

Fire Dynamics

Compartment fire phenomena I

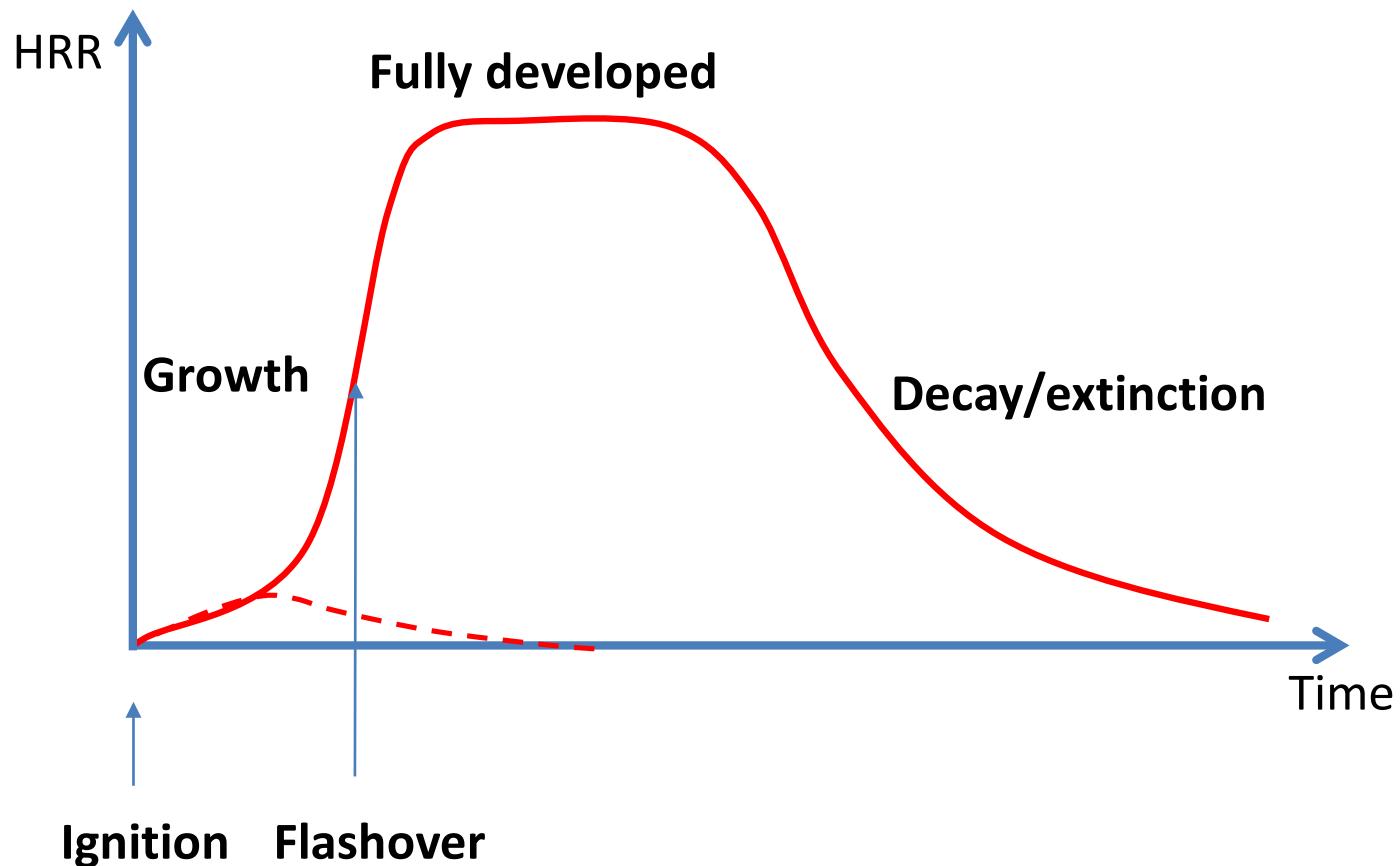
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Objectives

- Understanding flashover compartment fire phenomena

Compartment fire HRR curve



Growth period

- Growth rate: t^2 fire or t^3 fire

$$\dot{Q} = \alpha t^2, \dot{Q}[\text{kW}], t[\text{s}]$$

where,

$\alpha = 0.00293$ for slow growth [kW/s^2]

$\alpha = 0.01172$ for medium growth [kW/s^2]

$\alpha = 0.0469$ for fast growth [kW/s^2]

$\alpha = 0.1876$ for ultrafast growth [kW/s^2]

$$\dot{Q} = 1055 \left(\frac{t}{t_1} \right)^2, \dot{Q}[\text{kW}], t[\text{s}]$$

where,

$t_1 = 600$ s for slow

$t_1 = 300$ s for medium

$t_1 = 150$ s for fast

$t_1 = 75$ s for ultrafast

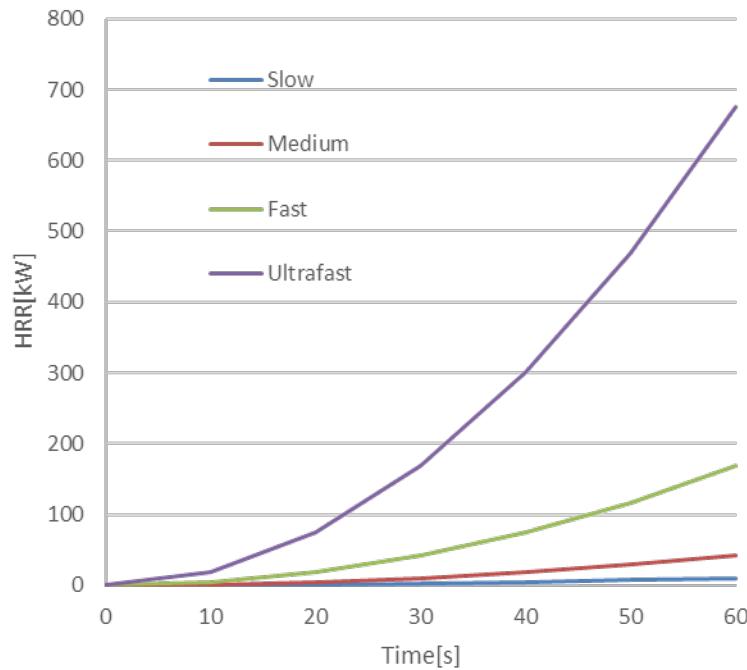
$$\dot{Q} = 0.00068t^3H, \dot{Q}[\text{kW}], t[\text{s}]$$

where,

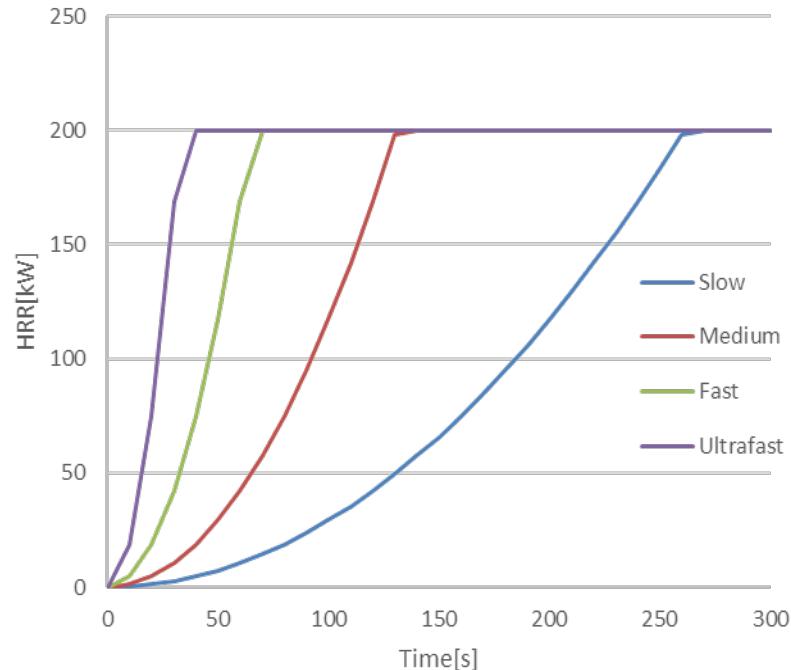
H = height to which storage is capable of [m] > 5 m

HRR of t-squared fire

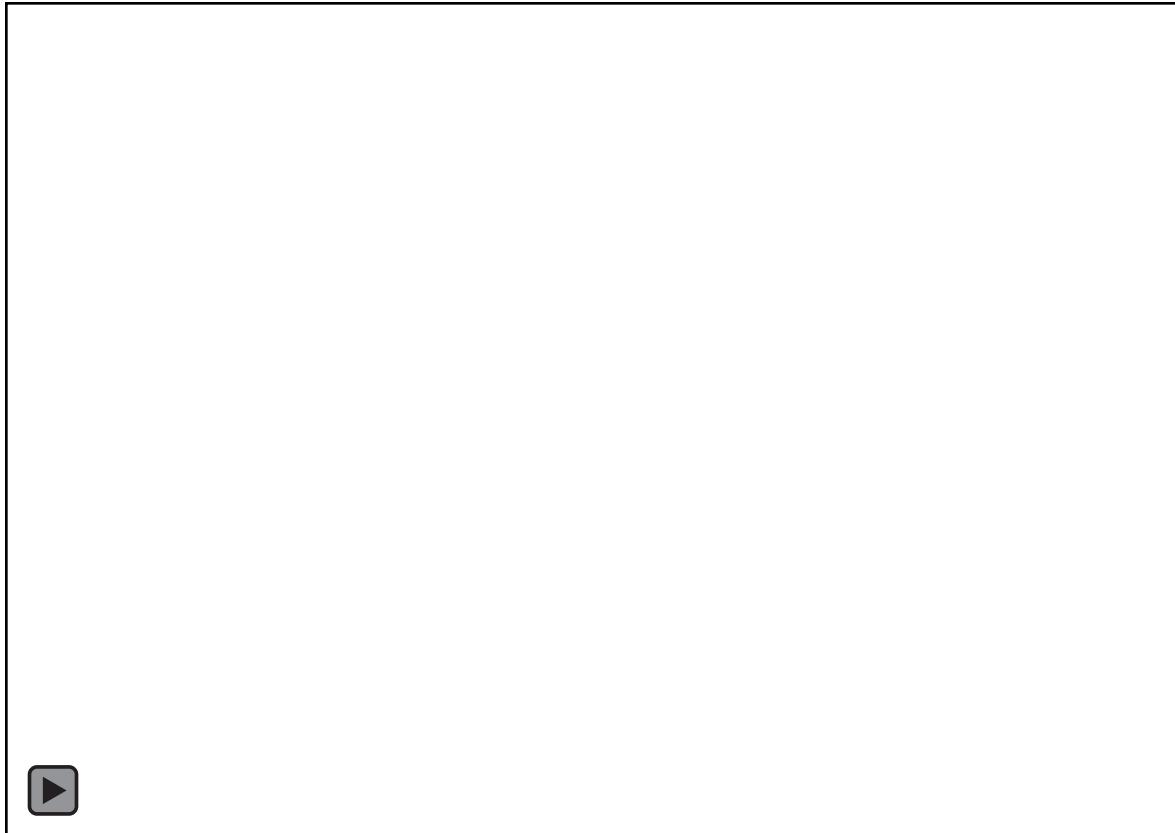
HRR [kW]



HRR [kW]_capped at 200 kW



Flashover phenomena (00:44 sec)



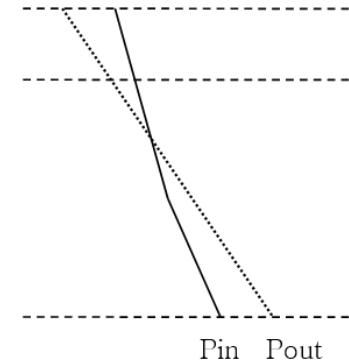
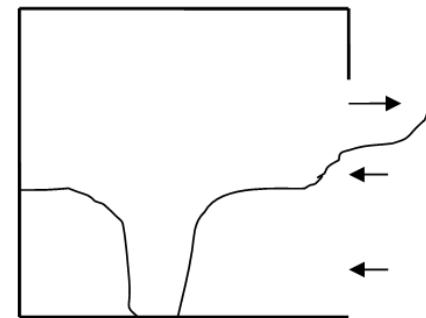
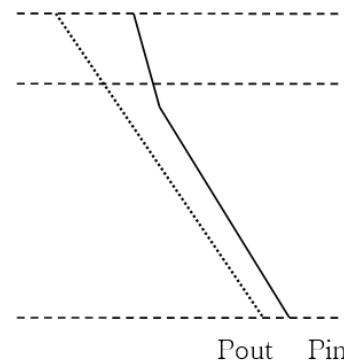
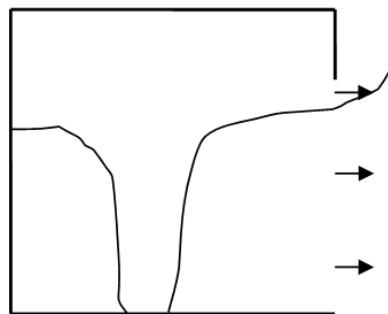
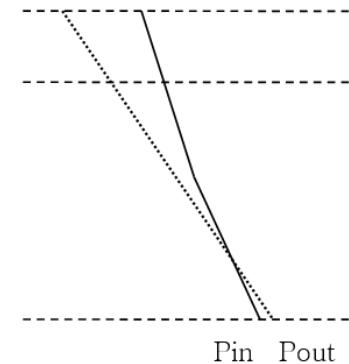
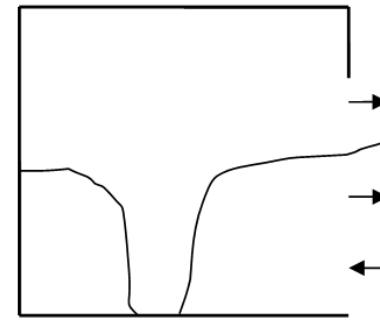
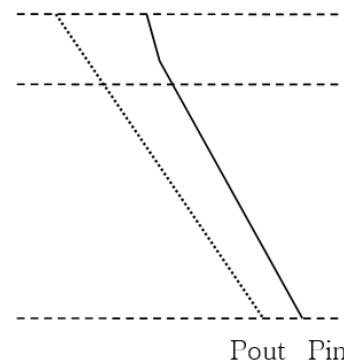
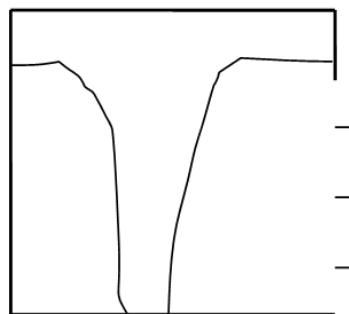
Flashover

- **600 °C in upper gas layer temperature (about 3 m high ceiling)**
- **450 °C in upper gas layer temperature (about 1 m high ceiling)**
- **~20 kW/m² at the floor level**
- **Ignition of crumpled paper at the floor**
- Projected flame out of an opening in the standard ISO room

Fully developed and decay period

- Typically less focused than pre-flashover.
Why?
- Important in terms of the performance of structural elements.

Pressure profile in pre-flashover



Pre-flashover compartment Temp.

- MQH correlation

$$\Delta T_g = 6.85 \left(\frac{\dot{Q}^2}{A_o \sqrt{H_o} h_k A_T} \right)^{1/3}$$

where,

$$\Delta T_g = T_g - T_\infty$$

T_g = temperature of upper gas layer [K]

T_∞ = ambient temperature[K]

\dot{Q} = heat release rate of fire in a compartment [kW]

A_o = opening area [m^2]

H_o = opening height [m]

h_k = effective heat transfer coefficient [kW/m-K], heat loss to walls and ceiling

A_T = total area of the compartment surface[m^2]

Pre-flashover compartment Temp.

- MQH correlation

$$\text{For } t > t_p, h_k = \frac{k}{\delta}$$

$$\text{For } t \leq t_p, h_k = \left(\frac{k\rho c}{t} \right)^{1/2}$$

where,

t = time of exposure [s]

$$t_p = \text{thermal penetration time [s]} = \left(\frac{\rho c}{k} \right) \left(\frac{\delta}{2} \right)^2$$

k = thermal conductivity [kW/m-K]

δ = thickness of compartment surface [m]

ρ = density of the compartment surface [kg/m³]

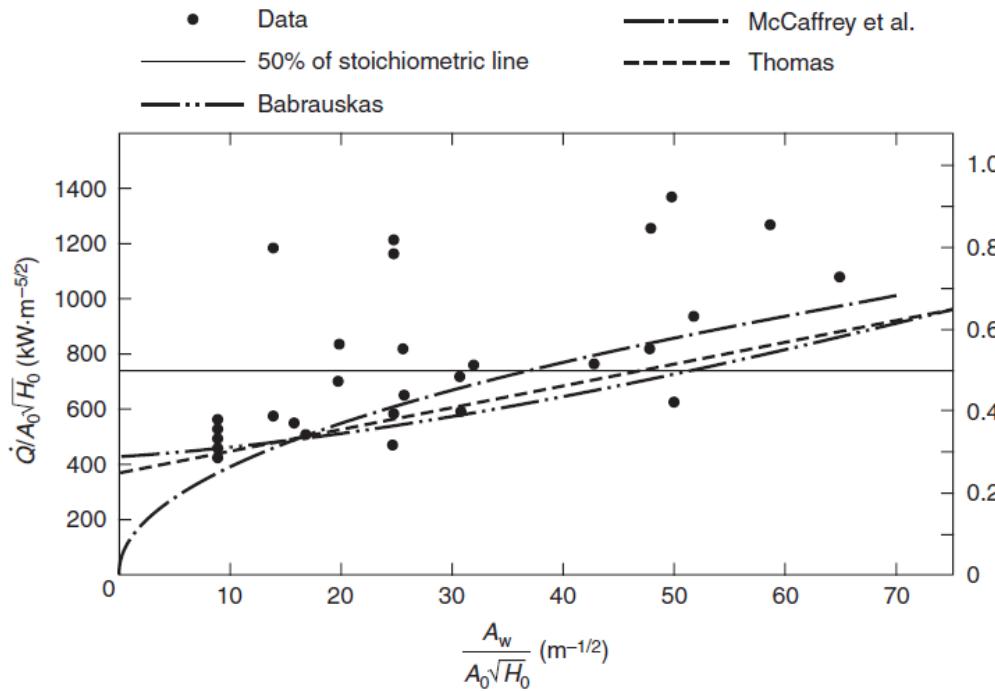
c = specific heat of the compartment surface [kJ/kg-K]

Prediction of flashover

$$\dot{Q}_{\text{flashover}} = 750 A_o \sqrt{H_o}, \text{ Babrauskas}$$

$$\dot{Q}_{\text{flashover}} = 610 \left(h_k A_T A_o \sqrt{H_o} \right)^{1/2}, \text{ MQH}$$

$$\dot{Q}_{\text{flashover}} = 7.8 A_T + 378 A_o \sqrt{H_o}, \text{ Thomas}$$



Example

- At 100 sec and 200 sec, Calculate ΔT_g of a room (3.6 m by 2.4 m by 2.4 m(H)) with an opening 2.1 m high and 0.9 m wide. HRR=750kW. The wall is 0.016 m gypsum boards on metal studs.

Gypsum board properties:

$$k = 0.48 \times 10^{-3} \text{ [kW/m-K]}$$

$$\delta = 0.016 \text{ [m]}$$

$$\rho = 1440 \text{ [kg/m}^3\text{]}$$

$$c = 0.84 \text{ [kJ/kg-K]}$$