

ELEC 3035, Lecture 7: Observer design

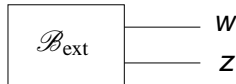
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- Observers
- Observer design by pole placement
- Duality between observer and controller design
- Pole placement by output feedback

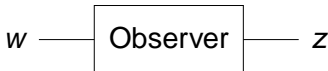
General observer design problem

Given dynamical system \mathcal{B}_{ext} with two types of external variables:

- observed variables w
- to-be-estimated variables z



find system (called observer) accepting w and producing z



We will consider the case: $\mathcal{B} = \mathcal{B}_{i/s/o}(A, B, C, D)$, $w = (u, y)$, $z = x$.

Lecture 6: nonrecursive, feedforward observer for the initial state $x(0)$

Now our goal is recursive **feedback observer for the current state $x(t)$**

Output feedback control separation and certainty principles

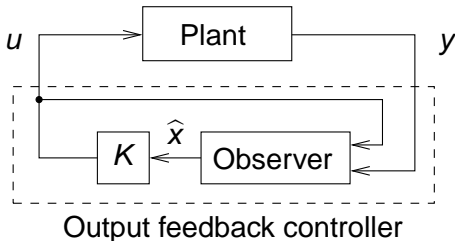
We can extend a given state-feedback controller

$$u = Kx$$

to output feedback controller

$$u = K\hat{x}$$

by using the observer state estimate \hat{x} in place of x .



Internal model and feedback principles

The observer design is based on the following principles:

1. **Internal model:** the model run by u , gives an estimate \hat{x} for x
2. **Feedback:** correct the estimate \hat{x} , so that the error

$$x(t) - \hat{x}(t) =: e(t) \rightarrow 0 \quad \text{as} \quad t \rightarrow \infty$$

Let the feedback be a linear function of the output error

$$\text{feedback correction} = L(y - \hat{y})$$

Then the observer for the model $\mathcal{B}_{i/s/o}(A, B, C, D)$ is

$$\begin{aligned}\sigma \hat{x} &= A\hat{x} + Bu - L(y - \hat{y}) \\ \hat{y} &= C\hat{x} + Du\end{aligned}$$

Error dynamics

Our goal is to choose L , so that the state error $e(t) \rightarrow 0$ as $t \rightarrow \infty$.

The dynamics of e is

$$\begin{aligned}\sigma e &= \sigma(x - \hat{x}) \\ &= Ax + Bu - A\hat{x} - Bu + L(y - \hat{y}) \\ &= A(x - \hat{x}) + LC(x - \hat{x}) \\ &= \underbrace{(A + LC)}_{A_0} e\end{aligned}$$

i.e., $e \in \mathcal{B}_{ss}(A_0)$ — an **autonomous LTI system**.

Therefore, $e(t) \rightarrow 0$ as $t \rightarrow \infty$ is equivalent to stability of $\mathcal{B}_{ss}(A_0)$.

Comparison with state-feedback stabilization

In the state feedback stabilization problem we have

$$\sigma x = Ax + Bu \quad \text{and} \quad u = Kx$$

which gives an autonomous LTI closed loop system

$$\sigma x = \underbrace{(A + BK)}_{A_c} x$$

and the aim is to choose K , so that $\mathcal{B}_{ss}(A_c)$ is stable.

Observer design by pole placement

The condition $e(t) \rightarrow 0$ as $t \rightarrow \infty$ is a minimum requirement.

In fact we want $e(t) \rightarrow 0$ fast

(possibly in a finite (small) number of steps \rightsquigarrow deadbeat observer)

The error dynamics is governed by the poles of the matrix

$$A_o := A + LC$$

so for desired error dynamics we can

select desired pole locations of A_o and choose L to achieve them.

Duality of the observer PP and controller PP problems

Observer PP problem: Choose L , so that

$$\det(zI - (A + LC)) = p_{\text{des}}(z)$$

Controller PP problem: Choose K , so that

$$\det(zI - (A + BK)) = p_{\text{des}}(z)$$

Observer PP is not a new problem:

$$\begin{aligned}\det(zI - (A + LC)) &= \det\left((zI - (A + LC))^{\top}\right) \\ &= \det\left(zI - (A^{\top} + C^{\top}L^{\top})\right) \\ &= \det\left(zI - (\tilde{A} + \tilde{B}\tilde{K})\right)\end{aligned}$$

\implies observer PP is controller PP for the dual system.

The results for state feedback PP can be restated for observer PP:

Theorem: The eigenvalues of $A + LC$ can be assigned choosing L to any locations in \mathbb{C} if and only if A, C is observable.

Observer canonical form \leftrightarrow Controller canonical form

Lemma:

- Let A, c and A', c' be two observable pairs and
- assume that A and A' have the same char. polynomials.

Then there is a unique similarity transformation given by the matrix

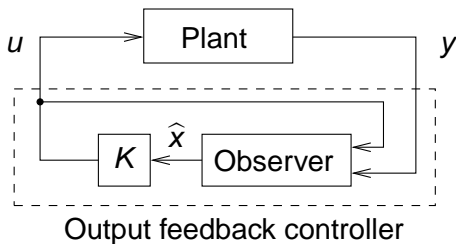
$$T := (\mathcal{O}(A', c'))^{-1} \mathcal{O}(A, c)$$

such that

$$T^{-1}AT = A' \quad \text{and} \quad cT = c'.$$

Closed-loop system with output feedback controller

Consider the closed loop system



where

Plant: $\sigma x = Ax + Bu, \quad y = Cx + Du$

Observer: $\sigma \hat{x} = A\hat{x} + Bu - L(y - C\hat{x} - Du)$

State feedback controller: $u = K\hat{x}$

Feedback controller:

$$\begin{aligned}\sigma \hat{x} &= (A + LC)\hat{x} + (B + LD)u - Ly, & u &= K\hat{x} \\ &= (A + LC + BK + LDK)\hat{x} - Ly\end{aligned}$$

Note: the feedback controller is a dynamical system

Closed-loop system:

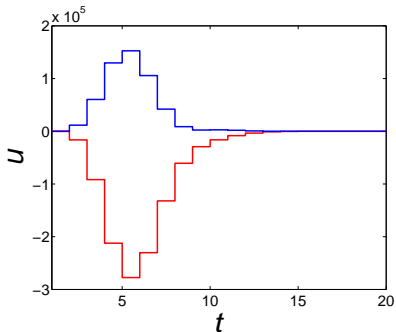
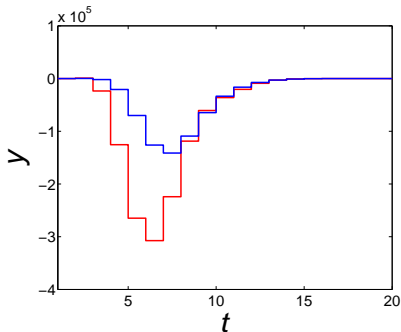
$$\sigma \begin{bmatrix} x \\ \hat{x} \end{bmatrix} = \begin{bmatrix} A & BK \\ -LC & A + LC + BK \end{bmatrix} \begin{bmatrix} x \\ \hat{x} \end{bmatrix}$$

Note: closed-loop system order = plant order + controller order

Error equation:

$$\sigma \begin{bmatrix} x \\ e \end{bmatrix} = \begin{bmatrix} A + BK & -BK \\ 0 & A + LC \end{bmatrix} \begin{bmatrix} x \\ e \end{bmatrix}$$

Example: output feedback deadbeat control



15th order single-input open-loop system, 30 order closed-loop system
(The same system as the one used in the example of Lecture 1)