

# Equalization

Combating ISI/frequency selectivity

---

Georgios Ropokis

CentraleSupélec, Campus Rennes

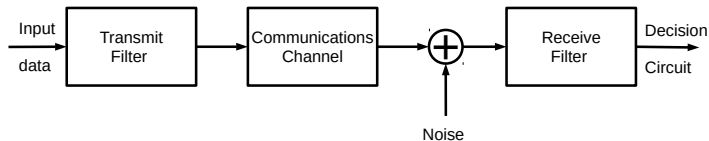
# Table of contents

1. The communications system chain
2. Channel induced distortions
3. Optimal (Maximum Likelihood) detection
4. Linear channel equalizers
5. Decision feedback equalizer

# The communications system chain

---

# The communications system chain



# The communications system chain

- The transmit and receive filters should be selected such as to eliminate Intersymbol Interference (ISI) and limiting the bandwidth of the communications signal.
- Nyquist criterion, if  $x(t)$  is the cascaded impulse response of the transmit filter, the channel and the receive filter, it must hold that:

$$x(nT) = \begin{cases} 1, & n = 0 \\ 0, & n \neq 0. \end{cases} \quad (1)$$

or equivalently that:

$$\sum_{m=-\infty}^{\infty} X\left(f + \frac{m}{T}\right) = T \quad (2)$$

- By designing the transmit and receive filters such that:

$$X(f) = \begin{cases} T, & 0 \leq |f| \leq \frac{(1-\alpha)}{2T} \\ \frac{T}{2} \left[ 1 + \cos \frac{\pi T}{a} \left( |f| - \frac{1-\alpha}{2T} \right) \right], & \frac{1-\alpha}{2T} \leq |f| \leq \frac{1+\alpha}{2T} \\ 0, & |f| > \frac{1+\alpha}{2T} \end{cases} \quad (3)$$

we can satisfy this condition.

- System design with an ideal channel:
  - The channel impulse response  $H_C(f) = 1$
  - We can select the transmit filter such that:  $H_T(f) = \sqrt{X(f)}e^{-j2\pi ft_0}$
  - and the receive filter such that:

$$H_R(f) = H^*(f). \quad (4)$$

## **Channel induced distortions**

---

- The channel frequency response can be expressed as:

$$H_C(f) = |H_C(f)| e^{j\Theta(f)}. \quad (5)$$

- Two types of distortion can be recognized:
  - Amplitude distortion: If  $H_C(f)$  is not-constant over the signal spectrum, different frequency components are treated differently by the channel.
  - Phase distortion: If  $\Theta(f)$  is not a linear function, the channel introduces different delays for the different channel frequency components.
  - Both effects result in introducing Intersymbol Interference.



# Combating channel effects with known channel

- Assuming knowledge of  $H_C(f)$  at both the transmitter and the receiver, we can construct the transmit  $h_T(t)$  and receive filters  $h_R(t)$  such that:

$$H_T(f) H_C(f) H_R(f) = X_{rc}(f) \quad (6)$$

- Drawbacks:
  - If the channel response changes with time (e.g., wireless channel), we need to readjust our transmit and/or receive filters such as to adjust them to these changes.
  - Perfect channel knowledge is required in order to totally avoid Intersymbol Interference.

- Since in most cases the channel response is unknown and/or time varying, we select fixed transmitter and receiver filters:

$$H_T(f) = \begin{cases} \sqrt{X_{rc}(f)} e^{-j2\pi f t_0}, & |f| \leq W, \\ 0, & |f| > W \end{cases} \quad (7)$$

and

$$|H_R(f)| = |H_T^*(f)|. \quad (8)$$

- The cascaded communication chain results in pulse per symbol having a shape:  $x(t) = h_T(t) \star h_C(t) \star h_R(t) = x_{rc}(t) \star h_c(t)$ , which does not satisfy the Nyquist criterion

# The received signal

- The received signal is expressed as:

$$y(t) = \sum_{n=-\infty}^{\infty} a_n x(t - nT) + n(t), \quad (9)$$

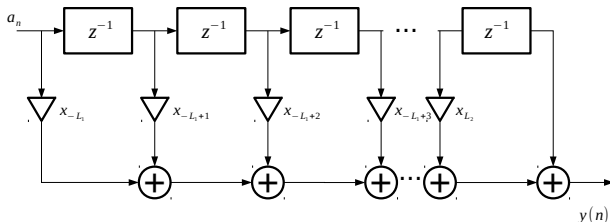
where  $n(t)$  the AWGN.

- After sampling the received signal at time instances that are multiples of the symbol duration, we obtain that:

$$\begin{aligned} y_m = y(mT) &= \sum_{n=-\infty}^{\infty} a_n x_{m-n} + n_m \\ &= \underbrace{x_0 a_m}_{\text{Desired signal}} + \underbrace{\sum_{n=-\infty, n \neq m}^{+\infty} a_n x_{m-n}}_{\text{ISI}} + \underbrace{n_m}_{\text{Noise}}. \end{aligned} \quad (10)$$

# Discrete time equivalent channel filter

- In practice, the length of pulse  $x(t)$  is small enough so that only a limited number of symbols are influenced.
- We therefore have that  $x_n = 0$  for  $n < -L_1$  and  $n > L_2$ .



## **Optimal (Maximum Likelihood) detection**

---

# Optimal detection for frequency selective channels

- Given a vector of observations  $\{y_m\}$ , we need to determine the vector of input symbols  $\{a_m\}$ .
- The channel can then be represented as a trellis diagram and a state diagram with  $M^L$ , ( $L = L_1 + L_2$ ) states.
- Assuming knowledge of the channel  $\{x_n\}$ , detection can then be done using Viterbi algorithm,
- As channel order  $L$  increases, the complexity increases exponentially.
- Practical only for small values of  $M$  and  $L$ .
- Suboptimal schemes:
  - Linear equalizers
  - Decision feedback equalizer

# Trellis and State diagram representation for frequency selective channels

Assuming a causal FIR channel:

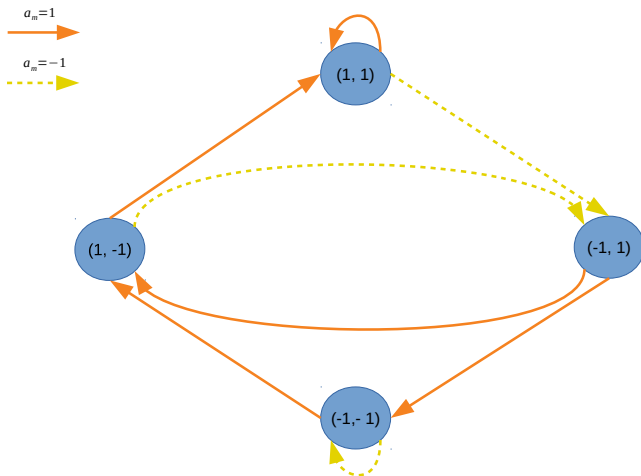
- Accounting for the fact that  $x_n = 0$  for  $n < 0$  and  $n > L$  we can write  $y_m$  as:

$$y_m = y(mT) = \underbrace{x_0 a_m}_{\text{Desired signal}} + \underbrace{\sum_{n=1, L_2}^{+\infty} a_{m-n} x_n}_{\text{ISI}} + \underbrace{n_m}_{\text{Noise}}. \quad (11)$$

- We can describe the channel as a state diagram where each state corresponds to the vector  $(a_{m-1}, \dots, a_{m-L})$

# State diagram representation of a channel: Example

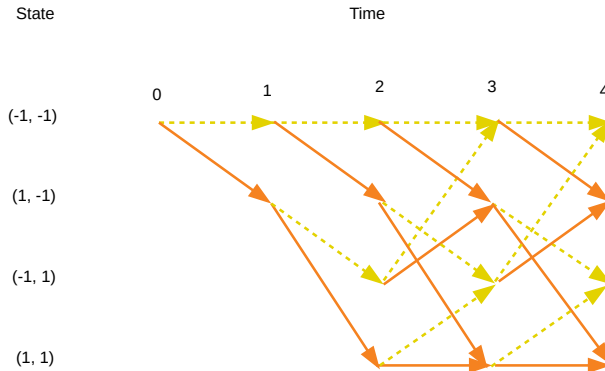
Transmission of BPSK over a channel with 3 taps:





# Trellis diagram representation of a channel: Example

Transmission of 4 BPSK symbols over a channel with 3 taps (assuming a starting state  $(-1, -1)$ ):



# Optimal detection for frequency selective channels

- Given the vector of observations corresponding to the transmission of  $M$  symbols:

$$\mathbf{y} = [y_M, y_{M-1}, \dots, y_0] \quad (12)$$

we decide in favor of the transmit sequence:

$$\mathbf{y} = [a_M, a_{M-1}, \dots, a_0] \quad (13)$$

that maximizes the likelihood function:

$$p(y_M, \dots, y_0 | a_M, \dots, a_0) \quad (14)$$

- Equivalently we select the sequences that maximizes the log-likelihood function

$$\begin{aligned} \log p(y_M, \dots, y_0 | a_M, \dots, a_0) &= \log p(y_M | a_M, \dots, a_{M-L}) \\ &\quad + \log p(y_{M-1}, \dots, y_0 | a_{M-1}, \dots, a_0) \end{aligned} \quad (15)$$

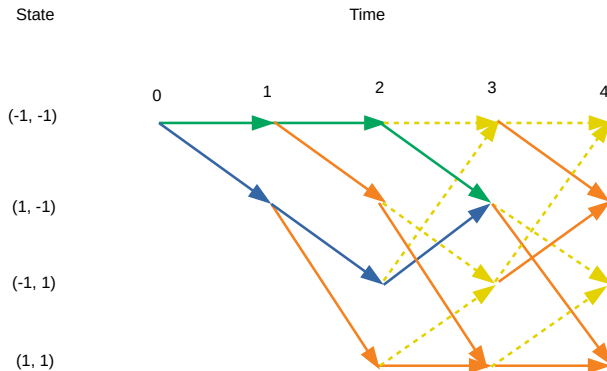
- When observing sample value  $y_M$  at the end of the  $M$ -th transmit period, associate to the transmission from state  $(a_{M-1}, \dots, a_{M-L})$  to state  $(a_M, \dots, a_{M-L+1})$  a weight equal to :

$$-\log p(y_M | a_M, \dots, a_{M-L}) \quad (16)$$

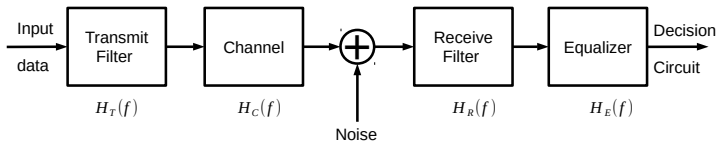
- The sequence detection problem then becomes a shortest path routing problem.
- If there are more than one paths that arrive at a particular state after observing  $y_M$ , we only need to consider the one that results in the shortest cost.

# Viterbi algorithm

Out of the two paths that arrive at state  $(1, -1)$  at the end of the third transmission period, select the one that results in the shortest path and eliminate the other one.



# (Linear) Channel equalizers



# Linear channel equalizers

---

- Preset Equalizers
  - The filter gains are selected in the beginning of the transmission and remain constant for the whole system duration.
  - Suitable for systems where the channel impulse response remains fixed during transmission.
- Adaptive equalizers: The tap weights of the equalizer are updated during system operation.

# Zero forcing equalizer

- If  $H_C(f) = |H_C(f)| e^{j\theta_c(f)}$ , the equalizer frequency response is selected to be equal to:

$$H_e(f) = \frac{1}{|H_C(f)|} e^{-j\theta_c(f)}, \quad |f| \leq W. \quad (17)$$

- The ISI effect is totally eliminated.
- If  $H_T(f)$  and  $H_R(f)$  satisfy the Nyquist criterion, the out of the equalizer can be expressed as:

$$y_m = y(mT) = a_m + \nu_m, \quad (18)$$

where  $\nu_m$  is Gaussian noise.

- If the channel impulse response causes deep fades in some frequency components, then the equalizer “amplifies” noise components in the particular frequencies.
- Generally, the noise variance at the output of the equalizer is higher than noise variance of the channel.



# FIR implementation of equalizers

- For practical purposes, equalizers are implemented as FIR filters
- Symbol spaced equalizer: The time delay  $\tau$  between adjacent taps is equal to the symbol period  $T$
- Fractionally spaced equalizer:  $\tau < T$ .
- A common choice for  $\tau$  is  $\tau = T/2$ .
- The impulse response of the equalizer:

$$h_e(t) = \sum_{n=-N}^N c_n \delta(t - n\tau), \quad (19)$$

- Frequency response of the equalizer:

$$H_e(f) = \sum_{n=-N}^N c_n e^{-j2\pi f n\tau} \quad (20)$$

- $N$  should be chosen large enough (i.e.,  $2N + 1 > L$ ) such as the length of the filter is at least as large as the ISI span.



# FIR implementation of the zero-forcing equalizer

- Ignoring noise, if  $h_T(t) \star h_R(t) = x(t)$ , the equalizer output is equal to:

$$z(t) = \sum_{n=-N}^N c_n x(t - n\tau) \quad (21)$$

- Samples obtained at  $mT$ :

$$z(mT) = \sum_{n=-N}^N c_n x(mT - n\tau), m \in \mathbb{Z}. \quad (22)$$

- How can we determine the coefficients  $c_k$  such as to eliminate ISI?

# FIR implementation of the zero-forcing equalizer

- The  $2N + 1$  tap weight gains need to be determined.
- Assuming knowledge of  $x(n)$  we can construct  $2N + 1$  equations such as to determine  $c_n$  as follows:

$$z(mT) = \sum_{n=-N}^N c_n x(mT - nT) = \begin{cases} 1, & m = 0 \\ 0, & m = \pm 1, \pm 2, \dots, \pm N \end{cases} \quad (23)$$

- Equivalent formulation:

$$\mathbf{X}\mathbf{c} = \mathbf{z} \quad (24)$$

where:

$$\mathbf{c} = [c_{-N}, c_{-N+1}, \dots, c_{-1}, c_0, c_1, \dots, c_N]^T \quad (25)$$

$$\mathbf{z} = \begin{bmatrix} \underbrace{0, \dots, 0}_{N \text{ elements}}, \underbrace{1, 0, \dots, 0}_{N \text{ elements}} \end{bmatrix}^T \quad (26)$$

# FIR implementation of the zero-forcing equalizer

and

$$\mathbf{X} = \begin{bmatrix} x(-NT + N\tau) & x(-NT + (N-1)\tau) & \cdots & x(-NT) & \cdots & x(-NT + N\tau) \\ \vdots & \vdots & \cdots & \vdots & \vdots & \vdots \\ x(NT + N\tau) & x(NT + (N-1)\tau) & \cdots & x(NT) & \cdots & x(NT + N\tau) \end{bmatrix} \quad (27)$$

Remark: Inverting an FIR channel requires an IIR equalizer. However by letting  $N \rightarrow \infty$ , the presented FIR equalizer converges to a channel inverting equalizer.

## Example

Consider a communication channel where the channel impulse response is such that  $x(t) = h_T(t) \star h_C(t) \star h_R(t)$ , with

$$x(t) = \frac{1}{1 + \left(\frac{2t}{T}\right)^2} \quad (28)$$

where  $1/T$  is the symbol rate. Determine the coefficients of a 5-tap half-symbol spaced zero forcing equalizer.

*Solution:* Since we have a five tap filter, half-symbol spaced equalizer, the equalizer filter will have  $N = 2$  and it will be defined by the vector of coefficients:

$$\mathbf{c} = [c_{-2}, c_{-1}, c_0, c_1, c_2]^T. \quad (29)$$

As explained earlier, the vector of coefficients  $\mathbf{c}$  can be obtained by solving the linear system:

$$\mathbf{X}\mathbf{c} = \mathbf{z} \quad (30)$$

where  $\mathbf{z} = [z(-2T), z(-T), z(0), z(T), z(2T)]^T = [0, 0, 1, 0, 0]^T$

## Example (continued)

and

$$\mathbf{X} = \begin{bmatrix} x(-T) & x(-3T/2) & x(-2T) & x(-5T/2) & x(-3T) \\ x(0) & x(-T/2) & x(-T) & x(-3T/2) & x(-3T) \\ x(T) & x(T/2) & x(0) & x(-T/2) & x(-T) \\ x(2T) & x(3T/2) & x(T) & x(T/2) & x(0) \\ x(3T) & x(5T/2) & x(2T) & x(3T/2) & x(T) \end{bmatrix} \quad (31)$$
$$= \begin{bmatrix} \frac{1}{5} & \frac{1}{10} & \frac{1}{17} & \frac{1}{26} & \frac{1}{37} \\ 1 & \frac{1}{2} & \frac{1}{5} & \frac{1}{10} & \frac{1}{17} \\ \frac{1}{5} & \frac{1}{2} & 1 & \frac{1}{2} & \frac{1}{5} \\ \frac{1}{17} & \frac{1}{10} & \frac{1}{5} & \frac{1}{2} & 1 \\ \frac{1}{37} & \frac{1}{26} & \frac{1}{17} & \frac{1}{10} & \frac{1}{5} \end{bmatrix}$$

As a result, we obtain that  $\mathbf{c} = \mathbf{X}^{-1}\mathbf{z}$ .

- Key idea: Instead of selecting  $c_n$  such as to eliminate ISI, select  $c_n$  such as to minimize the mean squares error between the received quantity and the transmitted symbol.
- Mathematical formulation: Expressing again the sampled equalizer output as:

$$z(mT) = \sum_{n=-N}^N c_n y(mT - n\tau), \quad (32)$$

the objective is to minimize:

$$MSE = \mathbb{E} \left\{ |z(mT) - a_m|^2 \right\} \quad (33)$$

Assuming real symbols  $a_m$  (e.g., PAM symbols) we have that:

$$MSE = \mathbb{E} \{a_m^2\} + \sum_{n=-N}^N \sum_{k=-N}^N c_n c_k R_y(n-k) - 2 \sum_{k=-N}^N c_k R_{ay}(k), \quad (34)$$

where:

$$R_y(n-k) = \mathbb{E} \{y(mT - n\tau) y(mT - k\tau)\} \quad (35)$$

and

$$R_{ay}(k) = \mathbb{E} \{y(mT - k\tau) a_m\} \quad (36)$$

The optimal (Minimum Mean Square Error - MMSE) equalizer is obtained as the solution to the following linear system:

$$\mathbf{Rc} = \mathbf{r} \quad (37)$$



where:

$$\mathbf{R} = \begin{bmatrix} R_y(0) & R_y(1) & \cdots & R_y(2N) \\ R_y(-1) & R_y(0) & \cdots & R_y(2N-1) \\ \vdots & \vdots & \ddots & \vdots \\ R_y(-2N) & R_y(-2N+1) & \cdots & R_y(0) \end{bmatrix} \quad (38)$$

and

$$\mathbf{r} = [R_{ay}(-N), \dots, R_{ay}(N)]^T. \quad (39)$$

- Implementing an MMSE equalizer in practice, requires knowledge of the autocorrelation and cross correlation functions  $R_y$  and  $R_{a,y}$ .
- In practice, these functions can be estimated using ensemble averages obtained by transmitting a pilot signal know both to Tx and Rx.
- In such a case,  $R_y$  and  $R_{ay}$  are estimated as:

$$\hat{R}_y(n) = \frac{1}{K} \sum_{k=1}^K y(kT - n\tau) y(kT) \quad (40)$$

and

$$\hat{R}_{ay}(n) = \frac{1}{K} \sum_{k=1}^K y(kT - n\tau) y(kT) \quad (41)$$

# Adaptive equalizers

- For both ZF and MMSE equalizer, we determine the coefficient vector  $\mathbf{c}$  by solving a linear system of the form:

$$\mathbf{c} = \mathbf{B}^{-1}\mathbf{d}. \quad (42)$$

- For practical purposes we wish to find ways for reaching the solution avoiding the use of matrix inversion.
- Iterative, gradient descent methods can be used.
  - Input: Initial estimate  $\mathbf{c}_0$ , matrix  $\mathbf{B}$ , vector  $\mathbf{d}$
  - Step  $k$ ,  $k = 1, \dots$ : Set:

$$\mathbf{c}_k = \mathbf{c}_{k-1} - \Delta \mathbf{g}_{k-1} \quad (43)$$

where  $\Delta$  a step size parameter, and  $\mathbf{g}_k$  the gradient vector corresponding to our optimization criterion.

# Adaptive implementation of MMSE equalizer

- For the MMSE equalizer, it can be proven that:

$$\mathbf{g}_k = -\mathbb{E} \{ (a_k - z_k) \mathbf{y}_k \} \quad (44)$$

- By replacing  $\mathbf{g}_k$  by the estimate

$$\hat{\mathbf{g}}_k = - (a_k - z_k) \mathbf{y}_k \quad (45)$$

the update rule:

$$\mathbf{c}_k = \mathbf{c}_{k-1} + \Delta (a_k - z_k) \mathbf{y}_k \quad (46)$$

is obtained.

- Applying this iterative process we obtain the so-called stochastic gradient of Least Mean Squares (LMS) algorithm.
- One iteration corresponds to one symbol transmission.

In practice adaptive equalizers operate in two modes

- Training mode: An initial mode where a known sequence is transmitted such as to obtain a relatively reliable estimate of the channel,
- Decision directed mode: The equalizer uses the outputs of the detector device  $\tilde{a}_k$  instead of the unknown  $a_k$  and uses  $\tilde{\mathbf{g}}_k = -(\tilde{a}_k - z_k) \mathbf{y}_k$  instead of the unknown  $\mathbf{g}_k$ .
- Infrequent detection errors during decision directed operation do not strongly influence the performance.
- The use of decision directed mode limits the need of frequent training data transmission.

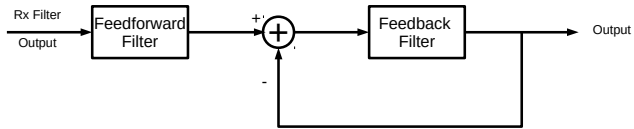
# Decision feedback equalizer

---

# Drawbacks of linear equalizers

- In practice, linear equalizers exhibit poor performance in case of severe ISI effects.
- ISI severity is not necessarily connected to the length  $N$  of the FIR channel.
- It is rather connected to whether or not the channel exhibits frequency nulls.
- Channels with deep fades in the frequency domain can not be efficiently equalized by a linear equalizer.
- This is due to the fact that linear equalizers tend to enhance noise components in deeply faded components.

# Decision feedback equalizer





- Feedforward filter: A linear equalizer of the form presented earlier (e.g., equalizer)
- Feedback filter
  - A symbol spaced FIR filter aiming at further suppressing ISI.
  - It subtracts from the current output of the feedforward filter, a linear combination of previous symbol decisions.
  - The weights for this linear combination is normally determined using the LMS algorithm.