

Flying Calligrapher: Contact-Aware Motion and Force Planning and Control for Aerial Manipulation

I. NEWTON EULER EQUATION

We define the position of the end-effector as \mathbf{p}_{ee} and the position of the vehicle center of gravity (cg) as \mathbf{p}_{cg} . Their velocity are denoted as \mathbf{v}_{ee} and \mathbf{v}_{cg} , respectively. We denote $\boldsymbol{\tau}_a = [\mathbf{f}_a, \mathbf{m}_a]$ as the control wrench and $\boldsymbol{\tau}_c = [\mathbf{f}_c, \mathbf{m}_c]$ as the contact wrench, where \mathbf{f} and \mathbf{m} denote the force component and torque component correspondingly. Denote m as the vehicle mass; J as the moment of inertia at the vehicle center of mass; $\mathbf{t}_B^\mathcal{E}$ as the relative translation between the vehicle body and the tip of the end-effector. All other definitions follow the main manuscripts.

Given the structure of the UAM, we have

$$\mathcal{B}\mathbf{p}_{cg} = \mathcal{B}\mathbf{p}_{ee} - \mathbf{t} \quad (1)$$

$$\mathcal{W}\mathbf{p}_{cg} = \mathcal{W}\mathbf{p}_{ee} - \mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t} \quad (2)$$

$$\mathcal{W}\mathbf{v}_{cg} = \mathcal{W}\mathbf{v}_{ee} - \boldsymbol{\Omega}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t} \quad (3)$$

$$\mathcal{W}\dot{\mathbf{v}}_{cg} = \mathcal{W}\dot{\mathbf{v}}_{ee} - (\dot{\boldsymbol{\Omega}}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t} + \boldsymbol{\Omega}\boldsymbol{\Omega}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}) \quad (4)$$

Here $\boldsymbol{\Omega}$ is the skew matrix corresponding to $\boldsymbol{\omega}$ in the body frame.

For the force component, under the world frame, we have

$$\mathcal{W}\mathbf{f}_a + \mathcal{W}\mathbf{f}_c - \mathcal{W}\mathbf{g} = m\dot{\mathbf{v}}_{cg} \quad (5)$$

Combining (4) and (5), we have:

$$\begin{aligned} \mathcal{W}\mathbf{f}_a + \mathcal{W}\mathbf{f}_c - \mathcal{W}\mathbf{g} &= m(\mathcal{W}\dot{\mathbf{v}}_{ee} - (\dot{\boldsymbol{\Omega}}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t} + \boldsymbol{\Omega}\boldsymbol{\Omega}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t})) \\ &= m\mathcal{W}\dot{\mathbf{v}}_{ee} + m[\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}]_\times\dot{\boldsymbol{\omega}} + m[\boldsymbol{\Omega}\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}]_\times\boldsymbol{\omega} \end{aligned} \quad (6)$$

Transforming back to the body frame (multiply $\mathbf{R}_{\mathcal{B}}^\mathcal{W}$) at both sides, we get the first half of the final equation.

$$\begin{aligned} \mathcal{E}\mathbf{f}_a + \mathcal{E}\mathbf{f}_c &= m\mathbf{R}_{\mathcal{E}}^\mathcal{W}\mathcal{W}\dot{\mathbf{v}}_{ee} \\ &\quad + m\mathbf{R}_{\mathcal{E}}^\mathcal{W}[\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}]_\times\dot{\boldsymbol{\omega}} \\ &\quad + m\mathbf{R}_{\mathcal{E}}^\mathcal{W}[\boldsymbol{\omega} \times \mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}]_\times\boldsymbol{\omega} + \mathcal{E}\mathbf{g} \end{aligned} \quad (7)$$

In terms of the torque component, we have:

$$\begin{aligned} \mathcal{B}\mathbf{m}_a + \mathcal{B}\mathbf{m}_c - \mathcal{B}\mathbf{g} &= \mathbf{J}_{cg}\dot{\boldsymbol{\omega}} + \boldsymbol{\omega} \times (\mathbf{J}_{cg}\boldsymbol{\omega}) \\ &= \mathbf{J}_{cg}\dot{\boldsymbol{\omega}} - [\mathbf{J}_{cg}\boldsymbol{\omega}]_\times\boldsymbol{\omega} \end{aligned} \quad (8)$$

Here $\mathbf{J}_{cg} = \mathbf{J}$ is the vehicle moment of inertia with respect to the cg in the body frame and is a constant value. Denote

\mathbf{J}_{ee} as the moment of inertia with respect to the ee in the body frame, we have:

$$\begin{aligned} \mathbf{J}_{ee} &= \mathbf{J}_{cg} + m\mathbf{t}_\times\mathbf{t}_\times^\top \\ &= \mathbf{J}_{cg} - m\mathbf{t}_\times\mathbf{t}_\times \end{aligned} \quad (9)$$

Focusing on the ee, we have:

$$\mathcal{E}\mathbf{m}_a + \mathcal{E}\mathbf{m}_c - \mathcal{E}\mathbf{g} = \mathbf{J}_{ee}\dot{\boldsymbol{\omega}} - [\mathbf{J}_{ee}\boldsymbol{\omega}]_\times\boldsymbol{\omega} \quad (10)$$

Combining (9) and (10), we have

$$\begin{aligned} (\mathbf{J}_{cg} - m\mathbf{t}_\times\mathbf{t}_\times)\dot{\boldsymbol{\omega}} - [(\mathbf{J}_{cg} - m\mathbf{t}_\times\mathbf{t}_\times)\boldsymbol{\omega}]_\times\boldsymbol{\omega} \\ = \mathcal{E}\mathbf{m}_a + \mathcal{E}\mathbf{m}_c - \mathcal{E}\mathbf{g} \end{aligned} \quad (11)$$

Combining (6) and (11), we have the final dynamic equation:

$$\mathbf{M}\dot{\mathbf{v}} + \mathbf{C}\mathbf{v} + \mathbf{A}d_{T_\mathcal{E}^\mathcal{B}}^\mathcal{B}\mathbf{g} = \mathbf{A}d_{T_\mathcal{E}^\mathcal{B}}^\mathcal{B}\boldsymbol{\tau}_a + \mathbf{A}d_{T_\mathcal{E}^\mathcal{C}}^\mathcal{C}\boldsymbol{\tau}_c \quad (12)$$

where

$$\mathbf{M} = \begin{bmatrix} m\mathbf{R}_{\mathcal{E}}^\mathcal{W} & m\mathbf{R}_{\mathcal{E}}^\mathcal{W}[\mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}_B^\mathcal{E}]_\times \\ \mathbf{0}_{3 \times 3} & \mathbf{J} - m[\mathbf{t}_B^\mathcal{E}]_\times[\mathbf{t}_B^\mathcal{E}]_\times \end{bmatrix} \quad (13)$$

$$\mathbf{C} = \begin{bmatrix} \mathbf{0}_{3 \times 3} & m\mathbf{R}_{\mathcal{E}}^\mathcal{W}[\boldsymbol{\omega} \times \mathbf{R}_{\mathcal{W}}^\mathcal{B}\mathbf{t}_B^\mathcal{E}]_\times \\ \mathbf{0}_{3 \times 3} & -[(\mathbf{J} - m[\mathbf{t}_B^\mathcal{E}]_\times[\mathbf{t}_B^\mathcal{E}]_\times)\boldsymbol{\omega}]_\times \end{bmatrix} \quad (14)$$