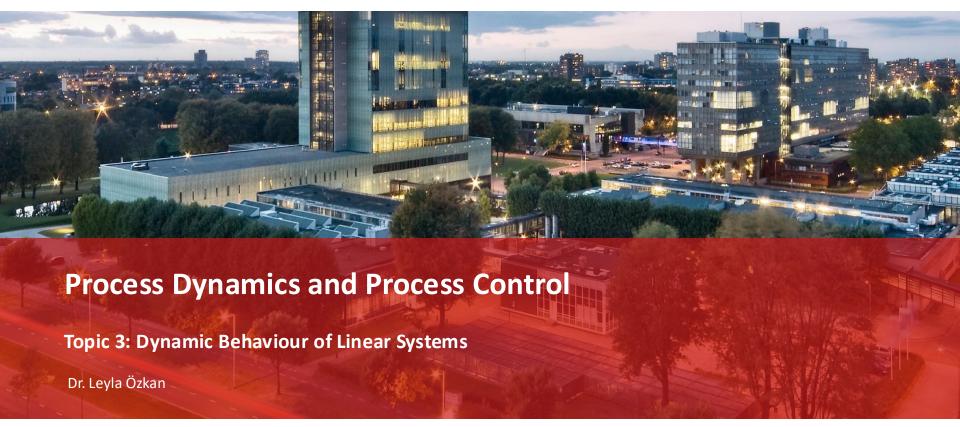
Overview of lecture topics

- Topic 1: Course introduction
- Topic 2: Introduction to frequency domain and Laplace transformation
- Topic 3: Dynamic Behavior of Linear systems
- Topic 4: Frequency Response Analysis and Bode plots
- Topic 5: Mathematical Description of Chemical Systems
- Topic 6: Nonlinear ODE's, Linearity, Linearization Feedback, Stability, Root Locus
- Topic 7: Feedback Controller Design and Bode stability
- Topic 8: Advanced (Enhanced) Process Control







Outline

Transfer functions

Linear systems: Some properties

Dynamic Behaviour of Low Order Systems

- First Order Systems
- Integrating Systems (Pure Capacity)
- Second Order Systems
- Lead/Lag Systems

Dynamic Behavior of High Order Systems

Dynamic Behavior of Some Typical Systems

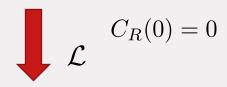
- System With Time Delay
- Inverse Response Systems



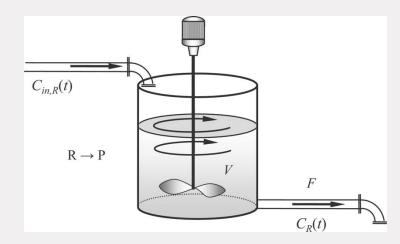
First Order Systems:

Example: CSTR,

$$\frac{d}{dt}(VC_R) = FC_{in,R} - FC_R - Vk_RC_R$$



$$sVC_R(s) - C_R(0) = FC_{in,R}(s) - FC_R(s) - Vk_RC_R(s)$$



An isothermal CSTR

$$\left(\frac{V}{Vk_r + F}s + 1\right)C_R(s) = \frac{F}{F + Vk_r}C_{R,in}(s) \longrightarrow \frac{C_R(s)}{C_{R,in}(s)} = \frac{\frac{F}{F + Vk_r}}{\left(\frac{V}{Vk_r + F}s + 1\right)}$$



First Order Systems, General Representation:

$$\tau \frac{dy(t)}{dt} = -y(t) + Ku(t) \qquad (\tau s + 1) Y(s) = KU(s)$$

Transfer Function:

 $= \frac{\text{Transformed forced function (output)}}{\text{Transformed forcing function (input)}}$

At zero initial conditions



Differential Equation:

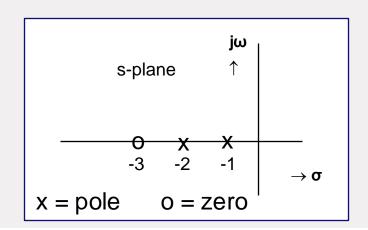
$$\ddot{y}(t) + 3\dot{y}(t) + 2y(t) = \dot{x}(t) + 3x(t)$$
 with $y(0) = y(0) = x(0) = 0$

$$\mathcal{L}\{\ddot{y}(t) + 3\dot{y}(t) + 2y(t)\} = \mathcal{L}\{\dot{x}(t) + 3x(t)\}$$

$$Y(s) (s^{2} + 3s + 2) = X(s) (s + 3)$$

$$\frac{Y(s)}{X(s)} = \frac{s+3}{s^2+3s+2}$$

$$H(s) = \frac{s+3}{(s+1)(s+2)}$$

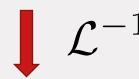




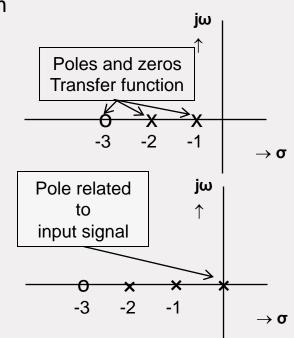
$$H(s) = \frac{s+3}{(s+1)(s+2)}$$

Transfer function

$$Y(s) = H(s)X(s) = \frac{s+3}{(s+1)(s+2)} \frac{1}{s}$$



$$y(t) = 1.5U(t) + 0.5e^{-2t} - 2e^{-t}$$





General Linear Differential Equation:

$$\sum_{i=0}^{N} a_i \frac{d^i y(t)}{dt^i} = \sum_{j=0}^{M} b_j \frac{d^j x(t)}{dt^j} \qquad i = 0, \dots, N \quad j = 0, \dots, M$$

$$a_N \frac{d^N y}{dt^N} + a_{N-1} \frac{d^{N-1} y}{dt^{N-1}} + \dots + a_1 \frac{dy}{dt} + a_0 y = b_M \frac{d^M x}{dT^M} + b_{M-1} \frac{d^{M-1} x}{dt^{M-1}} + \dots + b_1 \frac{dx}{dt} + b_0 x$$

Laplace transform of DE (all initial conditions are assumed zero)

$$\underbrace{(a_N s^N + a_{N-1} s^{N-1} + \dots + a_1 s + a_0) Y(s)}_{D(s)} = \underbrace{(b_M s^M + b_{M-1} s^{M-1} + \dots + b_1 s + b_0)}_{N(s)} X(s)$$

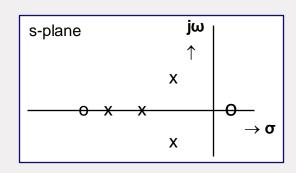
$$\frac{Y(s)}{X(s)} = H(s) = \frac{N(s)}{D(s)}$$
 $D(s)$: characteristic equation



Given a transfer function:
$$H(s) = \frac{N(s)}{D(s)}$$

zeros of $N(s) \Leftrightarrow \mathbf{zeros}$ of H(s)

zeros of $D(s) \Leftrightarrow \mathbf{poles}$ of H(s)



 n^{th} order DE $\Leftrightarrow n$ energy containers $\Leftrightarrow n$ integrators in simulation $\Leftrightarrow n^{\mathrm{th}}$ order system $\Leftrightarrow n$ poles $\Leftrightarrow n$ roots of characteristic equation

DE has real coefficients (real world!) therefore:

complex poles and zeros appear in conjugate pairs \rightarrow s-plane is symmetrical around real axis

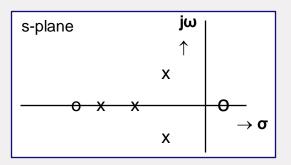


Given a transfer function: $H(s) = \frac{N(s)}{D(s)}$

H(s) has n poles and m zeros; $n \ge m$

poles in LHP: stable behaviour

poles in RHP: unstable behaviour





Linear systems

differential equation (DE) ⇔ time domain

$$\ddot{y}(t) + 3\dot{y}(t) + 2y(t) = \dot{x}(t) + 3x(t)$$

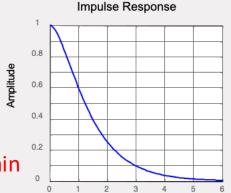
transfer function (TF) \Leftrightarrow complex frequency domain

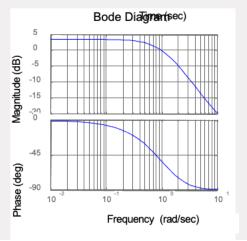
$$H(s) = \frac{s+3}{(s+1)(s+2)}$$

impulse response (IR) ⇔ time domain

Bode plots (BP)*)

⇔ frequency domain



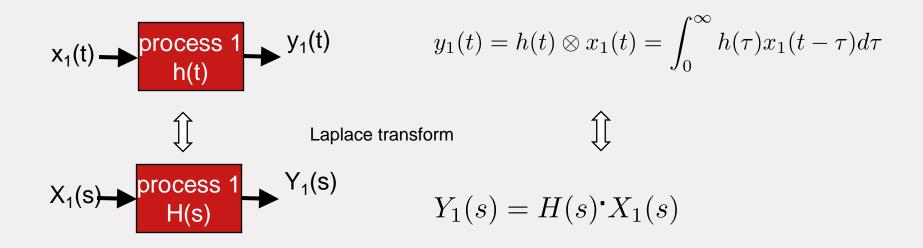




^{*)}Bode Plots will be introduced and explained in Lecture 4

Linear systems

Block diagram representation: visualization of system





Linear systems

$$Y_{1}(s) = H_{1}(s)X(s)$$

$$Y_{2}(s) = H_{2}(s)Y_{1}(s) = H_{2}(s)H_{1}(s)X(s) = H_{tot}X(s)$$

$$Y_{1}(s) = X(s)H_{1}(s)$$

$$Y_{2}(s) = H_{2}(s)H_{1}(s)X(s) = H_{tot}X(s)$$

$$Y_{1}(s) = X(s)H_{1}(s)$$

$$Y_{2}(s) = Y_{1}(s)H_{2}(s) = X(s)H_{1}(s)H_{2}(s) = H_{1}(s)H_{2}(s)X(s)$$



 $H_{\text{tot}}(s) = H_2(s)H_1(s) = H_1(s)H_2(s)$

First Order Systems:

Step response:

$$U(s) = \frac{A}{s}$$

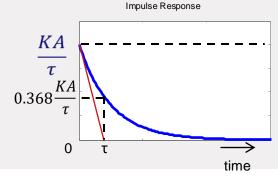
$$Y(s) = \frac{KA}{s(\tau s + 1)} \stackrel{\mathcal{L}}{\rightleftharpoons} y(t) = KA \left(1 - e^{-\frac{t}{\tau}}\right)$$

Step Response KA 0.632KA T time

Impulse response:

$$U(s) = A$$

$$Y(s) = \frac{KA}{(\tau s + 1)} \underset{\mathcal{L}^{-1}}{\overset{\mathcal{L}}{\Leftrightarrow}} y(t) = \frac{KA}{\tau} e^{-\frac{t}{\tau}}$$





First Order Systems:

Response to Ramp Input:

$$U(s) = \frac{A}{s^2} \Rightarrow Y(s) = \frac{K}{(\tau s + 1)} \frac{A}{s^2} = \frac{c_1}{s^2} + \frac{c_2}{s} + \frac{c_3}{(\tau s + 1)}$$

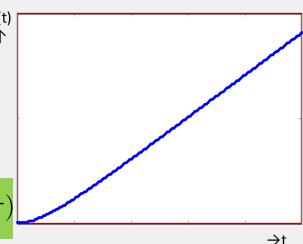
$$c_1 = s^2 |Y(s)|_{s=0} = KA$$

$$c_{1} = \frac{d(s^{2}Y(s))}{ds}\Big|_{s=0} = -KA\tau$$

$$c_{3} = (\tau s + 1)Y(s)\Big|_{s=-\frac{1}{\tau}} = KA\tau^{2}$$

$$c_3 = (\tau s + 1)Y(s)|_{s=-\frac{1}{\tau}} = KA\tau^2$$

$$Y(s) = \frac{KA}{s^2 (\tau s + 1)} \stackrel{\mathcal{L}}{\Longleftrightarrow} y(t) = KA\tau e^{-\frac{t}{\tau}} + KA(t - \tau)$$



Ramp Response



First Order Systems:

Response to sinusoidal input:

$$u(t) = A\sin(\omega t) \stackrel{\mathcal{L}}{\rightleftharpoons} U(s) = \frac{A\omega}{s^2 + \omega^2}$$

$$Y(s) = \frac{K}{(\tau s + 1)} \frac{A\omega}{(s^2 + \omega^2)} = \frac{c_1}{\tau s + 1} + \frac{c_2}{s + j\omega} + \frac{c_3}{s - j\omega}$$

$$c_1 = (\tau s + 1)Y(s)|_{s = \frac{-1}{\tau}} = \frac{KA\omega\tau}{(1 + \omega^2\tau^2)}$$

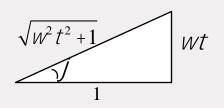
$$c_2 = (s+j\omega)Y(s)|_{s=-j\omega} = \frac{-KA\omega\tau}{2(\omega^2\tau^2 + j\omega\tau)} \quad c_3 = (s-j\omega)Y(s)|_{s=j\omega} = \frac{-KA\omega\tau}{2(\omega^2\tau^2 - j\omega\tau)}$$

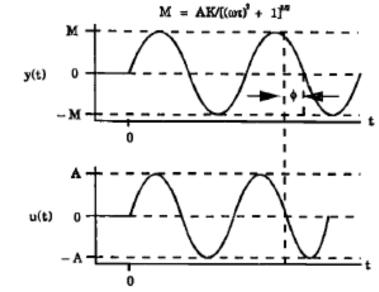


First Order Systems:

Response to sinusoidal input:

$$y(t) = KA \left(\frac{\omega \tau}{\omega^2 \tau^2 + 1}\right) e^{\frac{-t}{\tau}} + \frac{KA}{\sqrt{\omega^2 \tau^2 + 1}} \sin(\omega t - \varphi)$$





$$\sin(\omega t)\cos(\varphi) - \cos(\omega t)\sin(\varphi) = \sin(\omega t - \varphi)$$



$$Y(s) = \frac{KA\omega}{(\tau s + 1)(s^{2} + \omega^{2})} = \frac{c_{1}}{\tau s + 1} + \frac{c_{2}}{s + j\omega} + \frac{c_{3}}{s - j\omega}$$

$$c_{1} = (\tau s + 1)Y(s)\Big|_{s = -1/\tau} = \frac{KA\omega\tau}{(1 + \omega^{2}\tau^{2})}$$

$$c_{2} = (s + j\omega)Y(s)\Big|_{s = -j\omega} = \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} + j\omega\tau)}$$

$$c_{3} = \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} - j\omega\tau)}$$

$$Y(s) = \frac{KA\omega}{(\tau s + 1)(s^{2} + \omega^{2})} = \frac{KA\omega\tau}{(1 + \omega^{2}\tau^{2})} + \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} + j\omega\tau)} + \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} - j\omega\tau)}$$

$$y(t) = KA\left(\frac{\omega\tau}{\omega^{2}\tau^{2} + 1}\right)e^{-t/\tau} + \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} + i\omega\tau)}e^{-j\omega t} + \frac{-KA\omega\tau}{2(\omega^{2}\tau^{2} - i\omega\tau)}e^{j\omega t}$$



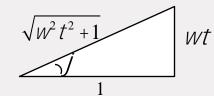
$$y(t) = KA\left(\frac{\omega\tau}{\omega^2\tau^2 + 1}\right)e^{-t/\tau} + \frac{-KA\omega\tau}{2(\omega^2\tau^2 + j\omega\tau)}e^{-j\omega t} + \frac{-KA\omega\tau}{2(\omega^2\tau^2 - j\omega\tau)}e^{j\omega t}$$

$$y(t) = KA \left(\frac{\omega \tau}{\omega^2 \tau^2 + 1} \right) e^{-t/\tau} + \frac{KA}{(\sqrt{\omega^2 \tau^2 + 1})} \left(\frac{-\omega \tau}{2(\sqrt{\omega^2 \tau^2 + 1})} \left(e^{-j\omega t} + e^{j\omega t} \right) + \frac{1}{2j(\sqrt{\omega^2 \tau^2 + 1})} \left(-e^{-j\omega t} + e^{j\omega t} \right) \right)$$

$$y(t) = KA\left(\frac{\omega\tau}{\omega^2\tau^2+1}\right)e^{-t/\tau} + \frac{KA}{(\sqrt{\omega^2\tau^2+1})}\left(\frac{-\omega\tau}{(\sqrt{\omega^2\tau^2+1})}\left(\frac{e^{j\omega t}+e^{-j\omega t}}{2}\right) + \frac{1}{(\sqrt{\omega^2\tau^2+1})}\left(\frac{e^{j\omega t}-e^{-j\omega t}}{2j}\right)\right)$$

$$y(t) = KA\left(\frac{\omega\tau}{\omega^2\tau^2 + 1}\right)e^{-t/\tau} + \frac{KA}{(\sqrt{\omega^2\tau^2 + 1})}(-\sin(\varphi)\cos(\omega t) + \cos(\varphi)\sin(\omega t))$$

$$y(t) = KA \left(\frac{\omega \tau}{\omega^2 \tau^2 + 1}\right) e^{-t/\tau} + \frac{KA}{(\sqrt{\omega^2 \tau^2 + 1})} \sin(\omega t - \varphi)$$





Integrating Systems:

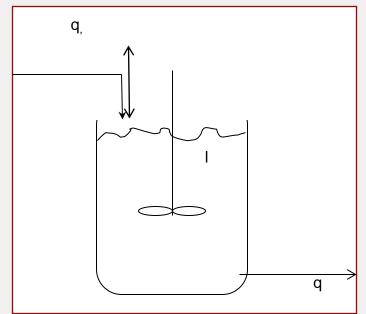
Example: Storage tank with constant outlet flow

$$A_r \frac{dl}{dt} = q_i - q$$
 Mass balance

$$\mathcal{L}\left\{A_r \frac{dl}{dt}\right\} = \mathcal{L}\left\{q_i - q\right\}$$

$$A_r s L(s) = Q_i(s) - q$$

$$L(s) = \frac{\frac{1}{A_r}}{s}Q_i(s) - \frac{\frac{q}{A_r}}{s}$$





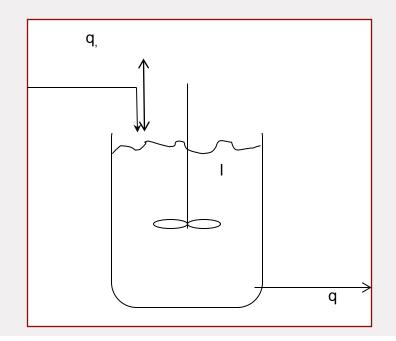
Integrating Systems:

General Representation:

$$\frac{dy(t)}{dt} = Ku(t)$$

Transfer Function:

$$\frac{Y(s)}{U(s)} = \frac{K}{s}$$





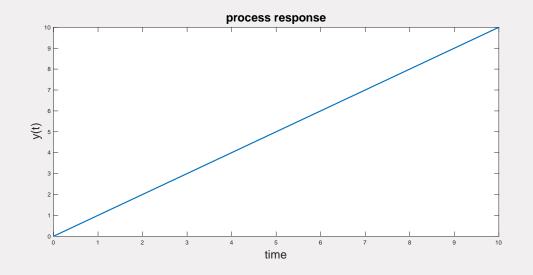
Integrating Systems:

Step response:

$$U(s) = \frac{A}{s}$$

$$Y(s) = \frac{K}{s} \frac{A}{s} = \frac{KA}{s^2}$$

$$y(t) = KAt$$





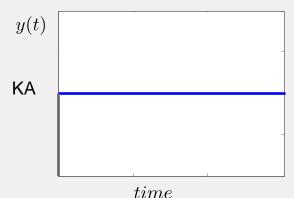
Integrating Systems:

Impulse response:

$$U(s) = A$$

$$Y(s) = \frac{K}{s}A$$

$$y(t) = KA$$





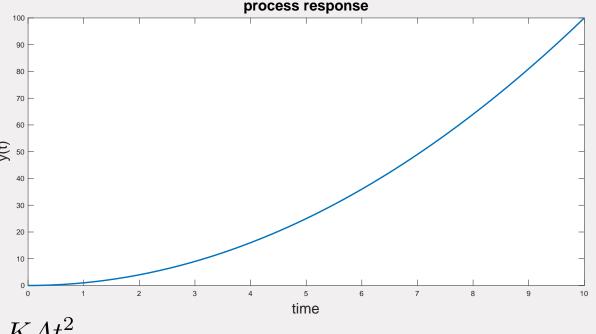
Integrating Systems:

Response to ramp input:

$$U(s) = \frac{A}{s^2}$$

$$Y(s) = \frac{K}{s} \frac{A}{s^2}$$

$$y(t) = \mathcal{L}^{-1} \left\{ \frac{KA}{s^3} \right\} = \frac{1}{2} KAt^2$$

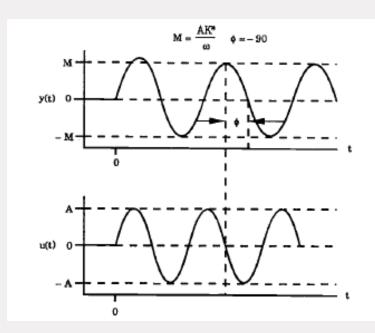


Integrating Systems:

Response to sinusoidal input:

$$U(s) = \frac{A\omega}{(s^2 + \omega^2)}$$
$$Y(s) = \frac{K}{s} \frac{A\omega}{(s^2 + \omega^2)}$$

$$\mathcal{L}^{-1} \{Y(s)\} = y(t) = \frac{KA}{\omega} [1 + \sin(\omega t - 90)]$$





Lead -Lag Systems:

$$G(s) = \frac{\xi s + 1}{\tau s + 1} = G_1(s).G_2(s)$$

$$G_1(s) = \xi s + 1$$
 $G_2 = \frac{1}{\tau s + 1}$

$$Y_1(s) = \frac{\omega}{(s^2 + \omega^2)} (\xi s + 1) \underset{\mathcal{L}^{-1}}{\Leftrightarrow} y_1(t) = \omega \xi \cdot \cos \omega t + \sin \omega t$$

$$y_t = \sqrt{\omega^2 \xi^2 + 1} \left(\frac{\omega \xi}{\sqrt{\omega^2 \xi^2 + 1}} \cos(\omega t) + \frac{1}{\sqrt{\omega^2 \xi^2 + 1}} \sin(\omega t) \right) = \sqrt{\omega^2 \xi^2 + 1} \sin(\omega t + \varphi)$$

With:
$$\varphi = \tan^{-1}(\omega \xi)$$

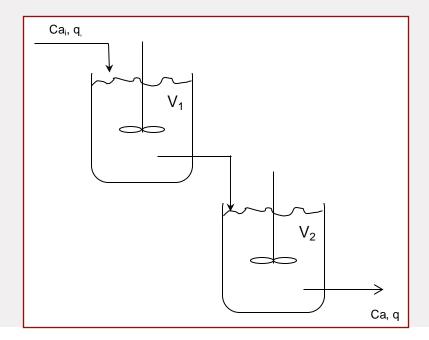


Second Order Systems:

$$V_1 \frac{dC_{a,1}}{dt} = qC_{a,i} - qC_{a,1}$$

$$V_2 \frac{dC_a}{dt} = qC_{a,1} - qC_a$$

$$\frac{C_a(s)}{C_{a,i}} = \frac{1}{\left(\frac{V_1}{q}s + 1\right)\left(\frac{V_2}{q}s + 1\right)}$$





Second Order Systems:

General Representation:

$$\tau^2 \frac{d^2 y(t)}{dt^2} + 2\xi \tau \frac{dy(t)}{dt} + y(t) = Ku(t)$$

Transfer Function:

$$\frac{Y(s)}{U(s)} = \underbrace{\frac{K}{\tau^2 s^2 + 2\xi \tau s + 1}}_{\text{Time constant}} \text{Gain}$$

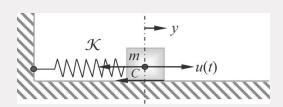
- Naturally arises from two first order processes in series.
- Processes with a controller (feedback)

Damping coefficient



Second Order Systems:

Mass Spring Systems:



pring Systems:
$$m\frac{d^2y(t)}{dt^2} + C\frac{dy}{dt} + \mathcal{K}y(t) = u(t) \qquad \mathcal{K}$$

$$\mathcal{L}$$

$$(ms^2 + Cs + \mathcal{K}) Y(s) = U(s)$$

Stiffness

Friction coefficient

Transfer Function:

$$\frac{Y(s)}{U(s)} = \frac{1}{(ms^2 + Cs + \mathcal{K})}$$

$$\frac{Y(s)}{U(s)} = \frac{1}{(ms^2 + Cs + \mathcal{K})} \qquad \frac{Y(s)}{U(s)} = \frac{K}{(\tau^2 s^2 + 2\xi \tau s + 1)}$$
$$K = \frac{1}{\mathcal{K}} \qquad \xi = \frac{C}{2\sqrt{m\mathcal{K}}} \qquad \tau = \sqrt{\frac{m}{\mathcal{K}}}$$



Second Order Systems:

Roots (Poles of transfer function)

$$s_{1,2} = \frac{-2\xi\tau \pm \sqrt{4\xi^2\tau^2 - 4\tau^2}}{2\tau^2}$$

$$s_{1,2} = -\frac{\xi}{\tau} \pm \frac{1}{\tau} \sqrt{\xi^2 - 1}$$

Transient Response: Depends on the roots

 $\xi > 0$ Real parts of the roots negative (stable)

 $\xi > 1$ Two distinct real roots (overdamped)

 $\xi = 1$ repeated real roots (critically damped)

 $0 < \xi < 1$ Complex roots (underdamped response)

 $\xi = 0$ pure imaginary roots (undamped)

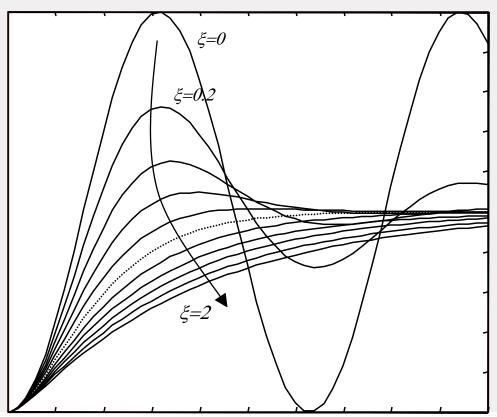


Second Order Systems:

y(t) 个

Step Response:

$$Y(s) = \frac{K}{(\tau^2 s^2 + 2\xi \tau s + 1)} \frac{A}{s}$$





Second Order Systems:

Sinusoidal response:

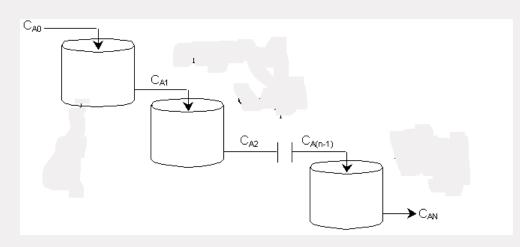
$$Y(s) = \frac{K}{\tau^2 s^2 + 2\xi \tau s + 1} \frac{A\omega}{(s^2 + \omega^2)}$$

Ultimate response:

$$y(t)|_{t\to\infty} = \frac{KA}{\sqrt{\left[1 - (\omega\tau)^2\right]^2}} \sin(\omega\tau + \varphi)$$
$$\varphi = -\tan^{-1}\left[\frac{2\xi\omega\tau}{1 - (\omega\tau)^2}\right]$$



High Order Systems:



$$V_1 \frac{dC_{A,1}}{dt} = qC_{A,0} - qC_{A,1}$$

$$V_2 \frac{dC_{A,2}}{dt} = qC_{A,1} - qC_{A,2}$$

$$\vdots$$

$$V_N \frac{dC_{A,N}}{dt} = qC_{A,N-1} - qC_{A,N}$$

$$\frac{C_{A,N}(s)}{C_{A,0}(s)} = \frac{1}{\left(\frac{V_1}{q}s+1\right)\left(\frac{V_2}{q}s+1\right)\cdots\left(\frac{V_N}{q}s+1\right)}$$



High Order Systems:

General Representation:

$$\frac{Y_N(s)}{U(s)} = \left(K \prod_{i=1}^N \frac{1}{\tau_i s + 1}\right)$$

N first order systems in series

General Nth Representation:

 $N^{\rm th}$ order system with zeros

$$\frac{Y_N(s)}{U(s)} = \frac{(\xi_1 s + 1)(\xi_2 s + 1)(\xi_3 s + 1) \cdots (\xi_M s + 1)}{(\tau_1 s + 1)(\tau_2 s + 1)(\tau_3 s + 1) \cdots (\tau_N s + 1)} = \frac{K \prod_{i=1}^{M} (\xi_i s + 1)}{\prod_{i=1}^{N} (\tau_i s + 1)}$$



High Order Systems:

Step response of Nth order system in series

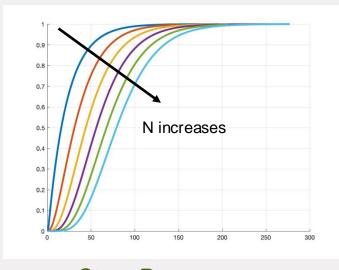
Partial fractions

$$Y_N(s) = \left(K \prod_{i=1}^N \frac{1}{\tau_i s + 1}\right) \cdot \frac{1}{s} \qquad Y_N(s) = K \cdot \left[\frac{A_0}{s} + \sum_{i=1}^N \frac{A_i}{\tau_i s + 1}\right]$$

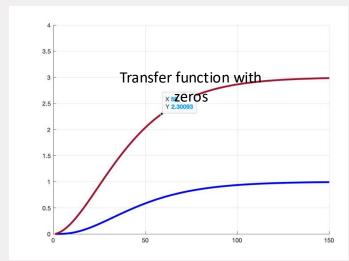
$$A_o = 1; \quad A_i = \lim_{s \to -\frac{1}{\tau_i}} \left[\frac{(\tau_i s + 1) \cdot Y_N(s)}{K} \right]$$
$$y_N(t) = K \cdot \left[1 + \sum_{i=1}^N \frac{A_i}{\tau_i} \cdot e^{-\frac{t}{\tau_i}} \right]$$



High Order Systems:



Step Response



Step Response of high order systems with zeros



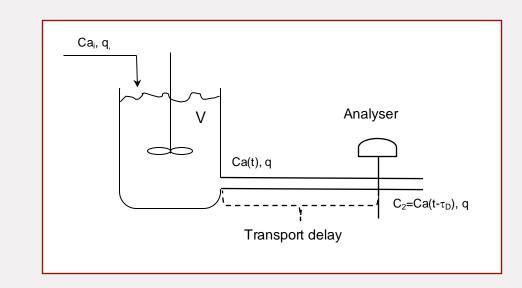
Systems with Time Delay (Deadtime):

Example: A tank with transport delay at the outlet

$$V\frac{dC_a}{dt} = qC_{a,i} - qC_a$$

$$\frac{C_a(s)}{C_{a,i}(s)} = \frac{q}{Vs + q} = \frac{1}{\frac{V}{q}s + 1}$$

$$C_2(t) = C_a(t - \tau_D)$$
$$C_2(s) = e^{-\tau_D s} C_a(s)$$

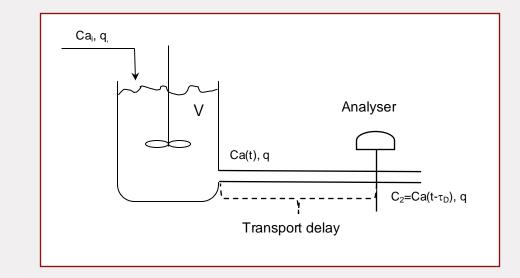




Systems with Time Delay (Deadtime):

Transfer function between C_{a,i} and C₂

$$\frac{C_2(s)}{C_{a,i}(s)} = e^{-\tau_D s} \frac{1}{\frac{V}{q}s + 1}$$





Laplace Transform of Systems with Time Delay (Deadtime):

$$h(t) = \begin{cases} 0 & t < \tau_D \\ f(t - \tau_D) & t > \geq \tau_D \end{cases}$$

$$\mathcal{L}\{h(t)\} = \int_0^{\tau_D} e^{-st} \cdot 0 \, dt + \int_{\tau_D}^{\infty} f(t - \tau_D) \cdot e^{-st} dt$$

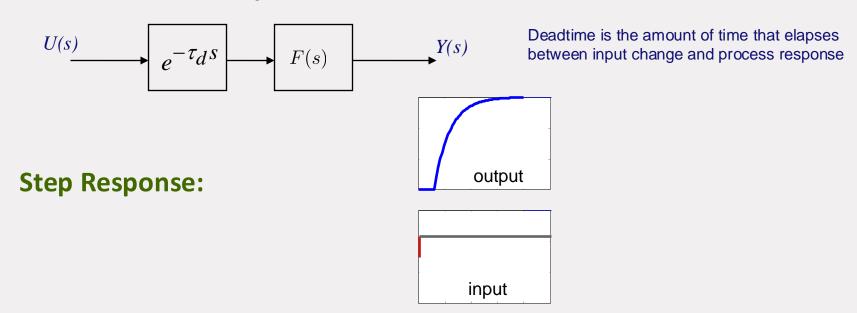
$$\mathcal{L}\{h(t)\} = 0 + \int_0^{\infty} f(l) \cdot e^{-s(l + \tau_D)} dl$$

$$= e^{-s\tau_D} \underbrace{\int_0^{\infty} f(l) \cdot e^{-sl} dl}_{F(s)}$$



Laplace Transform of Systems with Time Delay (Deadtime):

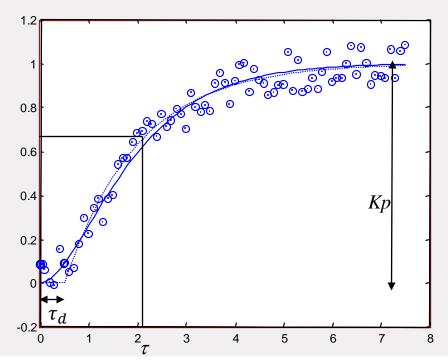
Transfer Function representation





Complex processes can be approximated as first order process with deadtime

$$G(s) = \frac{K_p}{\tau s + 1} e^{-\tau_D s}$$

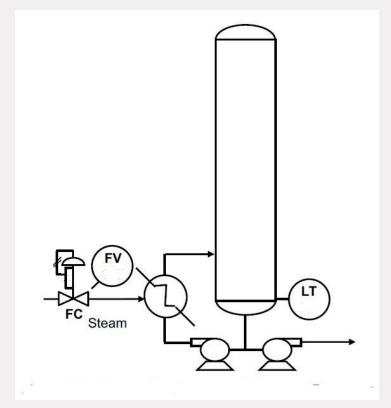




Inverse Response Systems

Example: the level in the bottom of the distillation

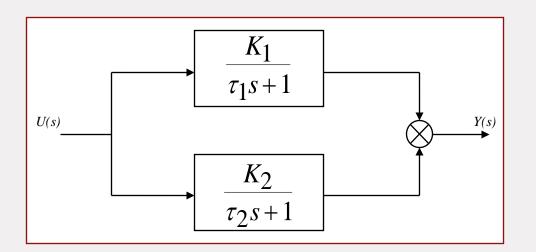
 The bottom level of the column illustrated may show an inverse response to a step change increase in heat input





Inverse Response Systems

Can result from two processes in parallel



$$\frac{Y(s)}{U(s)} = H(s) = \frac{K_1}{\tau_1 s + 1} + \frac{K_2}{\tau_2 s + 1}$$

$$H(s) = \frac{K_1(\tau_2 s + 1) + K_2(\tau_1 s + 1)}{(\tau_1 s + 1) \cdot (\tau_2 s + 1)}$$

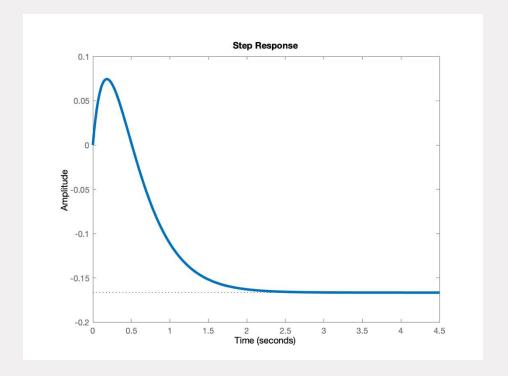
$$H(s) = \frac{(K_1\tau_2 + K_2\tau_1)s + (K_2 + K_1)}{(\tau_1 s + 1) \cdot (\tau_2 s + 1)}$$

It is observed when the zero lies in the right half of the s-plane

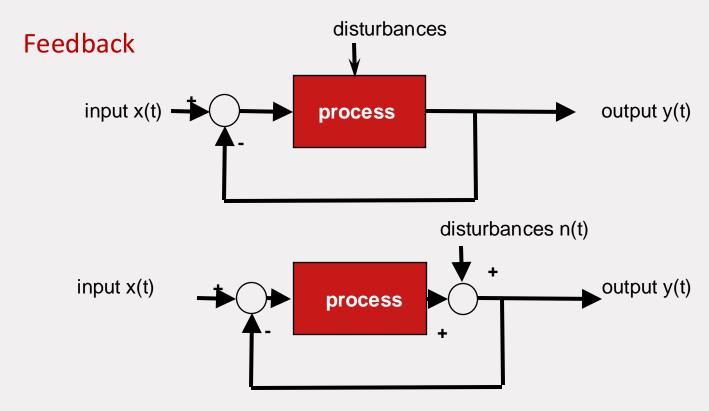


Inverse Response Systems

Step Response:

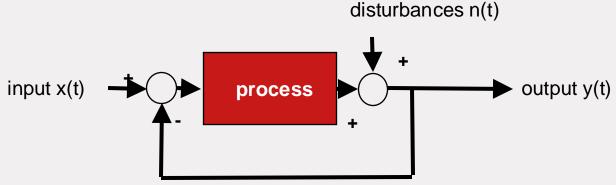








Feedback

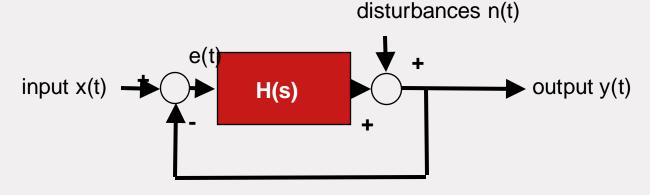


why feedback?

- stability
- change of dynamic behaviour
- reduction of influence of disturbance on output tracking



Feedback



$$Y(s) = H(s)E(s) + N(s) = H(s)[X(s) - Y(s)] + N(s)$$

$$Y(s) = \frac{H(s)}{1 + H(s)}X(s) + \frac{1}{1 + H(s)}N(s)$$



Closed loop system:

Open loop transfer system:
$$H(s) = \frac{Num(s)}{Den(s)}$$

Closed loop transfer system:
$$H_{cl}(s) = \frac{H(s)}{1 + H(s)} = \frac{\frac{Num(s)}{Den(s)}}{1 + \frac{Num(s)}{Den(s)}} = \frac{Num(s)}{Den(s) + Num(s)}$$

zeros of $H_{cl}(s)$: zeros of Num(s) = 0

poles of $H_{cl}(s)$: poles of Den(s) + Num(s) = 0

Poles are different than the poles of H(s)

The dynamic behaviour of transfer function H(s) is changed by feedback!



Example:

Open loop Process:
$$Y(s) = H(s)X(s) + N(s)$$

Assume

$$H(s) = \frac{1}{s+1}, \quad X(s) = \frac{1}{s}, \quad N(s) = \frac{1}{s}$$

Output

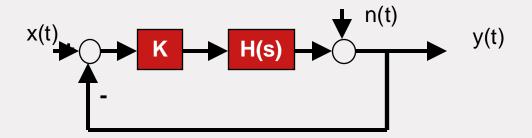
$$Y(s) = \frac{1}{s+1} \cdot \frac{1}{s} + \frac{1}{s}$$

Final Value of y(t)

$$y(\infty) = \lim_{s \to 0} (sY(s)) = \lim_{s \to 0} \left(s \frac{1}{s+1} \frac{1}{s} + s \frac{1}{s} \right) = 1 + 1 = 2$$



Feedback



$$Y(s) = H_{xy,cl}(s)X(s) + H_{ny,cl}N(s) = \frac{KH(s)}{1 + KH(s)}X(s) + \frac{1}{1 + KH(s)}N(s)$$



Closed loop Transfer Function:
$$H(s) = \frac{1}{s+1}$$

from input
$$x(t)$$
 to output $y(t)$

$$H_{xy,cl} = \frac{KH(s)}{1 + KH(s)} = \frac{\frac{K}{s+1}}{1 + \frac{K}{s+1}} = \frac{K}{s+1+K}$$

no zero; pole: -(1+K), Faster response for K>0

response to input step, final value

$$y_{xy}(\infty) = \lim_{s \to 0} (sY_{xy}(s)) = \lim_{s \to 0} \left(s \frac{K}{s+1+K} \cdot \frac{1}{s} \right) = \frac{K}{1+K}$$



Closed loop Transfer Function: $H(s) = \frac{1}{s+1}$

from disturbance n(t) to output y(t)

$$Y_{ny} = H_{ny,cl}N(s) = \frac{1}{1 + KH(s)}N(s) = \frac{1}{1 + \frac{K}{s+1}} \cdot \frac{1}{s}$$

response to disturbance step, final value

$$y_{ny}(\infty) = \lim_{s \to 0} \left(sY_{ny(s)} \right) = \lim_{s \to 0} \left(s \frac{s+1}{s+1+K} \cdot \frac{1}{s} \right) = \frac{1}{1+K}$$

