, the number of metal levels, the coil area, and its position to the Hall element. The area of the Hall element has been reduced to 14μm by 14μm as shown in Figure 4, and was optimized for the 0.35 CMOS mixed signal technology /5/.

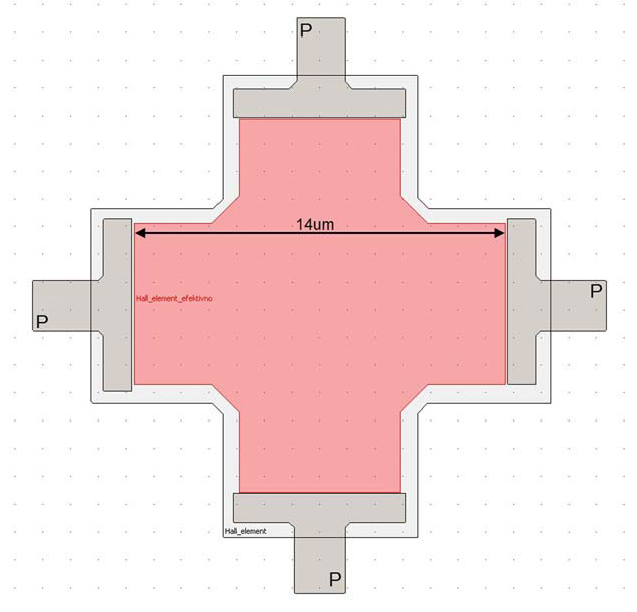


Fig.4. Hall element layout in 0,35um CMOS technology

In Figure 5a the 3D 12-turn micro coil layout is presented, and in Figure 5b a micro photograph of the element is shown. The four terminal Hall element is upgraded to the six terminal providing an on-board reference magnetic field generation of 5mT at a 10mA coil current. This is a decent level for a reference field, which cannot be compromised by noise even if a very short reference pulses would be applied. When using a bipolar reference pulse the problem of offset voltage is eliminated.

Furthermore, the reference magnetic field should not interfere with normal measurements, so it is necessary to perform the calibration at the higher frequency, which is outside the operating bandwidth of the system. A good candidate is a spinning frequency, which is usually up to two decades above the operating corner frequency of the magnetic system. If the reference current pulse starts in the first spinning cycle, it would contribute a positive reference voltage to the output, so the output voltage would be the sum of signal voltage *Vsig* and the reference voltage *Vref*. The resulting output voltage *Vout* is:

*Vout = Vsig + Vref.*

In the second spinning cycle the reference current is reversed and also the *Vout* is inverted and sampled to a negative input of the summator, so the residual output voltage *Vres* is:

*Vres = Vsig + Vref – (-Vsig + Vref).*

Therefore, *Vres* is not disturbed by the reference signal:

*Vres = Vsig + Vsig.*

The signal of the reference voltage in both spinning cycles is on the contrary sampled to a summator, so the residual voltage *Vrefres* of the reference voltage is:

*Vrefres = Vsig + Vref + (-Vsig + Vref) = Vref + Vref.*

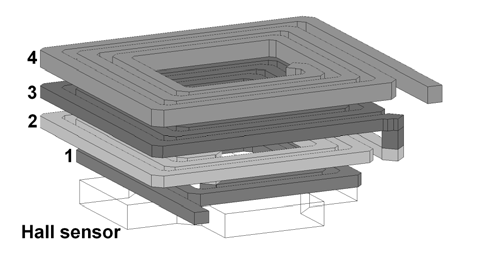


Fig.5a. 3D layout of the micro coil

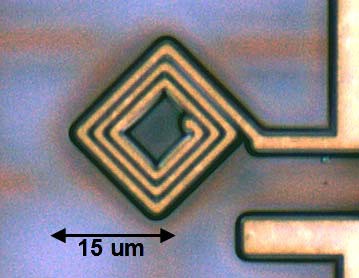
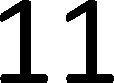
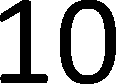
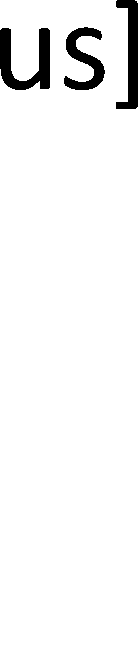
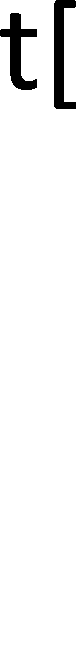
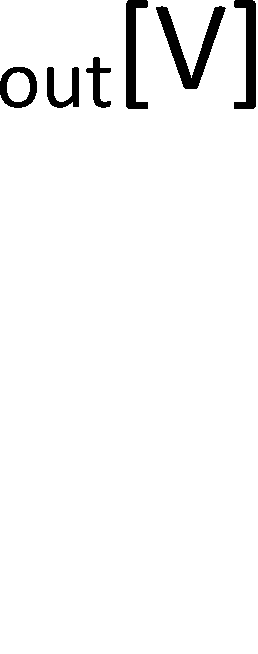
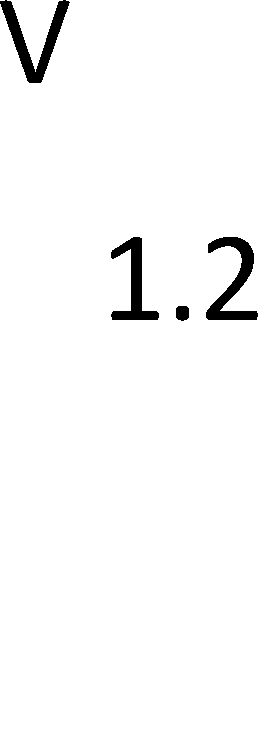
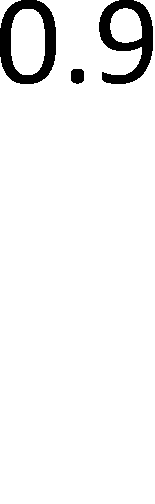
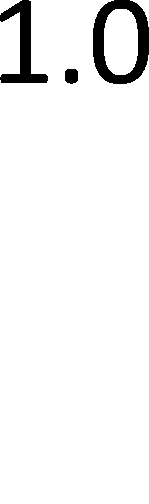
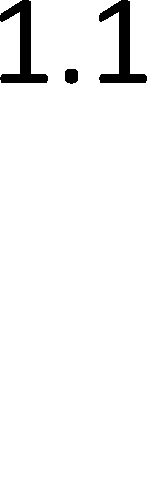


Fig.5b. Photomicrograph of the fabricated micro coil

This is an elegant, out of band generation of the reference voltage without disturbing the normal operation. The error signal is produced by comparing the residual reference voltage to a required voltage and simply adjusting the sensitivity of the system to an accurate level by changing the Hall element bias current. A high level model has been designed and the result of simulation is shown in Figure 6. The measured results match very well with the simulation, proving that it is an effective way to calibrate the sensor on-line, without disturbing the normal operation.

The red line is the preset reference voltage to be reached at reference field, generated by the micro coil. The blue line is the actual signal value reaching the required value after the self-regulation is completed. The step shows the digital or discrete gain settings. Therefore the output is alternating around the final value. This alternation frequency is outside of the system bandwidth and it is easily filtered out.

Fig.6. Automatic gain regulation of the sensor using the on-line calibration algorithm



# Conclusions

An accurate magnetic system on chip has been designed, simulated, fabricated, and characterized using what’s known as a six terminal Hall sensor with an incorporated near field micro coil. The measured results confirmed the concept.

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