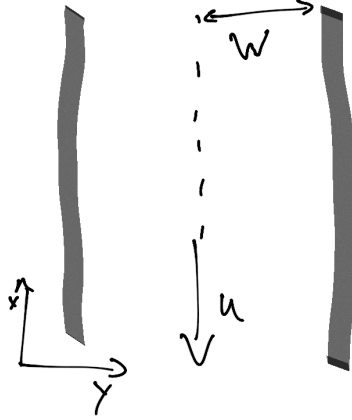


# Ice Stream Velocity

GT EAS 4803/8803

Let us consider an ice stream of half-width  $W$ , which is primarily flowing in one direction.



First, we can go back to the high-order ice flow approximation for ice flow along the x-direction:

$$4 \frac{\partial}{\partial x} \left( \eta \frac{\partial u}{\partial x} \right) + 2 \frac{\partial}{\partial x} \left( \eta \frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial y} \left( \frac{\eta}{2} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \right) + \frac{\partial}{\partial z} \left( \eta \frac{\partial u}{\partial z} \right) = \rho g \frac{\partial h}{\partial x} \quad (1)$$

Let us make two key assumptions: (1) flow is primarily along the x-direction ( $u \gg v$ ) and the changes in velocity along flow are negligible ( $\frac{\partial u}{\partial x}$  is small). This leaves

$$\frac{\partial}{\partial y} \left( \frac{\eta}{2} \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial z} \left( \eta \frac{\partial u}{\partial z} \right) = \rho g \frac{\partial h}{\partial x} \quad (2)$$

Reminding ourselves that  $\eta \frac{\partial u}{\partial z} = \tau_{xz}$  and  $\tau_d = \rho g \frac{\partial h}{\partial x}$ . We can then integrate this equation with respect to depth ( $z$ ), producing

$$h \frac{\partial}{\partial y} \left( \frac{\eta}{2} \frac{\partial u}{\partial y} \right) + (\tau_{xz}|_{z=h} - \tau_{xz}|_{z=0}) = \tau_d \quad (3)$$

Shear stress at the ice sheet surface should be negligible ( $\tau_{xz}|_{z=h} = 0$ ), and  $\tau_{xz}|_{z=0}$  is simply the basal shear stress,  $\tau_b$ , leaving

$$h \frac{\partial}{\partial y} \left( \frac{\eta}{2} \frac{\partial u}{\partial y} \right) = \tau_d - \tau_b \quad (4)$$

We can now integrate along the y-direction, starting from the center of the ice stream where  $\tau_{xy}$  will be small to the ice stream edge (i.e. the “shear margin”)

$$h \int_0^y \frac{\partial}{\partial y} \left( \frac{\eta}{2} \frac{\partial u}{\partial y} \right) dy = \int_0^y (\tau_d - \tau_b) dy \quad (5)$$

Giving

$$\frac{\eta}{2} \frac{\partial u}{\partial y} = \frac{y}{h} (\tau_d - \tau_b) \quad (6)$$

It is now useful to re-examine the effective viscosity of ice in the higher-order approximation

$$\eta = A^{-1/n} \left( \frac{1}{2} (\dot{\epsilon}_{xx}^2 + \dot{\epsilon}_{yy}^2 + \dot{\epsilon}_{zz}^2) + \dot{\epsilon}_{xz}^2 + \dot{\epsilon}_{xy}^2 \right)^{\frac{1-n}{2n}} \quad (7)$$

Vertical strain rates and along-flow strain rates are all negligible compared to the cross-flow strain rates, causing all these terms to drop out except the last one

$$\eta = A^{-1/n} \left( \frac{1}{2} \dot{\epsilon}_{xy} \right)^{\frac{1-n}{n}} \quad (8)$$

Inserting this back into the momentum balance above (noting that  $\dot{\epsilon}_{xy} = \frac{\partial u}{\partial y}$ ), we have

$$\frac{1}{2} \left( \frac{\partial u}{\partial y} \right)^{1/n} = \frac{y}{h} (\tau_d - \tau_b) \quad (9)$$

This equation can be integrated one final time in the y-direction

$$\int_0^y \frac{\partial u}{\partial y} dy = \int_0^y \frac{2^n A y^n}{h^n} (\tau_d - \tau_b)^n dy \quad (10)$$

Leading to (with some reorganization)

$$u(y) = U_d \left[ 1 - \left( \frac{y}{W} \right)^{n+1} \right] W^{n+1} (\tau_d - \tau_b)^n \quad (11)$$

where  $U_d = \frac{2^n A}{h^n (n+1)}$ .

A plot of the shape of velocity in an ice stream profile can be seen below.

