

Orientation Control With Angle-Axis Representation

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Abstract: In this article I provide some basic definitions and proofs of identities for rotation matrices $\mathbf{R} \in \mathbb{SO}(3)$. I show that a rotation matrix can be represented as a matrix exponential. From this, Rodrigues' formula follows which expresses the matrix in terms of the angle and axis of rotation. I then show how to reverse this formula to obtain the angle and axis from an arbitrary rotation matrix. Then using the exponential form, and the angle-axis, I derive a control law for the angular velocity to perform feedback control on orientation error.

1. Euler's Rotation Theorem

Euler's rotation theorem states that any change in orientation of a rigid body can be described by:

- A single rotation α (rad),
- About an axis $\hat{\mathbf{a}} \in \mathbb{R}^3$

where $\hat{\mathbf{a}}$ is a unit vector such that $\|\hat{\mathbf{a}}\|^2 = \hat{\mathbf{a}}^T \hat{\mathbf{a}} = 1$. So the 3 combined rotations in Fig. 1 can be to a single rotation about a single axis.

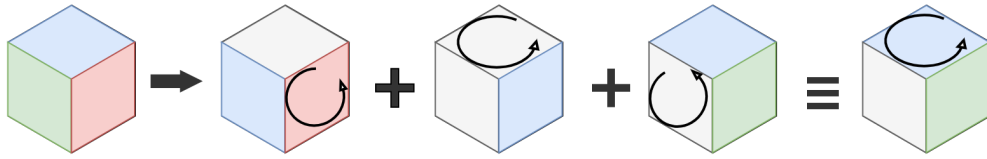


Figure 1: Any change in the orientation of a rigid body can be described by a single rotation about a single axis.

Any transformation of a vector $\mathbf{v} \in \mathbb{R}^n \rightarrow \mathbf{u} \in \mathbb{R}^n$ that preserves its length can be expressed with a product involving a rotation matrix:

$$\mathbf{u} = \mathbf{R}\mathbf{v}. \quad (1)$$

This matrix belongs to the Special Orthogonal group:

$$\mathbb{SO}(n) = \left\{ \mathbf{R} \in \mathbb{R}^{n \times n} \mid \mathbf{R}\mathbf{R}^T = \mathbf{I}, \det(\mathbf{R}) = 1 \right\} \quad (2)$$

Given an arbitrary rotation matrix $\mathbf{R} \in \mathbb{SO}(3)$ we may be interested in finding the angle and axis of rotation. To do this, we need to define some other properties of $\mathbb{SO}(3)$ that we can exploit.

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2. Time Derivative & Exponential

If we take the time derivative of Eqn. (1), and assuming $\dot{\mathbf{v}} = \mathbf{0}$, then we arrive at:

$$\dot{\mathbf{u}} = \dot{\mathbf{R}}\mathbf{v}. \quad (3)$$

But in 3D, the time derivative of a vector is given by the cross product with the instantaneous angular velocity $\boldsymbol{\omega} \in \mathbb{R}^3$ (rad/s):

$$\dot{\mathbf{u}} = \boldsymbol{\omega} \times \mathbf{u} = \underbrace{S(\boldsymbol{\omega})}_{\dot{\mathbf{R}}} \underbrace{\mathbf{R}\mathbf{v}}_{\mathbf{u}} \quad (4)$$

where $S(\cdot)$ is the skew-symmetric matrix operator:

$$S(\boldsymbol{\omega}) = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_y & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{bmatrix} \in \mathfrak{so}(3). \quad (5)$$

This is also the Lie algebra of $\mathbb{SO}(3)$. By equating Eqn. (3) with Eqn. (4), and substituting in Eqn. (1) we can see that the time derivative of the rotation matrix is "proportional" to itself:

$$\dot{\mathbf{R}} = S(\boldsymbol{\omega})\mathbf{R} \implies \mathbf{R}(t) = e^{S(\boldsymbol{\omega})t}\mathbf{R}(0) \quad (6)$$

This is a first-order differential equation whose solution is a (matrix) exponential. But the integral of the angular velocity is simply the angle-axis vector at any given point in time:

$$\int_0^t \boldsymbol{\omega} dt = \boldsymbol{\omega}t + \text{const.} \xrightarrow{0} \alpha \cdot \hat{\mathbf{a}} = \mathbf{a}. \quad (7)$$

Assuming we start from zero rotation ($\mathbf{R}(0) = \mathbf{I}$), then the rotation matrix is equivalent to a matrix exponential containing the angle-axis:

$$\mathbf{R} = e^{S(\mathbf{a})} \in \mathbb{SO}(3). \quad (8)$$

From the definition of the exponential:

$$e^{S(\mathbf{a})} = \sum_{k=0}^{\infty} \frac{\alpha^k}{k!} S(\hat{\mathbf{a}})^k \quad (9)$$

we can reduce Eqn. (8) to Rodrigues' formula which features the angle and axis as separate parameters:

$$\mathbf{R}(\alpha, \hat{\mathbf{a}}) = \mathbf{I} + \sin(\alpha)S(\hat{\mathbf{a}}) + (1 - \cos(\alpha))S(\hat{\mathbf{a}})^2. \quad (10)$$

3. Angle & Axis from Rotation Matrix

Rodrigues' formula, Eqn. (10), contains 3 matrices with a particular structure to their respective diagonal elements. If we take the trace¹ we can see that:

- $\text{trace}(\mathbf{I}) = 3$,
- $\text{trace}(S(\hat{\mathbf{a}})) = 0$, and
- $\text{trace}(S(\hat{\mathbf{a}}))^2 = -2$ since $\|\hat{\mathbf{a}}\| = 1$.

Hence the trace of a rotation matrix must be:

$$\text{trace}(\mathbf{R}) = 3 - 2 \cdot (1 - \cos(\alpha)) \quad (11a)$$

$$= 1 + 2 \cdot \cos(\alpha). \quad (11b)$$

¹Sum of diagonal elements

We can re-arrange this to solve for the angle of rotation:

$$\alpha = \cos^{-1} \left(\frac{\text{trace}(\mathbf{R}) - 1}{2} \right). \quad (12)$$

If the angle of rotation is zero $\alpha = 0$, then the axis of rotation is arbitrary since $0 \cdot \hat{\mathbf{a}} = \mathbf{0}$.

The axis for a rotation matrix does not change $\mathbf{R}\hat{\mathbf{a}} = \hat{\mathbf{a}}$. This implies that it is an eigenvector whose corresponding eigenvalue $\lambda = 1$.² For any arbitrary eigenvector of \mathbf{R} it must hold that:

$$\mathbf{R}\mathbf{v} = \mathbf{v}. \quad (13)$$

Multiplying this by the transpose of the rotation yields:

$$\overbrace{\mathbf{R}^T \mathbf{R}}^{\mathbf{I}} \mathbf{v} = \mathbf{R}^T \mathbf{v} \quad (14a)$$

$$\mathbf{v} = \mathbf{R}^T \mathbf{v}. \quad (14b)$$

Equating Eqn. (13) and Eqn. (14) we obtain:

$$\mathbf{R}\mathbf{v} = \mathbf{R}^T \mathbf{v} \quad (15a)$$

$$\underbrace{(\mathbf{R} - \mathbf{R}^T)}_{S(\mathbf{v})} \mathbf{v} = \mathbf{0}. \quad (15b)$$

The matrix $\mathbf{R} - \mathbf{R}^T$ must be skew-symmetric since $\mathbf{v} \times \mathbf{v} = S(\mathbf{v})\mathbf{v} = \mathbf{0}$. Expanding this we have:

$$\mathbf{R} - \mathbf{R}^T = \begin{bmatrix} 0 & r_{12} - r_{21} & r_{13} - r_{31} \\ r_{21} - r_{12} & 0 & r_{23} - r_{32} \\ r_{31} - r_{13} & r_{32} - r_{23} & 0 \end{bmatrix}. \quad (16)$$

Using what we know about the structure of skew-symmetric matrices, Eqn. (5), we can deduce that the eigenvector is:

$$\mathbf{v} = \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}. \quad (17)$$

We can then normalise this vector to obtain the axis of rotation $\hat{\mathbf{a}}$:

$$\hat{\mathbf{a}} = \begin{cases} \frac{\mathbf{v}}{\|\mathbf{v}\|} & \text{if } \alpha \neq 0 \\ \text{trivial} & \text{otherwise.} \end{cases} \quad (18)$$

Note that if $\mathbf{R} = \mathbf{I}$ (i.e. no rotation), then $\mathbf{v} = \mathbf{0}$ and hence $\nexists \|\mathbf{v}\|^{-1}$. In this case, we can assign any arbitrary value to the axis of rotation.

4. Orientation Feedback

We can use the angle-axis vector to perform feedback on the orientation of an automated system. Suppose $\mathbf{R}_d \in \mathbb{SO}(3)$ is the desired orientation, and $\mathbf{R} \in \mathbb{SO}(3)$ is our actual orientation. We can define our orientation error as:

$$\mathbf{E} \triangleq \mathbf{R}_d \mathbf{R}^T = e^{S(\epsilon)}. \quad (19)$$

If $\mathbf{R} = \mathbf{R}_d$ then $\mathbf{E} = \mathbf{I}$, implying no difference between orientations. From Eqn. (6) the time derivative of our rotation error is:

$$\dot{\mathbf{E}} = S(\dot{\epsilon})\mathbf{E}, \quad \dot{\epsilon} = \boldsymbol{\omega}_d - \boldsymbol{\omega}. \quad (20)$$

where:

- $\boldsymbol{\omega}_d \in \mathbb{R}^3$ is the desired angular velocity (rad/s), and

²For any arbitrary matrix $\mathbf{A} \in \mathbb{R}^{m \times m}$ the eigenvector $\mathbf{v} \in \mathbb{C}^m$ and eigenvalue $\lambda \in \mathbb{C}$ obey the identity $\mathbf{A}\mathbf{v} = \lambda\mathbf{v}$.

- $\omega \in \mathbb{R}^3$ is the actual angular velocity (rad/s).

Assuming ω is our control input, we can define the control law:

$$\omega \triangleq \omega_d + K\epsilon \quad (21)$$

where $K \in \mathbb{R}^{3 \times 3}$ is a positive-definite gain matrix.³ The desired angular velocity ω_d becomes a feed-forward term, whereas $K\epsilon$ is a proportional feedback on the orientation error.⁴

If we substitute Eqn. (21) in to Eqn. (20) we obtain:

$$\dot{\epsilon} = -K\epsilon \implies \epsilon(t) = e^{-Kt} \epsilon(0). \quad (22)$$

This form implies exponential decay. As the error angle approaches zero $\epsilon \rightarrow 0$ then the orientation error will approach the identity $E \rightarrow I$ such that $R \rightarrow R_d$.⁵

Figure 2 shows the ergoCub rotating a box using this method of orientation control.

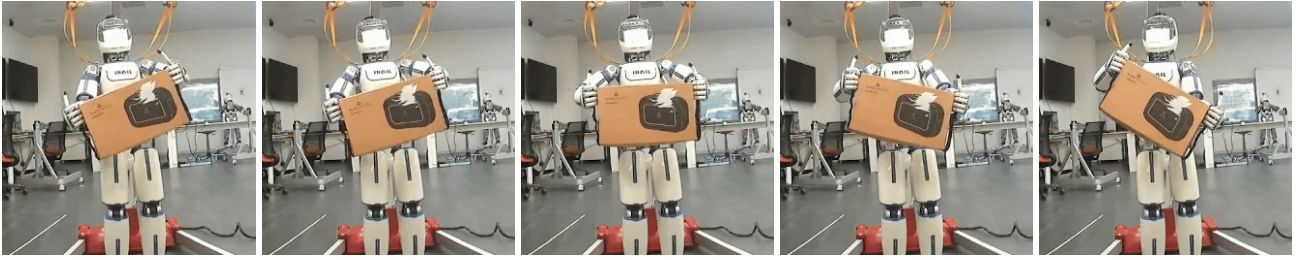


Figure 2: Orientation feedback control with angle-axis representation was used to control an object being held by the ergoCub robot.

³An easy choice here is a diagonal matrix with positive values.

⁴In such cases where ω_d is unavailable, then $\omega = K\epsilon$ is sufficient.

⁵This follows from the fact that $e^0 = 1$.