
Fire Dynamics

Fire plume II

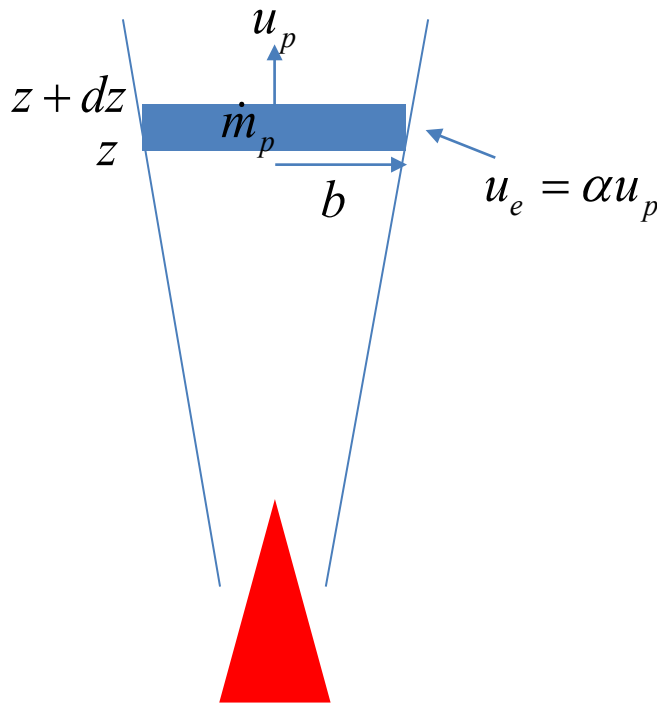
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Objectives

- Calculating flame height of a pool fire

Ideal fire plume



$$u_p = 1.94 \left(\frac{g}{\rho_\infty c_p T_\infty} \right)^{1/3} \dot{Q}_c^{1/3} z^{-1/3}$$

$$\dot{m}_p = 0.2 \left(\frac{\rho_\infty^2 g}{c_p T_\infty} \right)^{1/3} \dot{Q}_c^{1/3} z^{5/3}$$

$$\Delta T_p = 5.0 \left(\frac{T_\infty}{g c_p^2 \rho_\infty^2} \right)^{1/3} \dot{Q}_c^{2/3} z^{-5/3}$$

Zukoski plume

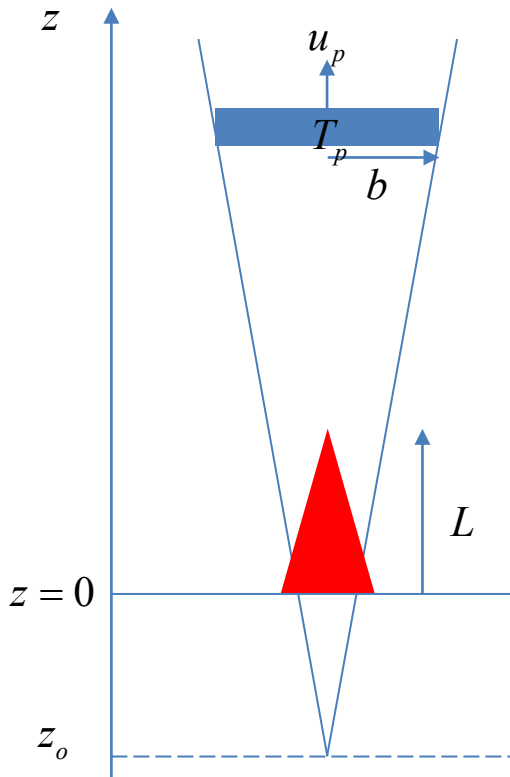
- Zukoski plume

$$\dot{m}_p = 0.21 \left(\frac{\rho_\infty^2 g}{c_p T_\infty} \right)^{1/3} \dot{Q}_c^{1/3} z^{5/3} = 0.071 \dot{Q}_c^{1/3} z^{5/3}$$

- Thomas plume for near-field
 - When diameter is larger than flame height

$$\dot{m}_p = 0.59 D z^{3/2}$$

Heskestad plume



Flame height: $L = 0.235\dot{Q}^{2/5} - 1.02D$

Virtual origin: $z_o = 0.083\dot{Q}^{2/5} - 1.02D$

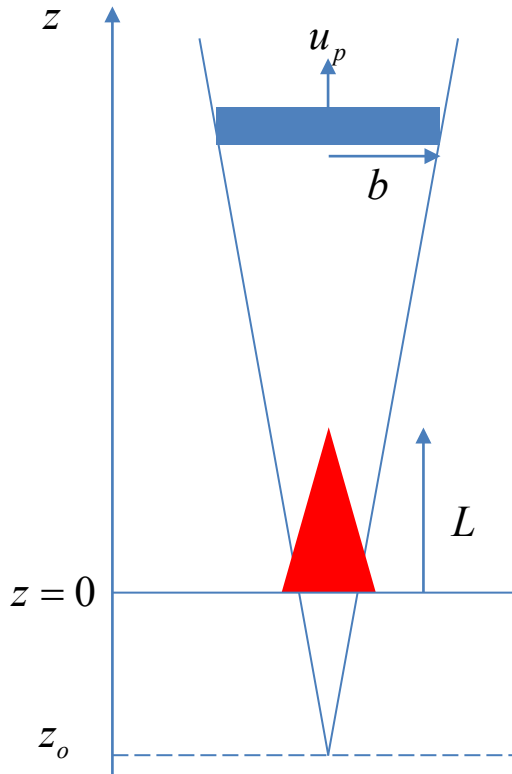
\dot{Q}_c [kW], and u_p [m/s]

$$b = 0.12 \left(\frac{T_p}{T_a} \right)^{1/2} (z - z_o)$$

$$\Delta T_p = T_p - T_a \approx 25 \left(\frac{\dot{Q}_c^{2/5}}{(z - z_o)} \right)^{5/3}$$

$$u_p \approx 1.0 \left(\frac{\dot{Q}_c}{(z - z_o)} \right)^{1/3}$$

Heskestad plume



For $z > L$, $\dot{m}_p [\text{kg/s}]$, $\dot{Q}_c [kW]$, $L [m]$

$$\dot{m}_p = 0.071 \dot{Q}_c^{1/3} (z - z_o)^{5/3} + (1.92 \times 10^{-3}) \dot{Q}_c$$

For $z < L$,

$$\dot{m}_p = 0.0056 \dot{Q}_c \left(\frac{z}{L} \right)$$

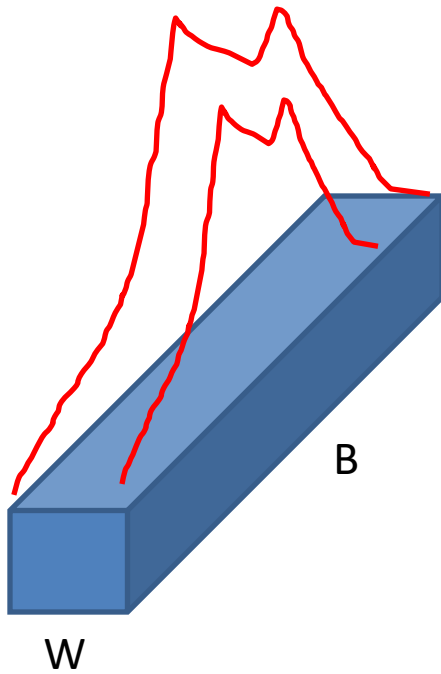
McCaffrey plume

| Region | $z/\dot{Q}^{2/5}$ [m/kW ^{2/5}] | η | κ |
|--------------|--|--------|---|
| Continuous | < 0.08 | 1/2 | 6.8 [m ^{1/2} /s] |
| Intermittent | 0.08–0.2 | 0 | 1.9 [m/(kW ^{1/5} s)] |
| Plume | > 0.2 | –1/3 | 1.1 [m ^{4/4} /(kW ^{1/3} s)] |

$$\Delta T_p = T_a \left(\frac{\kappa}{0.9\sqrt{2g}} \right)^2 \left(\frac{z}{\dot{Q}^{2/5}} \right)^{2\eta-1}$$

$$u_p = \kappa \left(\frac{z}{\dot{Q}^{2/5}} \right)^\eta \dot{Q}^{1/5}$$

Line fire



For $B > 3W$,

$$L = 0.035 \left(\frac{\dot{Q}}{B} \right)^{2/3}$$

Example

Calculate the flame height of heptane in a 1 m by 1 m pan.

| | ΔH_c [kJ/g] | \dot{m}''_{∞} [kg/m ² -s] | $k\beta$ [1/m] | density [kg/m ³] |
|----------|---------------------|---|----------------|------------------------------|
| Butane | 45.7 | 0.078 | 2.7 | 573 |
| Benzene | 40.1 | 0.085 | 2.7 | 874 |
| Hexane | 44.7 | 0.074 | 1.9 | 650 |
| Heptane | 44.6 | 0.101 | 1.1 | 675 |
| Gasoline | 43.7 | 0.055 | 2.1 | 740 |
| Kerosene | 43.2 | 0.039 | 3.5 | 820 |

Example

Equivalent diameter (D)

$$\frac{\pi D^2}{4} = (1)(1) \Rightarrow D = 1.13 \text{ m}$$

$$\begin{aligned}\dot{Q} &= \Delta H_c \dot{m}_f = \Delta H_c \dot{m}'' A = \Delta H_c \dot{m}'' (1 - e^{-k\beta D}) A \\ &= (44600 \left[\frac{\text{kJ}}{\text{kg}} \right]) (0.101 \left[\frac{\text{kg}}{\text{m}^2 \text{s}} \right]) (1 - e^{-(1.1)(1.13)}) (1 \text{ m}^2) \\ &= 3205 \text{ kW}\end{aligned}$$

$$\begin{aligned}L &= 0.235 \dot{Q}^{2/5} - 1.02 D \\ &= 0.235 (3205)^{2/5} - 1.02 (1.13) = 4.8 \text{ m}\end{aligned}$$

Example 2

Calculate the average values of pool diameter of the hydrocarbon fuels in the table below that results in the flame height of 3 m (10 ft ceiling).

->Excel spreadsheet

| | ΔH_c [kJ/g] | \dot{m}_∞ [kg/m ² -s] | $k\beta$ [1/m] | density [kg/m ³] |
|----------|---------------------|---|----------------|------------------------------|
| Butane | 45.7 | 0.078 | 2.7 | 573 |
| Benzene | 40.1 | 0.085 | 2.7 | 874 |
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