# **Engineering Thermodynamics**

## 1 Basic Definition

## 1.1 能量转换装置

- 热能动力装置:
  - o 蒸汽动力装置(Vapor Power Systems): 工质: Steam/Water
  - 燃气动力装置(Gas Power Systems): 工质: 燃气
    - 内燃机
    - 燃气轮机
    - 喷气发动机
- 制冷和热泵装置 (Refridgeration and Heat Pump Systems): 工质: 制冷剂

## 1.2 热力系

## 物质交换:

- 闭口系(closed system): 控制质量(C.M.)——与外界无物质交换
- 开口系 (open system): 控制体积 (C.V.) ——与外界有物质交换

## 能量交换:

- 简单热力系:与外界只交换热量和一种形式的准静功
- (简单压缩系(simple compressive system): 准静功为可逆体积变化功)
- 绝热系 (adiabatic system): 与外界无热量交换
- 孤立系 (isolated system): 与外界无能量交换也无物质交换

# 1.3 热力状态与基本状态参数

- Thermodynamic State
  - o steady state: 状态参数不随时间变化
  - o equilibrium state: 所有参数达到平衡,即不再变化

## • State Properties

- $\circ \$  extensive property: M,V,U,E,H,S
- $\circ\:$  intensive property: T,p, 广延量的比参数 (v,u,h,s)
- ${\tt o}\$  Basic Properties: T,p,v

#### • Process

#### irreversibility:

- o reversible:(quasi-steady & non-dissipative) (准稳态及无耗散)
- irreversible

## thermodynamic:

- o quasi-steady 准静态
- o isothermal 等温
- o adiabatic 绝热
- o isentropic 等熵

## • Process para

 $\circ \ \ Q,W$ 

# 1.4 Zeroth law of thermodynamics

"It's a matter of experience that when two objects are in thermal equilibrium with a third object, they are in thermal equilibrium with one another."

## 1.5 Temperature Scales

- Kelvin scale
- Rankine scale

$$T({}^{\circ}R)=1.8T(K)$$

• Celsius scale

$$T(^{\circ}C) = T(K) - 273.15$$

• Fahrenheit scale

$$T({}^{\circ}F) = T({}^{\circ}R) - 459.67 = 1.8T({}^{\circ}C) + 32$$

开尔文温标	摄氏度	华氏度
0K	-273.15 $^{\circ}C$	$-459.67^{\circ}F$
273.15K	$0\degree C$	$32\degree F$
373.15K	$100^{\circ}C$	$212^{\circ}F$

# 2 Energy and the First law of Thermodynamics

# 2.1 Energy

• Internal energy: U

• Kinetic energy:  $E_k$ 

• Potential energy:  $E_p$ 

Total energy:

$$E = U + E_k + E_p$$
  $\Delta E = \Delta U + \Delta E_k + \Delta E_p$ 

## 2.2 Work

• 输出功 Output work(对外输出总功量): W'

• 净输出功:  $W_{net}$ 、轴功(叶轮机械净输出功):  $W_s$ 

• 膨胀功/压缩功/体积功 Expansion or Compression work:

$$W=p\Delta V \ \delta W=pdV \ \delta w=pdv$$

• 推动功/推挤功:

流体进出系统系统所对流体做出的推动功量

$$W_p = pV$$

• 流动功 Flow work/energy(State property):

$$W_f = \sum_i W_{p,i} = \Delta(pV) \ \delta W_f = V dp + p dV \ \delta w_f = v dp + p dv$$

## • 技术功 Technical work:

$$W_t = \Delta E_k + \Delta E_p + W_{net} \ \delta W_t = \delta W - \delta W_f = -V dp \ \delta w_t = -v dp$$

Relation:

$$W' = W_{net} + W_f$$
  $W_t = \Delta E_k + \Delta E_p + W_{net}$   $W = W_t + W_f$ 

# 2.3 Heat

Conduction:

$$\dot{Q} = -\kappa A rac{dT}{dx}$$

Radiation:

$$\dot{Q}=\varepsilon\sigma AT^4$$

Convection:

$$\dot{Q} = hA\Delta T$$

# 2.4 The first law of Thermodynamics

"During an interaction, energy can change from one form to another but the total amount of energy remains constant."

general form:

$$\Delta E = Q - W$$
  $\Delta E_k + \Delta E_p + \Delta U = Q - W$ 

differential form:

$$dE = \delta Q - \delta W'$$

time rate form:

$$rac{dE}{dt}=\dot{Q}-\dot{W}'$$

# CLOSED SYSTEMS(C.M.)

1. differential form:

闭口系热一定律基本表达式:

$$dU = \delta Q - \delta W \tag{1}$$

$$du = dq - pdv \tag{2}$$

## OPEN SYSTEMS(C.V.)

## 1. differential form:

热一定律:

$$dE=\delta Q-\delta W'$$

输出总功量转化为净功量和流动功:

$$\delta W' = \delta W_{net} + d(pV)$$

技术功、焓的定义:

$$\delta W_t = \delta W_{net} + dE_k + dE_p \ dH = dU + d(pV)$$

# 开口系-热力学第一定律基本表达式:

$$dH = \delta Q - \delta W_t \tag{1.1}$$

$$dU = \delta Q - \delta W \tag{1.2}$$

$$\begin{split} dh &= du + vdp + pdv \\ dh &= dq + vdp \end{split} \tag{2.1}$$

$$du = dq - pdv (2.2)$$

# 2. time rate & intergral form:

热一定律:

$$\begin{split} \frac{dE}{dt} &= \dot{Q} - \dot{W}' \\ e &= u + \frac{V^2}{2} + gz \\ E &= \int_{CV} edm = \int_{CV} e\rho d\mathscr{V} \end{split} \tag{1}$$

 ${\it differential\ form:}$ 

$$dE_{CV} = \delta Q - \delta W + d(ms)$$

Steady Flow:

$$0 = \delta Q - \delta W + m ds$$

# 积分形式(Reynolds Transport Theorem)

$$rac{d}{dt}(E_{sys}) = \dot{Q} - \dot{W}' = rac{d}{dt}(\int_{CV}e
ho d\mathscr{V}) + \int_{CS}e
ho V_n dA$$

输出总功量转化为净功量和流动功:

$$\dot{W}' = \dot{W}_{net} + \int_{CS} p V_n dA$$

焓的定义:

$$h=u+pv \ \int_{CS} h 
ho V_n dA = \int_{CS} (u+rac{p}{
ho}) 
ho V_n dA$$

连续介质力学形式:

$$\begin{split} \dot{Q} - \dot{W}_{net} &= \frac{d}{dt} (\int_{CV} e \rho d\mathcal{V}) + \int_{CS} (h + \frac{V^2}{2} + gz) \rho V_n dA \\ or \\ \dot{Q} - \dot{W}_{net} &= \frac{\partial}{\partial t} \int_{CV} e \rho d\mathcal{V} + \int_{CS} (h + \frac{V^2}{2} + gz) \rho V_n dA \\ or \\ \dot{Q} - \dot{W}_{net} &= \frac{\partial}{\partial t} \int_{CV} e \rho d\mathcal{V} + \sum (h + \frac{V^2}{2} + gz)_e \dot{m}_e - \sum (h + \frac{V^2}{2} + gz)_i \dot{m}_i \end{split}$$

## 2.5 application

• 气轮机叶轮 Turbine Wheel

$$\dot{W}_{net}=\dot{m}(rac{V_1^2-V_2^2}{2})$$

• 热力发动机 Gas And Steam Turbine

$$egin{aligned} 0 &= \dot{Q}_{CV} - \dot{W}_{net} + \dot{m}(h_1 - h_2) \ \dot{W}_{net} &= \dot{m}(h_1 - h_2) \end{aligned}$$

• 压气机/泵 Compressor and Pump

$$egin{aligned} 0 &= \dot{Q}_{CV} - \dot{W}_{net} + \dot{m}(h_1 - h_2) \ \dot{W}_{net} &= \dot{m}(h_1 - h_2) \end{aligned}$$

• 喷管/扩散器 Nozzle/Diffuser

$$egin{aligned} 0 &= Q_{CV} + \dot{m}(h_1 + rac{V_1^2}{2}) - \dot{m}(h_2 + rac{V_2^2}{2}) \ 0 &= (h_1 - h_2) + (rac{V_1^2 - V_2^2}{2}) \end{aligned}$$

• 换热器 Heat Exchanger

$$\dot{Q}_{CV}=\dot{m}(h_2-h_1)$$

• 节流 Throttling Process

$$h_1 = h_2$$

# 3 Entropy and the Second Law of Thermodynamics

# 3.1 The Second Law of Thermodynamics

#### Clausius statement:

Heat can never pass from a colder to a warmer body without some other change, connected therewith, occurring at the same time.

#### Kelvin Statement:

It is impossible, by means of inanimate material agency, to derive mechanical effect from any portion of matter by cooling it below the temperature of the coldest of the surrounding objects.

#### Planck's Proposition:

It is impossible to construct an engine which will work in a complete cycle, and produce no effect except the raising of a weight and cooling of a heat reservoir.

## • 克劳修斯说法:

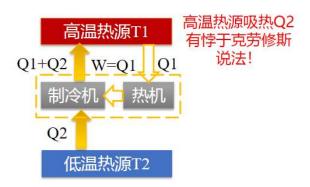
- o 热传导的不可逆性
- o 无法制造理想制冷机

#### • 开尔文-普朗克说法:

- o 热工转换的不可逆性
- o 无法制造第二类永动机
- o 单一热源下不可能做正输出功

$$\oint W_{cycle} = \oint Q_{cycle} \leq 0$$





- **熵增原理(能量贬值原理)**: 孤立系统总是朝着熵增方向进行
- 永动机:
  - o 第一类永动机(违背热一定律) 凭空产生能量
  - o 第二类永动机(违背热二定律)热量100%转化为功

## • 卡诺定理:

o 卡诺第一定理:不可能制造出在两个温度不同的热源间工作的热机,而使其效率超过在**同样热源**间工作的可逆 热机 o 卡诺第二定理: 在两个热源间工作的一切可逆热机具有相同的效率

o 卡诺定理推论: 在相同两个恒温热源间工作的一切不可逆热机的效率必小于可逆热机的效率

• 能量品位:

# 能量转换方向性的 实质是能质有差异 不可转换能——环境介质的热力学能

## 3.2 Reversible Process

Reversible Process  $\iff$  No internal irreversibilities

## 3.3 Propositions of The Second Law of Thermodynamics

#### I. Kelvin Scales

In Carnot Heat Engines:

$$(rac{Q_C}{Q_H})^{rev}_{cycle} = \phi(T_C, T_H) \stackrel{def}{=} rac{T_C}{T_H}$$

## II. Clausius Inequality

$$\oint \left(\frac{Q}{T}\right)_b = -\sigma_{cycle}, \; \sigma_{cycle} \left\{ \begin{array}{ll} > 0: & Internal \; irreversibilities \; present \\ = 0: & No \; internal \; irreversibilities \end{array} \right. \\ (system \; boundary \; heat \; exchange)$$

# III. Entropy

Definition:

$$dS = \left(rac{\delta Q}{T}
ight)_{rev} \ \Delta S = \int_{1}^{2} \left(rac{\delta Q}{T}
ight)_{rev}$$

TdS equation in reversible system:

$$TdS = dU + pdV$$
 $Tds = dH - Vdp$ 

$$Tds = du + pdv$$
  
 $Tds = dh - vdp$ 

## Closed System

basic relation:

$$egin{aligned} \oint \left(rac{Q}{T}
ight)_b &= \int_1^2 \left(rac{Q}{T}
ight)_b + \int_2^1 \left(rac{Q}{T}
ight)_{rev} \ \int_1^2 \left(rac{Q}{T}
ight)_b + S_1 - S_2 &= -\sigma \end{aligned}$$

differiential form:

$$dS = \left(rac{\delta Q}{T}
ight)_b + \delta \sigma$$
  $or$   $dS = dS_f + \delta S_g$ 

## Condition Relation:

Common:

$$dS = \left(rac{\delta Q}{T}
ight)_b + \delta \sigma$$

Adiabatic:

$$dS = \delta \sigma$$

Reversible:

$$dS = \left(rac{\delta Q}{T}
ight)_b$$

 $Isentropic:( \Longleftrightarrow Adiabatic + Reversible)$ 

$$dS = 0$$

# IV Increase of Entropy Principle

In isolated system:

$$\left(rac{\delta Q}{T}
ight)_b = 0 \ dS_{iso} = \delta S_g \geq 0$$

## Open System

differential form:

$$dS_{CV} = rac{\delta Q}{T} + \delta S_{g,CV} + d(ms)$$

Steady Flow:

$$0=rac{\delta Q}{T}+\delta S_{g,CV}+mds$$

time rate & intergral form:

$$(rac{dS}{dt})_{sys} = \sum rac{\dot{Q}}{T} + \dot{\sigma}$$

$$egin{aligned} \sum rac{\dot{Q}}{T} + \dot{\sigma} &= rac{\partial}{\partial t} \int_{CV} 
ho s d\mathscr{V} + \int_{CS} s 
ho V_n dA \ or \ &\sum rac{\dot{Q}}{T} + \dot{\sigma} &= rac{\partial}{\partial t} \int_{CV} 
ho s d\mathscr{V} + \sum \dot{m}_e s_e - \sum \dot{m}_i s_i \end{aligned}$$

# 3.4 Heat Engine and Heat Pump/Refrigerator

## Heat Engine

Thermal efficiency:

$$\eta = rac{W_{cycle}}{Q_H} = 1 - rac{Q_C}{Q_H} \ \eta_{max} = 1 - rac{T_C}{T_H}$$

## Refrigerator

Thermal efficiency:

$$arepsilon = rac{Q_C}{W_{cycle}} = rac{Q_C}{Q_H - Q_C} \ arepsilon_{max} = rac{T_C}{T_H - T_C}$$

## Heat Pump

Thermal efficiency:

$$arepsilon' = rac{Q_H}{W_{cycle}} = rac{Q_H}{Q_H - Q_C} \ arepsilon'_{max} = rac{T_H}{T_H - T_C}$$

# 3.5 application-efficiency

ullet is entropic turbine efficiency

$$egin{aligned} rac{\dot{W}_{net}}{\dot{m}} &= (h_1-h_2) \ \eta_t &= rac{h_1-h_2}{h_1-h_{2s}} \end{aligned}$$

• isentropic compressor and pump efficiency

$$rac{-\dot{W}_{net}}{\dot{m}} = (h_2 - h_1) \ \eta_c = rac{h_{2s} - h_1}{h_2 - h_1}$$

• isentropic nozzle efficiency

$$rac{V_2^2}{2} = h_1 - h_2 + rac{V_1^2}{2} \ \eta_{nozzle} = rac{V_2^2/2}{(V_2^2/2)_s}$$

# 3.6 Exergy 㶲 Anergy 墲

## • Exergy and Anergy in Heat

Environment at  $T_0$ , System at TExergy:

$$E_{x,Q}=W_{max}=(1-rac{T_0}{T})Q$$

Anergy:

$$E_{n,Q}=Q-E_{x,Q}=rac{T_0}{T}Q=Q_{emit}$$

## • Exergy and Anergy in System

**Definition:** Maximum theoretical work from system and environment to reach an equilibrium

#### Closed System

Overall:

$$0 = dU_s + dU_e + dW_x \ \delta S_q = dS_{iso} = dS_s + dS_e$$

System:

$$\delta Q_{rev} = dU_s + \delta W_{max} \ \delta W_{max} = \delta W_x + p_0 dV_s$$

Environment, at  $T_0,p_0\colon$ 

$$-\delta Q_{rev} = dU_e + p_0 dV_e \ -\delta Q_{rev} = T_0 dS_e$$

Maximum Work:

$$\delta W_x = -dU_s - p_0 dV_s - T_0 (dS_g - dS_s) \ W_x = (U - U_0) + p_0 (V - V_0) - T_0 (S - S_0) + (E_k + E_p) - T_0 S_g$$

Exergy(a kind of Potential):

$$E_x = (U - U_0) + p_0(V - V_0) - T_0(S - S_0) + (E_k + E_p)$$

$$or$$

$$E_x = (U - U_0) + p_0(V - V_0) - T_0(S - S_0)$$

$$e_x = (u + p_0v - T_0s) - (u_0 + p_0v_0 - T_0s_0)$$

Exergy Change:

$$dE_x = dU + p_0 dV - T_0 dS$$
  $dE_x = \delta Q - (\delta W - p_0 dV) - T_0 (rac{\delta Q}{T_b} + \delta S_g)$ 

$$dE_x = (1-rac{T_0}{T_b})\delta Q - (\delta W - p_0 dV) - T_0 \delta S_g \ E_2 - E_1 = \int_1^2 (1-rac{T_0}{T_b})\delta Q - [W - p_0(V_2-V_1)] - T_0 \Delta S_g$$

• Exergy transfer of Heat transfer

$$\int_{1}^{2} (1 - \frac{T_0}{T_b}) \delta Q$$

• Exergy transfer of Work

$$\left[W-p_0(V_2-V_1)\right]$$

• Exergy destruction

$$T_0 \Delta S_g$$

Simplization

$$E_2 - E_1 = E_q - E_w - E_d$$

Isolated and no work process:

$$\Delta E = -E_d$$

time rate form:

$$\dot{E}_x = \sum_j (1-rac{T_0}{T})\dot{Q}_j - [\dot{W}-p_0(rac{dV}{dt})] - T_0\dot{\sigma}$$

steady state:

$$0=\sum_j (1-rac{T_0}{T})\dot{Q}_j - \dot{W} - T_0\dot{\sigma}$$

## Open System

Exergy:

$$E_x = (H - H_0) - T_0(S - S_0) + (E_k + E_p)$$

$$or$$

$$E_x = (H - H_0) - T_0(S - S_0)$$

$$e_x = (h - T_0 s) - (h_0 - T_0 s_0)$$

Exergy Change

time rate form:

$$\sum_{j}(1-rac{T_{0}}{T_{j}})\dot{Q}_{j}-(\dot{W}_{CV}-p_{0}rac{dV_{CV}}{dt})-T_{0}\dot{\sigma}=rac{d}{dt}\int_{CV}e_{x}
ho d\mathscr{V}+\int_{CA}e_{x}
ho dV_{n}$$

steady state:

$$0 = \sum_{j} (1 - rac{T_0}{T_j}) \dot{Q}_j - \dot{W}_{CV} + \sum_{i} \dot{m}_i e_{fi} - \sum_{e} \dot{m}_e e_{fe} - T_0 \dot{\sigma}$$

specific flow exergy:

$$e_f = (h-h_0) - T_0(s-s_0) + rac{V^2}{2} + gz$$
  $e_f = e_x + v(p-p_0)$ 

## Other System

存在非体积功输出:

$$TdS = dU + \delta W + \delta W_u \ \delta W_{u,max} = TdS - dU - pdV$$

● 定温-定容

$$F = U - TS$$
 
$$f = u - Ts$$
 
$$E_x = W_{u,v,max} = (U - TS) - (U_0 - T_0S_0) = F - F_0$$

F为亥姆霍兹自由能[强度量]

• 定温-定压

$$G=H-TS$$
  $g=h-Ts=u+pv-Ts$   $E_x=W_{u,p,max}=(H-TS)-(H_0-T_0S_0)=G-G_0$ 

G为吉布斯自由能(自由焓)[强度量]

• Exergetic Efficiency

Turbines

$$\begin{split} e_{f1} - e_{f2} &= \frac{\dot{W}}{\dot{m}} + \frac{\dot{E}_d}{\dot{m}} \\ \varepsilon &= \frac{\dot{W}/\dot{m}}{e_{f1} - e_{f2}} \end{split}$$

Compressors and Pumps

$$egin{aligned} -rac{\dot{W}}{\dot{m}} &= e_{f2} - e_{f1} + rac{\dot{E}_d}{\dot{m}} \ arepsilon &= rac{e_{f2} - e_{f1}}{-\dot{W}/\dot{m}} \end{aligned}$$

Heat Exchanger Without Mixing

$$egin{aligned} \dot{m}_h(e_{f1}-e_{f2}) &= \dot{m}_c(e_{f4}-e_{f3}) + \dot{E}_d \ arepsilon &= rac{\dot{m}_c(e_{f4}-e_{f3})}{\dot{m}_h(e_{f1}-e_{f2})} \end{aligned}$$

Heat Exchanger With Mixing

$$egin{aligned} \dot{m}_h(e_{f1}-e_{f3}) &= \dot{m}_c(e_{f3}-e_{f2}) + \dot{E}_d \ arepsilon &= rac{\dot{m}_c(e_{f3}-e_{f2})}{\dot{m}_h(e_{f1}-e_{f3})} \end{aligned}$$

• Cost Rate

# 4 Evaluating Properties

## 4.1 Ideal gas