

Second Law of Thermodynamics

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Content

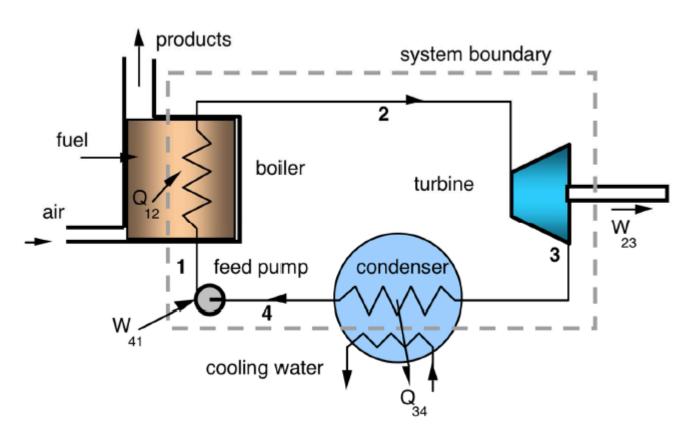


- Heat engines, heat work and energy
- Reversed heat engines
- The 2nd Law of Thermodynamics
- Reversibility and irreversibility
- The Carnot engine and Carnot cycle
- Thermodynamic temperature scale
- Entropy, T-s diagram, increase of entropy and Clausius inequality
- Entropy generation
- Entropy change for ideal gases
- Isentropic efficiency
- Exergy and 2nd Law efficiency

Heat engines



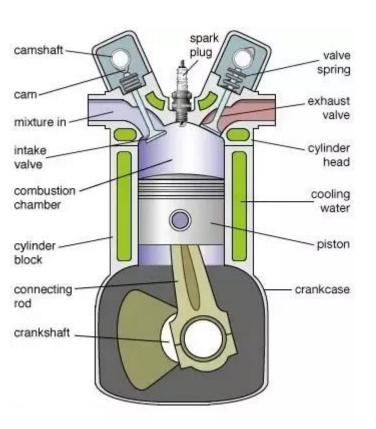
Steam plant

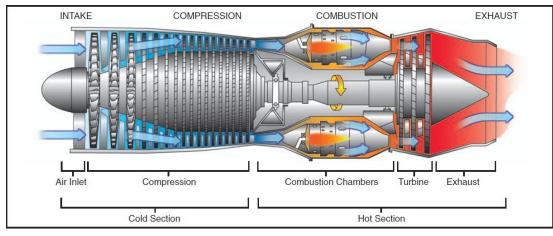


A heat engine is a device which operates in a cycle with only **heat transfer** and **work transfer** crossing the system boundary.

Other types of engines







Internal combustion engines

Gas turbine engines

Heat, work and energy



When the Watt steam engine of 1776 was installed to operate pumps in mines its performance was expressed in simple practical terms. Boulton, writing to a client in 1776, stated:

"We will guarantee that the engine shall raise 20,000 cubic feet of water 24 feet high with each hundredweight of coal burnt."

The relationship between heat and work transfers was not understood at this time and it was not until the latter half of the 19th century that the First Law of Thermodynamics was stated clearly.

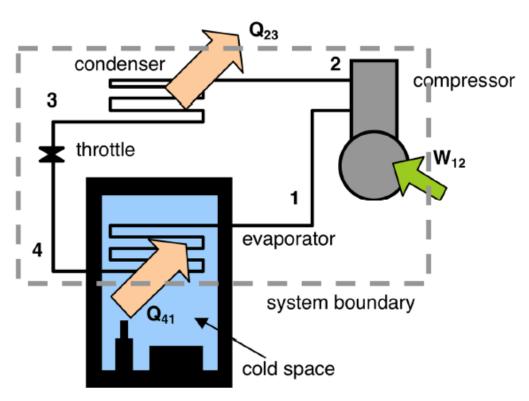
$$\eta_{\mathsf{th}} = rac{\mathsf{W}_{\mathsf{net}}}{\mathsf{Q}_{\mathsf{in}}}$$

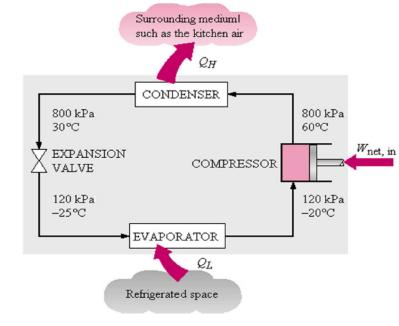
Reversed heat engines



The heat engine may be run in reverse, for example, domestic and industrial

refrigerators.



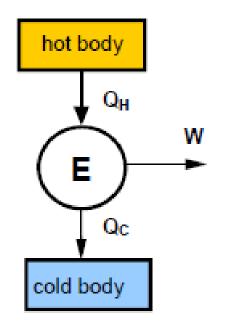


More details to be explained next chapter.

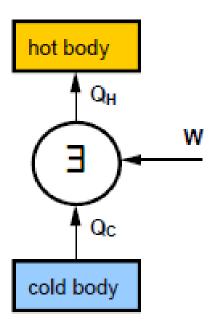




- Heat engines absorb heat from high temperature reservoir and generate mechanical work as output, in the meantime, reject heat to low temperature reservoir.
- Refrigerators absorb mechanical work and heat from low temperature reservoir, and reject heat to high temperature reservoir.



Normal Heat engine



Reversed heat engine

The second Law of Thermodynamics



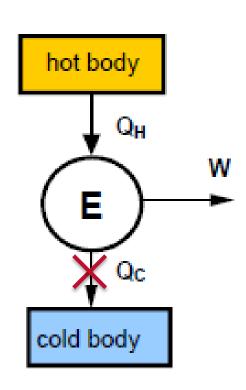
Thermal efficiency is defined as

$$\eta_t = \frac{W}{Q_H} = 1 - \frac{Q_C}{Q_H}$$

If Q_C can be reduced (to zero), efficiency could increase (to 100%)!

This is known as a "Perpetual Motion Machine of the second kind" (PMM2)

It is proved that it's impossible to make such a machine!



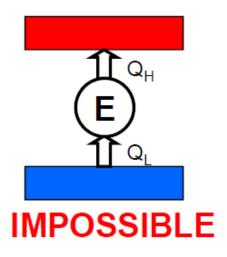
Normal Heat engine

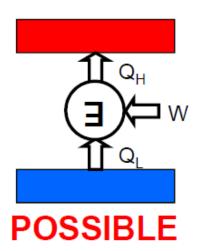
The Second Law of Thermodynamics



Clausius Statement

The Clausius statement of the second law states that no device can transfer heat from a cooler body to a warmer one without leaving an effect on the surroundings.





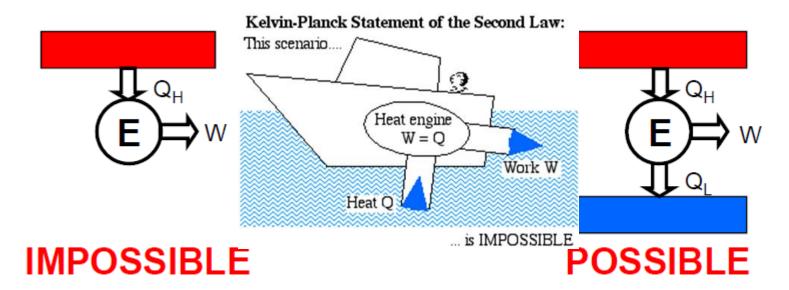
The Second Law of Thermodynamics



Kelvin-Planck Statement

The Kelvin -Planck statement of the second law of thermodynamics states that no heat engine can produce a net amount of work while exchanging heat with a **single reservoir only**.

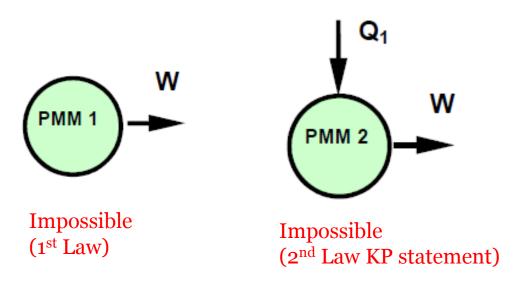
Any device that violates the first or the second law of thermodynamics is called a **second type perpetual-motion machine**.

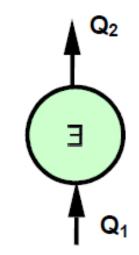


The Second Law of Thermodynamics

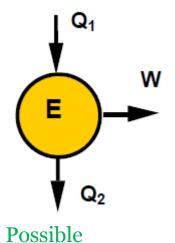


Summary of possible and impossible heat engines

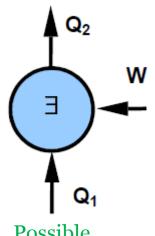




Impossible (2nd Law Clausius statement)



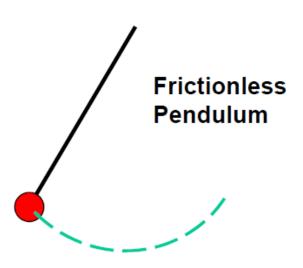
(Heat engine)

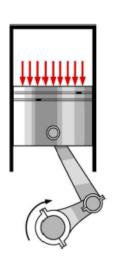


Possible (reversed heat engine)

Reversible and Irreversible processes







Quasiequilibrium
expansion
and
compression
of a gas



Reversible Process:

A process which can be reversed without leaving any trace on the surroundings

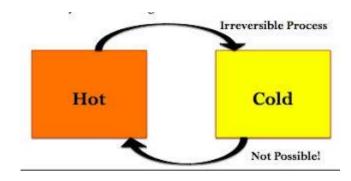
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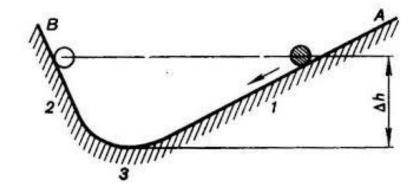
Reversible and irreversible processes



Causes of Irreversibility

- Friction
- Heat transfer
- Non-quasi-equilibrium processes i.e. rapid compression/expansion
- Mixing







Reversible heat engine

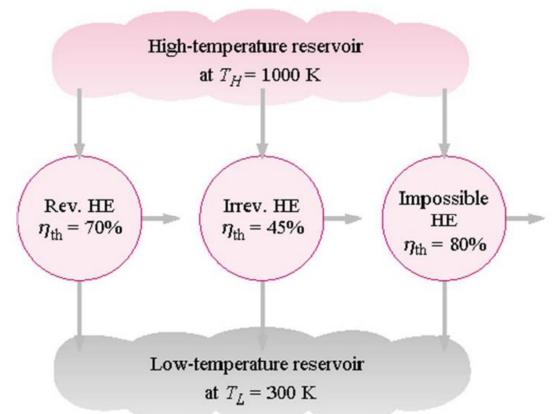


14

Carnot principle

No heat engine can have a higher efficiency than a **Reversible heat engine** operating between the same high- and low- temperature reservoirs.

The efficiencies of all reversible heat engines operating between the same two reservoirs are the same.

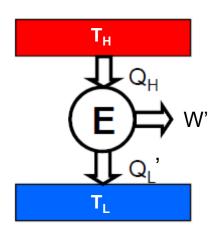


Prove of the Carnot principle

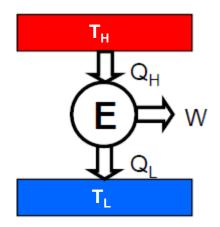


If there exists a hypothetical thermal engine that has higher efficiency than a reversible engine.

Operating in the same temperature reservoirs, assuming it has the same heat input Q_H , as it's more efficient, work output W' would be greater than W for the reversible engine, and Q_I ' would be lower than Q_I .



Hypothetical engine



Reversible engine

W'>W

 Q_L ' $< Q_L$

Prove of the Carnot principle

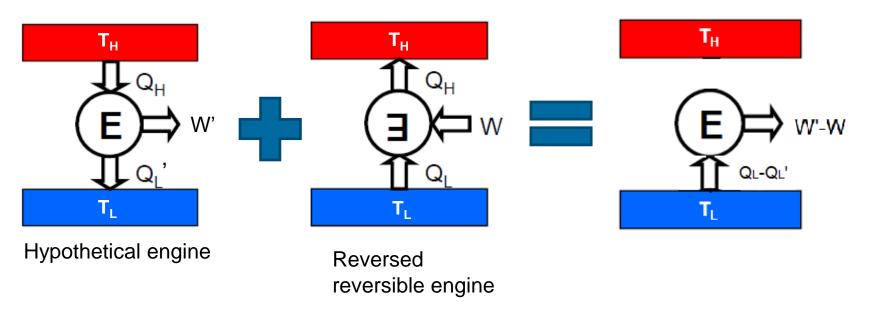


As the reversible engine is completely reversible, we can reverse all the process by just change the direct of the energy flow.

Combine these two engines together (consider as one big engine), we obtain a new engine. For the new engine, Q_H is cancelled out.

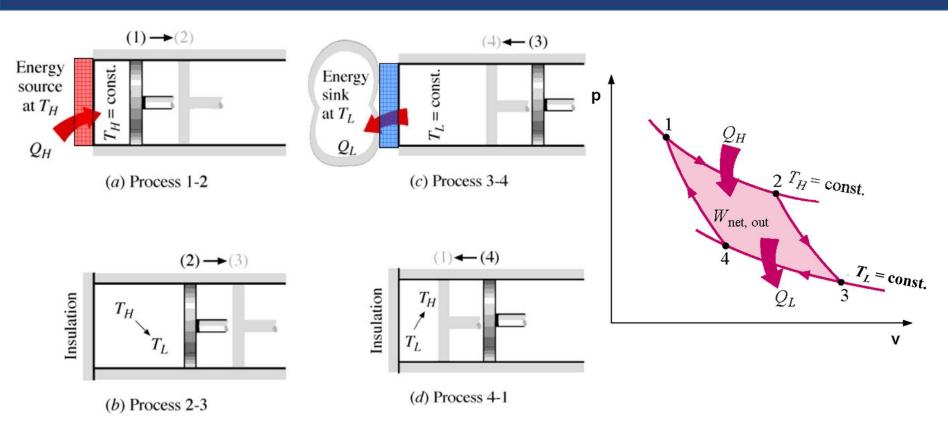
It absorbs heat from low temperature reservoir only, and output work.

From the second law, we know this is impossible. Therefore, it can be concluded that such an engine that has greater efficiency than a reversible engine is not possible.



Carnot cycle





1→2: isothermal heat addition (infinitesimally small temperature difference)

2→3: reversible adiabatic expansion

3→4: isothermal heat rejection (infinitesimally small temperature difference)

4→1: reversible adiabatic compression

NOTE: clockwise enclosed area, positive work (work output)

Thursday, 01 August 2019 17



A thermodynamic temperature scale is defined as a temperature scale that is independent of the properties of the substances that are used to measure temperature.

As all reversible heat engines have the same efficiency when operating between the same two reservoirs, the thermal efficiency is a function of the reservoir

temperatures only.

i.e.
$$\eta_{th,rev} = f(T_H,T_L) \quad \text{or}$$

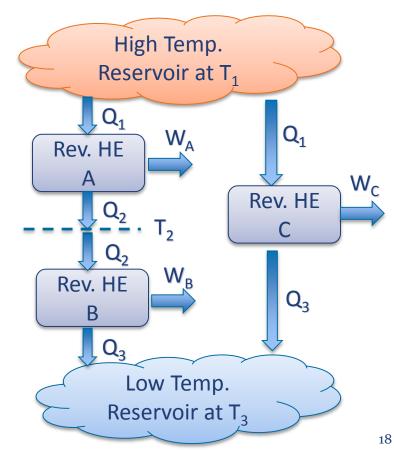
$$\frac{Q_H}{Q_L} = f'(T_H,T_L),$$

$$\text{as } \eta_{th,rev} = 1 - \frac{Q_L}{Q_H}$$

Consider the heat engines arrangement as shown on the right. As they are all reversible engines, based on Carnot principle:

If the heat addition is the same (Q_1) , the heat rejection must be the same (Q₃), and

$$W_A + W_B = W_C$$





For HE A,
$$\eta_A = \frac{Q_1 - Q_2}{Q_1}$$
, for HE B, $\eta_B = \frac{Q_2 - Q_3}{Q_2}$, and for HE C, $\eta_C = \frac{Q_1 - Q_3}{Q_1}$

From the previous slide, we can define a new function that:

$$\frac{Q_1}{Q_2} = f'(T_1, T_2)$$

Therefore:
$$\frac{Q_2}{Q_3} = f'(T_2, T_3), \frac{Q_1}{Q_3} = f'(T_1, T_3)$$

Because we have

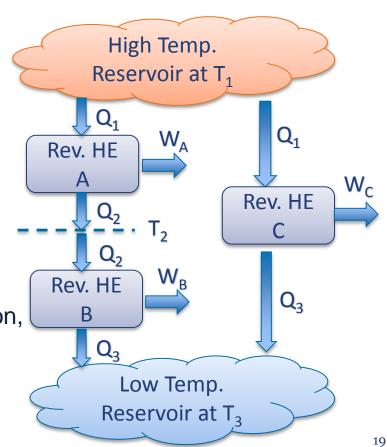
$$\frac{Q_1}{Q_3} = \frac{\frac{Q_1}{Q_2}}{\frac{Q_3}{Q_2}} = \frac{f'(T_1, T_2)}{f'(T_2, T_3)}$$

 T_2 must cancel from the right hand side, also because T_2 is arbitrarily selected. This yields a new relationship

$$f'(T_1, T_2) = \frac{\Psi(T_1)}{\Psi(T_2)}$$

There are many relationship satisfies this equation, and the simplest is

$$\Psi(T) = T$$





(continue...)

Thus we have

 $\frac{Q_1}{Q_2} = \frac{T_1}{T_2}$

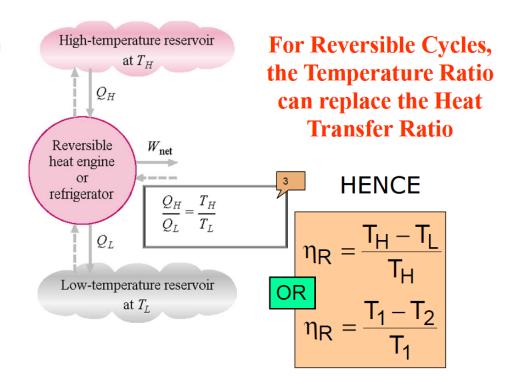
And for efficiency

$$\eta_{12} = 1 - \frac{Q_2}{Q_1} = 1 - \frac{T_2}{T_1}$$

This is firstly defined by Kelvin, and this temperature scale is known as absolute temperature scale.

The triple point of water is defined as 273.16 K (0.01 °C), and water boiling point at 1 atm is defined as 373.15 K (100 °C).

This definition is to be renewed this year which connects to Boltzmann constant.





For ideal gases

Let's also consider the Carnot cycle running with an ideal gas.

For a closed system, dw = pdv,

For an ideal gas, pv = RT, therefore $dw = \frac{RT}{v}dv$

Also for an ideal gas, $du = c_v dT$

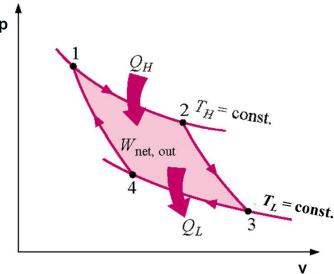
From 1st Law dq = dw + du

Substituting, $dq = \frac{RT}{v}dv + c_v dT$

For process $1\rightarrow 2$

$$q_H = 0 + RT_H \ln \left(\frac{v_2}{v_1}\right)$$

For process $3\rightarrow 4$



 $q_L = 0 + RT_L \ln \left(\frac{v_3}{v_4}\right)$ (here consider q_L as the magnitude of heat rejection)

For the adiabatic processes $2\rightarrow 3$ and $4\rightarrow 1$,

2
$$\rightarrow$$
3: $0 = \int_{T_H}^{T_L} \frac{c_v}{T} dT + R \ln \frac{v_3}{v_2}$ $4 \rightarrow$ 1: $0 = 0 = \int_{T_L}^{T_H} \frac{c_v}{T} dT + R \ln \frac{v_1}{v_4}$

Note:
$$\int_{T_H}^{T_L} \frac{c_v}{T} dT = -\int_{T_L}^{T_H} \frac{c_v}{T} dT$$
, we have $R \ln \frac{v_3}{v_2} = -R \ln \frac{v_1}{v_4}$



For ideal gases

Continue...

$$R \ln \frac{v_3}{v_2} = -R \ln \frac{v_1}{v_4}$$
 We have
$$\frac{v_3}{v_2} = \frac{v_4}{v_1}$$
 Or
$$\frac{v_2}{v_1} = \frac{v_3}{v_4}$$

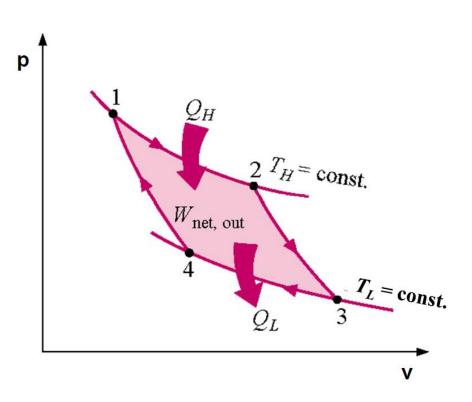
Therefore

Or

$$\frac{q_L}{q_H} = \frac{RT_L \ln\left(\frac{v_3}{v_4}\right)}{RT_H \ln\left(\frac{v_2}{v_4}\right)} = \frac{T_L}{T_H}$$

And efficiency of Carnot cycle is

$$\eta_T = 1 - \frac{q_L}{q_H} = 1 - \frac{T_L}{T_H}$$



This is the same conclusion from previous derivation.

Reversible cycle thermal efficiency is solely determined by the high ad low temperatures!

Entropy

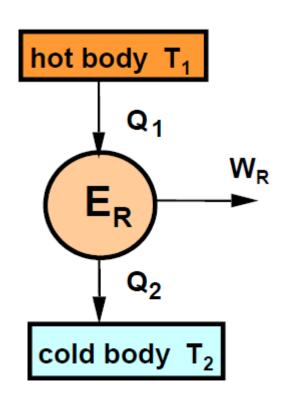


Reversible heat engine

$$\eta_T = 1 - \frac{Q_2}{Q_1} = 1 - T_2/T_1$$

$$\frac{Q_1}{T_1} - \frac{Q_2}{T_2} = 0$$
or
$$\oint \frac{dQ_R}{T} = 0$$

$$\int \frac{dQ_R}{T} = \text{property change} = S_1 - S_2$$

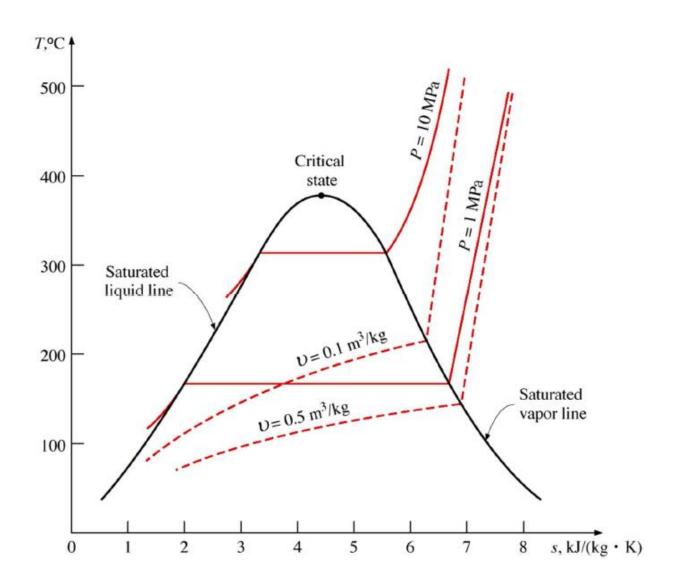


S=entropy (kJ/K)

Or s=S/m=specific entropy (kJ/kg K)

NOTE: subscript R denotes for a reversible process.





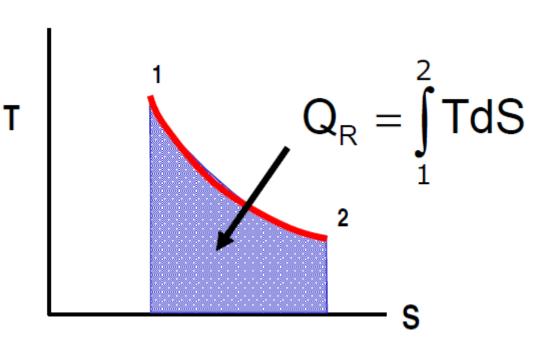
Entropy change and T-s diagram



Chosen T-s diagram as dq = Tds

Isentropic process Entropy change =0

$$\int \frac{dQ_R}{T} = 0$$

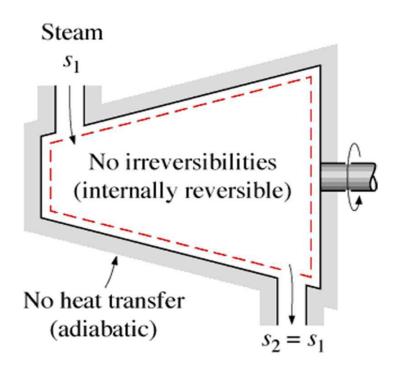


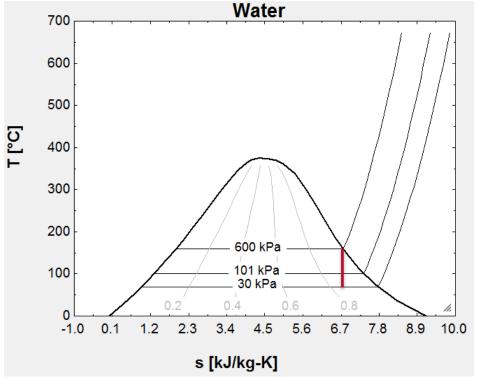
Isentropic = Adiabatic + Reversible

Note: If any 2 of these process descriptions is true then so is the 3rd.



Dry saturated steam at 600 kPa flows steadily into a turbine which exhausts to a condenser at 30 kPa. Neglecting the kinetic energy of the steam at inlet and exit calculate the maximum possible specific work transfer from the turbine.





Solution



From steam table, saturated steam at 600kPa has the following properties:

 h_1 =2757 kJ/kg; s_1 =6.761 kJ/kg K; T_1 =158.8 °C

Expand to 30 kPa in an isentropic process,

Therefore $s_2=s_1=6.761$ kJ/kg K.

Using data at 0.3 bar, $s_f=0.944$, $s_g=7.767$,

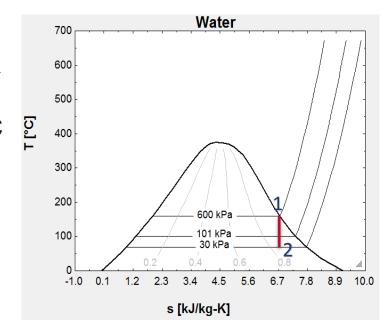
$$x = \frac{s_2 - s_f}{s_g - s_f} = 0.853$$

We can find enthalpy at 2:

$$h_2 = h_f(1-x) + h_q x = 289(1-0.853) + 2625 \times 0.853 = 2280.6 \text{ kJ/kg}$$

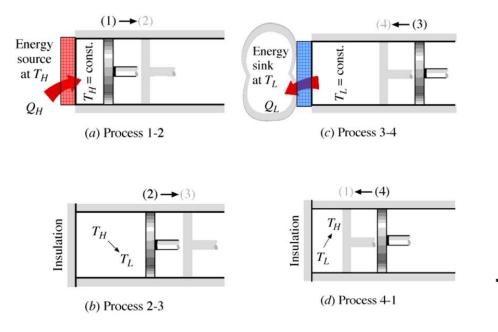
The maximum possible specific work transfer is the enthalpy change

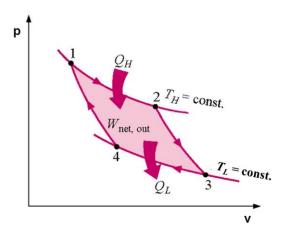
$$w_{ext_max} = -(2280.6 - 2757) = 476.4 \, kJ/kg$$



Revisit Carnot Cycle



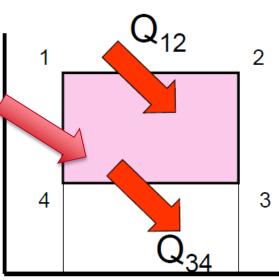




$W_{net} = \Sigma Q = area of T-s diagram$

for a reversible engine, the entropy decrease for the hot reservoir equals the entropy

increase for the cold reservoir $(s_3 - s_4 = s_2 - s_1)$.



28

Principle of increase of entropy



Consider two heat engines between same heat reservoirs: a reversible and an irreversible

$$\eta_R \geq \eta_I$$

For the reversible engine, we have

$$\eta_R = 1 - \frac{T_L}{T_H}$$

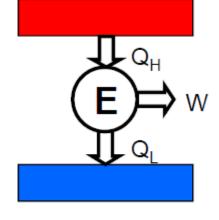
For the irreversible engine, we have

$$\eta_I = \frac{W}{Q_H}$$

Therefore

$$\frac{W}{Q_H} = \frac{Q_H - Q_L}{Q_H} \le \frac{T_H - T_L}{T_H}$$

$$\frac{Q_H}{T_H} - \frac{Q_L}{T_L} \le 0$$
 or in general



$$\oint \frac{dQ}{T} \le 0$$

Clausius Inequality



The definition of entropy is based on the Clausius inequality, given by

$$\oint \frac{dQ}{T} \le 0 \qquad (kJ/K)$$

where the equality holds for internally or totally reversible processes and the inequality for irreversible processes.

Note the previous equation we have is $\int \frac{dQ_R}{T} = 0$ Mind the difference!

Entropy generation



Consider a system that undergoes a cycle comprising an irreversible adiabatic process (1a2) and a reversible process (2b1)

For the adiabatic process (1a2)

$$\int_{1}^{2} \left(\frac{dq}{T} \right)_{q} = 0$$

But irreversible

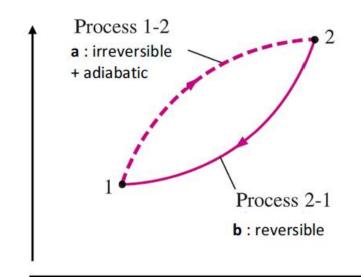
$$\int_{1}^{2} \left(\frac{dq}{T} \right)_{q} \neq \int_{1}^{2} ds$$

For the **reversible** process (2b1)

$$\int_2^1 \left(\frac{dq}{T}\right)_h = s_1 - s_2$$

Clausius inequality $\oint \frac{dQ}{T} \leq 0$

Therefore $\int_{1}^{2} \left(\frac{dq}{T}\right)_{a} + \int_{2}^{1} \left(\frac{dq}{T}\right)_{b} = 0 + (s_{1} - s_{2}) \le 0 = > s_{2} \ge s_{1}$



Entropy generation



Entropy always increases!!!

The inequality part of the Clausius inequality combined with the definition of entropy yields an inequality known as the *increase of* entropy principle, expressed as

$$S_{gen} \geq 0$$
 (kJ/K)

Where S_{gen} is the entropy generated during a process.

$$dS = \frac{dQ_R}{T}$$
 or $dS = \frac{dQ}{T} + S_{gen}$

Reversible process

Irreversible process

Entropy generation



The previous conclusion leads to an important observation, namely that the entropy of an isolated system must either **increase** or **remain constant**.

In any process within an adiabatic boundary, whether expansion or compression, the entropy always increases due to the irreversibility inherent in any real process – only in an idealised reversible cycle does $S_2=S_1$

What is entropy



By definition, entropy is a working fluid property defined as

$$dS = \frac{dQ_R}{dT} \quad \frac{dQ_R}{T}$$

When heat transfer in/out across the system boundary, S can increase/decrease.

Reversible work does not change S.

By irreversibilities, S is generated, told by the Clausius inequality.

In an isolated system (where Q & W and mass flow = 0), S **increases** because the integral must be zero. Entropy is not a **conserved property** like energy or mass. S_{gen} is a measure of irreversibility and therefore how close any system comes to its reversible ideal.

Another very subtle corollary is that things only happen in one direction i.e. to increase entropy.

What is Entropy



Entropy change is caused by heat transfer and irreversibility.

Heat transfer to a system increases the entropy, and heat transfer from a system decreases it.

The effect of irreversibility is always to increase the entropy.

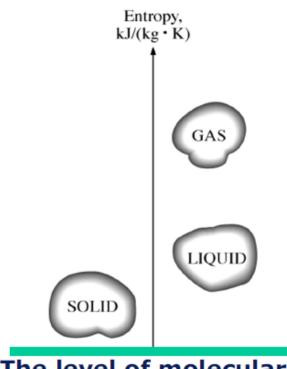
"It's the Second Law of Thermodynamics: Sooner or later everything turns to shit." Woody Allen, in Husbands and Wives (1992).

What is entropy?



Entropy: a measure of **DISORDER**

- Entropy is minimum for solids, is higher for liquids, and higher still for gases and thus has come to be seen as a measure of disorder.
- Heat transfer only flows from hot to colder bodies (unless there is some work input) and in doing so entropy increases as the disorder in the colder body increases.
- Entropy is also linked to the quality of energy. This is to be discussed later.



The level of molecular disorder (entropy) of a substance increases as it melts and evaporates

T-ds relations



From the first law,

$$dq = dw + du$$

If the process is reversible, and dw = pdv, we have

$$dq_R = pdv + du$$

By definition, $\frac{dq_R}{T} = ds$, we have

$$Tds = du + pdv$$

Or if we use enthalpy, as h = u + pv, dh = du + pdv + vdp

$$Tds = dh - vdp$$

provide simple relationships for evaluating the entropy changes in any process.





The entropy-change for a process involving an ideal gas can be summarized as follows:

$$s_2 - s_1 = c_V \ln \left(\frac{T_2}{T_1}\right) + R \ln \left(\frac{v_2}{v_1}\right)$$

And

$$s_2 - s_1 = c_p \ln \left(\frac{T_2}{T_1}\right) - R \ln \left(\frac{p_2}{p_1}\right)$$

For liquid of solid, as $v_2 \approx v_1$, and we don't distinguish c_p and c_v ,

$$s_2 - s_1 = c \ln \left(\frac{T_2}{T_1} \right)$$

Derivation of T-ds relations



(with pv = RT)

$$h = u + pv$$

$$dh = du + pdv + vdp$$

$$ds = \frac{dq_R}{T}$$

First Law:

$$dq_R = du + pdv$$

Hence:

$$Tds = du + pdv = dh - vdp$$

For an ideal gas:

$$c_V = \frac{du}{dT} \qquad c_p = \frac{dh}{dT}$$

Therefore:

$$Tds = du + pdv = c_V dT + pdv$$

And

$$ds = c_V \frac{dT}{T} + p \frac{dv}{T} = c_V \frac{dT}{T} + \frac{R}{v} dv$$

Hence:

$$\int_{1}^{2} ds = c_{V} \int_{1}^{2} \frac{dT}{T} + R \int_{1}^{2} \frac{dv}{v}$$

Hence:

$$s_2 - s_1 = c_V \ln \left(\frac{r_2}{r_1}\right) + R \ln \left(\frac{v_2}{v_1}\right)$$

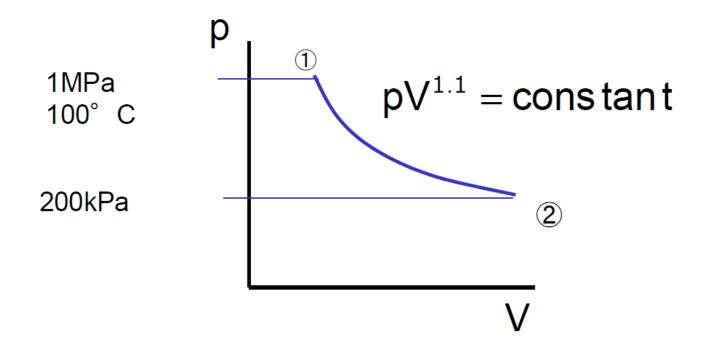
Try to derive:

$$s_2 - s_1 = c_p \ln \left(\frac{T_2}{T_1}\right) - R \ln \left(\frac{p_2}{p_1}\right)$$



• One kilogramme of air at 1MPa, 100° C expands to a pressure of 200kPa according to the relationship $pv^{1.1} = constant$

Calculate the change in entropy of the air.

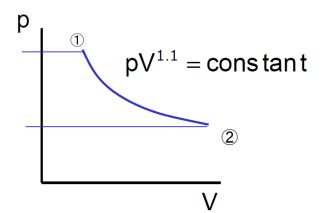


Solution



@initial state 1

$$p_1 = 1 \, MPa$$
 1MPa 100° C $T_1 = 373.15 \, K$ $v_1 = \frac{RT_1}{p_1} = \frac{287 \times 373.15}{10^6} = 0.1071 \, m^3/kg$ 200kPa



@final state 2

$$p_2 = 200 \text{ kPa}$$
 $p_1 v_1^{1.1} = p_2 v_2^{1.1} \Longrightarrow v_2 = 0.463 \text{ m}^3/\text{kg}$
 $T_2 = \frac{p_2 v_2}{R} = 322.4 \text{ K}$

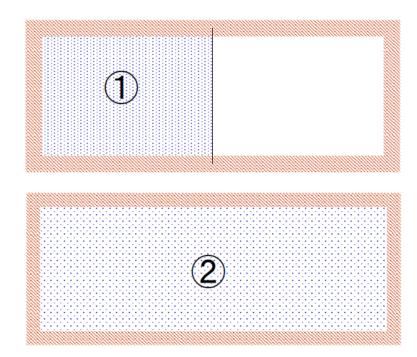
$$s_2 - s_1 = c_V \ln\left(\frac{T_2}{T_1}\right) + R \ln\left(\frac{v_2}{v_1}\right)$$

$$= 718 \ln\left(\frac{322.4}{373.15}\right) + 287 \ln\left(\frac{0.463}{0.1071}\right)$$

$$= 315.2 J/kgK$$



 One kilogramme of air at 600kPa, 300K expands into an evacuated insulated container so that its volume is doubled.
 Calculate the increase in entropy of the air.



Solution



We use the equation $s_2 - s_1 = c_V \ln \left(\frac{T_2}{T_1}\right) + R \ln \left(\frac{v_2}{v_1}\right)$

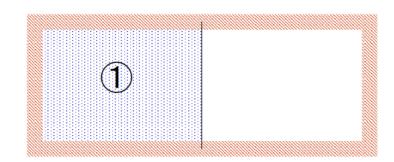
From 1-2, we have $q - w = \Delta u$

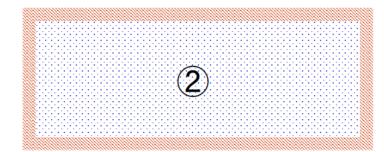
Where q = 0 (insulated) and w = 0 (evacuated)

Therefore $\Delta u = 0$, so $\Delta T = 0$

$$s_2 - s_1 = c_V \ln\left(\frac{T_2}{T_1}\right) + R \ln\left(\frac{v_2}{v_1}\right) = 0 + R \ln(2)$$

= 287 ln 2 = 198.9 J/kgK

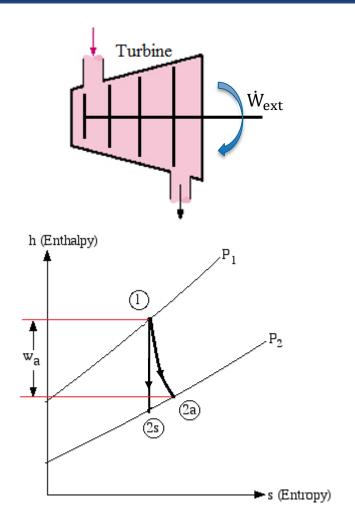




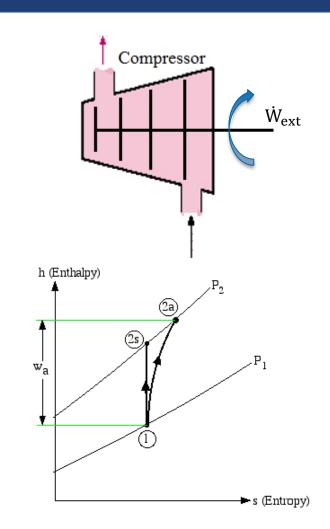
Thursday, 01 August 2019

Isentropic efficiency of turbine and compressor





$$\eta_T = rac{actual\ power\ output}{isentropic\ power\ output} = rac{h_1 - h_{2a}}{h_1 - h_{2s}}$$



$$\eta_T = \frac{actual\ power\ output}{isentropic\ power\ output} = \frac{h_1 - h_{2a}}{h_1 - h_{2s}} \qquad \eta_C = \frac{isentropic\ power\ input}{actual\ power\ input} = \frac{h_{2s} - h_1}{h_{2a} - h_1}$$

Exergy and availability



The First Law of thermodynamics defines the *quantity* of energy.

The Second Law of thermodynamics deals with the *quality* of energy.

1 kWh of electricity and a certain mount of hot water contains 1 kWh of energy, they have the same amount of energy (quantity), but are they of the same value (quality)? (Energy quality of different forms)

1 kg of warm water at 50 °C, 1 bar (209.4 kJ) and 75 g of hot steam at 150 °C, 1 bar have the same energy (209.4 kJ). Can they convert to the same amount of work? (Energy quality of different grade)

We introduce a new concept of **Exergy**, which is the <u>maximum useful work</u> that could be obtained from the system at a <u>given state in a specified environment</u>.



Exergy is the <u>maximum useful work</u> that could be obtained from the system at a <u>given state in a specified environment.</u>

Given state in a specified environment

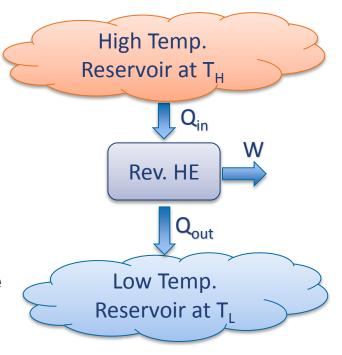
Not a variable, also know as

dead state

(As the Carnot efficiency is directly linked to low temperature reservoir conditions)

Maximum useful work

The work output is maximised when the process between the two states is executed in a **reversible manner**



Exergy



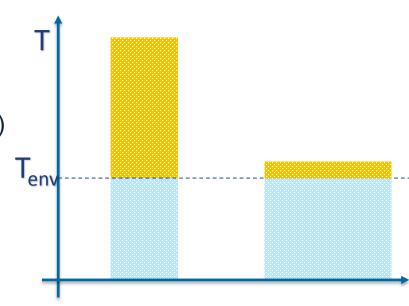
Therefore, a system delivers the maximum possible work as it undergoes a reversible process from the specified initial state to the state of its environment, that is, the dead state (for example, by Carnot cycle). This represents the useful work potential of the system at the specified state and is called **exergy**.

It represents the *upper limit* on the amount of work a device can deliver without violating any thermodynamic laws.

Previous question: electric energy vs. thermal energy, and thermal energy at different temperatures.

Electric/mechanical energy: pure exergy (100%)
Thermal energy: capped by the second law,
higher temperature → higher exergy

 Ψ/ψ is used to represent exergy.



Thursday, 01 August 2019





Kinetic energy is a form of mechanical energy, therefore kinetic energy is pure exergy (can be converted to work entirely)

$$\psi_{ke} = ke = \frac{c^2}{2}$$

Potential energy is also a form of mechanical energy, therefore can be converted to work entirely as well.

$$\psi_{pe} = pe = gz$$

Electric energy can be 100% converted to mechanical energy (and vice versa), so electric energy is pure exergy as well



Consider a large furnace that con transfer heat at a temperature of 1100 K at a steady rate of 3000 kW. Determine the rate of exergy flow associated with this heat transfer. Assume an environment temperature of 25°C.

The thermal efficiency of a reversible heat engine is

$$\eta_{t,max} = \eta_{t,rev} = 1 - \frac{T_L}{T_H} = 1 - \frac{298 \, K}{1100 \, K} = 72.9\%$$

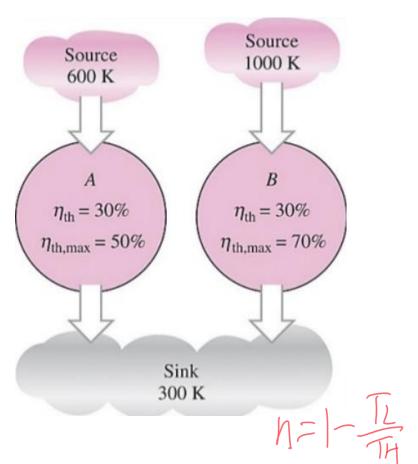
The most energy can be converted to work is 72.9% of the heat received from the furnace. Thus the exergy is equivalent to the power produced by the reversible heat engine:

$$\dot{\Psi} = \eta_{t,rev} \dot{Q}_{in} = 0.729 \times 3000 = 2187 \ kW$$

Second Law efficiency



Consider two heat engines have the same thermal efficiency. Are they equally well designed?



Obviously, as B has a higher T_H, the HE B should delivery higher efficiency, as it has higher maximum efficiency (in a reversible manner).

Therefore the second law efficiency, a.k.a exergy efficiency, takes into consideration of the available exergy, i.e. the maximum possible performance

The second law efficiency



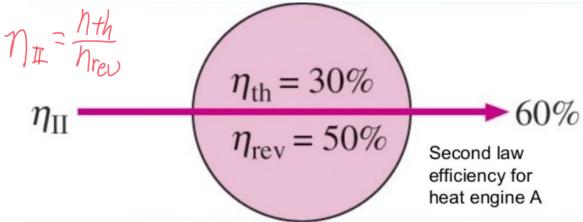
51

The second law efficiency is a measure of the performance of a device relative to what its maximum performance could be, which is under reversible conditions.

It provides a better view in comparison with the first law efficiency (thermal efficiency or energy efficiency) as not only it considers the quantity of heat source, also the quality.

What is the η_{II} of HE B?

What is the η_{II} of a reversible device?



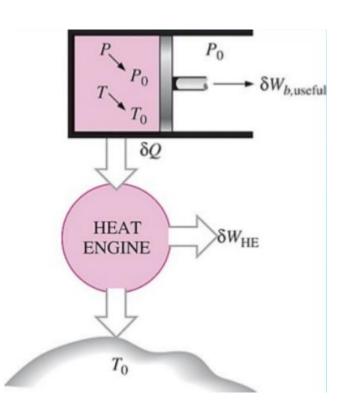
Exergy of a closed system



For a reversible process, the system work

$$\delta W = pdV = (p - p_0)dV + p_0dV = \delta W_{b,useful} + p_0dV$$

During this process, heat transferred from the system and assume there exists a heat engine to utilise the heat. The work can be produced by the heat engine is



$$\delta W_{HE} = \left(1 - \frac{T_0}{T}\right) \delta Q = \delta Q - \frac{T_0}{T} \delta Q$$
$$= \delta Q - \left(T_0 \frac{\delta Q}{T}\right) = \delta Q - (-T_0 dS)$$

Or
$$\delta Q = \delta W_{HE} - T_0 dS$$

And the first law

 $-\delta Q - \delta W = dU$ (taking the direction of Q as from the system)

Substitute and integrate (from initial to dead state):

$$W_{total \, useful} = W_{HE} + W_{b,useful}$$

= $(U - U_0) + p_0(V - V_0) - T_0(S - S_0)$
= Ψ

Exergy change of a closed system



From last slide,

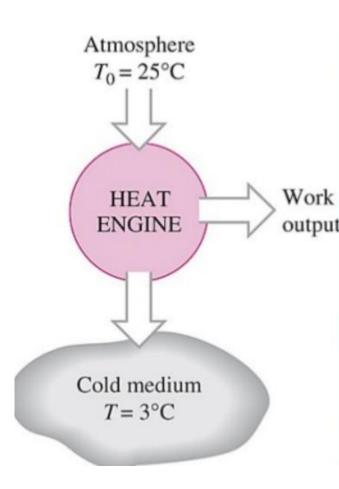
$$\Delta\Psi = (U_2 - U_1) + p_0(V_2 - V_1) - T_0(S_2 - S_1) + m(c_2^2 - c_1^2) + mg(z_2 - z_1)$$

Or in specific form:

$$\Delta \psi = (u_2 - u_1) + p_0(v_2 - v_1) - T_0(s_2 - s_1) + (c_2^2 - c_1^2) + g(z_2 - z_1)$$

The exergy change of a system is zero if the state of the system or the environment does not change, e.g. steady flow system

A closed system can only have positive or zero exergy. If the system has lower-than-environment temperature, it has the capability to deliver work.

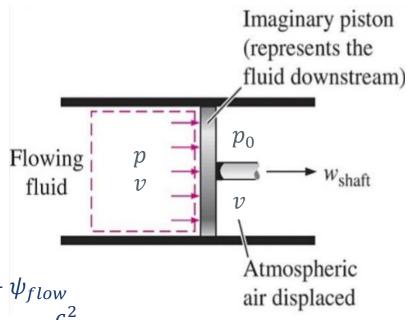


Exergy for open system



In open (flowing) systems, there is also flow energy.

The exergy of flow energy is the useful work that would be delivered by an imaginary piston in the flow v ($\psi_{flow} = pv - p_0v$)



$$\psi_{flowing fluid} = \psi_{nonflowing fluid} + \psi_{flow}$$

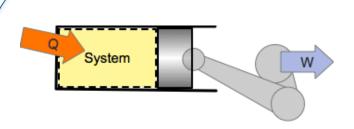
$$= (u - u_0) + p_0(v - v_0) - T_0(s - s_0) + \frac{c^2}{2} + gz + pv - p_0v$$

$$= (u + pv) - (u_0 + p_0v_0) - T_0(s - s_0) + \frac{c^2}{2} + gz$$

$$= (h - h_0) - T_0(s - s_0) + \frac{c^2}{2} + gz$$

Exergy for different system summary





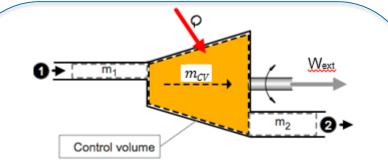
Closed system

Energy

$$e = u + \frac{1}{2}c^2 + gz$$

Exergy

$$\psi = (u - u_0) + p_0(v - v_0) - T_0(s - s_0) + \frac{1}{2}c^2 + gz$$



Open system

Energy

$$e = h + \frac{1}{2}c^2 + gz$$

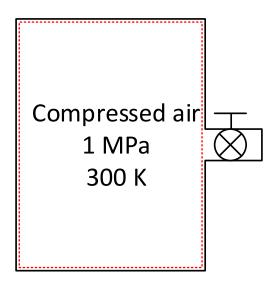
Exergy

$$\psi = (h - h_0) - T_0(s - s_0) + \frac{1}{2}c^2 + gz$$



A 200 m3 rigid tank contains compressed air at 1 MPa and 300 K. Determine how much work can be obtained from this are if the environment conditions are 100 kPa and 300 K.

Assume ideal gas, k.e. and p.e. negligible, R=287 J/kgK



Thursday, 01 August 2019



$$m = \frac{pV}{RT} = \frac{10^6(200)}{287(300)} = 2323 \times 10^3 g = 2323kg$$

$$\Psi = m\psi = m \left[(u - u_0)^{70} + p_0(v - v_0) - T_0(s - s_0) + \left(\frac{c^2}{2} + gz\right)^{70} \right]$$

$$= m[p_0(v - v_0) - T_0(s - s_0)]$$

We have
$$p_0(v - v_0) = p_0\left(\frac{RT}{p} - \frac{RT_0}{p_0}\right) = RT_0\left(\frac{p_0}{p} - 1\right)$$
 (because T=T₀)

$$T_0(s - s_0) = T_0 \left(c_p \ln \frac{T}{T_0} - R \ln \frac{p}{p_0} \right) = -T_0 R \ln \frac{p}{p_0}$$
 (because T=T₀)

Therefore

$$\psi = RT_0 \left(\frac{p_0}{p} - 1 \right) + RT_0 \ln \frac{p}{p_0} = RT_0 \left(\frac{p_0}{p} - 1 + \ln \frac{p}{p_0} \right)$$

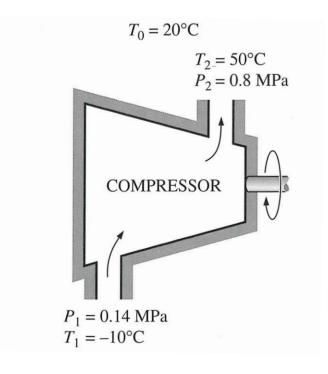
$$= 287(300) \left(\frac{10^5}{10^6} - 1 + \ln \frac{10^6}{10^5} \right) = 120.76 \times 10^3 J/kg = 120.76 \, kJ/kg$$

$$\Psi = 2323(120.76) = 281MJ$$

Thursday, 01 August 2019



Refrigerant R134a is to be compressed from 0.14 MPa and -10 °C to 0.8 MPa and 50 °C steadily by a compressor. Taking the environment conditions to be 20 °C and 95 kPa. Determine the exergy change of the refrigerant during this process and the minimum work input that needs to be supplied to the compressor per unit mass of the refrigerant.



Solution



At inlet (from property table):

$$p_1 = 0.14 \, MPa$$
, $T_1 = -10^{\circ}\text{C} \rightarrow h_1 = 246.36 \, kJ/kg$, $s_1 = 0.9724 \, kJ/kgK$

At exit (from property table):

$$p_2 = 0.8 MPa$$
, $T_2 = 50$ °C $\rightarrow h_2 = 286.69 \ kJ/kg$, $s_1 = 0.9802 \ kJ/kgK$

The exergy change can be calculated as:

$$\Delta \psi = \psi_2 - \psi_1 = (h_2 - h_1) - T_0(s_2 - s_1) + \Delta k.e.^{70} + \Delta p.e.^{70}$$

$$= (h_2 - h_1) - T_0(s_2 - s_1)$$

$$= (286.69 - 246.36) - 293(0.9802 - 0.9724)$$

$$= 38.0 \ kJ/kg$$

and the minimum work needs to be supplied is the reversible work, which is the change of exergy

$$w_{in,min} = \Delta \psi = 38 \ kJ/kg$$

Summary



- Heat engines, heat work and energy (understanding)
- Reversed heat engines (understanding)
- The 2nd Law of Thermodynamics (understanding)
- Reversibility and irreversibility (understanding)
- The Carnot engine and Carnot cycle (understanding)
- Thermodynamic temperature scale (understanding)
- Entropy, T-s diagram, increase of entropy and Clausius inequality (understanding & calculation)
- Entropy generation (understanding & calculation)
- Entropy change for ideal gases (understanding & calculation)
- Isentropic efficiency (understanding & calculation)
- Exergy and 2nd Law efficiency (understanding & calculation)