

數位濾波器設計與模擬 主題：可調式分數延遲 FIR 濾波器之設計 31 用途文 [U P2] 內容：

A New Criterion for the Design of Variable Fractional-Delay FIR Digital Filters

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it is reasonable to choose the coefficients of $G_m(z)$ to be symmetric for even M and antisymmetric for odd M , and obviously, $I = N/2$. In this paper, only even N is used, and the case for odd N can be extended in a similar manner. Notice that the first subfilter $G_0(z)$ is designed to approximate $e^{-j(N/2)\omega}$, so $h(n, 0) = \delta(n - (N/2))$. Hence, the frequency response of (7) can be written as

$$\begin{aligned} H(e^{j\omega}, p) &= e^{-j\frac{N}{2}\omega} \left[1 + \sum_{m=1}^{M_c} \sum_{n=0}^{N/2} a(n, m)p^{2m} \cos(n\omega) \right. \\ &\quad \left. + j \sum_{m=1}^{M_s} \sum_{n=1}^{N/2} b(n, m)p^{2m-1} \sin(n\omega) \right] \end{aligned} \quad (10)$$

where (11a)–(11c) are shown at the bottom of the page. Defining

$$\mathbf{a} = \left[a(0, 1), \dots, a\left(\frac{N}{2}, 1\right), \dots, \right. \quad (12a)$$

$$a(0, M_c), \dots, a\left(\frac{N}{2}, M_c\right) \Big]^T$$

$$\mathbf{b} = \left[b(1, 1), \dots, b\left(\frac{N}{2}, 1\right), \dots, \right. \quad (12b)$$

$$b(1, M_s), \dots, b\left(\frac{N}{2}, M_s\right) \Big]^T$$

$$\mathbf{c}(\omega, p) = \left[p^2, \dots, p^2 \cos\left(\frac{N}{2}\omega\right), \dots, p^{2M_c}, \dots, \right. \quad (12c)$$

$$p^{2M_c} \cos\left(\frac{N}{2}\omega\right) \Big]^T$$

$$\mathbf{s}(\omega, p) = \left[p \sin(\omega), \dots, p \sin\left(\frac{N}{2}\omega\right), \dots, \right. \quad (12d)$$

$$p^{2M_s-1} \sin(\omega), \dots, p^{2M_s-1} \sin\left(\frac{N}{2}\omega\right) \Big]^T.$$

Obviously, (7) can be implemented by the Farrow structure [7], [15].

Equation (4) can be further represented by

$$H_d(\omega, p) = e^{-jI\omega} \sum_{m=0}^{\infty} \frac{(-jp\omega)^m}{m!} \cong \sum_{m=0}^M \left(\frac{(-j\omega)^m}{m!} e^{-jI\omega} \right) p^m \quad (9)$$

for sufficiently large M . Comparing (7) and (9), it can be found that the frequency response of $G_m(z)$ is used inherently to approximate $((-j\omega)^m/m!)e^{-jI\omega}$ for $0 \leq m \leq M$. Therefore,

$$\begin{cases} M_c = M_s = \frac{M}{2}, & M: \text{even} \\ M_c + 1 = M_s = \frac{M+1}{2}, & M: \text{odd} \end{cases} \quad (11a)$$

$$a(n, m) = \begin{cases} h\left(\frac{N}{2}, 2m\right), & n = 0; 1 \leq m \leq M_c \\ 2h\left(\frac{N}{2} - n, 2m\right) = 2h\left(\frac{N}{2} + n, 2m\right), & 1 \leq n \leq \frac{N}{2}; 1 \leq m \leq M_c \end{cases} \quad (11b)$$

$$b(n, m) = 2h\left(\frac{N}{2} - n, 2m - 1\right) = -2h\left(\frac{N}{2} + n, 2m - 1\right), \quad 1 \leq n \leq \frac{N}{2}; \quad 1 \leq m \leq M_s \quad (11c)$$

$$H(e^{j\omega}, p) = e^{-j\frac{N}{2}\omega} [1 + \mathbf{a}^T \mathbf{c}(\omega, p) + j\mathbf{b}^T \mathbf{s}(\omega, p)] \quad (13)$$

where the superscript T denotes the transpose operator. The conventional objective error function for designing a VFD FIR filter is given by

$$e_c(\mathbf{a}, \mathbf{b}) = \int_{-0.5}^{0.5} \int_{-\omega_p}^{\omega_p} W(\omega) |H_d(\omega, p) - H(e^{j\omega}, p)|^2 d\omega dp$$

$$\begin{aligned}
&= \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) |\cos(p\omega) - j \sin(p\omega)| - 1 \\
&\quad - a^T c(\omega, p) - j b^T s(\omega, p) |^2 d\omega dp \\
&= e_c(a) + e_c(b)
\end{aligned} \tag{14}$$

where $W(\omega)$ is a weighting function

$$e_c(a) = \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) (\cos(p\omega) - 1 - a^T c(\omega, p))^2 d\omega dp \tag{15a}$$

$$\begin{aligned}
e_c(b) &= \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) (\sin(p\omega) + b^T s(\omega, p))^2 d\omega dp \\
&= s_b + r_b^T b + b^T Q_b b
\end{aligned} \tag{15b}$$

in which

$$s_a = \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) (\cos(p\omega) - 1)^2 d\omega dp \tag{16a}$$

$$\begin{aligned}
r_a &= -2 \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) (\cos(p\omega) - 1) c(\omega, p) d\omega dp \\
Q_a &= \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) c(\omega, p) c^T(\omega, p) d\omega dp
\end{aligned} \tag{16b}$$

$$s_b = 2 \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) \sin^2(p\omega) d\omega dp \tag{16c}$$

$$r_b = \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) s(\omega, p) s^T(\omega, p) d\omega dp. \tag{16d}$$

$$\begin{aligned}
Q_b &= \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) s(\omega, p) c^T(\omega, p) d\omega dp. \\
&\quad \text{which yield}
\end{aligned} \tag{16e}$$

$$Q_b = \int_{-0.5}^{0.5} \int_0^{\omega_p} W(\omega) c(\omega, p) s^T(\omega, p) d\omega dp. \tag{16f}$$

For LS design $W(\omega) = 1$ and by applying the technique in [22], the elements in r_a , Q_a , r_b , and Q_b can be represented in closed form as (17a) and (17b), shown at the bottom of the page, where $(x \bmod y)$ denotes the remainder when integer x is divided by integer y , and $\lfloor u \rfloor$ denotes the largest integer that is less than or equal to real number u . In (17), K must be chosen large enough as in [22], and $K = 10$ is used in this paper.

Once r_a , Q_a , r_b , and Q_b are obtained, the optimal solutions in the LS sense can be achieved by differentiating (14) with respect to a and b , respectively, and then setting the results to zero as follows:

$$\frac{\partial e_c(a, b)}{\partial a} = \frac{\partial e_c(a)}{\partial a} = r_a + 2Q_a a = 0 \tag{18a}$$

$$\frac{\partial e_c(a, b)}{\partial b} = \frac{\partial e_c(b)}{\partial b} = r_b + 2Q_b b = 0 \tag{18b}$$

in which

$$a = -\frac{1}{2} Q_a^{-1} r_a \tag{19a}$$

$$b = -\frac{1}{2} Q_b^{-1} r_b. \tag{19b}$$

which yield

$$\begin{cases} r_a(i) = -4 \sum_{k=1}^K \frac{(-1)^k}{(2k)!} \frac{0.5^{2m+2k+1}}{2m+2k+1} \int_0^{\omega_p} \omega^{2k} \cos(n\omega) d\omega \\ Q_a(i, l) = \frac{0.5^{2m+2\hat{n}+1}}{2m+2\hat{n}+1} \left(\frac{\sin((n-\hat{n})\omega_p)}{n-\hat{n}} + \frac{\sin((n+\hat{n})\omega_p)}{n+\hat{n}} \right) \\ 0 \leq i, l \leq (\frac{N}{2} + 1) M_c - 1, \quad n = (i \bmod \frac{N}{2} + 1), \quad m = \lfloor \frac{i}{N/2+1} \rfloor + 1 \\ \hat{n} = (l \bmod \frac{N}{2} + 1), \quad \hat{m} = \lfloor \frac{l}{N/2+1} \rfloor + 1 \end{cases} \tag{17a}$$

$$\begin{cases} r_b(i) = 4 \sum_{k=0}^K \frac{(-1)^k}{(2k+1)!} \frac{0.5^{2m+2k+1}}{2m+2k+1} \int_0^{\omega_p} \omega^{2k+1} \sin(n\omega) d\omega \\ Q_b(i, l) = \frac{0.5^{2m+2\hat{n}-1}}{2m+2\hat{n}-1} \left(\frac{\sin((n-\hat{n})\omega_p)}{n-\hat{n}} - \frac{\sin((n+\hat{n})\omega_p)}{n+\hat{n}} \right) \\ 0 \leq i, l \leq \frac{NM_s}{2} - 1, \quad n = (i \bmod \frac{N}{2}) + 1, \quad m = \lfloor \frac{i}{N/2} \rfloor + 1 \\ \hat{n} = (l \bmod \frac{N}{2}) + 1, \quad \hat{m} = \lfloor \frac{l}{N/2} \rfloor + 1 \end{cases} \tag{17b}$$

由式(17)：譯音上所提及之統計方法，大都為整數單位 (X^2) Type I 及 Type II linear-phase FIR filters。其應用主為之精神為可以採取凱茲信號間之任何位元傳輸。

Type I 及 Type II linear-phase FIR filters 之系統，本單元所要敘述之 Type II 為 FIR 濾波器，且可利用其延遲時序關係為任一整數位元傳輸之 FIR 濾波器。其應用主為之精神為可以採取凱茲信號間之任何位元傳輸。

複合內容原理推導及說明：

理想系統之頻率響應：

$$H_d(\omega, p) = e^{-j(I+p)\omega} \quad |w| \leq wp, \quad -0.5 \leq p \leq 0.5$$

I : a prescribed mean group delay

可調式 FIR 濾波器：

$$H(z, p) = \sum_{n=0}^N h_n(p) z^{-n} \quad p \text{為外部分之參數}$$

$$h_n(p) = \sum_{m=0}^M h(n, m)p^m$$

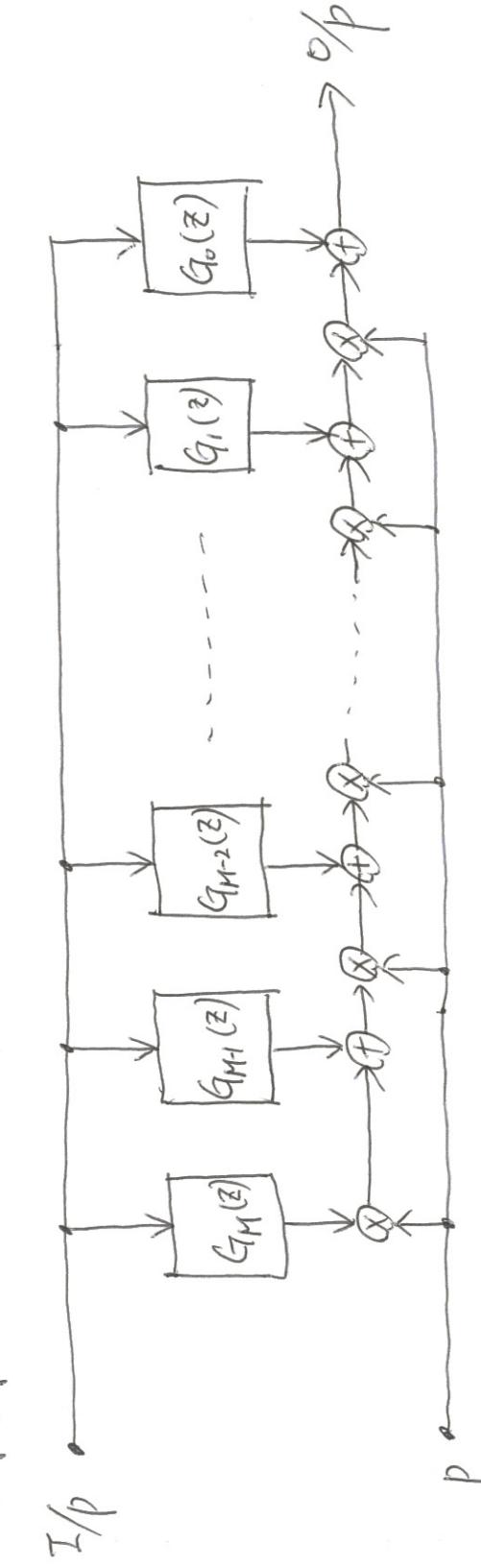
$$H(z, p) = \sum_{n=0}^N \sum_{m=0}^M h(n, m)p^m z^{-n} = \sum_{m=0}^M \left(\sum_{n=0}^N h(n, m)z^{-n} \right) p^m$$

$$\therefore G_m(z) = \sum_{n=0}^N h(n, m)z^{-n}$$

$$\Rightarrow H(z, p) = \sum_{m=0}^M G_m(z)p^m$$

$$= G_0(z) + G_1(z)p + G_2(z)p^2 + \dots + G_M(z)p^M$$

結構圖：



$G_0(z), G_1(z), \dots, G_M(z)$ 一般稱之為子濾波器 (subfilter).

各子濾波器扮演之角色：

$$H_d(w, p) = e^{-jIw} \sum_{m=0}^M \frac{(-j\omega)^m}{m!} e^{-jmw} \sum_{n=0}^N h(n, m) e^{-jnw} \approx \underbrace{\left[\sum_{m=0}^M \frac{(-j\omega)^m}{m!} e^{-jmw} \right] p^m}_{\text{e}^{-jPw} \text{之奉勤}} \underbrace{\text{層開式}}_{\text{approach}} \rightarrow e^{-jIw}$$

e^{-jPw} 之奉勤

層開式

$$m=0 \quad G_0(e^{j\omega}) \quad \text{approach} \rightarrow e^{-jIw}$$

$$\begin{aligned} & \parallel \\ & \sum_{n=0}^N h(n, 0) e^{-jnw} \end{aligned} \quad \text{C} \gamma \beta - \text{pure delay } I \in \mathbb{Z} \text{ 級}$$

$$\Rightarrow h(n, 0) = \delta(n - \frac{N}{2})$$

$$m: \text{even} \quad G_m(e^{j\omega}) \xrightarrow{\text{approach}} \frac{(-j)^m}{m!} e^{-j\omega} = (-1)^{\frac{m}{2}} \frac{\omega^m}{m!} e^{-j\omega}$$

||

$$\sum_{n=0}^N h(n, m) e^{-jn\omega} = e^{-j\frac{N\omega}{2}} \sum_{n=0}^{\frac{N}{2}} a(n, \frac{m}{2}) \cos(n\omega)$$

(Type I Subfilter)

$$m: \text{odd} \quad G_m(e^{j\omega}) \xrightarrow{\text{approach}} \frac{(-j)^m}{m!} e^{-j\omega} = (-j)^m \frac{\omega^m}{m!} e^{-j\omega}$$

$$\begin{aligned} & \sum_{n=0}^N h(n, m) e^{-jn\omega} \\ &= e^{-j\frac{N\omega}{2}} j^{\frac{N}{2}} \sum_{n=1}^{\frac{N}{2}} b(n, \frac{m+1}{2}) \sin(n\omega) \end{aligned}$$

(Type III Subfilter)

整体滤波器之频率响应：

$$H(e^{j\omega}, p) = e^{-j\frac{N\omega}{2}} \left[1 + \sum_{m=1}^{\frac{M_c}{2}} \sum_{n=0}^{\frac{N}{2}} a(n, m) p^{2m} \cos(n\omega) + j \sum_{m=1}^{\frac{M_s}{2}} \sum_{n=1}^{\frac{N}{2}} b(n, m) p^{2m-1} \sin(n\omega) \right]$$

$$= e^{-j\frac{N\omega}{2}} \left[1 + a^T(\omega, p) + j b^T S(\omega, p) \right]^T$$

$$a = [a(0, 1), \dots, a(\frac{N}{2}, 1), \dots, a(0, M_c), \dots, a(\frac{N}{2}, M_c)]^T$$

$$b = [b(1, 1), \dots, b(\frac{N}{2}, 1), \dots, -b(1, M_s), \dots, b(\frac{N}{2}, M_s)]^T$$

$$c(\omega, p) = \left[p^2, \dots, p^2 \cos(\frac{N}{2}\omega), \dots, p^{2M_c}, \dots, p^{2M_c} \cos(\frac{N}{2}\omega) \right]^T$$

$$S(\omega, p) = \left[p \sin(\omega), \dots, p \sin(\frac{N}{2}\omega), \dots, p^{2M_s-1} \sin(\omega), \dots, p^{2M_s-1} \sin(\frac{N}{2}\omega) \right]^T$$

$$\begin{cases} M_c = M_s = \frac{M}{2} & M: \text{even} \\ M_c + 1 = M_s = \frac{M+1}{2} & M: \text{odd} \end{cases}$$

$$a(n, m) = \begin{cases} h(\frac{N}{2}, 2m) & n=0 \\ 2h(\frac{N}{2}-n, 2m) & 1 \leq n \leq \frac{N}{2} \\ 2h(\frac{N}{2}-n, 2m-1) & 1 \leq n \leq \frac{N}{2} \end{cases} \quad 1 \leq m \leq M_c$$

$$b(n, m) = 2h(\frac{N}{2}-n, 2m-1) = -2h(\frac{N}{2}+n, 2m-1) \quad 1 \leq n \leq \frac{N}{2} \quad 1 \leq m \leq M_s$$

補題的證

$$e(a, b) = \int_{-0.5}^{0.5} \int_0^{\omega p} |H_a(\omega, p) - H(c, p)|^2 d\omega dp$$

$$\begin{aligned} &= \int_{-0.5}^{0.5} \int_0^{\omega p} |\cos(p\omega) - j \sin(p\omega) - |a^T c(\omega, p) - j b^T s(\omega, p)||^2 d\omega dp \\ &= \int_{-0.5}^{0.5} \int_0^{\omega p} (\cos(p\omega) - |a^T c(\omega, p)|^2 d\omega dp + \underbrace{\int_{-0.5}^{0.5} \int_0^{\omega p} (\sin(p\omega) + b^T s(\omega, p))^2 d\omega dp}_{\text{因此項僅對 } a \text{ 有影響}} \end{aligned}$$

因此項僅對 a 有影響

$$= e(a) + e(b)$$

$$e(a) = S_a + R_a a + a^T Q_a a$$

$$e(b) = S_b + R_b b + b^T Q_b b$$

$$S_a = \int_{-0.5}^{0.5} \int_0^{\omega p} (\cos(p\omega) - 1)^2 d\omega dp$$

$$R_a = -2 \int_{-0.5}^{0.5} \int_0^{\omega p} (\cos(p\omega) - 1) c(\omega, p) d\omega dp$$

$$Q_a = \int_{-0.5}^{0.5} \int_0^{\omega p} c(\omega, p) c^T(\omega, p) d\omega dp$$

$$\frac{\partial e(a, b)}{\partial a} = \frac{\partial e(a)}{\partial a} = R_a + 2 Q_a a = 0 \Rightarrow a = -\frac{1}{2} Q_a^{-1} R_a$$

$$\frac{\partial e(a, b)}{\partial b} = \frac{\partial e(b)}{\partial b} = R_b + 2 Q_b b = 0 \Rightarrow b = -\frac{1}{2} Q_b^{-1} R_b$$

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金工行之行

% Design of variable fractional-delay FIR digital filters
%
clear all;
clc;
N=50;
M=7;
wp=0.9*pi;
pointw=200;
pointp=60;
%
j=0+i;
NH=N/2;

if mod(M,2)==0

Mc=M/2;

Ms=M/2;

else

Mc=(M-1)/2;

Ms=(M+1)/2;

end

nma=(NH+1)*Mc;

nmb=NH*Ms;

del taw=wp/pointw;

del tap=1/pointp;

point=(pointw+1)*(pointp+1);

%

ra=zeros(nma,1);

Qa=zeros(nma,nma);

for iw=0:pointw

w=iw*del taw;

for ip=0:pointp

p=-0.5+ip*del tap;

c=zeros(nma,1);

for ic=0:nma-1

n=mod(ic,NH+1);

m=floor(ic/(NH+1))+1;

c(ic+1)=p^(2*m)*cos(n*w);

end

ra=ra-2*(cos(p*w)-1)*c;

Qa=Qa+c*c';

end

rb=wp*ra/point;

Qa=wp*Qa/point;

a=-0.5*inv(Qa)*ra;

%

rb=zeros(nmb,1);

Qb=zeros(nmb,nmb);

for iw=0:pointw

w=iw*del taw;

for ip=0:pointp

p=-0.5+ip*del tap;

s=zeros(nmb,1);

for is=0:nmb-1

n=mod(is,NH)+1;

m=floor(is/NH)+1;

s(is+1)=p^(2*m-1)*sin(n*w);

end

rb=rb+2*sin(p*w)*s;

Qb=Qb+s*s';

end

rb=wp*rb/point;

Qb=wp*Qb/point;

b=-0.5*inv(Qb)*rb;

%

%

```

a2=reshape(a,NH+1,Mc);
b2=reshape(b,NH,Ms);
h=zeros(N+1,M+1);
h(NH+1,1)=1;
for im=1:Mc
    h(NH+1,2*im+1)=a2(1,im);
    h(1:NH,2*im)=0.5*b2(NH:-1:2,im);
    h(NH+2:N+1,2*im)=0.5*a2(NH+1:-1:2,im);
    h(NH+2:N+1,2*im+1)=0.5*a2(2:NH+1,im);
end
for im=1:Ms
    h(1:NH,2*im)=0.5*b2(NH:-1:1,im);
    h(NH+2:N+1,2*im)=-0.5*b2(1:NH,im);
end
%
%
MR=zeros(pointw+1,pointp+1);
GD=zeros(pointw+1,pointp+1);
for ip=0:pointp
    p=-0.5+ip*deltap;
    hnp=h(:,1);
    for im=1:M
        hnp=hnp+h(:,im+1)*p^im;
    end
    MR(:,ip+1)=abs(freqz(hnp,1,0:deltaw:wp));
    GD(:,ip+1)=grpdelay(hnp,1,0:deltaw:wp);
end
for iw=0:pointw
    YY(iw+1,:)=0.5:deltap:0.5;
end
%
subplot(1,2,1);
plot3(XX,YY,MR);
axis([0,wp/pi,-0.5,0.5,0,1.1]);
xlabel('Frequency');
ylabel('Variable p');
zlabel('Magnitude response');
subplot(1,2,2);
plot3(XX,YY,GD);
axis([0,wp/pi,-0.5,0.5,NH-0.5,NH+0.5]);
xlabel('Frequency');
ylabel('Variable p');
zlabel('Group-delay response');
pause;
%
% magnitude responses of subfilters
%
for im=0:M
    MRS=abs(freqz(h(:,im+1),1,0:pi/200:pi));
    subplot(3,3,im+1);
    plot(0:1/200:1,MRS);
    axis([0,1,0,5]);
end
}

```

執行結果如下圖上圖

執行結果如下圖下圖

執行結果：

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