ELEC 3035, Lecture 7: Pole placement by state feedback Ivan Markovsky

- Motivation for control by pole placement
- State feedback control
- Controller canonical form
- Solution of the state feedback pole placement problem

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Dynamical behaviour ← pole location

LTI system dynamics is qualitatively determined by the pole locations

e.g., pole
$$z_i$$
 with $|z_i| < 1$ (DT) or $z_i < 0$ (CT) \implies stable mode

Stability is a minimum requirement for control.

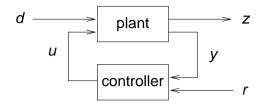
The poles of the closed-loop system should be in the

unit circle
$$\{z \mid |z| < 1\}$$
 (DT) $|z_i|$ and $\angle z_i$ (DT) moreover

half-plane
$$\{z \mid z < 0\}$$
 (CT) $\Re(z_i)$ and $\Im(z_i)$ (CT)

determine how "fast" and "oscillatory" the mode is.

Feedback control



- *r* reference signal
- u control signal
- d disturbance
- z performance criterion
- y measurement signal

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Motivation for pole placement

• The desired dynamics is specified by the pole locations

$$\{z_{\text{des},1},\ldots,z_{\text{des},n_{\text{cl}}}\}$$

of the closed-loop system

or equivalently by the characteristic polynomial

$$p_{\text{des}}(z) = \prod_{i=1}^{n_{\text{cl}}} (z - z_{\text{des},i}) = p_{\text{des},0} + p_{\text{des},1}z + \dots + p_{\text{des},n_{\text{cl}}}z^{n_{\text{cl}}}$$

of the closed-loop system.

- Feedback affects the characteristic polynomial
- The aim of pole placement control is to choose the feedback so that the closed-loop system achieve the desired char. polynomial

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Deadbeat control

In the DT case, if

$$z_{\text{des},1} = \cdots = z_{\text{des},n_{\text{cl}}} = 0$$

i.e.,

$$p_{\text{des}}(z) = z^{n_{\text{cl}}}$$

the closed-loop system state goes to zero in at most n_{cl} steps.

See the example on page 9.

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Example

Consider the system defined by the equation

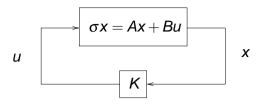
$$\sigma x = \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix}}_{A} x + \underbrace{\begin{bmatrix} 1 \\ 1 \end{bmatrix}}_{B} u$$

and the desired characteristic polynomial $p_{des}(z) = z^2$.

$$\begin{aligned} \det(zI - A - bk) &= \det\left(\begin{bmatrix} z & 0 \\ 0 & z \end{bmatrix} - \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} - \begin{bmatrix} 1 \\ 1 \end{bmatrix} \begin{bmatrix} k_1 & k_2 \end{bmatrix}\right) \\ &= \det\left(\begin{bmatrix} z - 1 - k_1 & -k_2 \\ -k_1 & z - 2 - k_2 \end{bmatrix}\right) \\ &= (z - 1 - k_1)(z - 2 - k_2) - k_2 k_1 \\ &= z^2 - (k_1 + k_2 + 3)z + 2 + 2k_1 + k_2 \end{aligned}$$

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State feedback



$$\sigma x = Ax + Bu, \quad u = Kx \implies \quad \sigma x = (A + KB)u$$

The closed-loop system is autonomous with state matrix

$$A_{c} = A + KB$$
.

Pole placement by state-feedback aims to choose K, so that

$$\det(zI - A_c) = p_{des}(z)$$

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Equating the closed-loop char. polynomial to the desired char. polyn.

$$\det(zI - A - bk) = p_{des}(z)$$

$$\implies z^2 + (k_1 + k_2 + 3)z + 2 + 2k_1 + k_2 = z^2$$

gives two equations in the unknowns k_1 and k_2

$$k_1 + k_2 + 3 = 0$$
$$2 + 2k_1 + k_2 = 0$$

which unique solution is $k_1 = 1$, $k_2 = -4 \implies$ the control law is

$$u = \begin{bmatrix} 1 & -4 \end{bmatrix} x$$

and the closed-loop system is

$$\sigma x = (A + bk)x = \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} x$$

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Let's calculate two particular responses of the closed-loop system.

$$x(0) = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mapsto x(1) = \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 2 \\ 1 \end{bmatrix} \mapsto x(2) = \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$x(0) = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mapsto x(1) = \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} -4 \\ -2 \end{bmatrix} \mapsto x(2) = \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} -4 \\ -2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\implies A^2 = 0$$

Therefore, the state of the closed-loop system goes to zero in two steps from any initial condition (dead-beat control).

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The controllability matrix, associated with the pair A, b is

$$\mathscr{C}(A,b) := \begin{bmatrix} b & Ab & \cdots & A^{n-1}b \end{bmatrix} = \begin{bmatrix} 0 & \cdots & 0 & 1 \\ \vdots & \ddots & \ddots & * \\ 0 & \ddots & \ddots & \vdots \\ 1 & * & \cdots & * \end{bmatrix}$$

 \implies A, b is controllable

Controller canonical form (SISO case)

Fact: Any controllable system $\mathscr{B}_{i/o}(p,q)$ can be represented in a state space form $\mathscr{B}_{i/s/o}(A,b,c,d)$ with parameters

$$A = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \ddots & \vdots \\ \vdots & & \ddots & \ddots & 0 \\ 0 & \cdots & \cdots & 0 & 1 \\ -p_0 & -p_1 & \cdots & \cdots & -p_{n-1} \end{bmatrix}, \qquad b = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 1 \end{bmatrix}$$

$$c = \begin{bmatrix} c_0 & c_1 & \cdots & c_{n-1} \end{bmatrix}, \qquad d = q_n$$

where c_0, c_1, \dots, c_{n-1} are the coefficients of $q(z) - q_n p(z)$

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Similarity transformation for controller canonical form

A more general result:

Lemma:

- Let A, b and A', b' be two controllable pairs and
- assume that A and A' have the same char. polynomials.

Then there is a unique similarity transformation given by the matrix

$$T := \mathscr{C}(A, b) \big(\mathscr{C}(A', b') \big)^{-1}$$

such that

$$T^{-1}AT = A'$$
 and $T^{-1}b = b'$

⇒ Any controllable representation of the system can be transformed to the controller canonical form.

Example

Consider again the system defined by the equation

$$\sigma x = \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix}}_{A} x + \underbrace{\begin{bmatrix} 1 \\ 1 \end{bmatrix}}_{b} u$$

The characteristic polynomial of A is

$$\det(Iz - A) = \det\begin{bmatrix} z - 1 & 0 \\ 0 & z - 2 \end{bmatrix} = (z - 1)(z - 2) = 2 - 3z + z^2$$

and the controllability matrix $\mathscr{C}(A,b) = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix}$ is full rank, so the system is controllable. Therefore,

$$A' = \begin{bmatrix} 0 & 1 \\ -2 & 3 \end{bmatrix}, \qquad b' = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

is the controller canonical form of A.b.

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State-feedback pole placement in controller form

Let the plant be given by $\mathcal{B}_{i/s/o}(A, b, c, d)$, with A, b in controller form.

Then

$$A_{cl} := A + bk = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \ddots & \vdots \\ \vdots & & \ddots & \ddots & 0 \\ 0 & \cdots & \cdots & 0 & 1 \\ k_1 - p_0 & k_2 - p_1 & \cdots & \cdots & k_n - p_{n-1} \end{bmatrix}$$

and the closed-loop characteristic polynomial is

$$p_{cl}(z) = (p_0 - k_1) + (p_1 - k_2)z + \dots + (p_{n-1} - k_n)z^{n-1} + z^n$$

The equation $p_{cl} = p_{des}$ has the unique solution

$$k_1 = p_0 - p_{\text{des},0}, \cdots, k_n = p_{n-1} - p_{\text{des},n-1}$$

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The controllability matrix of the pair A', b' is

$$\mathscr{C}(A',b') = \begin{bmatrix} 0 & 1 \\ 1 & 3 \end{bmatrix}$$

Therefore according to the lemma the similarity transformation that transforms A, b to A', b' is

$$T = \mathscr{C}(A,b) \left(\mathscr{C}(A',b') \right)^{-1} = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 3 \end{bmatrix}^{-1} = \begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix}$$

Verify that $T^{-1}AT$, $T^{-1}b$ is indeed the controller canonical form, *i.e.*,

$$\begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix}^{-1} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -2 & 3 \end{bmatrix}$$

and

$$\begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

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State-feedback pole placement in arbitrary basis

We know the solution in the controller form, so the approach is:

- 1. transform the given representation to controller canonical form,
- 2. solve the pole placement problem in the new basis,
- 3. convert the obtained state feedback gain to the original basis

Let the plant be given by $\mathcal{B}_{i/s/o}(A, b, c, d)$. If A, b is controllable, there is similarity transf. T, s.t. $T^{-1}AT$, $T^{-1}b$ is in controller form

Let k' be the state-feedback in the new basis. Then

$$k = k' T^{-1}$$

is the state-feedback law that solves the pole placement problem in the original basis.

State-feedback pole placement in arbitrary basis

We showed that controllability is a sufficient condition for pole placement. It turns out that controllability is also necessary.

Theorem: The eigenvalues of A + BK can be assigned choosing K to any locations in \mathbb{C} if and only if A, B is controllable.

Notes:

- The theorem holds for general multivariable systems.
- The multi-input pole placement problem can be reduced to an equivalent single input pole placement problem.
- Good numerical methods for pole placement do not compute the controller canonical form.

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Example

Consider the system example as before, but with A, b is controller form

$$\sigma x = \underbrace{\begin{bmatrix} 0 & 1 \\ -2 & 3 \end{bmatrix}}_{A} x + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_{b} u$$

The state-feedback law that achieves the char. polynomial $p_{des}(z) = z^2$

$$k = \begin{bmatrix} 2 & -3 \end{bmatrix}$$
.

In order to compare this state-feedback with the one obtained on page 8, we need to change the basis

$$kT^{-1} = \begin{bmatrix} 2 & -3 \end{bmatrix} \begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 1 & -4 \end{bmatrix}$$

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