

ACSE-2

Lecture 8

Conservation Equations &
Rheology

Outline

- Conservation equations
- Energy equation
- Rheology
- Elasticity and Wave Equation
- Newtonian Viscosity and Navier Stokes

Learning Objectives

- Learn main conservation equations used in continuum mechanics modelling and understand what different terms in these equations represent
- Be able to solve conservation equations for basic analytical solutions given boundary/initial conditions.
- Understand basic properties of elastic and viscous rheology and understand how the choice of rheology leads to different forms of the momentum conservation equation
- Using tensor analysis to obtain relations between the main isotropic elastic parameters

Continuum Mechanics Equations

General:

1. Kinematics – describing deformation and velocity without considering forces
2. Dynamics – equations that describe force balance, conservation of linear and angular momentum
3. Thermodynamics – relations temperature, heatflux, stress, entropy

Material-specific

4. Constitutive equations – relations describing how material properties vary as a function of T,P, stress,.... Such material properties govern dynamics (e.g., *density*), response to stress (*viscosity, elastic parameters*), heat transport (*thermal conductivity, heat capacity*)

Conservation equations

- Conservation of mass

- Kinematics

$$\frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} = 0$$

- Conservation of linear momentum

- Dynamics

- Newton's second law

$$\rho \mathbf{a} = \nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt}$$

- Conservation of energy

- First law of thermodynamics

$$\frac{D(K + U)}{Dt} = W + Q$$

K - kinetic energy, U - internal energy, W – power input, Q – heat input

2-D energy equation

*Spatial, constant ρ , C_p , k , incompressible
no heat sources*

- **Change in heat content**

$$\frac{\partial(\rho C_p T)}{\partial t} \delta x \delta y$$

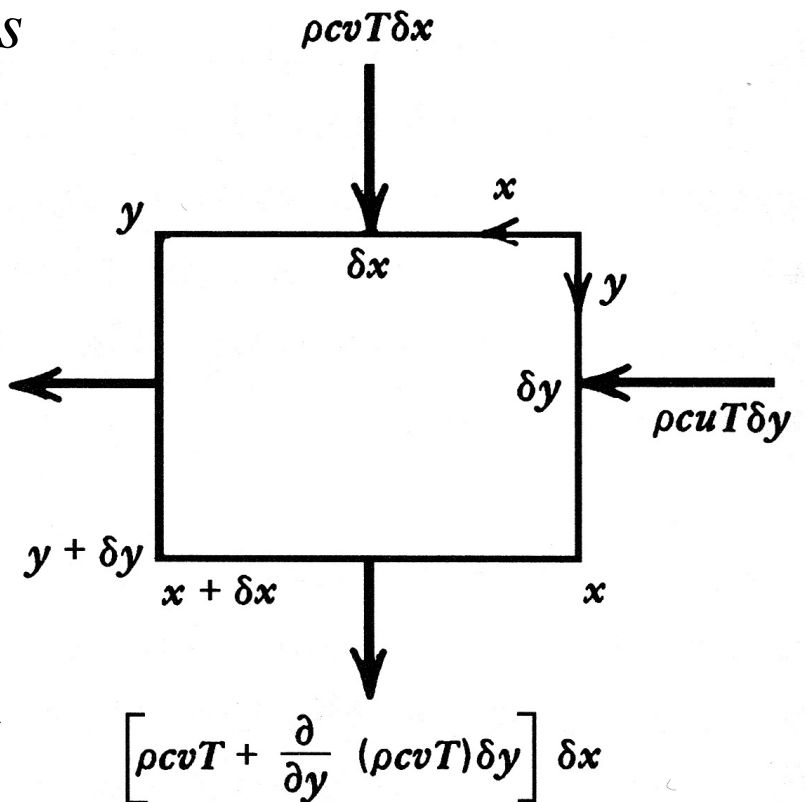
- **Advection**

$$\left[\frac{\partial(\rho C_p u T)}{\partial x} + \frac{\partial(\rho C_p v T)}{\partial y} \right] \delta x \delta y$$

conservation
of mass

How does this simplify?

- **Conduction**



C_p – heat capacity (J/kg/K)
 u, v – velocity

2-D energy equation

*Spatial, constant ρ , C_p , k , incompressible
no heat sources*

- **Change in heat content**

$$\frac{\partial(\rho C_p T)}{\partial t} \delta x \delta y$$

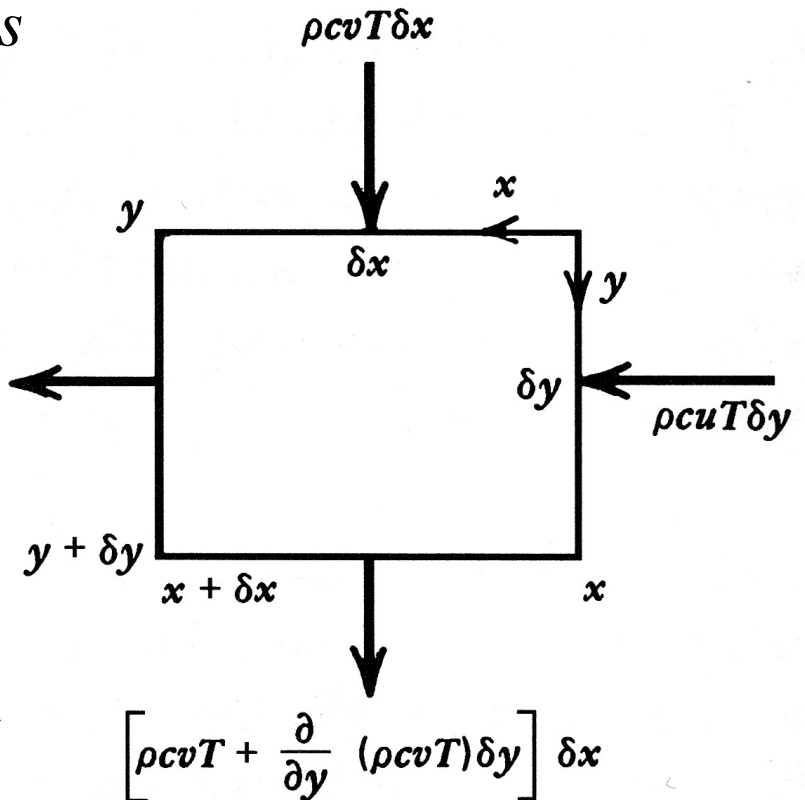
- **Advection**

$$\left[\frac{\partial(\rho C_p u T)}{\partial x} + \frac{\partial(\rho C_p v T)}{\partial y} \right] \delta x \delta y$$

$$\rho C_p \left[u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right] \delta x \delta y$$

conservation
of mass

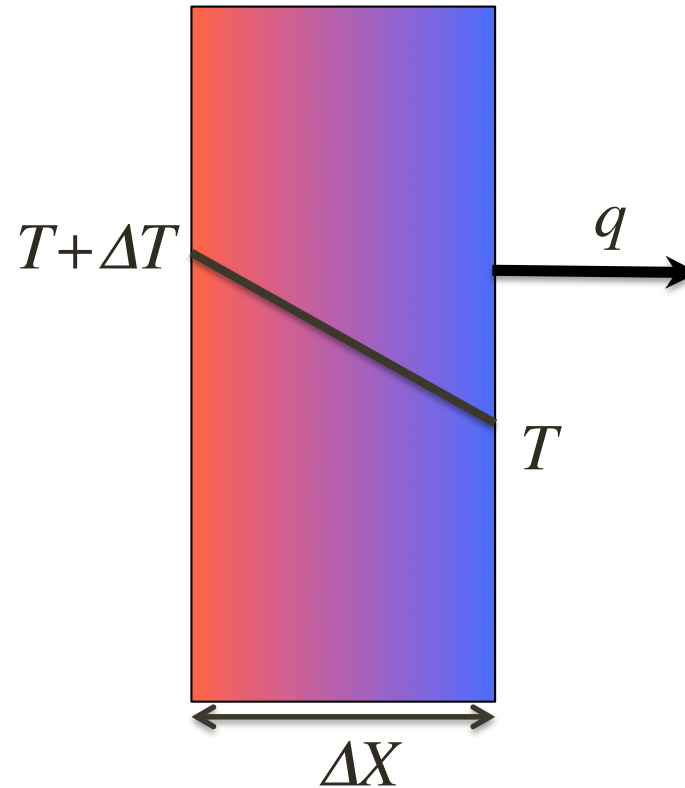
- **Conduction**



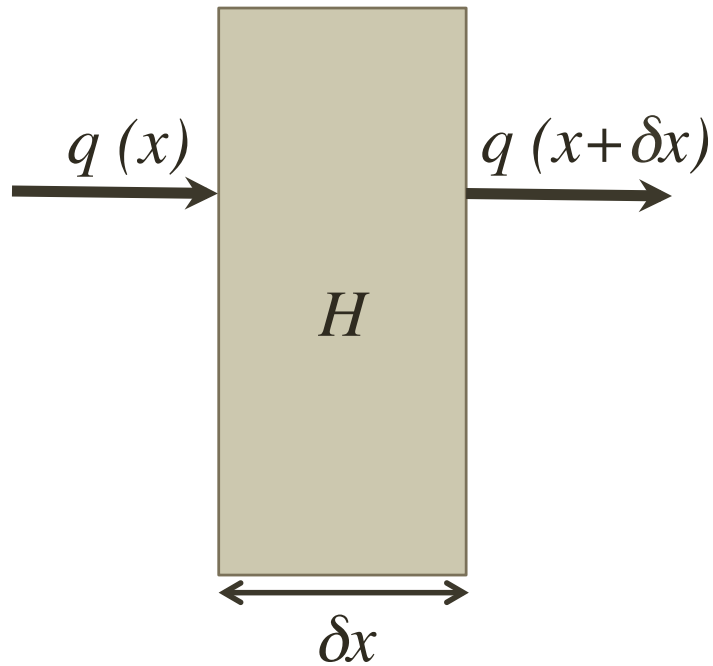
Fourier's Law for conduction

$$q = -k \frac{dT}{dx}$$

- *Heat flux*, q , = heat/area = energy/time/area,
unit: J/s/m² = W/m²
- Heat flux proportional to *temperature gradient*
- Minus sign because heat flows from hot to cold
- Constant of proportionality: *thermal conductivity*, k ,
unit: W/m/K



1-D Steady State Conduction



$$-k \frac{d^2 T}{dx^2} = \rho H = A$$

- **net heat flow/unit area/unit time =**

$$q(x + \delta x) - q(x)$$

$$q(x + \delta x) = q(x) + \delta x \frac{dq}{dx} + \dots$$

$$q(x + \delta x) - q(x) \approx \delta x \frac{dq}{dx}$$

$$\delta x \frac{dq}{dx} = \delta x \left[\frac{d}{dx} \left(-k \frac{dT}{dx} \right) \right]$$

$$\delta x \frac{dq}{dx} = \delta x \left[-k \frac{d^2 T}{dx^2} \right] \quad \text{for constant } k$$

- **heat produced = $\rho H \delta x = A \delta x$**

H - heat production rate/unit mass (W/kg)

A – heat production/unit volume (W/m³)

2-D energy equation

Spatial, constant ρ, C_p, k , , incompressible, no heat production

- **Change in heat content**

$$\frac{\partial(\rho C_p T)}{\partial t} \delta x \delta y$$

- **Advection**

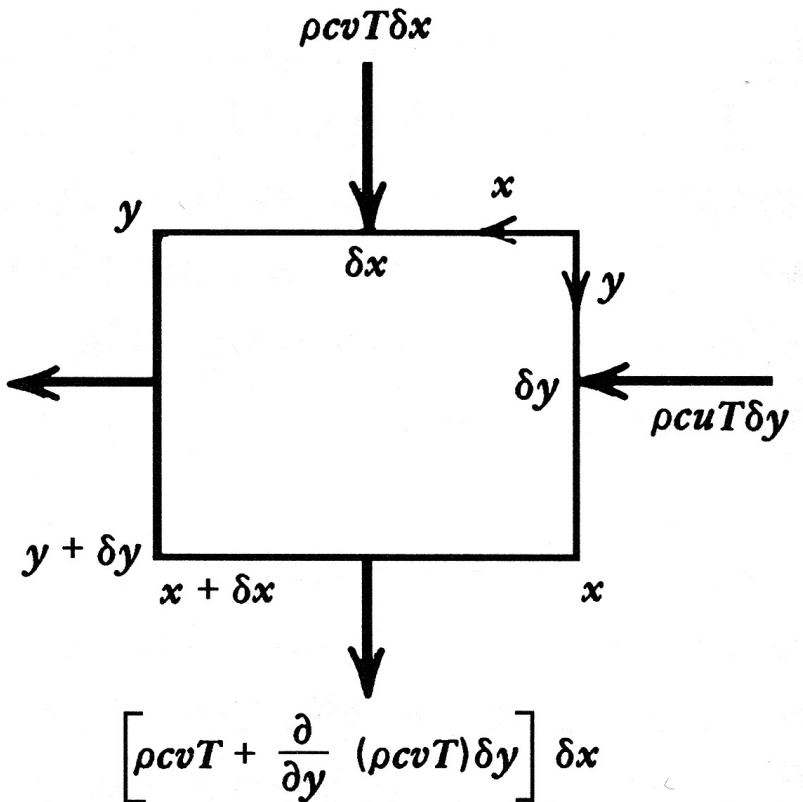
$$\left[\frac{\partial(\rho C_p u T)}{\partial x} + \frac{\partial(\rho C_p v T)}{\partial y} \right] \delta x \delta y$$

$$\rho C_p \left[u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right] \delta x \delta y$$

conservation
of mass

- **Conduction**

$$-k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) \delta x \delta y$$



2-D energy equation

Spatial, constant ρ, C_p, k , , incompressible, no heat production

- **Change in heat content**

$$\frac{\partial(\rho C_p T)}{\partial t} \delta x \delta y = \rho C_p \frac{\partial T}{\partial t} \delta x \delta y$$

- **Advection**

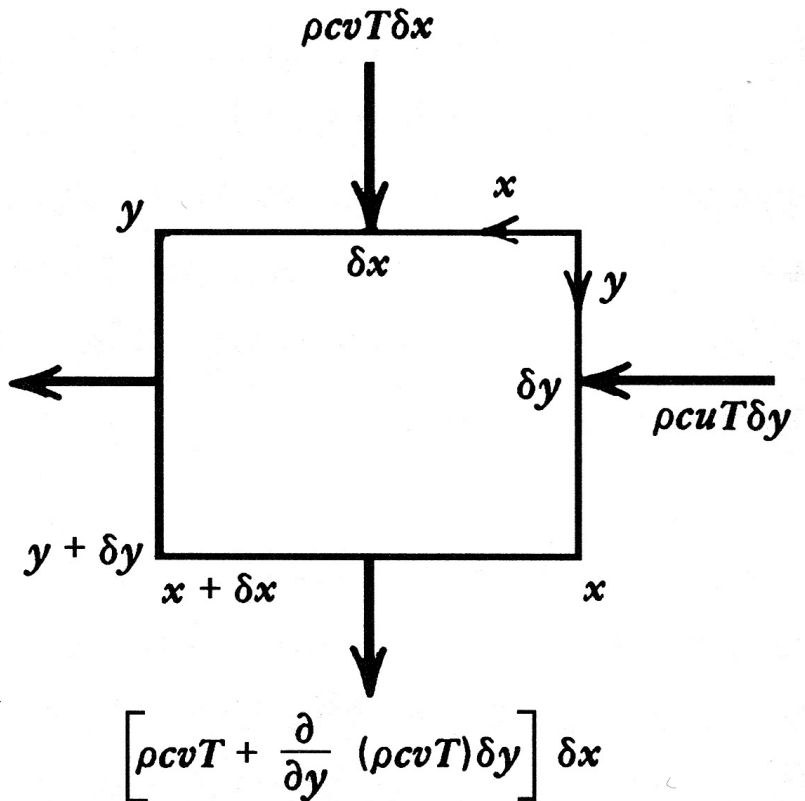
$$\left[\frac{\partial(\rho C_p u T)}{\partial x} + \frac{\partial(\rho C_p v T)}{\partial y} \right] \delta x \delta y$$

conservation
of mass

$$\rho C_p \left[u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right] \delta x \delta y$$

- **Conduction**

$$-k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) \delta x \delta y$$



$$\rho C_p \left[\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right] = k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$$

$$\rho C_p \left[\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right] = k \nabla^2 T$$

Energy equation

$$\frac{D(K + U)}{Dt} = W + Q$$

- **Material derivative internal heat**

$$\rho C_p \left[\frac{\partial T}{\partial t} + u \cdot \nabla T \right] = \rho C_p \frac{DT}{Dt} \Rightarrow \frac{D(\rho C_p T)}{Dt}$$

Allowing for
spatial
variations of
material
parameters

- **Heat input**

$$k \nabla^2 T \Rightarrow \nabla \cdot k \nabla T$$

Conduction

$$+A$$

Internal heat production

- **Work done**

\Rightarrow Changes in *motion* (kinetic energy) and *internal deformation*

Net effect of $W - \frac{DK}{Dt}$ becomes

$$\sigma : \mathbf{D}$$

\mathbf{D} – strain rate

1-D advection-diffusion solution

$$-v_z \frac{\partial T}{\partial z} = \kappa \frac{\partial^2 T}{\partial z^2}$$

$$\kappa = \frac{k}{\rho C_p}$$

Take $f(z) = \frac{\partial T}{\partial z}$ and $c = \frac{v_z}{\kappa}$

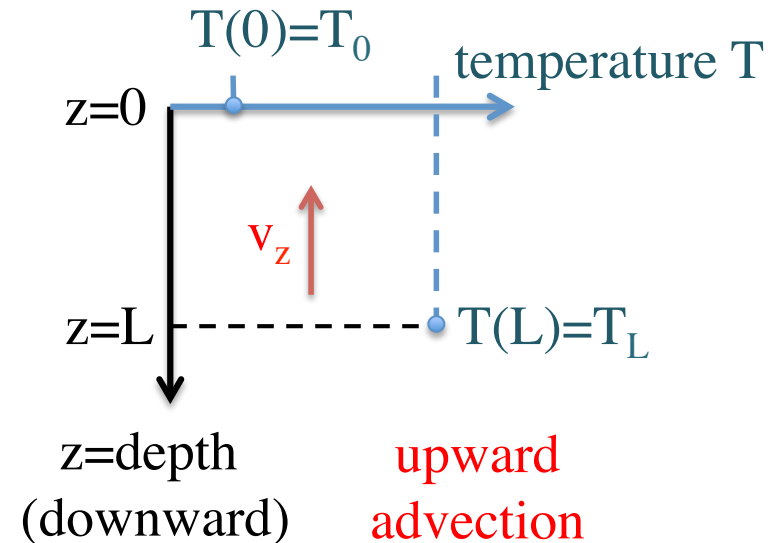
Then $\frac{\partial f}{\partial z} = -cf(z)$

\Rightarrow This yields $f(z) = f(0)e^{-cz}$, i.e. $\frac{\partial T}{\partial z}(z) = A e^{-v_z z / \kappa}$ where A, B are integration constants

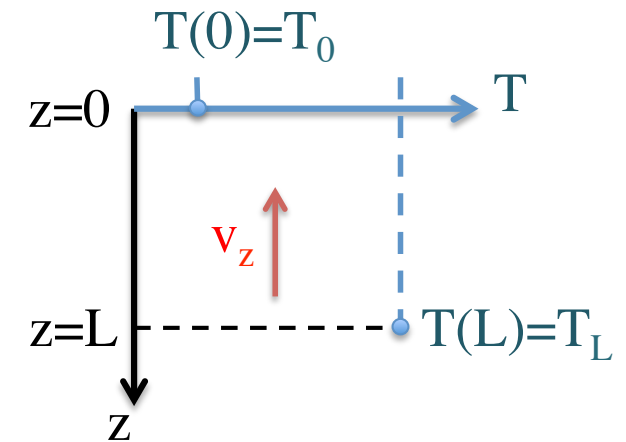
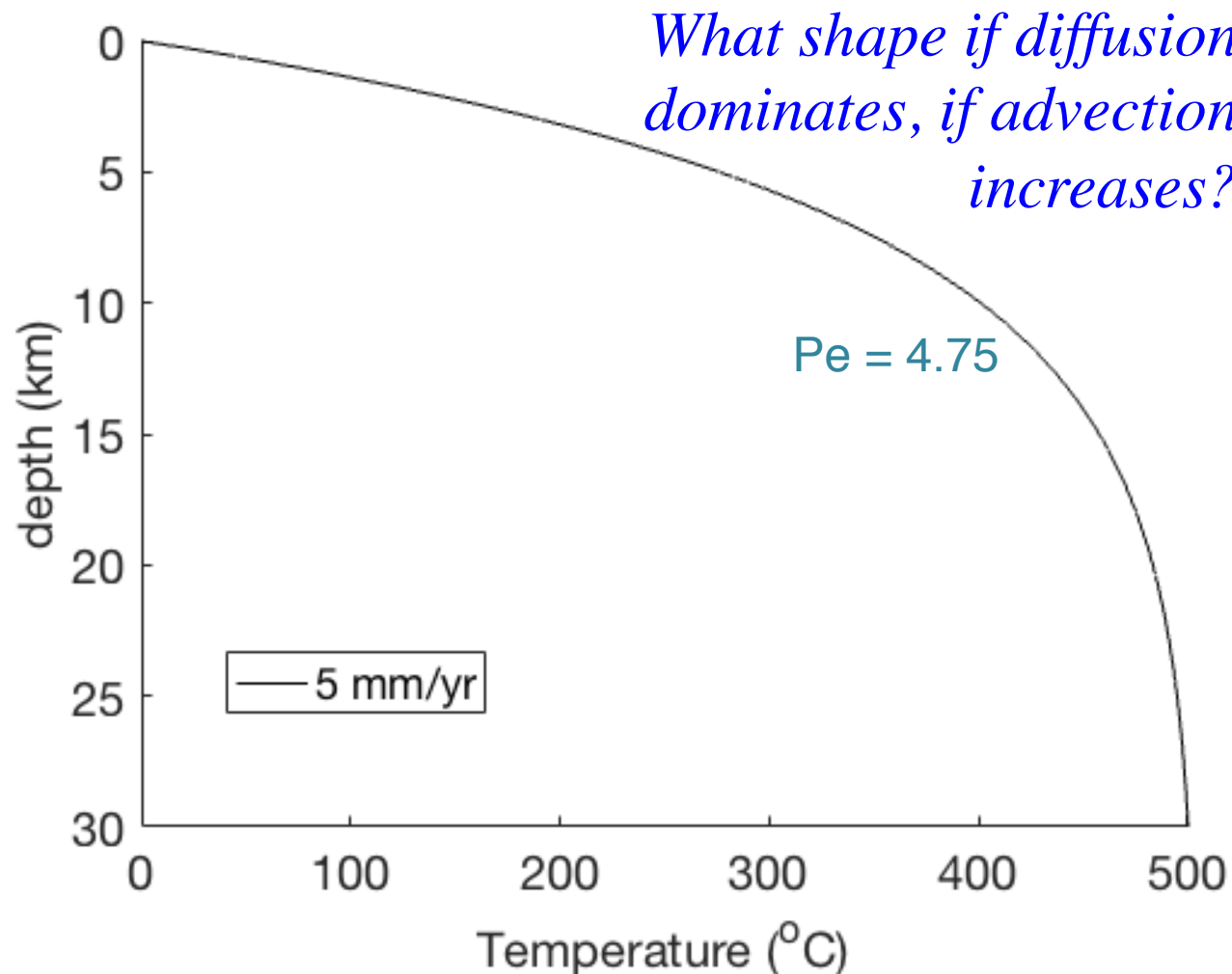
$$T(z) = B - \frac{A}{v_z / \kappa} e^{-v_z z / \kappa}$$

For constant temperature boundary conditions $T(z=0)=T_0$ and $T(z=L)=T_L$

\Rightarrow Integration gives:
$$T(z) = T_L \left[\frac{1 - e^{-v_z z / \kappa}}{1 - e^{-v_z L / \kappa}} \right]$$



1-D advection-diffusion solution



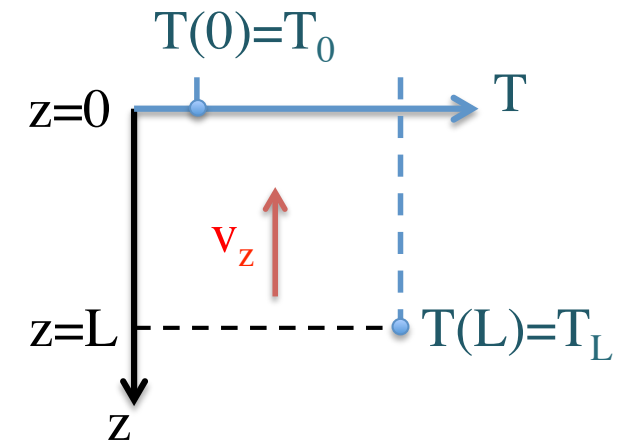
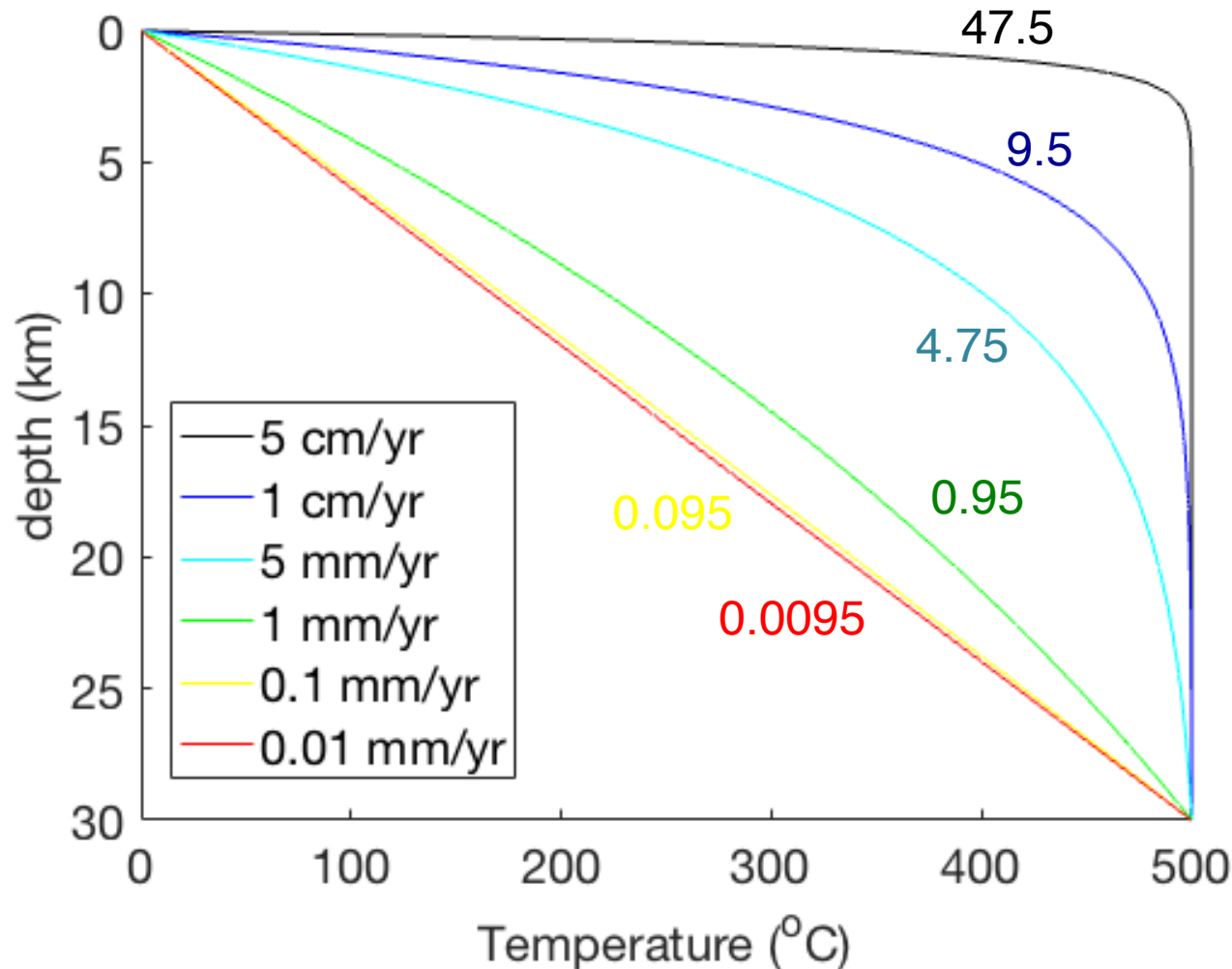
$$T(z) = T_L \left[\frac{1 - e^{-v_z z / \kappa}}{1 - e^{-v_z L / \kappa}} \right]$$

advdiff.ipynb

Peclet number, measure of relative importance advection/diffusion

$$Pe = \frac{v_z L}{\kappa} = \frac{[(m/s)m]}{[m^2/s]}$$

1-D advection-diffusion solution



$$T(z) = T_L \left[\frac{1 - e^{-v_z z / \kappa}}{1 - e^{-v_z L / \kappa}} \right]$$

advdiff.ipynb

Peclet number, measure of relative importance advection/diffusion

$$Pe = \frac{v_z L}{\kappa} = \frac{[(m/s)m]}{[m^2/s]}$$

Energy equation

conservation of heat

I	II	III	IV	V	VI
$D(\rho C_p T)/Dt =$	$\nabla \cdot \mathbf{k} \nabla T$	$+ A$	$+ \boldsymbol{\sigma} : \mathbf{D}$	$(+ \alpha T \mathbf{v} \cdot \nabla P$	$\dots)$

I - change in temperature with time

II - heat transfer by conduction (and radiation)

III - heat production (including latent heat)

IV - heat generated by internal deformation

V - heat generated by adiabatic compression

VI - other heat sources, e.g. latent heat

Conservation equations

- Conservation of mass $\frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} = 0$
- Conservation of linear momentum $\rho \frac{D\mathbf{v}}{Dt} = \nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f}$
- Conservation of angular momentum: $\boldsymbol{\sigma} = \boldsymbol{\sigma}^T$
- Conservation of energy $\frac{D(\rho C_p T)}{Dt} = \nabla \cdot k \nabla T + A + \boldsymbol{\sigma} : \mathbf{D}$
- Entropy inequality *Rate of entropy increase of a particle always \geq entropy supply*
 Which law is this?

Continuum Mechanics Equations

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Thermal parameters

Can you name 4 material parameters that affect temperatures
or how material responds to changes in temperature

*Each of these may depend on T , P , phase,
composition, ...*

Thermal parameters

k - thermal conductivity (W/m/K)

A - heat production (W/m³)

C_p - heat capacity (specific heat) at constant pressure (J/kg/K)

α - thermal expansion coefficient (1/K)

$$\alpha = (1/V)[\partial V/\partial T]_P = (1/\rho)[\partial \rho/\partial T]_P$$

κ - thermal diffusivity $k/\rho/C_p$ (m²/s)

Where used?

Each of these may depend on T, P, phase, composition, ...

Continuum Mechanics Equations

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Rheology

$$\text{deformation (E)} = \text{rheology} \cdot \text{stress } (\sigma)$$

material response to stress, depends on
material, P,T, time, deformation
history, environment (volatiles,
water)

- *elastic*
- *viscous*
- *brittle*
- *plastic*

- experiments under simple stress conditions
⇒ strain evolution under constant stress,
stress-strain rate diagrams
- thermodynamics + experimental parameters
- ab-initio calculations

Recap Fluid - Solid

- What is a solid?

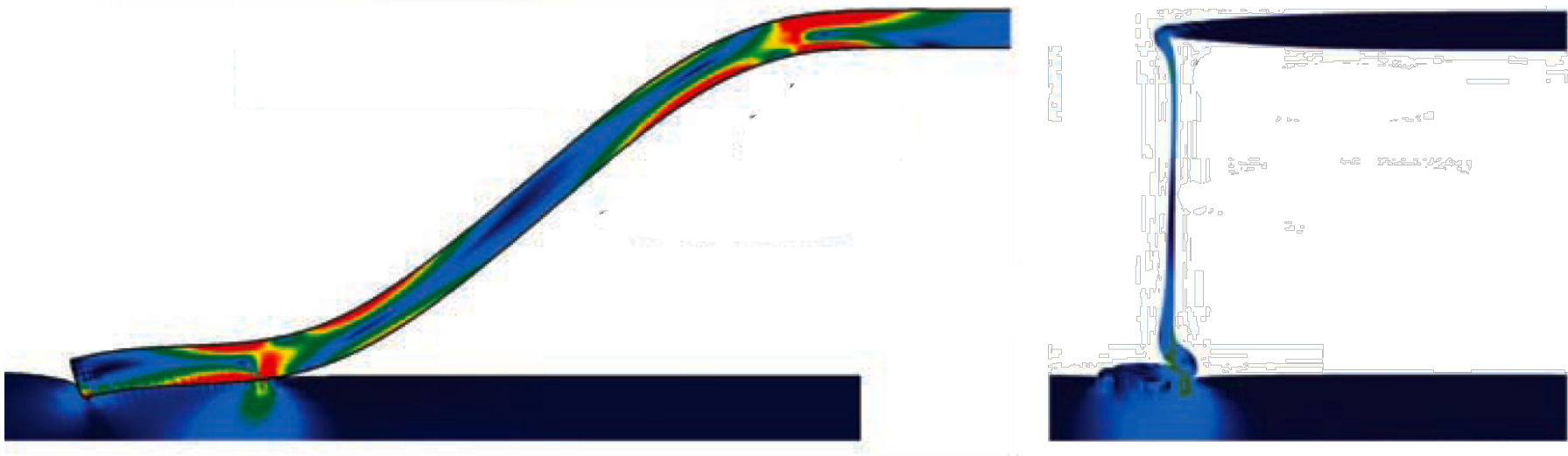
A solid acquires finite deformation under stress

stress $\sigma \sim$ strain ε

- What is a fluid?

A material that flows in response to applied stress

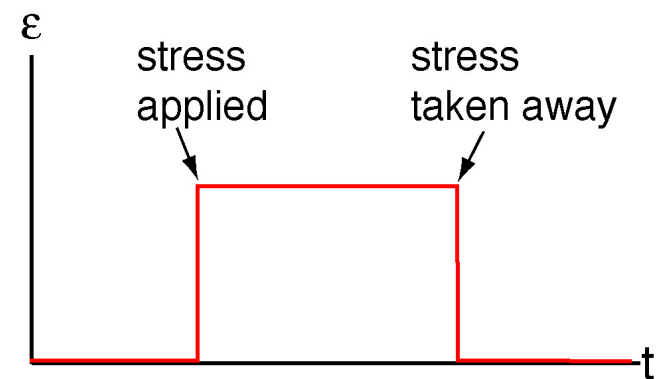
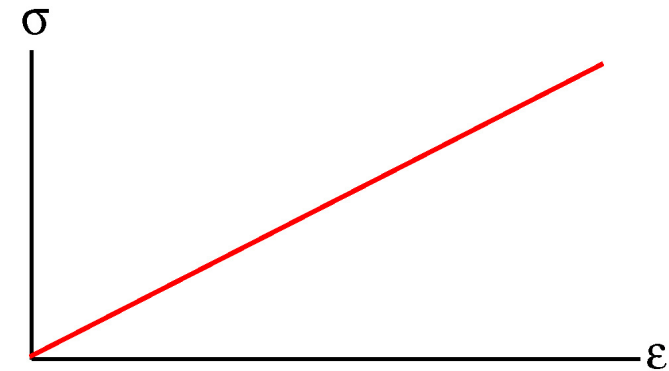
stress $\sigma \sim$ *strain rate* $D\varepsilon/Dt$



Figures from Funiciello et al. (2003a)

Elasticity

- linear response to load applied
- instantaneous
- completely recoverable
- below threshold (yielding) stress
- *dominates behaviour of coldest part of tectonic plates on time scales of up to 100 m.y. -> fault loading*
- *on time scale of seismic waves the whole Earth is elastic*
- $\sigma_{ij} = C_{ijkl} \epsilon_{kl}$ - Hooke's law
 C_{ijkl} - rank 4 elasticity tensor
 3^4 elements, up to 21 independent



$\epsilon = E$, to avoid confusion with Young's modulus E

Elasticity tensor

C_{ijkl} $3^4=81$ elements (for $n=3$)

- symmetry of σ_{ij} and ε_{kl}
 \Rightarrow only 36 independent elements

Why 36?

- conservation of elastic energy $U=\boldsymbol{\sigma}:\boldsymbol{\varepsilon}=\mathbf{C}:\boldsymbol{\varepsilon}:\boldsymbol{\varepsilon} \geq 0$
 $\Rightarrow C_{ijkl}=C_{klij}$
 \Rightarrow only 21 independent elements - most general form of \mathbf{C}
- other symmetries further reduce the number of independent elements

Elasticity tensor

- for example for isotropic media

Only 2 independent elements (λ, μ):

$$\begin{aligned}\sigma_{ij} &= \lambda \delta_{ij} \delta_{kl} \varepsilon_{kl} + \alpha \delta_{ik} \delta_{jl} \varepsilon_{kl} + \beta \delta_{il} \delta_{jk} \varepsilon_{kl} \\ &= \lambda \delta_{ij} \varepsilon_{kk} + \alpha \varepsilon_{ij} + \beta \varepsilon_{ji} \\ &= \lambda \delta_{ij} \theta + (\alpha + \beta) \varepsilon_{ij}\end{aligned}$$

$$\Rightarrow \underline{\sigma_{ij} = \lambda \theta \delta_{ij} + 2\mu \varepsilon_{ij}}$$

What is isotropic?

3 isotropic rank

4 tensors:

$$\delta_{ij} \delta_{kl}, \delta_{ik} \delta_{jl}, \delta_{il} \delta_{jk}$$

Hooke's law for isotropic material: 2 independent coefficients

Lamé constants

λ and μ : $\sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}$

Bulk and shear modulus

\mathbf{K} and $\mu=\mathbf{G}$: $\sigma_{ij} = -p\delta_{ij} + \sigma'_{ij}$
where: $-p = \frac{\sigma_{kk}}{3} = \left(\lambda + \frac{2}{3}\mu \right) \theta = K\theta$
 $\sigma'_{ij} = \lambda\theta\delta_{ij} + 2\mu\varepsilon_{ij} + p\delta_{ij} = 2\mu\varepsilon'_{ij}$

hydrostatic

deviatoric

Young's modulus and Poisson's ratio

\mathbf{E} and ν : $E = \sigma_{11}/\varepsilon_{11}$, $\nu = -\varepsilon_{33}/\varepsilon_{11}$ (uniaxial stress)

Determine in homework set

Wave equation

For infinitesimal deformation:

spatial coordinates \approx material coordinates

$$v_i \text{ (spatial)} \approx \partial u_i / \partial t$$

$$a_i \text{ (spatial)} \approx \partial v_i / \partial t = \partial^2 u_i / \partial t^2$$

$$\text{Equation of motion: } f_i + \partial \sigma_{ji} / \partial x_j = \rho \partial^2 u_i / \partial t^2 \quad (1)$$

$$\text{Elastic rheology: } \sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij} \quad (2)$$

Substitute (2) in (1) if (infinitesimal) deformation is consequence of force balance

Wave equation

Equation of motion: $\mathbf{f}_i + \partial \sigma_{ji} / \partial x_j = \rho \partial^2 \mathbf{u}_i / \partial t^2$

Elastic rheology: $\sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}$

$$\begin{aligned} \partial \sigma_{ji} / \partial x_j &= \lambda \partial \varepsilon_{kk} / \partial x_i + \mu \partial (\partial u_i / \partial x_j + \partial u_j / \partial x_i) / \partial x_j \\ &= \lambda \partial (\partial u_k / \partial x_k) / \partial x_i + \mu \partial^2 u_i / \partial^2 x_j + \mu \partial (\partial u_j / \partial x_j) / \partial x_i \end{aligned}$$

$\nabla \cdot \boldsymbol{\sigma} =$ Write vector equation

Using: $\nabla^2 \mathbf{u} = \nabla(\nabla \cdot \mathbf{u}) - \nabla \times \nabla \times \mathbf{u}$

$$\Rightarrow \boxed{\rho \partial^2 \mathbf{u} / \partial t^2 = \mathbf{f} + (\lambda + 2\mu) \nabla(\nabla \cdot \mathbf{u}) - \mu \nabla \times \nabla \times \mathbf{u}}$$

what type of deformation do the two terms represent?

Wave equation

Equation of motion: $\mathbf{f}_i + \partial \sigma_{ji} / \partial x_j = \rho \partial^2 \mathbf{u}_i / \partial t^2$

Elastic rheology: $\sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}$

$$\begin{aligned} \partial \sigma_{ji} / \partial x_j &= \lambda \partial \varepsilon_{kk} / \partial x_i + \mu \partial (\partial u_i / \partial x_j + \partial u_j / \partial x_i) / \partial x_j \\ &= \lambda \partial (\partial u_k / \partial x_k) / \partial x_i + \mu \partial^2 u_i / \partial^2 x_j + \mu \partial (\partial u_j / \partial x_j) / \partial x_i \end{aligned}$$

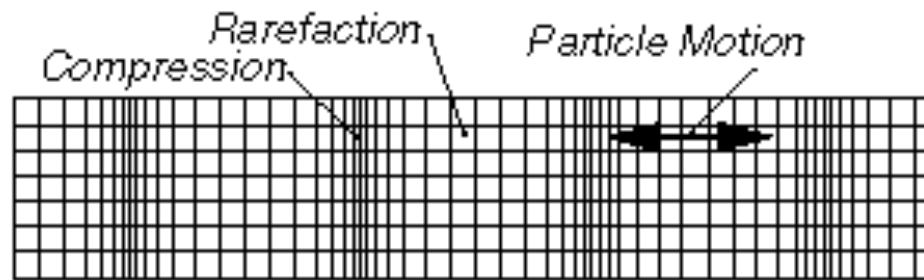
$$\nabla \cdot \boldsymbol{\sigma} = (\lambda + \mu) \nabla (\nabla \cdot \mathbf{u}) + \mu \nabla^2 \mathbf{u}$$

Using: $\nabla^2 \mathbf{u} = \nabla (\nabla \cdot \mathbf{u}) - \nabla \times \nabla \times \mathbf{u}$

$$\Rightarrow \boxed{\rho \partial^2 \mathbf{u} / \partial t^2 = \mathbf{f} + (\lambda + 2\mu) \nabla (\nabla \cdot \mathbf{u}) - \mu \nabla \times \nabla \times \mathbf{u}}$$

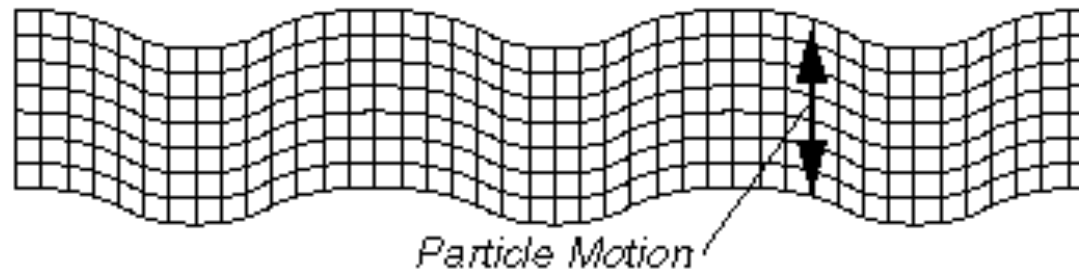
what type of deformation do the two terms represent?

P wave



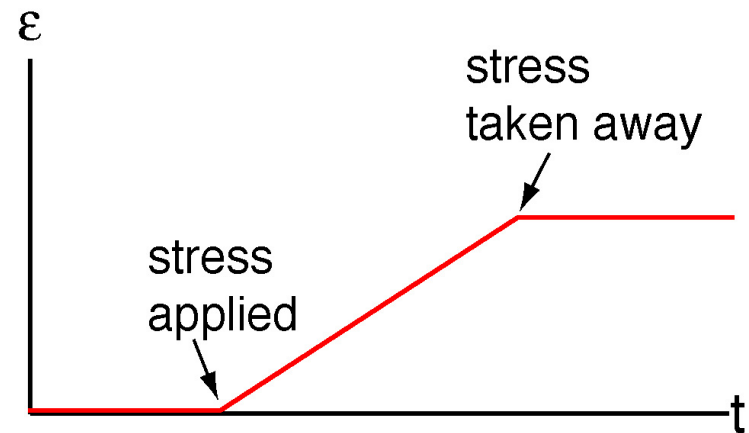
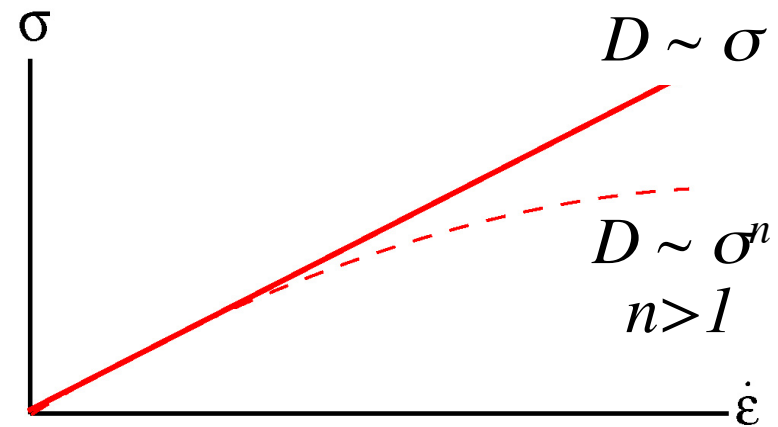
Travel Direction →

S wave



Viscous Flow

- steady state flow at constant stress
- permanent deformation
- linear (Newtonian) or non-linear (e.g., Powerlaw) relation between strain rate and stress
- isotropic stress does not cause flow
- *on timescales > years lower tectonic plates and mantle deform predominantly viscously -> plate motions, postseismic deformation, but also glaciers, magmas*



Hydrostatics

Fluids can not support shear stresses

i.e. if in rest/rigid body motion:

$$\boldsymbol{\sigma} \cdot \hat{\mathbf{n}} = \lambda \hat{\mathbf{n}}$$

and this normal stress is the same on any plane: $\boldsymbol{\sigma} = -p\mathbf{I}$

p is *hydrostatic pressure*

In force balance:
$$\nabla \cdot \boldsymbol{\sigma} + \mathbf{f} = 0$$
$$\underline{-\nabla p = -\mathbf{f}}$$

In gravity field
$$\frac{\partial p}{\partial z} = \rho g \quad \Rightarrow \quad p_2 - p_1 = \rho g h$$

Newtonian Fluids

In general motion: $\boldsymbol{\sigma} = -p\mathbf{I} + \boldsymbol{\sigma}'$

In Newtonian fluids,
deviatoric stress varies *linearly* with *strain rate*, \mathbf{D}

$$D_{ij} = (\partial v_i / \partial x_j + \partial v_j / \partial x_i) / 2$$

For *isotropic*, Newtonian fluids, 2 *material parameters*:

Viscous stress tensor $\sigma'_{ij} = -\zeta D_{kk} \delta_{ij} + 2\eta D_{ij}$

where ζ is *bulk viscosity* and η *(shear) viscosity*, $\Delta = D_{kk} = \nabla \cdot \mathbf{v}$

$$\boldsymbol{\sigma} = (-p + \zeta \Delta) \mathbf{I} + 2\eta \mathbf{D}$$

p not always mean normal stress: $\sigma_{kk} = -3p + (3\zeta + 2\eta) D_{kk}$

Consider a Newtonian shear flow with
velocity field $v_1(x_2)$, $v_2=v_3=0$

What is **D**? What is **σ** ?

Consider a Newtonian shear flow with
velocity field $v_1(x_2)$, $v_2=v_3=0$

What is **D**? What is **σ** ?

$$D_{11}=D_{22}=D_{33}=0$$

$$\sigma_{11}=\sigma_{22}=\sigma_{33}=-p$$

$$D_{12}=D_{21}= \frac{1}{2} \frac{\partial v_1}{\partial x_2}$$

$$\sigma_{12}=\sigma_{21}= \eta \frac{\partial v_1}{\partial x_2}$$

$$D_{13}=D_{31}=D_{23}=D_{32}=0$$

$$\sigma_{13}=\sigma_{31}=\sigma_{23}=\sigma_{32}=0$$

Illustrates that η represents resistance to shearing

Navier-Stokes for incompressible Newtonian Flow

For incompressible fluids $\Delta=0$, so that: $\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta\mathbf{D}$

Force balance: $\nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt}$

Show that: $\frac{\partial \sigma_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \eta \frac{\partial^2 v_i}{\partial x_j \partial x_j}$ Assuming constant η

$$\nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} = -\nabla p + \eta \nabla^2 \mathbf{v}$$

Navier-Stokes for incompressible Newtonian Flow

For incompressible fluids $\Delta=0$, so that: $\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta\mathbf{D}$

Force balance: $\nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt}$

Show that:

$$\frac{\partial \sigma_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \eta \frac{\partial^2 v_i}{\partial x_j \partial x_j}$$

Assuming
constant η

$$\sigma_{ij} = -p\delta_{ij} + \eta \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right)$$

Because

$$\frac{\partial \sigma_{ij}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \eta \left(\frac{\partial^2 v_i}{\partial x_j \partial x_j} + \cancel{\frac{\partial^2 v_j}{\partial x_i \partial x_j}} \right)$$

$$\frac{\partial v_j}{\partial x_j} = \Delta = 0$$

$$\nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} = -\nabla p + \eta \nabla^2 \mathbf{v}$$

Navier-Stokes for incompressible Newtonian Flow

For incompressible fluids $\Delta=0$, so that: $\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta\mathbf{D}$

Force balance: $\nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt}$

Navier Stokes equation of motion:

$$-\nabla p + \eta \nabla^2 \mathbf{v} + \mathbf{f} = \rho \left[\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right] \quad \text{Assuming constant } \eta$$

Together with continuity, 4 equations, 4 unknowns (p, v_x, v_y, v_z)

$$\nabla \cdot \mathbf{v} = 0$$

Navier-Stokes for compressible Newtonian Flow

$$\boldsymbol{\sigma} = (-p + \zeta \Delta) \mathbf{I} + 2\eta \mathbf{D} \qquad \nabla \cdot \underline{\underline{\boldsymbol{\sigma}}} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt}$$

Navier Stokes equation of motion:

$$-\nabla p + (\zeta + \eta) \nabla \Delta + \eta \nabla^2 \mathbf{v} + \mathbf{f} = \rho \left[\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right] \quad \begin{array}{l} \text{Assuming} \\ \text{constant} \\ \zeta, \eta \end{array}$$

+ Conservation of mass:

$$\frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} = 0$$

6 equations

6 unknowns

$$(p, v_x, v_y, v_z, \rho, T)$$

+ Energy equation

+ Equation of state for $\rho(T, p)$

Continuum Mechanics Equations

General:

1. Kinematics – describing deformation and velocity without considering forces
2. Dynamics – equations that describe force balance, conservation of linear and angular momentum
3. Thermodynamics – relations temperature, heatflux, stress, entropy

Material-specific

4. Constitutive equations – relations describing how material properties vary as a function of T,P, stress,.... Such material properties govern dynamics (e.g., *density*), response to stress (*viscosity, elastic parameters*), heat transport (*thermal conductivity, heat capacity*)

Outline

- Conservation equations
- Energy equation
- Rheology
- Elasticity and Wave Equation
- Newtonian Viscosity and Navier Stokes

More reading on the topics covered in this lecture can be found in, for example: Lai et al. Ch 4.14-4-16, 6.18, Ch 5.1-5.6, Ch 6.1-6.7; Reddy parts of Ch 5 & Ch 6

Outline of course

- **1.** Mathematical essentials – *Matthew Piggott*
- **2.** Linear Algebra I – *Matthew Piggott*
- **3.** Linear Algebra II, ODEs– *Matthew Piggott*
- **4.** Verifying models– *Matthew Piggott*
- **5.** Vector and Tensor Calculus - *Saskia Goes*
- **6.** Stress principles - *Saskia Goes*
- **7.** Kinematics and strain - *Saskia Goes*
- **8.** Rheology and conservation equations - *Saskia Goes*
- **9.** Potential flow - *Stephen Neethling*
- **10.** Fluid flow I - *Stephen Neethling*
- **11.** Fluid flow II - *Stephen Neethling*
- **12.** Wave propagation - *Adrian Umpleby*

Exam

- **1.5 hours on Friday 10 January, 10-11:30**
- Analytical/short essay questions
- Questions as shorter non-computational ones from the problem sets/lecture examples
- Only most basic equations expected to remember. Others will be given.
- Study guide for exam to be released next week.
- An example exam will be released before Christmas break
- **Question and answer session Wednesday 8 January 10-12 am, Room 1.47**