

1 Announcements

Next Friday will be a lecture by Prof. Hansen.

2 Permanent and Transitory Shocks

We illustrate them using the VAR example:

$$\begin{aligned} X_{t+1} &= AX_t + BW_{t+1} \\ Y_{t+1} - Y_t &= \nu + D^T X_t + F^T W_{t+1} \end{aligned}$$

where A is stable and $X_0 = 0$. X_{t+1} is a $k \times 1$ vector; Y_t is a scalar.

▷ In class, we saw the following decomposition:

$$Y_t = Y_0 + \nu t + \underbrace{\sum_{j=1}^t \left(F^T + D^T (I - A)^{-1} B \right) W_j - D^T (I - A)^{-1} X_t}_{= \text{martingale component}}$$

▷ Using the lag operator, rewrite the process as

$$(I - AL) X_t = BW_t$$

and plug this back into the decomposition:

$$Y_t = Y_0 + \nu t + \sum_{j=1}^t \left(F^T + D^T (I - A)^{-1} B \right) W_j - D^T (I - A)^{-1} \underbrace{(I - AL)^{-1} BW_t}_{(1)}$$

Note that (1) is

$$(I + AL + A^2 L^2 + \dots) BW_t = BW_t + ABW_{t-1} + A^2 BW_{t-2} + \dots$$

so we have

$$Y_t = Y_0 + \nu t + \sum_{j=1}^t \left(F^T + D^T (I - A)^{-1} B \right) W_j - D^T (I - A)^{-1} \sum_{j=0}^{t-1} A^j BW_{t-j}$$

▷ Assume $W_1 = 0$ and $W_t = 0, \forall t \geq 2$. Then

$$Y_t = Y_0 + \nu t + \underbrace{\left(F^T + D^T (I - A)^{-1} B \right) W_1}_{\text{permanent part}} - \underbrace{D^T (I - A)^{-1} A^{t-1} BW_1}_{\text{transient part}}$$

The transiency comes from the decay that comes from A^{t-1} .

* Permanent part is just a linear combination of W_1 .

* If W_1 is *orthogonal* to $F^T + D^T (I - A)^{-1} B$, we call it the *transitory* shock.

* If W_1 is *parallel* to $F^T + D^T (I - A)^{-1} B$, we call it the *permanent* shock.

▷ For a transitory impulse response, the impulse should just decay exponentially.

▷ For all shocks that are not transitory, the impulse response will converge to

▷ The permanent shock can be found by fixing the magnitude of the impulse response and finding the W_1 that gives the largest steady-state.

* Even if the shock is entirely parallel, you still have a convergence over time to the steady state.

3 Small Shock Approximation, Lombardo and Uhlig (2018)

3.1 Setup

Consider the following setup:

$$\begin{aligned} X_{t+1} &= AX_t + BW_{t+1} \\ y_{t+1} - y_t &= \nu + D^T X_t + F^T W_{t+1} \end{aligned}$$

where $y_t := \log Y_t$. We will illustrate how the previous technique can be applied in a macroeconomic framework.

▷ Technology: transfer 1 unit time t good to $\exp(\rho)$ units of time $t + 1$ good. The $\{Y_t\}$ s are the fruits.

▷ The feasibility constraint:

$$K_{t+1} + C_t = \exp(\rho) K_t + Y_t$$

This is equivalent to Prof. Stokey's formulation:

$$K_{t+1} + C_t = A_t K_t + (1 - \delta) K_t$$

▷ The RA maximizes

$$\mathbb{E} \left[\sum_{j=0}^{\infty} \exp(-\delta j) \log C_{t+j} \right]$$

▷ The Euler Equation:

$$U'(C_t) = \mathbb{E} [\exp(\rho) \exp(-\delta) u'(C_{t+1}) | X_t]$$

which yields

$$1 = \mathbb{E} \left[\exp(-\delta + \rho) \frac{C_t}{C_{t+1}} | X_t \right]$$

3.2 Solving for Response in Consumption

We want to linearize the $\mathbb{E}[\cdot]$.

▷ To solve this, define

$$\hat{K}_t = \frac{K_t}{Y_t}, \quad \hat{C}_t = \log C_t - \log Y_t$$

and re-write the feasibility constraint:

$$\hat{K}_{t+1} \exp(\log Y_{t+1} - \log Y_t) + \exp(\hat{C}_t) - \exp(\rho) \hat{K}_t - 1 = 0$$

and the Euler equation:

$$\exp(-\delta + \rho) \mathbb{E} \left[\exp \left(- \left(\hat{C}_{t+1} - \hat{C}_t \right) - (\log Y_{t+1} - \log Y_t) \right) | X_t \right] - 1 = 0$$

Essentially, we are detrending to get the stationary distribution.

- ▷ Now consider perturbing the system by q i.e. changing the exposure of Y_t s to the stochastic component:

$$\begin{aligned} X_{t+1} &= AX_t + BW_{t+1} \\ y_{t+1}(q) - y_t(q) &= \nu + [D^T X_t + F^T W_{t+1}] q \end{aligned}$$

This allows us to reformulate the previous variables as a function of q

$$\begin{aligned} [1] : \hat{K}_{t+1}(q) \exp(\log Y_{t+1}(q) - \log Y_t(q)) + \exp(\hat{C}_t(q)) - \exp(\rho) \hat{K}_t(q) - 1 &= 0 \\ [2] : \exp(-\delta + \rho) \mathbb{E} \left[\exp \left(- \left(\hat{C}_{t+1}(q) - \hat{C}_t(q) \right) - (\log Y_{t+1}(q) - \log Y_t(q)) \right) | X_t \right] - 1 &= 0 \end{aligned}$$

- ▷ Consider a Taylor expansion around 0:

$$\begin{aligned} \hat{C}_t(q) &\approx \hat{C}_t(0) + \hat{C}'_t(q) \\ \hat{K}_{t+1}(q) &\approx \hat{K}_{t+1}(0) + \hat{K}'_{t+1}(q) \end{aligned}$$

The reason we do it around 0 is because $\hat{C}_t(0)$ results in a deterministic fruits process $\{Y_t\}$ and thus it is very easy to compute.

- ▷ Note that the individual components above are processes, not numbers. Similarly to the macro class, we want to do

$$\hat{C}_t = C(X_t, \hat{K}_t), \quad \hat{K}_{t+1} = K(X_t, \hat{K}_t)$$

where X_t is the exogenous state and K_t is the endogenous state.

Now define a new function

$$F_1(\hat{K}_{t+1}(q), \hat{C}_t(q), \hat{K}_t(q), \Delta y_{t+1}(q)) \equiv [1]$$

where $\Delta y_{t+1}(q) = y_{t+1}(q) - y_t(q)$

- ▷ Since F_1 is equal to zero for all q , we have

$$F_1(q) \approx F_1|_{q=0} + q \frac{\partial F_1}{\partial q}|_{q=0} \approx 0$$

as well. Similar argument holds for $F_2 = 0$:

$$F_2(q) \approx F_2|_{q=0} + q \frac{\partial F_2}{\partial q}|_{q=0} \approx 0$$

- ▷ Obtaining $F_1|_{q=0}$: Making the assumption that $\delta = \rho - \nu$, the economy has a steady state of:

$$\hat{C}_t(0) = 0, \quad \hat{K}_{t+1}(0) = 0$$

which yields

$$\begin{aligned} \log C_t - \log Y_t = 0 &\Rightarrow C_t = Y_t \\ \hat{K}_{t+1}(0) = \frac{K_{t+1}}{Y_{t+1}} &= 0 \end{aligned}$$

so you consume fruit everyday and save nothing.

▷ Obtaining $\partial F_1 / \partial q$:

$$\frac{\partial F_1}{\partial q} \Big|_{q=0} = \hat{C}'_t(0) \frac{\partial F_1}{\partial \hat{C}_t} \Big|_{q=0} + \hat{K}'_{t+1}(0) \frac{\partial F_1}{\partial \hat{K}_{t+1}} \Big|_{q=0} + \hat{K}'_t(0) \frac{\partial F_1}{\partial \hat{K}_t} \Big|_{q=0} + \Delta y'_{t+1}(0) \frac{\partial F_1}{\partial \Delta y_{t+1}} \Big|_{q=0} = 0$$

* Note that we already know

$$\frac{\partial F_1}{\partial \hat{C}_t} \left(\hat{K}_{t+1}(q), \hat{C}_t(q), \hat{K}_t(q), \Delta y_{t+1}(q) \right) \Big|_{q=0}$$

since we've computed the relevant quantities evaluated at zero in the previous step. The similar argument follows for the other derivatives.

* Deriving analogously for F_2 , we have two linear equations of $\hat{K}'_{t+1}(0)$ and $\hat{C}'_t(0)$.

* The term with $\Delta y'_{t+1}$ is good since

$$\frac{\partial F_1}{\partial \Delta y_{t+1}} \Big|_{q=0} = 0$$

and the term vanishes.

* The term with $\hat{K}'_t(0)$ is also good since the derivative is simply $\exp(\rho)$.

Going through a similar process with F_2 , we obtain:

$$[3] : \hat{K}_{t+1}^1 \exp(\nu) + \hat{C}_t^1 - \exp(\rho) \hat{K}_t^1 = 0$$

$$[4] : \mathbb{E} \left[\left(\hat{C}_{t+1}^1 - \hat{C}_t^1 \right) + \Delta y'_{t+1} \right] = 0$$

To solve this, guess and verify:

$$\hat{C}_t^1 := C'_t(q=0) = M X_t + \Gamma_K \hat{K}_t^1$$

▷ Plug this into [3] and express \hat{K}_{t+1} as a function of \hat{K}_t and \hat{X}_t .

▷ Plug this into [4] and replace X_{t+1} as a function of X_t and solve for M and Γ_K .

The resulting solution is

$$\begin{aligned} \hat{C}_t^1 &= \lambda D' (I - \lambda A)^{-1} X_t + \{\exp(\rho)\} \\ \hat{K}_{t+1}^1 &= \hat{K}_t^1 - \exp(-\nu) \lambda D' (I - \lambda A)^{-1} X_t \end{aligned}$$

where $\lambda = \exp(\nu - \rho)$. We also obtain

$$\hat{C}_{t+1}^1 - \hat{C}_t^1 = -D^T X_t + \lambda D^T (I - \lambda A)^{-1} B W_{t+1}$$

This allows us to compute the log consumption progress:

$$\begin{aligned} \log C_{t+1} - \log C_t &= -D^T X_t + \lambda D^T (I - \lambda A)^{-1} B W_{t+1} + \nu + D^T X_t + F^T W_{t+1} \\ &= \left(\lambda D^T (I - \lambda A)^{-1} B + F^T \right) W_{t+1} + \nu \end{aligned}$$

This is the function that Professor Hansen plotted in class. He provided two plots – one is the permanent shock to the log Y_t process and one is the transitory shock to the log Y_t process.

- ▷ If λ is really close to one, then the permanent shock which is parallel to

$$D^T (I - \lambda A)^{-1} B + F^T$$

will be almost parallel to

$$\lambda D^T (I - \lambda A)^{-1} B + F^T$$

in which case the permanent shock will have a big impact on consumption.

- ▷ There is no D which is why you see the impulse response as a constant. This is contrast with the general response with the long-term convergence (adjustment takes time due to the transitory part, which was $D [\dots]$). If $D = 0$, then it will be just a straight line.

3.3 Comparison with Log-linearization

If you want to attain the second order in log-linearization, you have to deal with

$$\hat{X}_{t+1} = a\hat{X}_t + b\hat{X}_t^2 + \dots$$

which fucks with stationarity. But for this methodology, even if you go to second order:

$$\hat{X}_{t+1} = \hat{X}_{t+1}(0) + [\dots] \hat{X}_t'(0) + [\dots] \hat{X}_t''(0)$$

you are taking the square of the derivative so it's okay.