

# Report

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## Proofs

Thm1. Angular acceleration derivation for rigid body:  $\beta = I^{-1}\tau - I^{-1}[\omega]I\omega$ , where  $I$  is momentum of inertia according to centroid under ground reference frame,  $\tau$  is total moment of force according to centroid,  $\omega$  is angular velocity,  $[\omega]$  is the skew matrix of  $\omega$  which is defined as

$$[\omega] = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{bmatrix} \quad (1)$$

(In this case:  $\omega \times v = [\omega]v$ )

Proof: Firstly prove some lemmas.

Lemma 1.  $I_{\text{centroidsystem}} = RI_{\text{rigidbodysystem}}R^\top$ , where  $R$  is the rotation matrix that transfer position vector from rigid body system to centroid system (Notice: this is a **translational system**), i.e.  $r^{(\text{centroidsystem})} = Rr^{(\text{rigidbodysystem})}$ .

Proof: From definition of  $I$ :

$$\begin{aligned} I_{\text{centroidsystem}} &= \int \left[ \|r^{(\text{centroidsystem})}\|^2 I_3 - r^{(\text{centroidsystem})}r^{(\text{centroidsystem})^\top} \right] dm \\ &= \int \left[ \|Rr^{(\text{rigidbodysystem})}\|^2 I_3 - Rr^{(\text{rigidbodysystem})}(Rr^{(\text{rigidbodysystem})})^\top \right] dm \\ &= \int \left[ \|Rr^{(\text{rigidbodysystem})}\|^2 I_3 - Rr^{(\text{rigidbodysystem})}r^{(\text{rigidbodysystem})^\top} R^\top \right] dm \\ &= \int \left[ \|r^{(\text{rigidbodysystem})}\|^2 I_3 - Rr^{(\text{rigidbodysystem})}r^{(\text{rigidbodysystem})^\top} R^\top \right] dm \\ &= \int \left[ R\|r^{(\text{rigidbodysystem})}\|^2 I_3 R^\top - Rr^{(\text{rigidbodysystem})}r^{(\text{rigidbodysystem})^\top} R^\top \right] dm \\ &= R \left\{ \int \left[ \|r^{(\text{rigidbodysystem})}\|^2 I_3 - r^{(\text{rigidbodysystem})}r^{(\text{rigidbodysystem})^\top} \right] dm \right\} R^\top \\ &= RI_{\text{rigidbodysystem}}R^\top \end{aligned} \quad (2)$$

Notice that  $I$  is an (positive) symmetric matrix, so carefully choosing reference frame of rigid body system results  $I_{\text{rigidbodysystem}}$  to be a **diagonal** matrix.

Lemma 2: Angular momentum theorem according to the reference point on the rigid body:  $\tau = \frac{dL}{dt} = I_{\text{centroidsystem}}\beta + \frac{dI_{\text{centroidsystem}}}{dt}\omega$ .

Proof: From definition of angular momentum,

$$L = \int r \times v dm \quad (3)$$

Thus

$$\frac{dL}{dt} = \int v \times v + r \times a dm = \int r \times a dm \quad (4)$$

Applying Newton's second law,

$$\frac{dL}{dt} = \int r \times dF = \tau \quad (5)$$

where  $\tau$  is total moment of force according to this reference point.

Calculating  $L$ :

$$L = \int r \times (\omega \times r) dm = \int (r \cdot r)\omega - r(r \cdot \omega) dm = \int \|r\|^2 \omega - r r^\top \omega dm = \left[ \int \|r\|^2 - r r^\top dm \right] \omega = I \omega \quad (6)$$

where  $I$  is the momentum of inertia under centroid (translational) reference, i.e.  $I = I_{\text{centroidsystem}}$ . (Also is the momentum of inertia calculated under ground system. ) Omit subscripts where there is no ambiguity in the following text.

Without proof, using a conclusion in derivative of exponential matrix, we introduce that  $\frac{dR}{dt} = [\omega]R$ .

Lemma 3:  $\frac{dR^\top}{dt} = -R^\top[\omega]$ .

Proof: From  $RR^\top \equiv I_3$ , take derivative of both side:

$$\frac{dR}{dt}R^\top + R\frac{dR^\top}{dt} = 0 \quad (7)$$

Where

$$L.H.S. = [\omega]RR^\top + R\frac{dR^\top}{dt} = [\omega] + R\frac{dR^\top}{dt} \quad (8)$$

Which draws the result.

Lemma 4:  $\frac{dI}{dt} = [\omega]I - I[\omega]$ .

This follows from Lemma 1 and 3 immediately.

Then the proof of Thm. 1 begins:

From Angular momentum theorem according to centroid on the rigid body, combining previous lemmas,

$$\tau = \frac{dL}{dt} = I\beta + \frac{dI}{dt}\omega = I\beta + ([\omega]I - I[\omega])\omega = I\beta + [\omega]I\omega \quad (9)$$

Last step follows from  $[\omega]\omega = \mathbf{0}$ . Thus

$$\beta = I^{-1}\tau - I^{-1}[\omega]I\omega \quad (10)$$

Proof 2. Collision of rigid body

TODO.

Proof 3. Updating error of velocity, angular velocity ( $O(\delta t)^3$ ); position, rotation matrix ( $O(\delta t)^4$ )

Updating rules:

$$v_{t+\delta t} = v_t + \frac{3a_t - a_{t-\delta t}}{2} \delta t \quad (11)$$

$$\omega_{t+\delta t} = \omega_t + \frac{3\beta_t - \beta_{t-\delta t}}{2} \delta t \quad (12)$$

$$x_{t+\delta t} = x_t + v_t \delta t + \frac{4a_t - a_{t-\delta t}}{6} (\delta t)^2 \quad (13)$$

$$R_{t+\delta t} = \left\{ e^{[\omega(t) + \frac{4\beta(t) - \beta(t-\delta t)}{6} \delta t] \delta t} - \frac{1}{12} ([\beta(t)][\omega(t)] + [\omega(t)][\beta(t)])(\delta t)^3 \right\} R(t) \quad (14)$$

Proof: For the first 2 terms,

$$f(t + \delta t) = f(t) + f'(t) \delta t + \frac{1}{2} f''(t) (\delta t)^2 + O((\delta t)^3) \quad (15)$$

$$f'(t - \delta t) = f'(t) - f''(t) \delta t + O((\delta t)^2) \quad (16)$$

Combining those two we get

$$\begin{aligned} f(t + \delta t) &= f(t) + f'(t) \delta t + \frac{1}{2} (f'(t) - f'(t - \delta t) + O((\delta t)^2)) \delta t + O((\delta t)^3) \\ &= f(t) + \frac{1}{2} (3f'(t) - f'(t - \delta t)) \delta t + O((\delta t)^3) \end{aligned} \quad (17)$$

For position  $x$ :

$$f(t + \delta t) = f(t) + f'(t) \delta t + \frac{1}{2} f''(t) (\delta t)^2 + \frac{1}{6} f'''(t) (\delta t)^3 + O((\delta t)^4) \quad (18)$$

$$f''(t - \delta t) = f''(t) - f'''(t) \delta t + O((\delta t)^2) \quad (19)$$

Combining those two

$$\begin{aligned} f(t + \delta t) &= f(t) + f'(t) \delta t + \frac{1}{2} f''(t) (\delta t)^2 + \frac{1}{6} (f''(t) - f''(t - \delta t) + O((\delta t)^2)) (\delta t)^2 + O((\delta t)^4) \\ &= f(t) + f'(t) \delta t + \frac{1}{6} (4f''(t) - f''(t - \delta t)) (\delta t)^2 + O((\delta t)^4) \end{aligned} \quad (20)$$

For the last term (Here big- $O$  means F-norm):

$$R(t + \delta t) = R(t) + \dot{R}(t) \delta t + \frac{1}{2} \ddot{R}(t) (\delta t)^2 + \frac{1}{6} \ddot{\ddot{R}}(t) (\delta t)^3 + O((\delta t)^4) \quad (21)$$

$$\dot{R}(t) = [\omega]R \quad (22)$$

$$\ddot{R}(t) = [\beta]R + [\omega]^2 R \quad (23)$$

$$\ddot{\dot{R}}(t) = [\dot{\beta}]R + 2[\beta][\omega]R + [\omega][\beta]R + [\omega]^3 R \quad (24)$$

Thus

$$\begin{aligned} R(t + \delta t) = & \left\{ I + [\omega(t)]\delta t + \frac{1}{2}([\beta(t)] + [\omega(t)]^2)(\delta t)^2 \right. \\ & \left. + \frac{1}{6}([\dot{\beta}(t)] + 2[\beta(t)][\omega(t)] + [\omega(t)][\beta(t)] + [\omega(t)]^3)(\delta t)^3 \right\} R(t) + O((\delta t)^4) \end{aligned} \quad (25)$$

From the fact that  $[a][b] = ba^\top - \langle a, b \rangle I_3$ ,  $[a \times b] = ba^\top - ab^\top$  (actually this is from  $a \times (b \times c) = b(a \cdot c) - c(a \cdot b)$ ,  $(a \times b) \times c = b(a \cdot c) - a(b \cdot c)$ )

$$([\beta][\omega] - [\omega][\beta]) = \omega\beta^\top - \beta\omega^\top = [\beta \times \omega] \quad (26)$$

Combine with  $\dot{\beta}(t) = \frac{\beta(t) - \beta(t - \delta t)}{\delta t} + O(\delta t)$ :

$$\begin{aligned} R(t + \delta t) = & \left\{ I + [\omega(t)]\delta t + \left( \frac{1}{2}[\beta(t)] + \frac{1}{2}[\omega(t)]^2 + \frac{1}{6}[\beta(t) - \beta(t - \delta t)] \right) (\delta t)^2 \right. \\ & \left. + \frac{1}{6}(2[\beta(t)][\omega(t)] + [\omega(t)][\beta(t)] + [\omega(t)]^3)(\delta t)^3 \right\} R(t) + O((\delta t)^4) \\ = & \left\{ e^{[\omega(t) + \frac{4\beta(t) - \beta(t - \delta t)}{6}\delta t]\delta t} + \frac{1}{12}([\beta(t)][\omega(t)] - [\omega(t)][\beta(t)])(\delta t)^3 \right\} R(t) + O((\delta t)^4) \\ = & \left\{ e^{[\omega(t) + \frac{4\beta(t) - \beta(t - \delta t)}{6}\delta t + \frac{1}{12}\beta(t) \times \omega(t)(\delta t)^2]\delta t} \right\} R(t) + O((\delta t)^4) \end{aligned} \quad (27)$$

ACK: huang-wj22@mails.tsinghua.edu.cn, idea on applying Taylor's expansion of rotation matrix and checking proof details.