

Rail Geometry Gauge Change Calculations - Equivalence Verification

Rail Geometry Analysis

1 Problem Statement

Given interpolated rail coordinates for left and right rails, verify that two computational approaches for calculating gauge parameter changes produce identical results:

Parameter-First Approach: Calculate gauge parameters, then compute parameter changes

Delta-First Approach: Calculate coordinate deltas, then compute parameter changes directly

This verification demonstrates mathematical equivalence between both computational methods for gauge calculations.

2 Notation

Variable Definitions:

- ch_c = Chainage location (distance along track centerline) where gauge is calculated
- τ_0 = Baseline time (reference measurement)
- τ_m = Current measurement time ($m = 1, 2, 3, \dots$)
- L = Left rail (subscript)
- R = Right rail (subscript)
- X, Y, Z = 3D coordinates (X = Easting, Y = Northing, Z = Elevation)
- Δ = Change or difference operator

Coordinate Notation:

- $X(ch_c, \tau_m)_L$ = X-coordinate of left rail at chainage ch_c and time τ_m
- $Y(ch_c, \tau_m)_L$ = Y-coordinate of left rail at chainage ch_c and time τ_m
- $Z(ch_c, \tau_m)_L$ = Z-coordinate of left rail at chainage ch_c and time τ_m
- $\Delta X(ch_c, \tau_m)_L$ = Change in X-coordinate: $X(ch_c, \tau_m)_L - X(ch_c, \tau_0)_L$

Parameter Notation:

- $Gauge(ch_c, \tau_m)$ = Rail gauge at chainage ch_c and time τ_m
- $\Delta Gauge(ch_c, \tau_m)$ = Change in gauge from baseline to time τ_m

3 Input Dataset

Assume we have interpolated rail coordinates available at a specific chainage location:

$$\text{Left Rail: } X(ch_c, \tau_0)_L, Y(ch_c, \tau_0)_L, Z(ch_c, \tau_0)_L \quad (\text{baseline}) \quad (1)$$

$$X(ch_c, \tau_m)_L, Y(ch_c, \tau_m)_L, Z(ch_c, \tau_m)_L \quad (\text{current}) \quad (2)$$

$$\text{Right Rail: } X(ch_c, \tau_0)_R, Y(ch_c, \tau_0)_R, Z(ch_c, \tau_0)_R \quad (\text{baseline}) \quad (3)$$

$$X(ch_c, \tau_m)_R, Y(ch_c, \tau_m)_R, Z(ch_c, \tau_m)_R \quad (\text{current}) \quad (4)$$

Example: At chainage 1000m, we have baseline and current 3D coordinates for both left and right rails.

4 Parameter-First Approach

4.1 Step 1: Calculate Baseline Gauge

For 3D gauge (true spatial distance):

$$\text{Gauge}(ch_c, \tau_0) = \sqrt{(X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R)^2 + (Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R)^2 + (Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R)^2} \quad (5)$$

4.2 Step 2: Calculate Current Gauge

$$\text{Gauge}(ch_c, \tau_m) = \sqrt{(X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R)^2 + (Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R)^2 + (Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)^2} \quad (6)$$

4.3 Step 3: Calculate Gauge Change

$$\Delta \text{Gauge}(ch_c, \tau_m)_{\text{param}} = \text{Gauge}(ch_c, \tau_m) - \text{Gauge}(ch_c, \tau_0) \quad (7)$$

Substituting the gauge definitions:

$$\begin{aligned} \Delta \text{Gauge}(ch_c, \tau_m)_{\text{param}} &= \sqrt{(X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R)^2 + (Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R)^2 + (Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)^2} \\ &\quad - \sqrt{(X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R)^2 + (Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R)^2 + (Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R)^2} \end{aligned} \quad (8)$$

5 Delta-First Approach

5.1 Step 1: Calculate Coordinate Deltas

$$\Delta X(ch_c, \tau_m)_L = X(ch_c, \tau_m)_L - X(ch_c, \tau_0)_L \quad (9)$$

$$\Delta Y(ch_c, \tau_m)_L = Y(ch_c, \tau_m)_L - Y(ch_c, \tau_0)_L \quad (10)$$

$$\Delta Z(ch_c, \tau_m)_L = Z(ch_c, \tau_m)_L - Z(ch_c, \tau_0)_L \quad (11)$$

$$\Delta X(ch_c, \tau_m)_R = X(ch_c, \tau_m)_R - X(ch_c, \tau_0)_R \quad (12)$$

$$\Delta Y(ch_c, \tau_m)_R = Y(ch_c, \tau_m)_R - Y(ch_c, \tau_0)_R \quad (13)$$

$$\Delta Z(ch_c, \tau_m)_R = Z(ch_c, \tau_m)_R - Z(ch_c, \tau_0)_R \quad (14)$$

5.2 Step 2: Define Separation Vectors

Define baseline separation vector:

$$\vec{S}_0 = (X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R, Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R, Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R) \quad (15)$$

Define delta separation vector:

$$\begin{aligned}\vec{\Delta S} &= (\Delta X(ch_c, \tau_m)_L - \Delta X(ch_c, \tau_m)_R, \\ &\quad \Delta Y(ch_c, \tau_m)_L - \Delta Y(ch_c, \tau_m)_R, \\ &\quad \Delta Z(ch_c, \tau_m)_L - \Delta Z(ch_c, \tau_m)_R)\end{aligned}\tag{16}$$

5.3 Step 3: Calculate Gauge Change Using Vector Addition

$$\Delta \text{Gauge}(ch_c, \tau_m)_{\text{delta}} = |\vec{S}_0 + \vec{\Delta S}| - |\vec{S}_0|\tag{17}$$

6 Equivalence Proof

6.1 Expand Current Separation Vector

The current separation vector is:

$$\vec{S}_0 + \vec{\Delta S} = (X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R, Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R, Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)\tag{18}$$

6.2 Expand Delta-First Method

Substituting vector definitions:

$$\begin{aligned}\Delta \text{Gauge}(ch_c, \tau_m)_{\text{delta}} &= |\vec{S}_0 + \vec{\Delta S}| - |\vec{S}_0| \\ &= \sqrt{(X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R)^2 + (Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R)^2 + (Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)^2} \\ &\quad - \sqrt{(X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R)^2 + (Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R)^2 + (Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R)^2}\end{aligned}\tag{19}$$

6.3 Final Comparison

Both methods yield identical expressions:

$$\begin{aligned}\Delta \text{Gauge}(ch_c, \tau_m)_{\text{param}} &= \sqrt{(X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R)^2 + (Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R)^2 + (Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)^2} \\ &\quad - \sqrt{(X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R)^2 + (Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R)^2 + (Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R)^2}\end{aligned}\tag{20}$$

$$\begin{aligned}\Delta \text{Gauge}(ch_c, \tau_m)_{\text{delta}} &= \sqrt{(X(ch_c, \tau_m)_L - X(ch_c, \tau_m)_R)^2 + (Y(ch_c, \tau_m)_L - Y(ch_c, \tau_m)_R)^2 + (Z(ch_c, \tau_m)_L - Z(ch_c, \tau_m)_R)^2} \\ &\quad - \sqrt{(X(ch_c, \tau_0)_L - X(ch_c, \tau_0)_R)^2 + (Y(ch_c, \tau_0)_L - Y(ch_c, \tau_0)_R)^2 + (Z(ch_c, \tau_0)_L - Z(ch_c, \tau_0)_R)^2}\end{aligned}\tag{21}$$

7 Worked Example

Consider a specific numerical example to demonstrate both computational methods.

7.1 Given Data

At chainage $ch_c = 1000\text{m}$:

$$\begin{aligned}\text{Baseline } (\tau_0): \quad & X(1000, \tau_0)_L = 500.125\text{m}, \quad Y(1000, \tau_0)_L = 200.345\text{m}, \quad Z(1000, \tau_0)_L = 102.345\text{m} \\ & X(1000, \tau_0)_R = 498.590\text{m}, \quad Y(1000, \tau_0)_R = 200.355\text{m}, \quad Z(1000, \tau_0)_R = 102.330\text{m}\end{aligned}\tag{22}$$

$$\begin{aligned}\text{Current } (\tau_m): \quad & X(1000, \tau_m)_L = 500.120\text{m}, \quad Y(1000, \tau_m)_L = 200.350\text{m}, \quad Z(1000, \tau_m)_L = 102.358\text{m} \\ & X(1000, \tau_m)_R = 498.598\text{m}, \quad Y(1000, \tau_m)_R = 200.352\text{m}, \quad Z(1000, \tau_m)_R = 102.340\text{m}\end{aligned}\tag{23}$$

7.2 Parameter-First Calculation

Step 1: Calculate baseline gauge

$$\begin{aligned}
\text{Gauge}(1000, \tau_0) &= \sqrt{(500.125 - 498.590)^2 + (200.345 - 200.355)^2 + (102.345 - 102.330)^2} \\
&= \sqrt{(1.535)^2 + (-0.010)^2 + (0.015)^2} \\
&= \sqrt{2.356225 + 0.000100 + 0.000225} \\
&= \sqrt{2.356550} = 1.5351\text{m}
\end{aligned} \tag{24}$$

Step 2: Calculate current gauge

$$\begin{aligned}
\text{Gauge}(1000, \tau_m) &= \sqrt{(500.120 - 498.598)^2 + (200.350 - 200.352)^2 + (102.358 - 102.340)^2} \\
&= \sqrt{(1.522)^2 + (-0.002)^2 + (0.018)^2} \\
&= \sqrt{2.316484 + 0.000004 + 0.000324} \\
&= \sqrt{2.316812} = 1.5222\text{m}
\end{aligned} \tag{25}$$

Step 3: Calculate gauge change

$$\Delta\text{Gauge}(1000, \tau_m)_{\text{param}} = 1.5222 - 1.5351 = -0.0129\text{m} \tag{26}$$

7.3 Delta-First Calculation

Step 1: Calculate coordinate deltas

$$\Delta X(1000, \tau_m)_L = 500.120 - 500.125 = -0.005\text{m} \tag{27}$$

$$\Delta Y(1000, \tau_m)_L = 200.350 - 200.345 = 0.005\text{m} \tag{28}$$

$$\Delta Z(1000, \tau_m)_L = 102.358 - 102.345 = 0.013\text{m} \tag{29}$$

$$\Delta X(1000, \tau_m)_R = 498.598 - 498.590 = 0.008\text{m} \tag{30}$$

$$\Delta Y(1000, \tau_m)_R = 200.352 - 200.355 = -0.003\text{m} \tag{31}$$

$$\Delta Z(1000, \tau_m)_R = 102.340 - 102.330 = 0.010\text{m} \tag{32}$$

Step 2: Define separation vectors

Baseline separation vector (left rail - right rail at baseline):

$$\begin{aligned}
\vec{S}_0 &= (X(1000, \tau_0)_L - X(1000, \tau_0)_R, Y(1000, \tau_0)_L - Y(1000, \tau_0)_R, Z(1000, \tau_0)_L - Z(1000, \tau_0)_R) \\
&= (500.125 - 498.590, 200.345 - 200.355, 102.345 - 102.330) \\
&= (1.535, -0.010, 0.015)
\end{aligned} \tag{33}$$

Delta separation vector (difference in coordinate deltas):

$$\begin{aligned}
\vec{\Delta S} &= (\Delta X(1000, \tau_m)_L - \Delta X(1000, \tau_m)_R, \Delta Y(1000, \tau_m)_L - \Delta Y(1000, \tau_m)_R, \Delta Z(1000, \tau_m)_L - \Delta Z(1000, \tau_m)_R) \\
&= ((-0.005) - (0.008), (0.005) - (-0.003), (0.013) - (0.010)) \\
&= (-0.013, 0.008, 0.003)
\end{aligned} \tag{34}$$

Step 3: Calculate gauge change using vector addition

$$\vec{S}_0 + \vec{\Delta S} = (1.535 - 0.013, -0.010 + 0.008, 0.015 + 0.003) = (1.522, -0.002, 0.018) \tag{35}$$

$$|\vec{S}_0 + \vec{\Delta S}| = \sqrt{(1.522)^2 + (-0.002)^2 + (0.018)^2} = 1.5222\text{m} \tag{36}$$

$$\Delta\text{Gauge}(1000, \tau_m)_{\text{delta}} = 1.5222 - 1.5351 = -0.0129\text{m} \tag{37}$$

7.4 Verification

Both methods yield identical results:

$$\Delta\text{Gauge}(1000, \tau_m)_{\text{param}} = \Delta\text{Gauge}(1000, \tau_m)_{\text{delta}} = -0.0129\text{m} \tag{38}$$

8 Conclusion

$$\boxed{\Delta\text{Gauge}(ch_c, \tau_m)_{\text{param}} = \Delta\text{Gauge}(ch_c, \tau_m)_{\text{delta}}} \quad (39)$$

VERIFIED: Both approaches produce identical results for gauge change calculations.

Mathematical Basis: The equivalence holds because the vector addition $\vec{S}_0 + \vec{\Delta S}$ produces the same current separation vector used in the parameter-first approach, ensuring identical distance calculations.

9 Implementation Notes

- **Parameter-First:** More intuitive, provides intermediate gauge values for analysis
- **Delta-First:** More computationally efficient, reuses coordinate deltas across multiple parameters
- Both methods are mathematically equivalent and produce identical numerical results
- Gauge calculations involve 3D distance computations using all coordinate components
- The vector approach in delta-first method provides clear geometric interpretation
- Choice depends on computational efficiency needs and whether intermediate gauge values are required